

1131 & 1151 Teron Road

TIA Strategy Report Final

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TIA Plan Reports

On 14 June 2017, the Council of the City of Ottawa adopted new Transportation Impact Assessment (TIA) Guidelines. In adopting the guidelines, Council established a requirement for those preparing and delivering transportation impact assessments and reports to sign a letter of certification.

Individuals submitting TIA reports will be responsible for all aspects of development-related transportation assessment and reporting, and undertaking such work, in accordance and compliance with the City of Ottawa's Official Plan, the Transportation Master Plan and the Transportation Impact Assessment (2017) Guidelines.

By submitting the attached TIA report (and any associated documents) and signing this document, the individual acknowledges that s/he meets the four criteria listed below.

CERTIFICATION

- I have reviewed and have a sound understanding of the objectives, needs and requirements of the City of Ottawa's Official Plan, Transportation Master Plan and the Transportation Impact Assessment (2017) Guidelines;
- I have a sound knowledge of industry standard practice with respect to the preparation of transportation impact assessment reports, including multi modal level of service review;
- I have substantial experience (more than 5 years) in undertaking and delivering transportation impact studies (analysis, reporting and geometric design) with strong background knowledge in transportation planning, engineering or traffic operations; and
- 4. I am either a licensed1 or registered 2 professional in good standing, whose field of expertise [check ✓ appropriate field(s)] is either transportation engineering ✓ or transportation planning □.

License of registration body that oversees the profession is required to have a code of conduct and ethics guidelines that will ensure appropriate conduct and representation for transportation planning and/or transportation engineering works.

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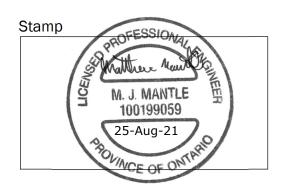
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FINAL REPORT

Parsons has been retained by Manor Park Management to prepare a Transportation Impact Assessment (TIA) in support of a Site Plan Application (SPA) for a residential development located at the joint addresses of 1131 and 1151 Teron Road in Kanata. This document follows the new TIA process, as outlined by the City Transportation Impact Assessment (TIA) Guidelines (2017). The following report represents Step 5 – Final Report. Note that this report begins as a Step 4 Report given that a recent step 5 submission for this location was completed by Parsons. The new SPA features slight changes from the previously submitted Step 5 Report.

1. SCREENING FORM

The screening form confirmed the need for a TIA in support of the proposed development based on the Trip Generation, Location and Safety Triggers, as follows: the envisioned land use consist for the combined development consists of approximately 131 residential units; the site is located between the March and Teron Road spine cycling network and within the March Road Transit Oriented Development (TOD) area; and due to the proximity of the Teron Road access point to the existing Steacie/Teron intersection. The screening form has been provided in **Appendix A**.

2. SCOPING REPORT

2.1. Existing and Planned Conditions

2.1.1. Proposed Development

The proposed development is located at the municipal addresses of 1131 and 1151 Teron Road. The existing site is currently an empty field with overhead hydro wires.

A two-phased project is proposed. Phase 1 will consist of a 3-storey, 18-unit residential building located at 1131 Teron Road. Phase 2 will consist of the addition of a 9-storey, 113-unit residential building located at 1151 Teron Road. Phase 1 is anticipated to be built by the year 2022 and Phase 2 is expected to follow promptly after. For the purpose of this study, full buildout will be assumed for the year 2022 and the horizon full buildout plus 5 years will be 2027. The site is currently zoned as R5A [2144] S327 which allows mid-rise buildings up to 9-storeys or 30 meters high and 01[2143] which allows parks and open space, making the development be within zoning allowances. The site's context is displayed in **Figure 1**.

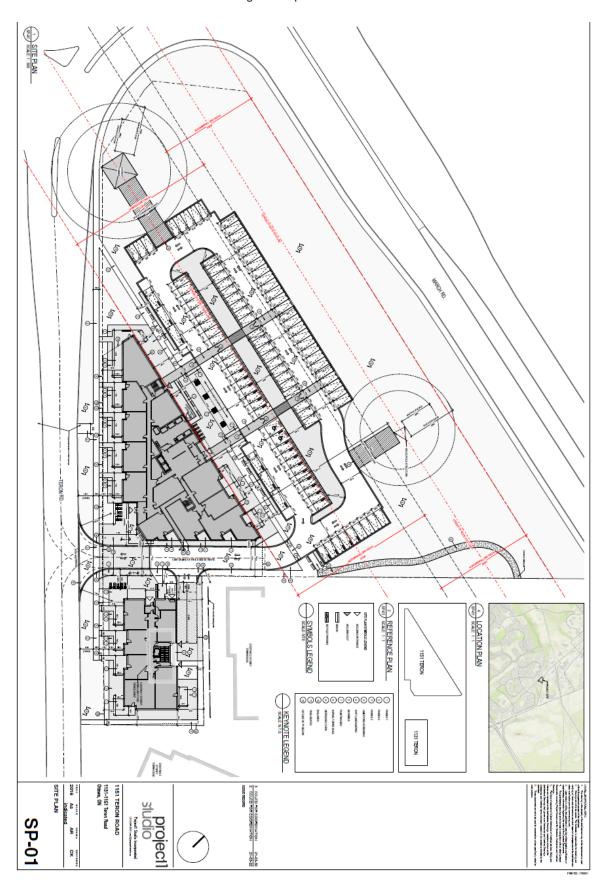
The future site proposes a single full movement vehicle access to Teron Road. A total of 102 underground and 98 surface parking spots are proposed. The latest site plan concept is shown in **Figure 2**.



Figure 1: Local Context



Figure 2: Proposed Site Plan





2.1.2. Existing Conditions

Area Road Network

March Road is a north-south arterial roadway, which extends from the Highway 417 in the south (continues as Eagleson south of the highway) to the town of Almonte in the north-west. The cross section within the study area is a divided roadway with two travel lanes in each direction and has auxiliary left-turn and right-turn lanes at main intersections. March Road is identified as a future bus rapid transit (BRT) corridor. The posted speed limit within the study area is 80 km/h.

Teron Road is a north-south major collector roadway which extends from Campeau Drive in the south to Carling Avenue in the north. The cross section within the study area consists of one lane per direction with auxiliary left and right turn lanes at main intersections and no median. The posted speed limit is 50 km/h.

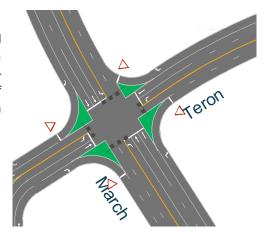
Beaverbrook Road is an east-west collector roadway which extends from Weslock Way in the west to Teron Road in the east and then continues as Penfield Drive which functions as a large crescent collector for a local neighbourhood. The cross section west of Teron Road consists of one travel lane per direction with no residential driveways, while the cross section east of Teron Road (Penfield Drive) consists of a one travel lane per direction with multiple residential driveway accesses. The posted speed limit is 40 km/h.

Steacie Drive is an east-west local roadway extending west of Teron Rd and finishing in a cul-de-sac. The cross section consists of a single travel lane in each direction with a multi-use pathway on the south side. The unposted speed limit is assumed to be 50 km/h.

Existing Study Area Intersections

March/Teron

The March/Teron intersection is a signalized four-legged intersection. The eastbound and westbound approaches both consist of a left-turn lane, a through lane and a channelized right-turn lane. The north and southbound approaches both consist of a left-turn lane, two through lanes and a channelized right-turn lane. All movements are permitted at this location.



Steacie/Teron

The Steacie/Teron intersection is a non-signalized three-legged intersection. The eastbound approach consists of a single left-turn lane controlled by a stop sign and a channelized right-turn lane controlled by a yield sign. The northbound approach consists of a left-turn lane and right-turn lane that extends past this intersection into the following March/Teron intersection. The northbound approach also has a through lane. The southbound approach consists of a channelized right-turn and a through lane. All movements are permitted at this location.



Beaverbrook/Teron

The Beaverbrook/Teron intersection is a signalized four-legged intersection. All approaches consist of a single left-turn lane and a shared through/right-turn lane. The south approach has a pedestrian crossing prohibition. All vehicular movements are permitted at this location.



Existing Driveways to Adjacent Developments

There are no private driveways located on March Road near the site. There are two existing driveways on Teron Road between March Road and Bethune Way on the northeast side which belong to a single house located on the future development site. There are no driveways on the southwest side of Teron Road between March Road and Bethune Way. The existing driveways adjacent to the proposed site are shown as red boxes in **Figure 3.**



Figure 3: Existing Driveways Adjacent to Development



Existing Area Traffic Management Measures

There are no existing traffic management measures along Teron Road and March Road in the vicinity of the proposed development.

Pedestrian/Cycling Network

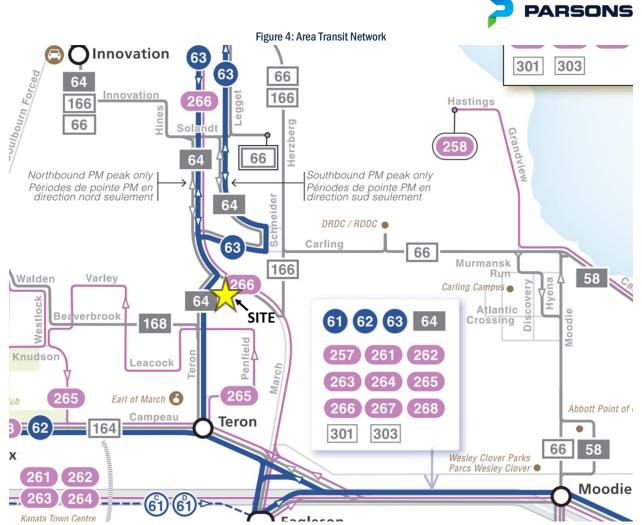
Sidewalk facilities in the vicinity of the site are provided along both sides of Teron Road from Beaverbrook Road to Bethune Way, but discontinued on the east side of Teron Road between Bethune Way and March Road (site frontage). March Road and Steacie Drive only provide sidewalk on the south side, and Beaverbrook Road only provides sidewalks on the north side of the roadway.

According to the City's Cycling Plan, March Road and nearby Herzberg Road are classified as "Spine Routes." On the west side of March Road, there are major separated pathway which lead to the proposed site but are not continued past this point. Steacie Drive has a major separated pathway on the south side of the road which begins at Teron Road adjacent to the site. Teron Road has a paved shoulder on both sides of the roadway. **Section 2.1.3.** discusses the future Ultimate Cycling Network.

Transit Network

The transit network for the study area is illustrated in **Figure 4**. The following OC Transpo routes currently operate within 600-meter radius of the site frontage:

- Route #63 (Briarbrook <-> Tunney's Pasture): identified by OC Transpo as a "Rapid Route", this route operates at all time periods with high frequency, 7 days a week. Route #63 provides quick connection to the Confederation LRT Line at Tunney's Pasture and provides connection to Bayshore Shopping Center. Bus stops for this route are available on both sides of Teron Road, fronting the site.
- Route #64 (Morgan's Grant <-> Tunney's Pasture): identified by OC Transpo as a "Local Route", this route operates on customized routing and schedules, to serve local destinations with connection to the Confederation LRT Line at Tunney's Pasture, Innovation Complex and provides connection to Bayshore Shopping Center. Bus stops for this route are available on both sides of Teron Road, fronting the site.
- Route #166 (Innovation <-> Eagleson): identified by OC Transpo as a "Local Route", this route operates on
 customized routing and schedules, to serve local destinations such as Eagleson Station and Innovation
 Complex. Bus stops for this route are available on both sides of Teron Road, fronting the site.
- Route #266 (Maxwell Bridge<-> Tunney's Pasture): identified by OC Transpo as a "Connection Route", this
 route provides convenient connection to the Confederation LRT Line at Tunney's Pasture during weekday
 peak periods only and provides connection to Bayshore Shopping Center. Bus stops for this route are
 available on both sides of March Road, approximately 150 meters from the site.
- Routes #660 & 674 (Various): identified by OC Transpo as a "Local Custom Route", these routes operate
 on customized routing and schedules, to serve local destinations such as Bell High School and All Saints
 High School. Bus stops for these routes are available on both sides of Teron Road, fronting the site.



Source: https://www.octranspo.com/images/files/maps/systemmap.pdf

Peak Hour Travel Demands

The existing peak hour traffic volumes within the study area are illustrated in **Figure 5** and pedestrian/cyclist volumes are illustrated in **Figure 6**, obtained from the City of Ottawa. The peak hour traffic volume count data has been provided in **Appendix B**.



Figure 5: Existing Peak Hour Traffic Volumes

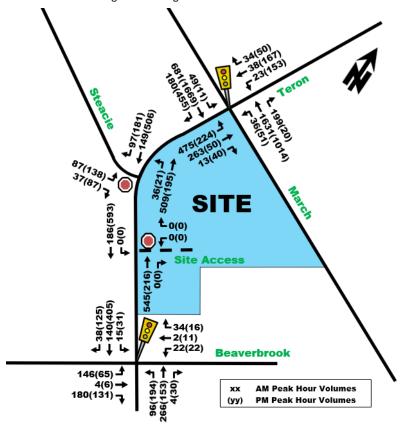


Figure 6: Existing Pedestrian/Cyclist Peak Hour Volumes 151010) 00017 001/2 F/1619 **★ 6 1 0** SITE **Site Access** ○↑ 1(2) | → 1 12(6) Teron **∜**0(10) **≮** 0(4) Beaverbrook 1(14) **AM Peak Hour Volumes** 9(3) **1**0/ (yy) **PM Peak Hour Volumes**



Existing Road Safety Conditions

Collision history for study area intersections and roads (2013 to 2017, inclusive) was obtained from the City of Ottawa with 76 reported collisions within the 5-year time period. Most collisions 57 (75%) involved property damage only, indicating likely low impact speeds, and 19 (25%) involved personal injuries. The reported collisions by classification include: 28 (37%) rear end, 16 (21%) single vehicle, 12 (16%) angle, 12 (16%) turning movement, 7 (9%) sideswipe and 1 (1%) approaching type collisions.

To help quantify the relative safety risk at intersections within the study area, an industry standard unit of measure for assessing collisions at an intersection was used based on the number of collisions per million entering vehicles (MEV). An MEV value greater than 1.00 indicates a relatively high frequency of collisions; however, it does not explain the type or severity of collision. A secondary analysis is done to determine the severity of collision by representing the number of personal injuries as a percentage of the total number of collisions at a given intersection.

A high propensity (MEV > 1.00 or %PIR > 30%) would signal a potential intersection design deficiency or other contributing factor, such as poor intersection geometry, blind spots, poor lighting, excessive speeds, high amount of entry/exit driveways etc.

At intersections within the study area, reported collisions have historically taken place at a rate of:

- 0.36/MEV at the March/Teron intersection with a total of 27 collisions, 26% causing non-fatal injuries. The most common types of collisions involved rear end with 10 (37%) of the total collisions and turning movement with 8 (30%) of all collisions. The medium to high %PIR is likely due to the high operating speeds, including the south approach which enters from a long straightaway on a wide multi-lane cross-section arterial and high turning movements at this intersection. Turning movement type of collisions tend to yield higher %PIR;
- 0.05/MEV at the Steacie/Teron intersection with a total of 1 collision; and,
- 0.31/MEV at the Beaverbrook/Teron intersection with a total of 6 collisions and 50% causing non-fatal injury. The high %PIR is linked with 3 of 6 (50%) of the collisions involving pedestrians or cyclists.

All study intersections displayed a low to mid MEV value indicating that collisions happen at a low rate compared to other intersections around the City. Within the five-years of recorded collision data there were two collisions involving pedestrians and one involving a cyclist at Beaverbrook/Teron, all resulting in non-fatal injuries. These three collisions involving the active modes represent one half of all collisions at this intersection. There was one collision involving a pedestrian at March/Teron.

The source collision data as provided by the City of Ottawa and related analysis is provided as Appendix C.

2.1.3. Planned Conditions

Planned Study Area Transportation Network Changes

Transit Network

Based on the City of Ottawa's Transportation Master Plan (TMP), a future bus rapid transit (BRT) corridor is proposed on March Road, between Eagleson Rd and Solandt Rd. The BRT would have a major station near the subject development's site, which would be located at the March/Teron intersection. Further north along March Rd, between Solandt Road and Maxwell Bridge Road, the TMP's affordable network illustrates transit priority (isolated measures).

The improved transit priority corridor is anticipated to improve transit travel times between the proposed site and the Confederation Line as displayed in **Figure 7.** While these changes are illustrated in the TMP's 2031 Affordable Network, City of Ottawa staff have confirmed that construction of the BRT and transit priority measures will likely take place beyond 2031.



Figure 7: 2031 Affordable Network CARLING SITE LADIUM TIMM ROBERTSON

Source: Transportation Master Plan 2013 - 2031 Affordable Network

Cycling Network

Within the City of Ottawa Ultimate Cycling Plan, cycling facilities are proposed for Teron Road between Campeau Drive and Beaverbrook Road. Cycling improvements are also proposed at Beaverbrook Road between Weslock Way and Teron Road and from Teron Road to March Road via the continuation of Beaverbrook Road (Penfield Drive) to the east.

Figure 8 depicts the existing and future Ultimate Cycling Network.

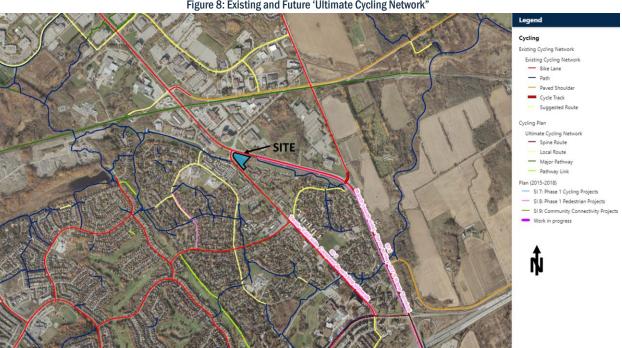


Figure 8: Existing and Future 'Ultimate Cycling Network"



Other Area Developments

The following section outlines adjacent developments in the general area that were considered in the TIA. The criteria for inclusion of other area developments are either approved developments or developments that have an active planning application in the City. **Figure 9** illustrates the location and relative size of relevant other area developments. Note that no nearby developments south of the proposed development were found.

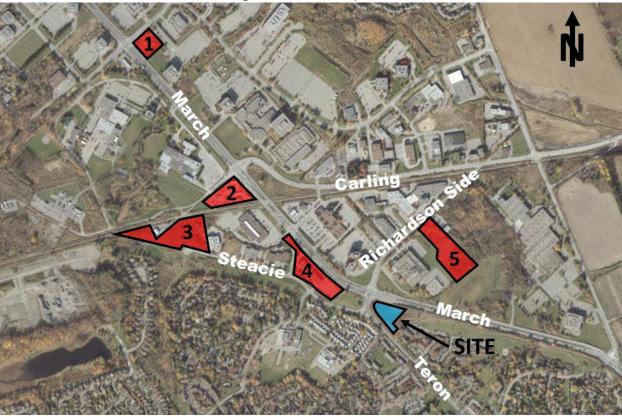


Figure 9: Other Area Developments

1 - 3026 Solandt Road

An office building is proposed by Colonnade Bridgeport consisting of approximately 100,000 ft² of total floor area. The anticipated buildout year of the development is 2021. Based on the TIA prepared by CIMA+ on March, 2020, the development is expected to generate 101 and 95 veh/h during the morning and afternoon peak hours, respectively.

2 - 401 March Road

Proposed one storey commercial plaza containing a gas bar, car wash, two restaurants with drive-thru facilities and a commercial building that would contain a medical facility. The Transportation Impact Assessment (prepared by Burnside) projected vehicle trip generation of approximately 265 and 190 veh/h during both the morning and afternoon peak hours. *Note: Development Apps status date Oct.* 13, 2016 identifies agreement registered; however, this development has been open since as early as May 2016. Therefore, trips generated by this development are assumed to already be accounted for in the traffic count data.

3 - 100 Steacie Drive

Brigil is proposing the construction of two 4-storey apartment buildings with a total of 258 residential units. A TIA is currently being developed by Parsons. The projected volumes will be individually layered to background volumes



4 - 329 March Road

Proposed 4,102 ft² of commercial, including a restaurant and a coffee shop. The Transportation Brief (prepared by McIntosh Perry) projects vehicle trip generation of approximately 40 to 100 veh/h during peak hours.

5 - 1243 Teron Road

An industrial building is proposed at 1243 Teron Rd and will consist of a total area of 9,281 m². The estimated year of occupancy for the development is 2020. Based on the TIA prepared by BT Engineering in January 2020, the volumes generated by the development at study area intersections are minimal. Therefore, the volumes will be accounted for in the projected background traffic growth.

2.2. Study Area and Time Periods

Although the development is proposed as a 2-phased development with phase 1 being built by 2022 and phase 2 prior to 2026, for the purpose of this development a single full is assumed for 2022. Given that the network for full buildout and full buildout plus 5 years are anticipated to be the same the horizon years being analyzed in this report are the more critical full buildout plus 5, 2027, using the weekday morning and afternoon peak hour time periods.

Proposed study area intersections and boundary roads are outlined below and highlighted in Figure 10.

- March/Teron intersection;
- Steacie/Teron intersection;
- Beaverbrook/Teron intersection;

- Site/Teron intersection:
- Along Teron Road adjacent to the site; and,
- Along March Road adjacent to the site.



Figure 10: Study Area Boundaries and Intersections

2.3. Exemption Review

The following modules/elements of the TIA process recommended to be exempt in the subsequent steps of the TIA process, based on the City's TIA guidelines and the subject site:



Table 1: Exemptions Review Summary

| Module | Element | Exemption Consideration | | | | |
|-------------------------------------|-------------------------------|---|--|--|--|--|
| 4.1 Development Design | 4.1.3 New Streets Networks | Not required for applications involving site plans | | | | |
| 4.2 Parking | 4.2.2 Spillover Parking | Development anticipated to provide sufficient parking. This will be verified in Section 4.2. | | | | |
| 4.6 Neighborhood Traffic Management | 4.6.1 Adjacent Neighborhoods | Only required when development relies on local or collector streets for access. Driveway will have direct access to Teron Road (arterial) | | | | |
| 4.8 Review of Network Concept | All elements | The site is not expected to generate 200 trips more than the established zoning. | | | | |

3. FORECASTING REPORT

3.1. Development-Generated Travel Demand

3.1.1. Trip Generation and Mode Shares

Appropriate trip generation rates for the proposed development consisting of approximately 131 mid-rise apartment units were obtained from the City's 2009 TRANS Trip Generation – Residential Trip Rates Report. These rates are summarized in **Table 2**.

Table 2: 2009 TRANS Residential Trip Generation Rates

| Land Use | Data | Data Trip Rates | | | |
|---|---------------|-----------------|--------------|--|--|
| Land Use | Source | AM Peak | PM Peak | | |
| Mid-Rise Apartments | 223 | T = 0.29(du) | T = 0.37(du) | | |
| Note: T = Average Vehicle Trip Ends; du = c | welling units | ; | | | |

Using the TRANS Trip Generation rates, the total amount of vehicle trips generated by the proposed 131 residential units was calculated. The results are summarized in **Table 3**.

Table 3: Projected Site Vehicle Trip Generation - TRANS Model

| Londilloo | Aron | AM | 1 Peak (Veh | /h) | PM Peak (Veh/h) | | |
|---------------------|-----------|----|-------------|-------|-----------------|-----|-------|
| Land Use | Area | In | Out | Total | In | Out | Total |
| Mid-Rise Apartments | 131 units | 9 | 29 | 38 | 29 | 19 | 48 |

As shown in **Table 3**, a total of 40 to 50 veh/h two-way are projected to travel to/from the proposed development during the weekday morning and afternoon commuter peak hours. Using the TRANS Auto Trips projected in **Table 3** and the mode share percentages in the TRANS Trip Generation Report (Table 3.13), the total projected number of person trips by mode for the residential development were calculated and are summarized in **Table 4**. The 'person trip generation' for the development was then converted to 'vehicle trip generation' using mode shares extrapolated from the 2011 OD-Survey for Kanata District Area and are summarized in **Table 5**.

Table 4: Site Person Trip Generation

| Travel Mode | Mode | AM Peak (Person Trips/h) | | | Mode | PM Peak (Person Trips/h) | | | |
|--------------------|-------|--------------------------|-----|-------|-------|--------------------------|-----|-------|--|
| Travel Mode | Share | In | Out | Total | Share | In | Out | Total | |
| Auto Driver | 44% | 9 | 29 | 38 | 44% | 29 | 19 | 48 | |
| Auto Passenger | 9% | 2 | 5 | 7 | 14% | 10 | 5 | 15 | |
| Transit | 34% | 8 | 22 | 30 | 33% | 22 | 14 | 36 | |
| Non-motorized | 13% | 3 | 8 | 11 | 9% | 7 | 3 | 10 | |
| Total Person Trips | 100% | 22 | 64 | 86 | 100% | 68 | 41 | 109 | |



Table 5: Site Vehicle Trip Generation with Kanata Mode Shares

| Travel Mode | Mode AM Peak (veh | | | /h) Mode | | PM Peak (veh/h) | | |
|------------------------|------------------------|----|-----|----------|-------|-----------------|-----|-------|
| Travel Mode | Share | In | Out | Total | Share | In | Out | Total |
| Auto Driver | 60% | 12 | 40 | 52 | 60% | 40 | 25 | 65 |
| Auto Passenger | 15% | 4 | 9 | 13 | 15% | 9 | 7 | 16 |
| Transit | 15% | 2 | 10 | 12 | 15% | 10 | 7 | 17 |
| Non-motorized | 10% | 2 | 7 | 9 | 10% | 6 | 5 | 11 |
| Total People Trips | 100% | 20 | 66 | 86 | 100% | 65 | 44 | 109 |
| Total 'New' Auto Trips | Total 'New' Auto Trips | | 40 | 52 | - | 40 | 25 | 65 |

As shown in **Table 5**, based on the TRANS Trip Generation method and 2011 OD-Survey modal shares, the proposed site is projected to generate approximately 50 to 65 new auto-trips per hour during the weekday commuter peak hours. The increase in two-way transit trips is estimated to be approximately 10 to 15 persons per hour, and the increase in bike/walk trips is approximately 10 persons per hour for the and afternoon peak hours.

3.1.2. Mode Shares

Given the location of the site, within close proximity to existing rapid route #63 and 4 other OC-Transpo existing transit routes, plus future proposed BRT transit priority with isolated measures proposed along March Road adjacent to the site a higher transit modal share is appropriate. **Table 6** illustrates future modal shares which reflect the site's location within close proximity to the existing bus stations and future BRT.

Table 6: Future Mode Share Targets for the Development

| Travel Mode | Mode Share Target | Rationale | | | | |
|----------------|----------------------|--|--|--|--|--|
| Auto Driver | 35% | Given the close proximity to transit and commercial services, the driver and passenger mode splits are forecasted to be lower than | | | | |
| Auto Passenger | 5% | other areas of the City. | | | | |
| Transit | 45% | Development is located in close proximity to future rapid transit station at March/Teron. March Road is in the TMP's affordable network for transit priority with major updates in transit services. | | | | |
| Walking | 10% | This is consistent with the City's TMP and existing mode shares. | | | | |
| Biking | 5% | This is consistent with the oity's Tivir and existing mode shales. | | | | |

The future mode shares summarized in **Table 6** were applied to the total person-trips for residential uses outlined in **Table 5**, to estimate future trip generation at ultimate buildout, as shown in **Table 7**.

Table 7: Future Projected Site Generated Traffic Based on TOD Mode Shares

| Travel Mode | Mode | AM Peak (veh/h) | | | Mode | PM Peak (veh/h) | | |
|------------------------|-------|-----------------|-----|-------|-------|-----------------|-----|-------|
| Travel Mode | Share | In | Out | Total | Share | In | Out | Total |
| Auto Driver | 35% | 8 | 23 | 31 | 35% | 23 | 15 | 38 |
| Auto Passenger | 5% | 2 | 3 | 5 | 5% | 3 | 2 | 5 |
| Transit | 45% | 9 | 29 | 38 | 45% | 31 | 18 | 49 |
| Walk | 10% | 2 | 6 | 8 | 10% | 8 | 4 | 12 |
| Bike | 5% | 1 | 3 | 4 | 5% | 3 | 2 | 5 |
| Total People Trips | 100% | 22 | 64 | 86 | 100% | 68 | 41 | 109 |
| Total 'New' Auto Trips | | 8 | 23 | 31 | - | 23 | 15 | 38 |

Based on **Table 7**, it is anticipated that the proposed development will generate approximately 30 to 40 'new' vehicles trips, 40 to 50 'new' transit trips, 10 'new' walk trips and 5 'new' bike trips, two-way during the weekday morning and afternoon peak hours.



3.1.3. Trip Distribution

Based on the OD Mode Share Survey, existing traffic volume counts and the location of adjacent arterial roadways and neighborhoods, the distribution of site-generated traffic volumes is as follows:

(From/To) the North: 25%;

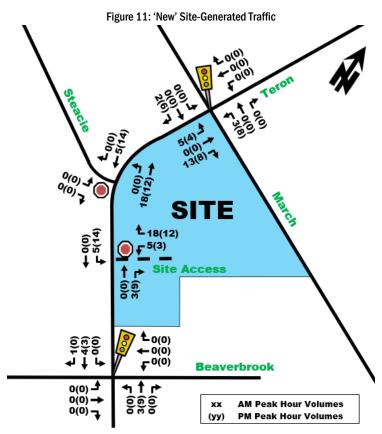
(From/To) the East: 60%;

(From/To) the South: 10%; and,

(From/To) the West: 5%.

3.1.4. Trip Assignment

A full movement driveway on to Teron Road is proposed. The new driveway will be approximately 145 meters south of the intersection of Steacie/Teron and approximately 120 meters north of Bethune Way. The 'new' site-generated vehicle trips outlined in **Table 7** were assigned to the study area network and are illustrated as **Figure 11**.



3.2. Background Network Travel Demands

3.2.1. Transportation Network Plans

Refer to section 2.1.3 Planned Conditions - Planned Study Area Transportation Network Changes.

3.2.2. Background Growth

The background traffic growth through the immediate study area (summarized in **Table 8**) was calculated based on historical traffic count data (years 2009, 2010, 2011, and 2017) provided by the City of Ottawa at the March/Teron intersection. Detailed analysis of the background growth is included in **Appendix D**.



Table 8: March/Teron Historical Background Growth (2009 - 2017)

| Time Period | Percent Annual Change | | | | | | | | |
|-------------|-----------------------|-----------|----------|----------|---------|--|--|--|--|
| Time Period | North Leg | South Leg | East Leg | West Leg | Overall | | | | |
| 8 hrs | -0.62% | -1.11% | 1.06% | 0.39% | -0.58% | | | | |
| AM Peak | -1.30% | -3.16% | 2.04% | 3.13% | -1.08% | | | | |
| PM Peak | -1.05% | -0.92% | -1.55% | -1.39% | -1.07% | | | | |

As shown in Table 8, in past years March Road and Teron Road have experienced an average annual decrease in traffic volumes ranging from -0.6% to -1.1%. It is important to note however, that a positive growth trend was evident between 2009 to 2011, indicating that data from 2017 could have been abnormally low due to many possible factors such as construction, area road closures, nearby events detouring traffic, etc. It is also possible that network changes such as the expansion of Terry Fox Drive between 2011 and 2017 or changes in mode shares has reduced traffic volumes. For the purpose of this study, a very conservative +2% annual growth rate for vehicle traffic on March Road and Teron Road 'through' movements will be applied in the future analysis.

3.2.3. Other Area Developments

Other area developments were outlined in Section 2.1.3. Traffic volumes generated by the following future adjacent area developments will be taken into account with regards to the analysis, with their respective traffic volume figures obtained directly from approved TIA Reports Some developments were not included and are captured within the 2% annual growth as either their location was not likely to influence this study area or vehicle trip generations was less than a vehicle per minute thus making them have negligible impacts to the study area. Figure 12 illustrates the projected traffic volumes for all other area development vehicle trips at full build-out, obtained from their respective TIA Reports.

Figure 12: All Other Area Development Vehicle Trip Generation - Full Build Out **1**-0(0) Beaverbrook **AM Peak Hour Volumes PM Peak Hour Volumes**

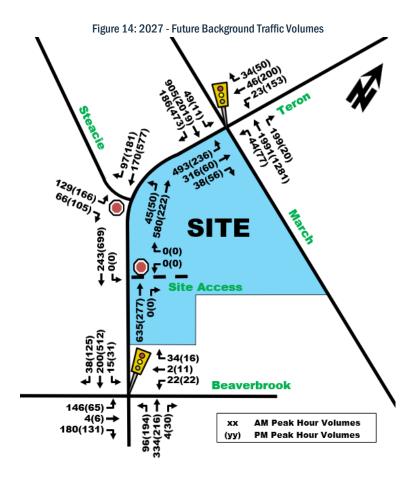
The future background traffic volumes were then generated by summing all the other area developments to existing volumes and including a 2% growth factor on through movements as described in Section 3.2.2. The resulting 2022 background volumes is illustrated in Figure 13 and the 2027 background volumes in Figure 14.



Figure 13: 2022 - Future Background Traffic Volumes * 188(20) 179) 129(166) **1** 66(105) **7** SITE ← 223(635) ` **€** 0(0) **L**₀₍₀₎ **₽**0(0) **Site Access** 576(254) **-**0(0) **-£** 38(125) **←** 186(472) **£** 15(31) **1**34(16) **←** 2(11) **Beaverbrook** 96(194) ∆ 307(200) **→** 4(30) **→** 146(65) 4(6) → 180(131) **→** хx **AM Peak Hour Volumes**

(yy)

PM Peak Hour Volumes





3.3. Demand Rationalization

Capacity of the study area intersections in existing and future conditions will be examined in detail in the proceeding sections of the TIA Report. As an initial review, the total project future traffic volumes can be determined by superimposing the site-generated traffic volumes in **Figure 11** onto the respective total future background traffic volumes in **Figure 13** and **Figure 14**.

The purpose of the Demand Rationalization module is to provide an initial review of future traffic volumes, to determine the future capacity limitations of the transportation network. Looking at the above total projected traffic volume figures, along with the existing conditions volumes in **Figure 5**, capacity limitations may be experienced at the intersection of March/Teron due to the following reasons:

- The volume of through traffic on March Road is expected to increase from approximately 1,650 veh/h at the peak times of both directions in existing conditions to approximately 2,000 veh/h by horizon year 2027. At the intersection of March/Teron, March Road is an arterial road intersected by a major collector road Teron, both of which service a high number of traffic volumes during peak hours. Therefore, providing sufficient green times to service the high number of traffic on March Road during peak hours may not be possible. By extent, the two through lanes of the NB and SB approaches at March/Teron would have capacity limitations.
- The EBL from Teron Road onto March Road experiences a high traffic volume that ranges from 475 veh/h in existing conditions to 500 veh/h by horizon year 2027, during the AM peak hour. Typically, this volume would require two left-turn lanes to operate within acceptable standards. However, only a single left-turn lane is currently available.

To address these potential capacity limitations, the following modifications may be considered to increase capacity or reduce vehicular demand along March Road.

Widening March Road to Six-Lane Cross-Section through Teron Road

March Road already consists of a six-lane cross-section from Campeau Drive to Herzberg Road, approximately 1km east of Teron Road. At the intersection of March/Teron, March Road consists of two-through lanes in each direction, as well as auxiliary left and right-turn lanes. A third through lane may be feasible to increase capacity by converting the north and southbound right-turn lanes to through/right-turn lane. The receiving lanes may need to be extended to allow enough distance for through traffic to safely merge.

There would be significant financial and geometric implications of this modification. There may also be safety concerns with the existing on-street bike lanes, which may trigger even further modifications to segregate cyclists through the intersection. Therefore, this modification to the intersection may not be appropriate from a traffic operations improvement perspective.

There is also the concern with induced demand, whereby increasing supply/capacity of a corridor triggers higher long-term demand, and the bottleneck simply shifts downstream and causes even larger capacity constraints.

Teron Road Double Left-Turn Lane

The EB approach of Teron Road currently consists of a through lane, a channelized auxiliary right-turn lane and an auxiliary left-turn lane. However, less than 60 vehicles are projected for the EBR movement at any peak hour, compared to over 450 vehicles on the EBL today. Therefore, there may be reason to reallocate lane assignments to have two EB left-turn lanes and a shared through/right-turn lane.

However, this sort of modification is expected to increase the amount of traffic along Teron Road, which already acts as a bypass to March Road through Kanata. Therefore, there are community and traffic management implications. to proposing this option.



March Road BRT

The March Road conversion to BRT was cited in the 2013 City TMP within the 2031 affordable network. City staff recently confirmed this project has been delayed and is no longer within the affordable network plan. Although we have adjusted the TIA to reflect this new information, it is important to stress the importance of this infrastructure to the Kanata North community, particularly as it relates to March Road adjacent to the site. As discussed in Section 3.2.2. Background Growth, the Carling Avenue Transit Priority Study estimated transit lanes could reduce vehicle traffic volumes by up to 20%, which is a significant result if applied to March Road. Therefore, of all the options that could be implemented to improve capacity along March Road at Teron Road, the BRT would be the most impactful as it provides long-term benefits for the entire corridor and region, rather than a short-term ease to a single intersection.

4. STRATEGY REPORT

4.1. Development Design

4.1.1. Design for Sustainable Modes

Location of Transit Facilities

There are existing OC-Transpo bus stops located adjacent to the development site on Teron Road with service for bus routes #63, #64 and #166. Additional connection bus route #266 has a bus stop located approximately 150 meters walk on March Road. A bus rapid transit (BRT) route is proposed for March Road, which when complete, will provide a major rapid transit station less than 200 meters from the site located at the intersection of March/Teron. Note that the exact timing for the BRT has not been determined yet.

Pedestrian/Cycling Routes and Facilities

Existing sidewalks are provided along the site's frontage on March Road. There are currently no sidewalks built on the site's Teron Road frontage. It is anticipated that when the development is built, that a sidewalk will be provided along the site's frontage of Teron Road.

A multi-use pathway (MUP) is proposed on the north side of the subject property, which would connect the existing MUP east of the site to the MUP south of Steacie Drive. Internal surface sidewalks within the site are proposed, which would offer pedestrian connectivity between both 1131 and 1151 Teron Road as well as connection to March/Teron intersection via a pathway through the parking lot.

Bicycle Parking

Bicycle parking is anticipated to meet and exceed the minimum City By-Law requirements of 0.5 spaces per units by providing a rate of approximately 0.69 spaces per unit. 82 of the Bicycle parking spaces are proposed indoors in a secure, well-lit area located within the underground parking lot and are proposed to be horizontal parking spaces. The remaining 14 bike parking spaces are proposed outdoors at ground level.

4.1.2. Circulation and Access

The proposed development driveway will provide two-way vehicular access to Teron Road via a 6.7-meter-wide driveway, which follows City By-Law requirements. The ramp for the underground parking lot is located approximately 30m north of Teron Road, is approximately 6 meters wide and provides access to the underground parking structure that is underneath both buildings.

The surface parking lot has a road loop is proposed to two-way circulation along the north, east-west drive aisle and have two-way travel until the T-intersection with the main driveway connection, where it becomes an exit only. The circuitous design makes it convenient for garbage trucks to access the garbage bins without the need of turning around within the lot. Garbage pick-up is proposed to take place on site along the backside of both buildings within the drive aisles. **Figure 15** displays the circulation of an HSU (emergency vehicle) circulating the site.



Figure 15: Emergency Vehicle Maneuvering

4.1.3. New Streets Network

Exempt. See Table 1.

4.2. Parking

4.2.1. Parking Supply

According to Part 4 – Parking, Queueing and Loading Provisions for the City of Ottawa By-Laws, the site is located within Area C according to Schedule 1, Area C in Schedule 1A and is not within Rapid Transit Stations within Schedule 2A and 2B. **Table 9** summarizes the vehicle parking minimum and maximums allowed within the parking by-law. **Table 10** summarizes the bicycle parking requirements as per City of Ottawa Zoning By-Law-Part 4, sections 100-114.

Table 9: Vehicle Parking Space Supply

| Land Use | Rate per Unit | | Requ | Proposed | | | |
|-------------------------------|---------------|------|---------|----------|---------|----------|--------|
| Land Use | | Base | Visitor | Base | Visitor | Min Req. | Spaces |
| Residential Phase 1 | 18 units | 1.2 | 0.2 | 22 | 4 | 26 | 32 |
| Residential Phase 2 113 units | | 1.2 | 0.2 | 136 | 23 | 159 | 168 |
| | | | Totals | 158 | 27 | 185 | 200 |



Table 10: Bicycle Parking Requirements

| Land Use | | Rate | Required Bicycle Spaces | Proposed |
|---------------------|-----------|--------------|-------------------------|----------|
| | | nate | Required | Spaces |
| Residential Phase 1 | 18 units | 0.5 per unit | 9 | 29 |
| Residential Phase 2 | 113 units | 0.5 per unit | 57 | 67 |
| | | Totals | 66 | 96 |

The latest site plan suggests a grand total of 200 parking spaces, with 98 being above ground including 27 catered to visitors while the remaining 71 surface lots for residents. Additionally, 102 parking spots are proposed underground for residents. The underground lot is shared between both buildings and has a vehicular ramp to the south of the site access, behind 1131 Teron Road building. The proposed number of parking spaces meets City of Ottawa Parking Guidelines.

The bicycle parking spaces proposed meet and exceed the by-laws, with 96 bicycle parking spaces proposed and 66-minimum required. A total of 14 spots will be provided outdoors on ground level and 82 located in the underground parking lot in three secure, well-lit storage rooms.

4.2.2. Spillover Parking

Exempt. See table **Table 1**.

4.3. Boundary Street Design

4.3.1. Existing Conditions

The boundary streets for the development are March Road and Teron Road. The existing roadway geometry consists of the following features:

- March Road
 - 2 vehicle travel lanes in each direction:
 - o 2m sidewalk with no boulevard on south side of the roadway only; and,
 - More than 3,000 vehicles per day.
- Teron Road
 - 1 vehicle travel lane in each direction;
 - 2m multi-use pathway with boulevard on west side of the roadway east side of the roadway proposed; and,
 - More than 3,000 vehicles per day.

The multi-modal level of service analysis for the subject road segments adjacent to the site is summarized in **Table 11** with detail analysis provided in **Appendix E**.

Table 11: MMLOS - Boundary Street Segment Existing

| | Level of Service | | | | | | | | |
|--|------------------|--------|----------------|--------|----------------|--------|---------------|--------|--|
| Road Segment | Pedestrian | | Bicycle (BLoS) | | Transit (TLoS) | | Truck (TkLoS) | | |
| | PLoS | Target | BLoS | Target | TLoS | Target | TkLoS | Target | |
| March Road adjacent to development | F | Α | E | С | D | Α | Α | D | |
| Teron Road west side across from development | В | Α | Α | В | D | D | - | n/a | |
| Teron Road east side adjacent to development | F | Α | С | В | D | D | - | n/a | |
| Teron Road east side Future | В | Α | С | В | D | D | - | n/a | |

Pedestrian

• All road segments do not meet pedestrian PLoS due fast operating speeds and number of daily traffic volumes. The proposed construction of the east sidewalk on Teron Road improves PLoS from 'F' to 'B'.



<u>Bicycle</u>

- **Teron Road** east side does not meet cyclist BLoS given the local route higher targets and the lack of cycling facilities. The west side meets the BLoS target given the physically separated MUP
- March Road does not meet cyclist BLoS given the high operation speeds and number of travel lanes

Transit

- Teron Road meets transit TLoS on both sides
- March Road does not meet transit TLoS given that March Road is a proposed rapid transit corridor

Truck

- Teron Road is not a truck route
- March Road meets truck TkLoS targets

4.4. Access Intersection Design

4.4.1. Location and Design of Access

The proposed access to the site includes a main driveway connection to Teron Road which has a small branch into the underground parking structure directly behind 1131 Teron Road structure and access to surface parking behind 1151 Teron Road structure. The access will create a new driveway on to Teron Road, located approximately 150 meters south of Steacie/Teron and 115 meters north of Bethune Way. This distance adheres to the By-law (No. 2003-447) Section 24(m)(ii), which suggests a separation between the site access and nearest intersection of 45 meters for a site with 200 to 299 parking spaces. There are no nearby private approaches.

4.4.2. Intersection Control

A traffic signal warrant and an all-way stop control warrant was completed at Site Access/Teron and neither were warranted due to the very low traffic volumes. All warrant analysis has been provided in **Appendix F**.

The proposed stop control on the side street is therefore acceptable. The access driveway is proposed as a full-movement intersection.

4.4.3. Intersection Design

The access driveway will compose of a single northbound through-right and a southbound through-left on Teron Road, and a single left-right shared lane on the westbound site egress. The driveway access consists of a single lane per direction. Auxiliary turn lanes were not warranted at the access driveway based on queue lengths from Synchro (V10). With approximately 30 meters of driveway length to the first conflict point, where the underground parking garage ramp is located, the site meets the minimum clear throat length requirements for this location.

4.5. Transportation Demand Management

4.5.1. Context for TDM

Based on the type of development, it is assumed that most trips generated by the proposed site will be residents leaving the site in the AM peak to go to work and returning from work to the proposed site in the PM peak. Sections 3.1.1 and 3.1.2 describe how many trips are anticipated per travel mode and anticipates the likely locations that they will travel to and from based on the OD-Survey 2011 for Ottawa. The site is not located within 600 meters of existing rapid transit; however, it is located within 600 meters of a future proposed transit priority corridor with a BRT on March Road.

4.5.2. Need and Opportunity

Since the development is located near a future transit priority corridor with BRT on March Road, measures to provide sustainable active mode shares are encouraged. Such measures are described in more detail in Section 4.5.3 below, but can include reduced parking, more aggressive Multi-Modal Levels of Service (MMLOS) as described in Section 4.3 and 4.9 and safe and efficient connectivity to public transit as described in Section 4.7, to name a few.



4.5.3. TDM Program

The TDM infrastructure checklist and TDM Measures are attached as Appendix G, but some examples include

- The development proposes to construct a sidewalk fronting the site and extending it past their site to create an integrated sidewalk network
- Development will exceed minimum bicycle parking spots
- Proposed multi-use pathway on the north side of the site fronting March Road

4.6. Neighborhood Traffic Management

4.6.1. Adjacent Neighborhoods

Exempt. See table Table 1.

4.7. Transit

4.7.1. Route Capacity

With less than 40 to 50 'new' two-way transit passenger trips per hour generated for the AM and PM peak hours, it is not anticipated that this development will place buses at capacity. Given the transit priority with BRT measures are planned for March Road, it is anticipated that the future transit network will have additional capacity to accommodate the subject development transit demand. Additionally, added capacity is available on local bus routes on Teron Road and March Road.

4.7.2. Transit Priority

Minor delays may occur on Teron Road transit routes occasionally as through busses on Teron Road may have to wait for turning vehicles to and from the site access, however, delays are anticipated to be minor. Once the March Road BRT is built, it is anticipated that the site will have negligible impacts on routes using the BRT given that the site does not have an access on to March Road and forecasted vehicle volumes are minimal.

4.8. Review of Network Concept

Exempt. See table **Table 1**.

4.9. Intersection Design

4.9.1. Intersection Control

Refer to Section 4.4.2.

4.9.2. Intersection Design

Multi-Modal Level of Service

As stated in the MMLOS Guidelines, only signalized intersections are considered for the intersection Level of Service measures. The March/Teron and Beaverbrook/Teron intersections are signalized intersections within the study area. The MMLOS analysis is summarized in **Table 12**, with detailed analyses provided in **Appendix H**.

Level of Service Intersection **Pedestrian Bicycle (BLoS)** Transit (TLoS) Truck (TkLoS) **PLoS** Target **BLoS Target** TLoS **Target TkLoS Target** March/Teron F F С F D Α Α Ε Α В Ε Beaverbrook/Teron D n/a

Table 12: MMLOS - Intersections

Pedestrian

 For both intersections, pedestrians must cross at least 5 lanes of traffic based on the distance from curb to curb divided by 3.5 meters. There are no options that can help improve the PLoS significantly enough to come anywhere near the target PLoS 'A'



<u>Bicycle</u>

 For both intersections, the bicycle BLoS target was not met given the absence of bicycle facilities and number of lanes needed to cross to perform a left turn. Providing cycling facilities and lowering the speed limit to 40 km/h on Teron Road would meet the cyclist BLoS targets

Transit

Transit TLoS targets were not met for either intersection as it relies on average signal delay. To reach
the target goal for Beaverbook/Teron, buses must wait no longer than 30 seconds at the intersection

Truck

 Truck target level of service was met for March/Teron intersection. Beaverbrook nor Teron Road are classified as truck routes

Existing Intersection Performance

The following **Table 13** provides a summary of the existing traffic operations at the study area intersection based on the Synchro (V10) traffic analysis software. The subject intersections were assessed in terms of the volume-to-capacity (v/c) ratio and the corresponding Level of Service (LoS) for the critical movement(s). The Synchro model outputs of existing conditions are provided within **Appendix I** and the volumes used were obtained from **Figure 5**.

Weekday AM Peak (PM Peak) **Critical Movement** Intersection Intersection max. v/c or LoS LoS Delay (s) Movement V/C avg. delay (s) **Signalized Intersections** March/Teron F(F) 1.88(1.01) EBL(SBT) 84.7(39.1) F(E) 1.12(0.96) Beaverbrook/Teron A(D) 0.47(0.83) NBT(SBT) 9.7(19.9) A(B) 0.40(0.67) **Unsignalized Intersections** Steacie/Teron B(C) 12(17) EB(EB) 2(4) A(A) Note: Analysis of signalized intersections assumes a PHF of 0.9 and a saturation flow rate of 1800 veh/h/lane.

Table 13: Existing Intersection Performance

As seen in **Table 13**, all intersections operate overall at good LoS 'B' or better with critical movements operating at LoS 'D' or better during the existing conditions with the exception of March/Teron which is operating at capacity in the AM and near capacity in the PM. The critical movements at capacity for March/Teron include EBL which is well over capacity in the AM given that it has 475 left-turns from Teron Road to March Road using a single turn lane. The critical movement for the PM is the southbound through on March Road.

Background Conditions 2027

The future background 2027 conditions are anticipated to operate worse than 2022 as more developments were accounted for and the future background volumes have been increased by 2% annually for a longer period. Since 2027 background has the same intersection layouts as 2022 and is the more critical of the two scenarios, only 2027 will be analyzed. The future projected 2027 background volumes are illustrated in **Figure 14** with projected operation outputs in **Table 14**. The detailed Synchro results can be found in **Appendix J**.



Table 14: 2027 Background Intersection Performance

| | Weekday AM Peak (PM Peak) | | | | | | | | |
|--|---------------------------|-------------------------------|----------------------|-----------------------|---------|------------|--|--|--|
| Intersection | | Critical Movem | ent | Intersection | | | | | |
| intercooper. | LoS | max. v/c or avg. delay (s) | Movement | Delay (s) LoS | | v/c | | | |
| Signalized Intersections | | | | | | | | | |
| March/Teron | F(F) | 1.68(1.17) | EBL(SBT) | 80.4(64.4) | F(F) | 1.14(1.09) | | | |
| Beaverbrook/Teron | A(D) | 0.50(0.84) | NBT(SBT) | 10.0(19.9) | A(B) | 0.42(0.68) | | | |
| Unsignalized Intersections | | | | | | | | | |
| Steacie/Teron B(C) 13(20) EB(EB) 3(4) A(A) - | | | | | | | | | |
| Note: Analysis of signalized inte | rsections a | assumes a PHF of 1.0 | and a saturation flo | ow rate of 1800 veh/h | n/lane. | | | | |

As seen in **Table 14**, all intersections operate overall similar with to existing intersection performance with the exception of March/Teron which continues to deteriorate in performance due to very conservative background growths of 2% assumed.

Future Conditions 2022

The future full build-out 2022 volumes were derived by superimposing background 2022 volumes which include other area developments and background growth, with future site-generated volumes. The future projected 2022 volumes are illustrated in **Figure 16** with projected operation outputs in **Table 15**. The detailed Synchro results can be found in **Appendix K**.

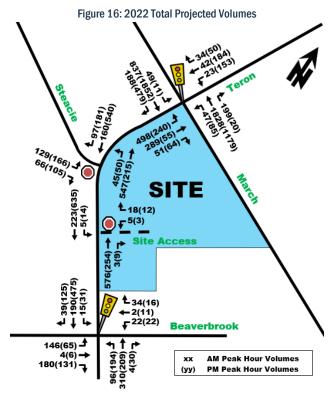




Table 15: 2022 Full Build-out Intersection Performance

| | Weekday AM Peak (PM Peak) | | | | | | | | |
|-----------------------------------|----------------------------|-------------------------------|----------------------|---------------------|---------|------------|--|--|--|
| Intersection | | Critical Movem | ent | Intersection | | | | | |
| moloodasii | LoS | max. v/c or avg. delay (s) | Movement | Delay (s) LoS | | v/c | | | |
| Signalized Intersections | | | | | | | | | |
| March/Teron | F(F) | 1.77(1.06) | EBL(SBT) | 75.7(45.5) | F(E) | 1.09(1.00) | | | |
| Beaverbrook/Teron | A(D) | 0.48(0.84) | NBT(SBT) | 9.8(19.7) | A(B) | 0.41(0.67) | | | |
| Unsignalized Intersections | Unsignalized Intersections | | | | | | | | |
| Steacie/Teron | B(C) | 12(18) | EB(EB) | 3(4) | A(A) | - | | | |
| Site Access/Teron B(C) | | 13(11) | WB(WB) | 1(1) | A(A) | - | | | |
| Note: Analysis of signalized inte | rsections a | ssumes a PHF of 1.0 | and a saturation flo | w rate of 1800 veh/ | h/lane. | | | | |

As seen in Table 15, all study area intersections are expected to operate similarly to existing conditions.

Future Conditions 2027

The future full build-out 2027 volumes were derived by superimposing background 2027 volumes which include other area developments and background growth, with future site-generated volumes. The future projected 2027 volumes are illustrated in **Figure 17** with projected operation outputs in **Table 16**. The detailed Synchro results can be found in **Appendix K**.

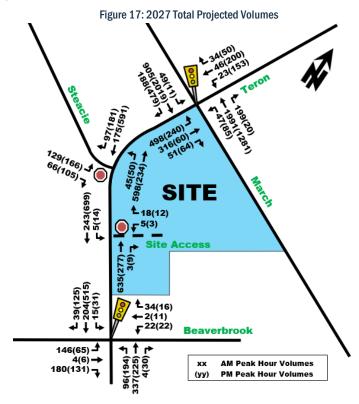




Table 16: 2027 Full Build-out Intersection Performance

| | Weekday AM Peak (PM Peak) | | | | | | | | | |
|---------------------------------------|---|----------------|-----------|--------------|------|------------|--|--|--|--|
| Intersection | | Critical Movem | ent | Intersection | | | | | | |
| ilitoiseedell | LoS max. v/c or avg. delay (s) Movement | | Delay (s) | LoS v/c | | | | | | |
| Signalized Intersections | | | | | | | | | | |
| March/Teron | F(F) | 1.70(1.17) | EBL(SBT) | 81.2(65.6) | F(F) | 1.15(1.09) | | | | |
| March/Teron Improvements ₁ | <i>E(D)</i> | 0.99(0.84) | EBL(EBL) | 36.4(27.9) | D(D) | 0.88(0.81) | | | | |
| Beaverbrook/Teron | A(D) | 0.51(0.84) | NBT(SBT) | 10.0(20.0) | A(B) | 0.43(0.69) | | | | |
| Unsignalized Intersections | | | | | | | | | | |
| Steacie/Teron | B(C) | 13(20) | EB(EB) | 3(4) | A(A) | - | | | | |
| Site Access/Teron | B(C) | 14(12) | WB(WB) | 1(1) | A(A) | - | | | | |

As seen in **Table 16**, all study area intersections are expected to operate similarly to background 2027 conditions with acceptable delays on all intersections except for March/Teron which is operating at capacity, similarly to existing and 2027 background. A large factor into worsening conditions at March/Teron include aggressive future background growths. A sensitivity test was done by extending the 6-lane cross-section from March/Herzburg intersection to March/Teron which is located approximately 1-kilometer further north on March Road. The addition of the March Road through lanes yields acceptable levels of service but would require large investments. Twinning the eastbound left from Teron Road to March Road would significantly improve the critical movement in the AM but would likely lead to additional traffic choosing Teron Road as their primary route and would eventually lead to new capacity issues at this intersection and at other Teron Road intersections.

The transit improvements proposed on March Road, including the BRT corridor are anticipated to change commuter habits by increasing transit ridership and decreasing vehicle dependency, thus, reducing vehicles in the network and improving intersection performance.

Future Conditions if Custom Mode Share not Met

The trips generated based on Kanata mode share are shown in **Figure 18** in the event that the custom mode shares are not met. The projected intersection performance for the critical scenario 2027 with Kanata mode shares is shown in **Table 17** with detailed output in **Appendix L**.



129(166) 4 66(105) 7 **Site Access** £34(16) 22(22) Beaverbrook 146(65) 4(6) **AM Peak Hour Volumes** хx 180(131) **PM Peak Hour Volumes**

Figure 18: 2027 Total if Custom Mode Share Not Met Projected Volumes

Table 17: Intersection Performance if TOD Mode Shares Not Met

| | Weekday AM Peak (PM Peak) | | | | | | | | |
|-----------------------------------|----------------------------|-------------------------------|----------------------|-----------------------|--------|------------|--|--|--|
| Intersection | | Critical Movem | ent | Intersection | | | | | |
| intersection | LoS | max. v/c or avg. delay (s) | Movement | Delay (s) | LoS | v/c | | | |
| Signalized Intersections | | | | | | | | | |
| March/Teron | F(F) | 1.72(1.18) | EBL(SBT) | 82.2(66.5) | F(F) | 1.15(1.10) | | | |
| Beaverbrook/Teron | A(D) | 0.51(0.84) | NBT(SBT) | 10.0(20.0) | A(B) | 0.43(0.69) | | | |
| Unsignalized Intersections | Unsignalized Intersections | | | | | | | | |
| Steacie/Teron | B(C) | 13(21) | EB(EB) | 3(5) | A(A) | - | | | |
| Site Access/Teron | B(C) | 14(12) | WB(WB) | 1(1) | A(A) | - | | | |
| Note: Analysis of signalized inte | rsections a | ssumes a PHF of 1.0 | and a saturation flo | ow rate of 1800 veh/h | /lane. | | | | |

As seen in Table 17, intersections are expected to perform very similarly to 2027 with TOD mode shares, meaning that this development does not have a big impact on worsening traffic conditions.

FINDINGS AND RECOMMENDATIONS

Based on the results summarized herein the following findings and recommendations are provided:

Existing Conditions

• The site is currently an empty field with overhead hydro wires and is zoned as O1[2143] and R5A[2144] S327



- The site is located in a future transit priority corridor with a BRT on March Road
- Overall, there are no existing safety concerns along the proposed development frontage and study area intersections. Therefore, no mitigation measures were considered
- Existing intersections operate at good overall LoS 'B' or better with critical movements of 'D' or better during
 the weekday peak hours, with the exception of March/Teron which is performing overall at or near capacity
 and with critical movements surpassing capacity for AM and PM peak hours

Proposed Development

- The proposed development will have 131 residential units combined in a 3-storey and a 9-storey building located at 1131 and 1151 Teron Road respectively
- The proposed development is projected to generate 'new' vehicle volumes of approximately 30 to 40 veh/h two-way total during the weekday morning and afternoon peak hours respectively
- The proposed development is projected to generate approximately 40 to 50 'new' transit trips during the AM and PM peak hour periods, which can be accommodated by rapid route #63 and other local bus routes.
 Additional capacity will be available once March Road becomes a BRT corridor
- A total of 200 parking spaces are proposed which meet the City's minimum and maximum parking requirements for this development
- The development will be accessed by a single two-way driveway on to Teron Road

Future Conditions

- Other nearby developments and a 2% growth rate to through movements were applied to existing volumes
 to estimate 2027 background conditions, which operated worse than existing conditions, predominantly to
 do with the high annual growth rate assumed
- Future conditions with the addition of site generated traffic performs similar to background 2027 volumes, implying that the development does not play a large role in worsening future conditions
- If the TOD modal shares are not met, the study area intersection performance is anticipated to operate similarly to 2027 future conditions
- The MMLOS road segment analysis shows that existing and future conditions on boundary streets do not meet MMLOS area targets for pedestrians due to high vehicular volumes and vehicle travel speeds. The bike, transit and truck targets are met for some segments but fail in others. The addition of cycling facilities would improve the BLoS to target levels
- The MMLOS intersection analysis shows that only truck target goals are met. All other targets including
 pedestrian, cyclist and transit targets were not met due to the number of lanes required to be crossed,
 operating speeds or delays at certain approaches
- The development proposes to construct a multi-use pathway on the north side of the site fronting March Road and connecting to existing MUP network
- The development is proposing to provide 96 bicycle parking spaces which is higher than the minimum required of 67
- The development proposes to construct a sidewalk fronting the site on Teron Road. In addition to the site
 frontage, the developer plans to extend the sidewalk south past their site to the existing sidewalk starting
 at Bethune Way. This sidewalk extension would create an integrated sidewalk network

Based on the foregoing findings, the proposed development located at 1131 and 1151 Teron Road is recommended from a transportation perspective.

Prepared By:

Juan Lavin, E.I.T.

Reviewed By:

Matthew Mantle, P.Eng. Transportation Engineer



SCREENING FORM & CITY CORRESPONDANCE



City of Ottawa 2017 TIA Guidelines Date 24-Feb-21 **TIA Screening Form** Project 1131 & 1151 Teron Road

Project Number 477778 - 01000

| Results of Screening | Yes/No |
|---|--------|
| Development Satisfies the Trip Generation Trigger | Yes |
| Development Satisfies the Location Trigger | Yes |
| Development Satisfies the Safety Trigger | Yes |

| Module 1.1 - Description of Proposed Development | | | | | | |
|--|--|--|--|--|--|--|
| Municipal Address | 1131 & 1151 Teron Road | | | | | |
| Description of location | Currently a vacant lot, located between Teron Road to the southwest and March Road to the north. | | | | | |
| Land Use | Proposed 3-storey and 9-storey Residential | | | | | |
| Development Size | 131 Residential Apartments | | | | | |
| Number of Accesses and Locations | Single 2-way access to Teron Road, approximately 150 m south of Steacie/Teron | | | | | |
| Development Phasing | 2 Phases | | | | | |
| Buildout Year | 2022 and before 2026 | | | | | |
| Sketch Plan / Site Plan | See attached | | | | | |

| Module 1.2 - Trip Generation Trigger | | | |
|--------------------------------------|-------------------------|-------|--|
| Land Use Type | Townhomes or Apartments | | |
| Development Size | 131 | Units | |
| Trip Generation Trigger Met? | Yes | | |

| Module 1.3 - Location Triggers | | |
|--|-----|--|
| Development Proposes a new driveway to a boundary street that is designated as part of the City's Transit Priority, Rapid Transit, or Spine Bicycle Networks (See Sheet 3) | Yes | Teron Road and March Road are both Spine Bicycle Network according to TMP Map1 |
| Development is in a Design Priority Area (DPA) or Transit- oriented Development (TOD) zone. (See Sheet 3) | Yes | Property parcel within March Road Transit Oriented Development |
| Location Trigger Met? | Yes | |

| Module 1.4 - Safety Triggers | | |
|--|-----|---|
| Posted Speed Limit on any boundary road | <80 | km/h |
| Horizontal / Vertical Curvature on a boundary street limits sight lines at a proposed driveway | Yes | Sight triangles on March/Teron required for final plan |
| A proposed driveway is within the area of influence of an adjacent traffic signal or roundabout (i.e. within 300 m of intersection in rural conditions, or within 150 m of intersection in urban/ suburban conditions) or within auxiliary lanes of an intersection; | Yes | The access on Teron Road is less than 150m from the Teron Road/Steacie Drive intersection |
| A proposed driveway makes use of an existing median break that serves an existing site | No | |
| There is a documented history of traffic operations or safety concerns on the boundary streets within 500 m of the development | No | |
| The development includes a drive-thru facility | No | |
| Safety Trigger Met? | Yes | |



25 August 2021

City of Ottawa Development Review Services 110 Laurier Avenue West Ottawa, ON K1P 1J1

Attention: Josiane Gervais, P.Eng.

Dear Josiane:

Re: 1131 & 1151 Teron Road TIA

Step 4 – Response to City Comments

The following response has been prepared in response to City of Ottawa comments received on July 15, 2021. City comments have been noted in black with the corresponding responses from Parsons in Green.

Transportation Engineering Services

- 1. Confirm that sidewalk will be provided along the entire frontage of the site and that the missing link to Bethune Way will also be constructed as part of the site development (as indicated in previous circulations and indicated in section 4.5.3). This sidewalk extension will require an RMA as it is outside the property limits. The sidewalk is planned to extend to the southern property limit along Teron Road.
- 2. The TIA Strategy report has been updated to remove the commercial component of the strategy report submitted for the zoning application. Staff clarified that the timing for the March Road BRT from Corkstown to Solandt is tentatively scheduled for funding in 2027/2028. Review this information and modify the Demand Rationalization module as required. Indicate if the modal shares (Table 6) used to forecast trips by mode require adjustment to reflect this information. An adjustment may also be required for the background growth. Resubmission of the report is not required if the change does not impact the recommendations. Our background growth is not impacted by the change in BRT construction, in fact, a very conservative 2% annual growth rate was assumed. The change in site generated vehicle trips forecasted before and after mode share assumptions is less than 30 new vehicles which will have a negligible impact on the network.
- 3. Transit Services should be contacted with regard to facilities to support transit modal share. Noted

Traffic Signal Operations

4. The eastbound left-turn queues from Teron Road onto March Road stretch beyond the site access. Review how this will impact the level of service at the access during peak periods. Eastbound left-turn queues from Teron/March are anticipated to queue beyond the site access. This will cause longer delays, however, vehicles exiting and entering the site will likely have breaks in the queues when northbound vehicles are stopped or slowly moving allowing them access to or from Teron Road/site.

Traffic Signal Design

5. No comments. Noted

Street Lighting

- 6. No comments with initial TIA for this circulation. Street Lighting reserves the right to make future comments based on subsequent submissions. Noted
- 7. Future considerations are as follows:
 - a) If there are any proposed changes to the existing roadway geometry, the City of Ottawa Street Light Asset Management Group is required to provide a full street light design. Upon completion of proposed roadway geometry design changes, please submit digital Micro Station drawings with proposed roadway geometry changes to the Street Lighting Department, so that we may proceed with the detailed street light design and coordination with the Street Light maintenance provider and all necessary parties. Be advised that the applicant will be 100% responsible for all costs associated with any Street Light design as a result of the roadway geometry change. Noted
 - b) Alterations and/or repairs are required where the existing street light plant is directly, indirectly, or adversely affected by the scope of work under this circulation, due to the proposed road reconstruction process. All street light plant alterations and/or repairs must be performed by the City of Ottawa's Street Light maintenance provider. Noted
 - c) Be advised that the applicant will be 100% responsible for all costs associated with any relocations/modifications to the existing street light plant. Should a conflict arise or if you have any questions please contact Barrie Forrester at (613) 580-2424 ext 23332 or Barrie.Forrester@ottawa.ca. Noted

Transit Services

8. Comments were not provided at the time of this letter. Comments have been requested and will be forwarded directly to Parsons once received. Noted

Development Review - Transportation

9. Please address the above comments and re-submit the TIA and digital files of ICA outputs (Synchro/Sidra/Rodel, if applicable), as per comment # 2 above. Alternative, please address the above comments and proceed to submitting the Step 5: Final TIA (remove draft watermark, sign and include Certification Form). See attached



APPENDIX B

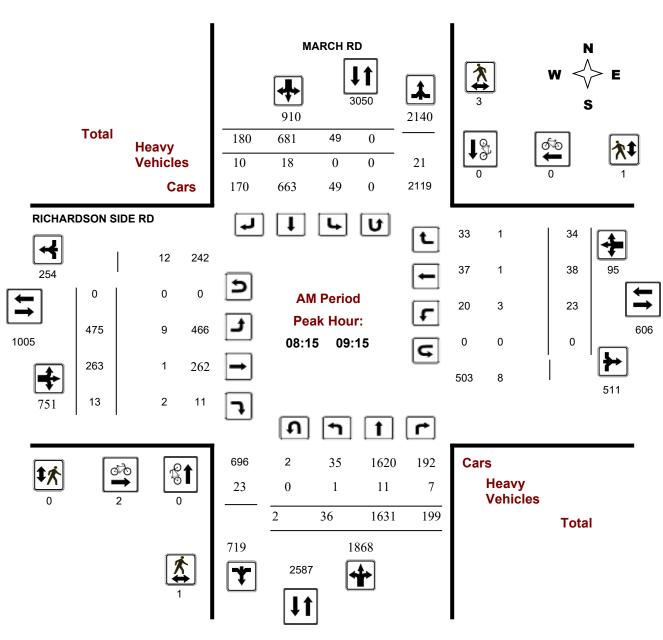
TRAFFIC COUNT DATA



Turning Movement Count - Full Study Peak Hour Diagram

MARCH RD @ RICHARDSON SIDE RD

Survey Date: Thursday, November 02, 2017 WO No: 37345
Start Time: 07:00 Device: Miovision



Comments

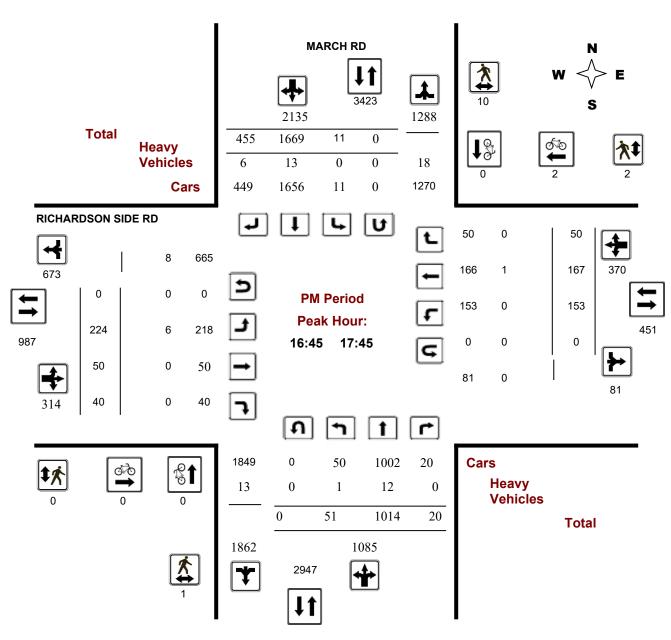
2019-Jun-14 Page 1 of 4



Turning Movement Count - Full Study Peak Hour Diagram

MARCH RD @ RICHARDSON SIDE RD

Survey Date: Thursday, November 02, 2017 WO No: 37345
Start Time: 07:00 Device: Miovision



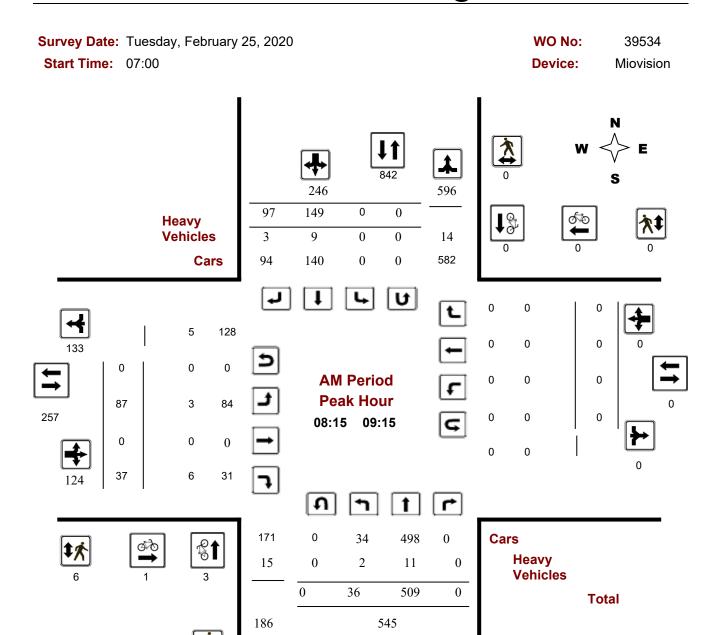
Comments

2019-Jun-14 Page 4 of 4



Turning Movement Count - Peak Hour Diagram

RICHARDSON SIDE RD/TERON RD @ STEACIE DR



Comments 5476125 - FEB 25, 2020 - 8HRS - CHRIS MORRIS

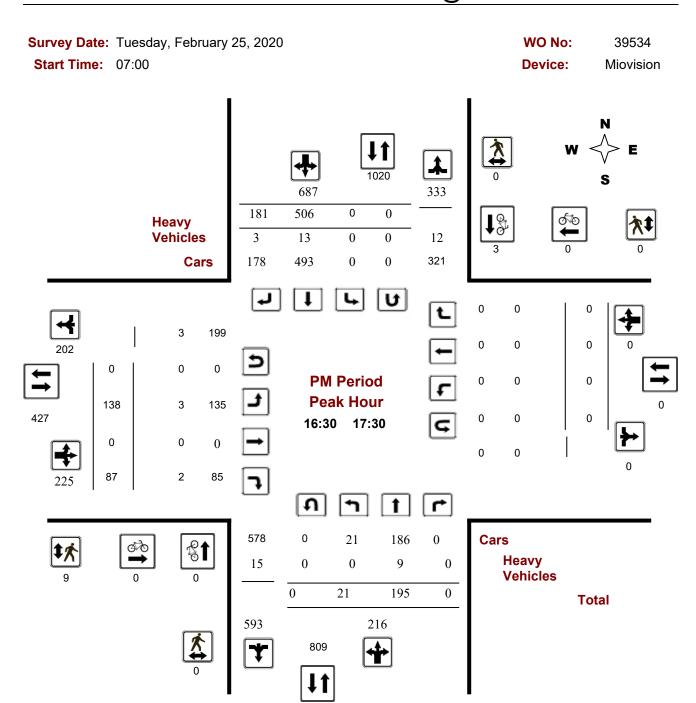
2020-Oct-09 Page 1 of 3

731



Turning Movement Count - Peak Hour Diagram

RICHARDSON SIDE RD/TERON RD @ STEACIE DR



Comments 5476125 - FEB 25, 2020 - 8HRS - CHRIS MORRIS

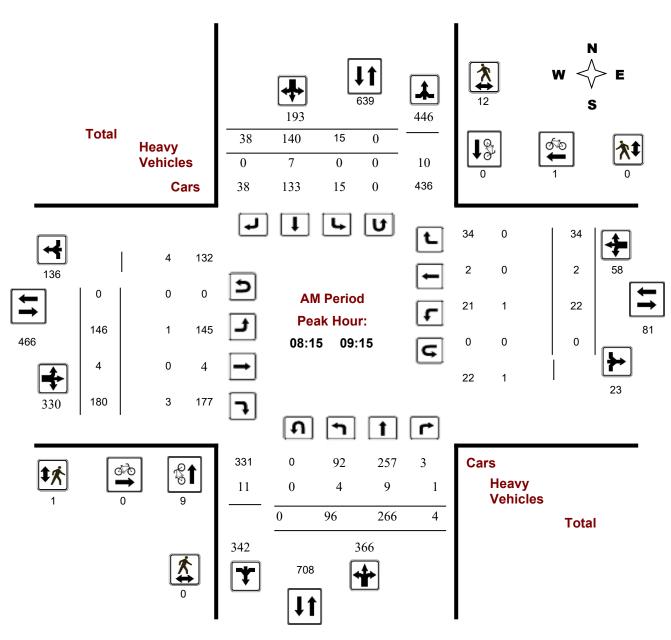
2020-Oct-09 Page 3 of 3



Turning Movement Count - Full Study Peak Hour Diagram

TERON RD @ BEAVERBROOK RD/PENFIELD DR N

Survey Date: Wednesday, August 10, 2016 WO No: 36159
Start Time: 07:00 Device: Miovision



Comments

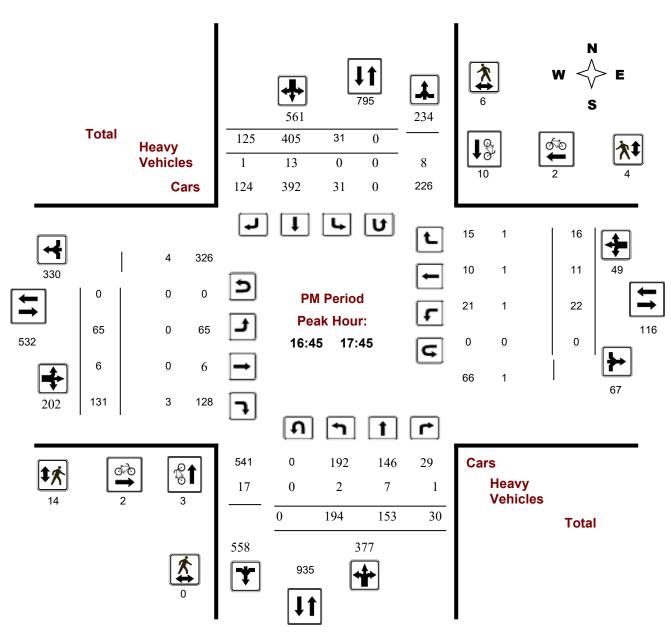
2019-Jun-14 Page 1 of 4



Turning Movement Count - Full Study Peak Hour Diagram

TERON RD @ BEAVERBROOK RD/PENFIELD DR N

Survey Date: Wednesday, August 10, 2016 WO No: 36159
Start Time: 07:00 Device: Miovision



Comments

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COLLISION DATA

| 1 | [ota | al A | rea |
|---|------|------|-----|

| Classification of Accident | Rear End | Turning Movement | Sideswipe | Angle | Approaching | Single Vehicle (other) | Single vehicle (Unattended vehicle) | Other | Total | |
|-------------------------------|-----------|---------------------|-----------|-----------|-------------|---------------------------|---|----------|-------|------|
| P.D. only | 23 | 6 | 6 | 11 | 0 | 11 | 0 | 0 | 57 | 75% |
| Non-fatal injury | 5 | 6 | 1 | 1 | 1 | 5 | 0 | 0 | 19 | 25% |
| Fatal Injury | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0% |
| Non reportable | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0% |
| Total | 28 | 12 | 7 | 12 | 1 | 16 | 0 | 0 | 76 | 100% |
| | #1 or 37% | #3 or 16% | #5 or 9% | #3 or 16% | #6 or 1% | #2 or 21% | #7 or 0% | #7 or 0% | - | • |

MARCH RD / RICHARDSON SIDE RD

| Years | Total # Collisions | 24 Hr AADT Veh Volume | Days | Collisions/MEV |
|-------|-----------------------|--------------------------|------|----------------|
| - | 27 | 40.547 | 1025 | 0.36 |

| • | Classification of Accident | Rear End | Turning Movement | Sideswipe | Angle | Approaching | Single Vehicle (other) | Single vehicle (Unattended vehicle) | Other | Total | |
|---|-------------------------------|----------|---------------------|-----------|-------|-------------|---------------------------|---|-------|-------|------|
| Р | .D. only | 8 | 5 | 4 | 2 | 0 | 1 | 0 | 0 | 20 | 74% |
| N | on-fatal injury | 2 | 3 | 0 | 1 | 0 | 1 | 0 | 0 | 7 | 26% |
| N | on reportable | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0% |
| Т | otal | 10 | 8 | 4 | 3 | 0 | 2 | 0 | 0 | 27 | 1009 |
| _ | | 37% | 30% | 15% | 11% | 0% | 7% | 0% | 0% | | - |

HERZBERG RD / MARCH RD

| Years | 1 7 | Total # 24 Hr AADT | | Davs | Collisions/MEV |
|--------|-----|--------------------|------------|------|----------------|
| 1 cars | | ollisions | Veh Volume | Days | COMISIONS/PILV |
| - | | 22 | 41 907 | 1035 | 0.42 |

| Classification of Accident | Rear End | Turning Movement | Sideswipe | Angle | Approaching | Single Vehicle (other) | Single vehicle (Unattended vehicle) | Other | Total | |
|-------------------------------|----------|---------------------|-----------|-------|-------------|---------------------------|---|-------|-------|---|
| P.D. only | 12 | 0 | 2 | 5 | 0 | 6 | 0 | 0 | 25 | ĺ |
| Non-fatal injury | 2 | 2 | 1 | 0 | 0 | 2 | 0 | 0 | 7 | ĺ |
| Non reportable | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | i |
| Total | 14 | 2 | 3 | 5 | 0 | 8 | 0 | 0 | 32 | |
| | 44% | 6% | 9% | 16% | 0% | 25% | 0% | 0% | | |

TERON RD / BEAVERBROOK RD/PENFIELD DR N

| Years | Total # Collisions | 24 Hr AADT Veh Volume | Days | Collisions/MEV |
|-------|-----------------------|--------------------------|------|----------------|
| - 5 | 6 | 10 559 | 1875 | 0.31 |

| Classification of Accident | Rear End | Turning Movement | Sideswipe | Angle | Approaching | Single Vehicle (other) | Single vehicle (Unattended vehicle) | Other | Total | |
|-------------------------------|----------|---------------------|-----------|-------|-------------|---------------------------|---|-------|-------|-----|
| P.D. only | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 3 | 509 |
| Non-fatal injury | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 3 | 50 |
| Non reportable | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 09 |
| Total | 0 | 1 | 0 | 2 | 0 | 3 | 0 | 0 | 6 | 100 |
| | | | | | | | | | | |

BETHUNE CRT / TERON RD

| Years | Total # Collisions | 24 Hr AADT Veh Volume | Days | Collisions/MEV |
|-------|-----------------------|--------------------------|------|----------------|
| 5 | 1 | 10,200 | 1825 | 0.05 |

| Classification of Accident | Rear End | Turning Movement | Sideswipe | Angle | Approaching | Single Vehicle (other) | Single vehicle (Unattended vehicle) | Other | Total | |
|-------------------------------|----------|---------------------|-----------|-------|-------------|---------------------------|---|-------|-------|------|
| P.D. only | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 100% |
| Non-fatal injury | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0% |
| Non reportable | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0% |
| Total | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 100% |
| | | | | | | | | | | |

RICHARDSON SIDE RD/TERON RD / STEACIE DR

| Years | Collisions | Veh Volume | Days | Collisions/MEV |
|-------|------------|------------|------|----------------|
| 5 | 1 | 12.074 | 1825 | 0.05 |

| Classification of Accident | Rear End | Turning Movement | Sideswipe | Angle | Approaching | Single Vehicle (other) | Single vehicle (Unattended vehicle) | Other | Total | |
|-------------------------------|----------|---------------------|-----------|-------|-------------|---------------------------|---|-------|-------|-----|
| P.D. only | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | |
| Non-fatal injury | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Non reportable | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | i . |
| Total | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | |
| | 0% | 100% | 0% | 0% | 0% | 0% | 0% | 0% | | |

MARCH RD /twn RICHARDSON SIDE RD & HERZBERG RD

| Years | Total # Collisions | 24 Hr AADT Veh Volume | Days | Collisions/MEV |
|-------|-----------------------|--------------------------|------|----------------|
| | 6 | n/a | 1075 | n/2 |

| Classification of Accident | Rear End | Turning Movement | Sideswipe | Angle | Approaching | Single Vehicle (other) | Single vehicle (Unattended vehicle) | Other | Total | |
|-------------------------------|----------|---------------------|-----------|-------|-------------|---------------------------|---|-------|-------|--|
| P.D. only | 1 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 4 | |
| Non-fatal injury | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 2 | |
| Non reportable | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Total | 2 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 6 | |
| | 33% | 0% | 0% | 0% | 17% | 50% | 0% | 0% | | |

TERON RD /twn CHISHOLM CRT & BEAVERBROOK LANE

| Years | Total # Collisions | 24 Hr AADT Veh Volume | Days | Collisions/MEV |
|-------|-----------------------|--------------------------|------|----------------|
| 5 | 1 | n/a | 1825 | n/a |

| Classification of Accident | Rear End | Turning Movement | Sideswipe | Angle | Approaching | Single Vehicle (other) | (Unattended vehicle) | Other | Total | |
|-------------------------------|----------|---------------------|-----------|-------|-------------|---------------------------|----------------------|-------|-------|---|
| P.D. only | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| Non-fatal injury | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | i |
| Non reportable | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Total | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| | 100% | 0% | 0% | 0% | 0% | 0% | 0% | 0% | | - |

TERON RD /twn BEAVERBROOK LANE & BEAVERBROOK RD

| Years | Total # Collisions | 24 Hr AADT Veh Volume | Days | Collisions/MEV |
|-------|-----------------------|--------------------------|------|----------------|
| 5 | 1 | n/a | 1825 | n/a |

| Classification of Accident | Rear End | Turning Movement | Sideswipe | Angle | Approaching | Single Vehicle (other) | (Unattended vehicle) | Other | Total | |
|-------------------------------|----------|---------------------|-----------|-------|-------------|---------------------------|----------------------|-------|-------|------|
| P.D. only | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 100% |
| Non-fatal injury | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0% |
| Non reportable | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0% |
| Total | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 100% |
| | 0% | 0% | 0% | 100% | 0% | 0% | 0% | 0% | | |



TRAFFIC GROWTH DATA

Teron/March <u>8 hrs</u>

| Year | Date | Norti | h Leg | Sout | h Leg | East | : Leg | West Leg | | Total |
|------|--------------|-------|-------|-------|-------|------|-------|----------|------|-------|
| rear | Date | SB | NB | NB | SB | WB | EB | EB | WB | iotai |
| 2009 | Tues July 14 | 10195 | 10467 | 9220 | 9616 | 1221 | 1559 | 3011 | 2405 | 47694 |
| 2010 | Thurs Aug 12 | 11632 | 12297 | 10911 | 10631 | 1446 | 1611 | 3432 | 2882 | 54842 |
| 2011 | Tues June 21 | 11215 | 14819 | 13681 | 10670 | 1798 | 2154 | 3514 | 2565 | 60416 |
| 2017 | Thurs Nov 2 | 10160 | 11305 | 9977 | 8851 | 1563 | 1734 | 3085 | 2895 | 49570 |
| | | | | | | | | | | |

| North | Leg |
|-------|-----|
|-------|-----|

| Year | | Cou | ınts | | % Change | | | |
|------|-------|-------|-------|-------|----------|-------|--------|--------|
| Teal | NB | SB | NB+SB | INT | NB | SB | NB+SB | INT |
| 2009 | 10467 | 10195 | 20662 | 47694 | | | | |
| 2010 | 12297 | 11632 | 23929 | 54842 | 17.5% | 14.1% | 15.8% | 15.0% |
| 2011 | 14819 | 11215 | 26034 | 60416 | 20.5% | -3.6% | 8.8% | 10.2% |
| 2017 | 11305 | 10160 | 21465 | 49570 | -23.7% | -9.4% | -17.6% | -18.0% |
| | | | | | | | | |

Regression Estimate Regression Estimate 2009 2017

12369 11942 11046 10331 23415 22273

Average Annual Change

-0.44% -0.83% -0.62%

West Leg

| Year | | Cou | ınts | | % Change | | | |
|-------|------|------|-------|-------|----------|--------|-------|--------|
| i cai | EB | WB | EB+WB | INT | EB | WB | EB+WB | INT |
| 2009 | 3011 | 2405 | 5416 | 47694 | | | | |
| 2010 | 3432 | 2882 | 6314 | 54842 | 14.0% | 19.8% | 16.6% | 15.0% |
| 2011 | 3514 | 2565 | 6079 | 60416 | 2.4% | -11.0% | -3.7% | 10.2% |
| 2017 | 3085 | 2895 | 5980 | 49570 | -12.2% | 12.9% | -1.6% | -18.0% |

Regression Estimate Regression Estimate 2009 2017

3312 2572 3162 2906

5884 6068 0.39%

Average Annual Change

-0.58%

1737

1816

11113

10631

0.56%

1.54%

East Leg

| Year | | Cou | ınts | | % Change | | | |
|------|------|------|-------|-------|----------|--------|--------|--------|
| rear | EB | WB | EB+WB | INT | EB | WB | EB+WB | INT |
| 2009 | 1559 | 1221 | 2780 | 47694 | | | | |
| 2010 | 1611 | 1446 | 3057 | 54842 | 3.3% | 18.4% | 10.0% | 15.0% |
| 2011 | 2154 | 1798 | 3952 | 60416 | 33.7% | 24.3% | 29.3% | 10.2% |
| 2017 | 1734 | 1563 | 3297 | 49570 | -19.5% | -13.1% | -16.6% | -18.0% |
| | | | | | | | | |

Regression Estimate Regression Estimate
Average Annual Change 2009 2017

1438 1638 1.64%

3176 3454 1.06%

South Leg

| Year | | Cou | ınts | | % Change | | | |
|------|-------|-------|-------|-------|----------|--------|--------|--------|
| Tear | NB | SB | NB+SB | INT | NB | SB | NB+SB | INT |
| 2009 | 9220 | 9616 | 18836 | 47694 | | | | |
| 2010 | 10911 | 10631 | 21542 | 54842 | 18.3% | 10.6% | 14.4% | 15.0% |
| 2011 | 13681 | 10670 | 24351 | 60416 | 25.4% | 0.4% | 13.0% | 10.2% |
| 2017 | 9977 | 8851 | 18828 | 49570 | -27.1% | -17.0% | -22.7% | -18.0% |
| | | | | | | | | |

Regression Estimate Regression Estimate **Average Annual Change**

2009 2017 -0.55%

10409 9050 -1.73%

21522 19682 -1.11%

Teron/March AM Peak

| Year | Date | North Leg | | South Leg | | East Leg | | West Leg | | Total |
|------|--------------|-----------|------|-----------|------|----------|-----|----------|-----|-------|
| Teal | Date | SB | NB | NB | SB | WB | EB | EB | WB | iotai |
| 2009 | Tues July 14 | 1123 | 1902 | 1990 | 1084 | 32 | 412 | 580 | 157 | 7280 |
| 2010 | Thurs Aug 12 | 1366 | 2324 | 2242 | 1274 | 99 | 418 | 579 | 270 | 8572 |
| 2011 | Tues June 21 | 1220 | 2707 | 2672 | 1102 | 78 | 702 | 726 | 185 | 9392 |
| 2017 | Thurs Nov 2 | 910 | 2140 | 1868 | 719 | 95 | 511 | 751 | 254 | 7248 |
| | | | | | | | | | | |

North Leg

| Year | | Coi | unts | | % Change | | | |
|------|------|------|-------|------|----------|--------|--------|--------|
| Tear | NB | SB | NB+SB | INT | NB | SB | NB+SB | INT |
| 2009 | 1902 | 1123 | 3025 | 7280 | | | | |
| 2010 | 2324 | 1366 | 3690 | 8572 | 22.2% | 21.6% | 22.0% | 17.7% |
| 2011 | 2707 | 1220 | 3927 | 9392 | 16.5% | -10.7% | 6.4% | 9.6% |
| 2017 | 2140 | 910 | 3050 | 7248 | -20.9% | -25.4% | -22.3% | -22.8% |
| | | | | | | | | |

Regression Estimate Regression Estimate 2009 2017

2275 2256 1269 936 3544 3191

Average Annual Change

-0.11% -3.74% -1.30%

West Leg

| Year | | Cou | ınts | | % Change | | | | |
|-------|-----|-----|-------|------|----------|--------|-------|--------|--|
| 1 Cai | EB | WB | EB+WB | INT | EB | WB | EB+WB | INT | |
| 2009 | 580 | 157 | 737 | 7280 | | | | | |
| 2010 | 579 | 270 | 849 | 8572 | -0.2% | 72.0% | 15.2% | 17.7% | |
| 2011 | 726 | 185 | 911 | 9392 | 25.4% | -31.5% | 7.3% | 9.6% | |
| 2017 | 751 | 254 | 1005 | 7248 | 3.4% | 37.3% | 10.3% | -22.8% | |
| | | | | | | | | | |

Regression Estimate Regression Estimate 2009 2017

766

256

799 1022

553

651

Average Annual Change

3.04%

3.40% 3.13%

East Leg

| Year | | Col | unts | | % Change | | | | |
|------|-----|-----|-------|------|----------|--------|--------|--------|--|
| real | EB | WB | EB+WB | INT | EB | WB | EB+WB | INT | |
| 2009 | 412 | 32 | 444 | 7280 | | | | | |
| 2010 | 418 | 99 | 517 | 8572 | 1.5% | 209.4% | 16.4% | 17.7% | |
| 2011 | 702 | 78 | 780 | 9392 | 67.9% | -21.2% | 50.9% | 9.6% | |
| 2017 | 511 | 95 | 606 | 7248 | -27.2% | 21.8% | -22.3% | -22.8% | |
| | | | | | | | | | |

Regression Estimate Regression Estimate
Average Annual Change 2009 2017 490 550

63 100 2.04%

1.46%

5.92%

South Leg

| Year | | Cou | ınts | | % Change | | | |
|------|------|------|-------|------|----------|--------|--------|--------|
| Teal | NB | SB | NB+SB | INT | NB | SB | NB+SB | INT |
| 2009 | 1990 | 1084 | 3074 | 7280 | | | | |
| 2010 | 2242 | 1274 | 3516 | 8572 | 12.7% | 17.5% | 14.4% | 17.7% |
| 2011 | 2672 | 1102 | 3774 | 9392 | 19.2% | -13.5% | 7.3% | 9.6% |
| 2017 | 1868 | 719 | 2587 | 7248 | -30.1% | -34.8% | -31.5% | -22.8% |
| | | | | | | | | |

Regression Estimate Regression Estimate **Average Annual Change**

2009 2306 1977 2017

-1.90%

1205 738

-5.94%

3511 2715 -3.16%

Teron/March PM Peak

| Year | Date | North Leg | | South Leg | | East Leg | | West Leg | | Total |
|------|--------------|-----------|------|-----------|------|----------|-----|----------|-----|-------|
| Teal | Date | SB | NB | NB | SB | WB | EB | EB | WB | IOLAI |
| 2009 | Tues July 14 | 2043 | 1398 | 1180 | 1625 | 329 | 80 | 370 | 602 | 7627 |
| 2010 | Thurs Aug 12 | 2164 | 1848 | 1505 | 1995 | 420 | 165 | 585 | 666 | 9348 |
| 2011 | Tues June 21 | 1989 | 1992 | 1820 | 1884 | 569 | 150 | 429 | 781 | 9614 |
| 2017 | Thurs Nov 2 | 2135 | 1288 | 1085 | 1862 | 370 | 81 | 314 | 673 | 7808 |
| | | | | | | | | | | |

North Leg

| Year | | Cou | unts | | % Change | | | |
|------|------|------|-------|------|----------|-------|--------|--------|
| Tear | NB | SB | NB+SB | INT | NB | SB | NB+SB | INT |
| 2009 | 1398 | 2043 | 3441 | 7627 | | | | |
| 2010 | 1848 | 2164 | 4012 | 9348 | 32.2% | 5.9% | 16.6% | 22.6% |
| 2011 | 1992 | 1989 | 3981 | 9614 | 7.8% | -8.1% | -0.8% | 2.8% |
| 2017 | 1288 | 2135 | 3423 | 7808 | -35.3% | 7.3% | -14.0% | -18.8% |
| | | | | | | | | İ |

Regression Estimate Regression Estimate 2009 1760 2017 1386 2061 2125

3511

3821

Average Annual Change

0.39% -2.94%

-1.05%

West Leg

| Year | Counts | | | | % Change | | | | | |
|------|--------|-----|-------|------|----------|--------|--------|--------|--|--|
| real | EB | WB | EB+WB | INT | EB | WB | EB+WB | INT | | |
| 2009 | 370 | 602 | 972 | 7627 | | | | | | |
| 2010 | 585 | 666 | 1251 | 9348 | 58.1% | 10.6% | 28.7% | 22.6% | | |
| 2011 | 429 | 781 | 1210 | 9614 | -26.7% | 17.3% | -3.3% | 2.8% | | |
| 2017 | 314 | 673 | 987 | 7808 | -26.8% | -13.8% | -18.4% | -18.8% | | |
| | | | | | | | | | | |

Regression Estimate Regression Estimate 2009 2017

672 328 698 0.48%

1147 1025

Average Annual Change

-4.54%

-1.39%

East Leg

| Year | | Coi | unts | | % Change | | | | |
|------|-----|-----|-------|------|----------|--------|--------|--------|--|
| Teal | EB | WB | EB+WB | INT | EB | WB | EB+WB | INT | |
| 2009 | 80 | 329 | 409 | 7627 | | | | | |
| 2010 | 165 | 420 | 585 | 9348 | 106.3% | 27.7% | 43.0% | 22.6% | |
| 2011 | 150 | 569 | 719 | 9614 | -9.1% | 35.5% | 22.9% | 2.8% | |
| 2017 | 81 | 370 | 451 | 7808 | -46.0% | -35.0% | -37.3% | -18.8% | |
| | | | | | | | | | |

Regression Estimate Regression Estimate
Average Annual Change 2009 2017 431 405

564 498

-4.44%

133

92 -0.76%

-1.55%

South Leg

| Year | | Cou | ınts | | % Change | | | | |
|-------|------|------|-------|------|----------|-------|--------|--------|--|
| i eai | NB | SB | NB+SB | INT | NB | SB | NB+SB | INT | |
| 2009 | 1180 | 1625 | 2805 | 7627 | | | | | |
| 2010 | 1505 | 1995 | 3500 | 9348 | 27.5% | 22.8% | 24.8% | 22.6% | |
| 2011 | 1820 | 1884 | 3704 | 9614 | 20.9% | -5.6% | 5.8% | 2.8% | |
| 2017 | 1085 | 1862 | 2947 | 7808 | -40.4% | -1.2% | -20.4% | -18.8% | |
| | | | | | | | | | |

Regression Estimate Regression Estimate **Average Annual Change**

2009 1507 1188 2017

-2.93%

1813 1896

0.56%

3320 3084 -0.92%

APPENDIX E

MMLOS: ROAD SEGMENTS

Multi-Modal Level of Service - Segments Form

| Consultant | Parsons | Project | 1131 Teron |
|------------|----------|---------|------------|
| Scenario | Segments | Date | 31-Jul-19 |
| Comments | | | |
| | | | |

| SEGMENTS | | Street A | Existing | Existing | Existing | Future | Section | Section | Section | Section | Section |
|----------------|--|----------|-----------------------------|-----------------------------|---------------------|-----------------------------|---------|---------|---------|---------|---------|
| | Sidewalk Width | | March ≥ 2 m | Teron East no sidewalk | Teron West ≥ 2 m | Teron East ≥ 2 m | 5 | 6 | | 8 | 9 |
| | Boulevard Width | | < 0.5 | n/a | > 2 m | > 2 m | | | | | |
| | Avg Daily Curb Lane Traffic Volume | | > 3000 | > 3000 | > 3000 | > 3000 | | | | | |
| E E | Operating Speed | | > 60 km/h | > 30 to 50 km/h | > 30 to 50 km/h | > 30 to 50 km/h | | | | | |
| Pedestrian | On-Street Parking | | no | no | no | no | | | | | |
| es. | Exposure to Traffic PLoS | F | F | F | В | В | - | - | - | - | - |
| eq | Effective Sidewalk Width | | 2.0 m | | 2.0 m | 2.0 m | | | | | |
| صّ | Pedestrian Volume | | 250 ped/hr | | 250 ped/hr | 250 ped/hr | | | | | |
| | Crowding PLoS | | В | - | В | В | | - | - | - | - |
| | Level of Service | | F | - | В | В | - | - | - | - | - |
| | Type of Cycling Facility | | Curbside Bike Lane | Curbside Bike Lane | , , | Curbside Bike Lane | | | | | |
| | Number of Travel Lanes | | 2 ea. dir. (w median) | 2 ea. dir. (no median) | | 2 ea. dir. (no median) | | | | | |
| | Operating Speed | | > 70 km/h | >50 to 70 km/h | | >50 to 70 km/h | | | | | |
| | # of Lanes & Operating Speed LoS | | Е | С | - | С | - | - | - | - | - |
| Bicycle | Bike Lane (+ Parking Lane) Width | | ≥ 1.8 m | ≥1.5 to <1.8 m | | ≥1.5 to <1.8 m | | | | | |
| Š | Bike Lane Width LoS | E | Α | В | - | В | - | - | - | - | - |
| <u></u> | Bike Lane Blockages | | Rare | Rare | | Rare | | | | | |
| | Blockage LoS | | A 0 m nofuno | A 0 70 70 ft 170 | - | A | - | - | - | - | - |
| | Median Refuge Width (no median = < 1.8 m) No. of Lanes at Unsignalized Crossing | | < 1.8 m refuge ≤ 3 lanes | < 1.8 m refuge ≤ 3 lanes | | < 1.8 m refuge ≤ 3 lanes | | | | | |
| | Sidestreet Operating Speed | | ≤ 40 km/h | ≤ 40 km/h | | ≤ 40 km/h | | | | | |
| | Unsignalized Crossing - Lowest LoS | | A | A | A | A A | | - | - | - | - |
| | Level of Service | | Е | С | Α | С | - | - | - | - | - |
| i , | Facility Type | | Mixed Traffic | Mixed Traffic | Mixed Traffic | | | | | | |
| Transit | Friction or Ratio Transit:Posted Speed | D | Vt/Vp ≥ 0.8 | Vt/Vp ≥ 0.8 | Vt/Vp ≥ 0.8 | | | | | | |
| T.S. | Level of Service | | D | D | D | - | - | - | - | - | - |
| | Truck Lane Width | | ≤ 3.5 m | | | | | | | | |
| 3 | Travel Lanes per Direction | _ | > 1 | | | | | | | | |
| Truck | Level of Service | Α | Α | - | - | - | - | - | - | - | - |

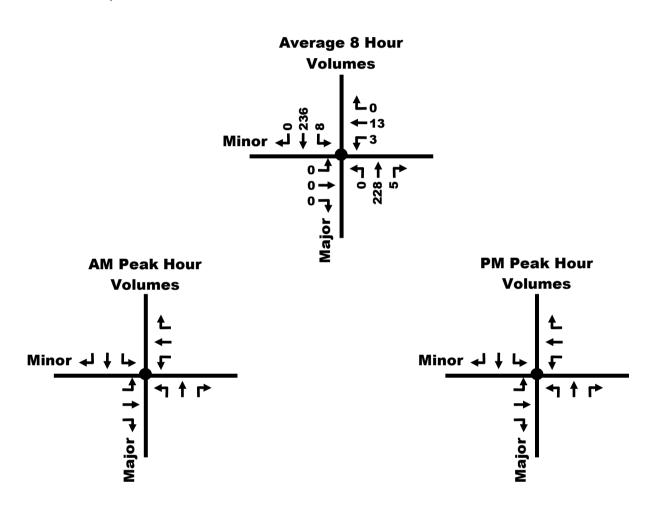


WARRANT ANALYSIS

Teron/Site - AWSC Warrant for Kanata mode share (most critical)

| | AWSC Warrant | | Description | Minimum Requirement for a 'T' intersection | | | | |
|--------------|---|---|---|--|---------------------|----------|---------|--|
| | | Α | Vehicle Volume, All Approaches for Each of the Heaviest 8 Hours of on Average Day, or | 200 | Sectional % 247% | Entire % | Warrant | |
| | 1. Minimum Volume Criterion | В | Vehicle Volume, All Approaches for the Heaviest Peak Hour, and | 350 | 0% | 10% | | |
| Intersection | | С | Vehicle and pedestrian Volume, Along Minor Streets for Each of the Same 8 Hours, <u>and</u> | 80 | 20% | 10% | No | |
| Inte | | D | The volume split between the major and minor streets | 75/25 | 10% | | | |
| | 2. Minimum Collision Criterion | Α | Vehicle Volume, Along Major Street for Each of the Heaviest 8 Hours of an Average Day, and | 9 | 0% | 0% | | |

Note: • preventable by AWSC collisions (i.e. right angle and turning movement collisions) were reported during a 3 year time period



| | | Major | | | | | | | Minor | | | | |
|----------------|-----------|------------|----------|-------------------|------------|----------|-----|-----|----------|-----|-----|----------|----------|
| | | | A | Teron | | | | | Si | ite | | | |
| | | ● 1 | T | Γ > | L ▶ | + | 4 | _ | — | 7 | ▼ | — | _ |
| | Peak | NBL | NBT | NBR | SBL | SBT | SBR | EBL | EBT | EBR | WBL | WBT | WBR |
| Existing | 8 hr | | | | | | | | | | | | |
| _ | AM | | | | | | | | | | | | |
| | PM | | | | | | | | | | | | |
| Site Generated | AM | | 635 | 5 | 7 | 243 | | | | | 8 | 32 | |
| | PM | | 277 | 16 | 24 | 699 | | | | | 5 | 20 | |
| | Avg. 8 hr | 0 | 228 | 5 | 8 | 236 | 0 | 0 | 0 | 0 | 3 | 13 | 0 |

Teron/Site - (peak hour signal warrant using Kanata mode share, most critical)

| _ | | ony site (| P | nour signar warrant asing Kana | | , c o c. cu., | | |
|---------|--------------|---------------------------------|-------------|--|--|---------------|---------|-----|
| | | Signal | | Description | Minimum Requirement for Two- Lane Roadways | Compliance | | |
| Warrant | | | Description | Restricted Flow - Operating Speed Less Than 70 km/h | Sectional % | Entire % | Warrant | |
| | | 1. Minimum | (1) A | Vehicle Volume, All Approaches for Each of the Heaviest 8 Hours of on Average Day, and | 720 | 68% | 6% | |
| : | ection | Vehicular Volume | (4) B | Vehicle Volume, Along Minor Streets for Each of the Same 8 Hours | 255 | 6% | 070 | 21% |
| | Intersection | 2. Delay to Cross Traffic | (1) A | Vehicle Volume, Along Major Street for Each of the Heaviest 8 Hours of an Average Day, and | 720 | 66% | 21% | No |
| | | | (2) B | Combined Vehicle and Pedestrian Volume <u>Crossing</u> the Major Street for Each of the Same 8 Hours | 75 | 21% | 2170 | |

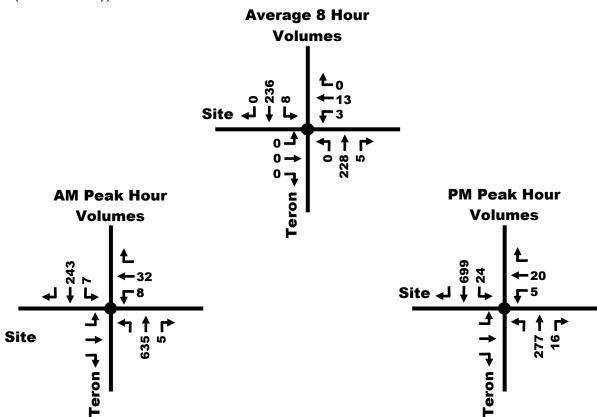
Notes

1 Vehicle Volume Warrants (1A), (2A) and (5B) for Roadways Having Two or More Moving Lanes in one Direction Should Be 25% Higher Than Values Given Above

No

- 2 For Definition of Crossing Volume Refer to Note 4 on the Signal Warrant Analysis Form B2.03.08
- 3 The Lowest Sectional Percentage Governs the Entire Warrant
- 4 For "T" Intersections the Warrant Values for Minor Street Should be Increased by 50% (Warrant 1B only)

Yes

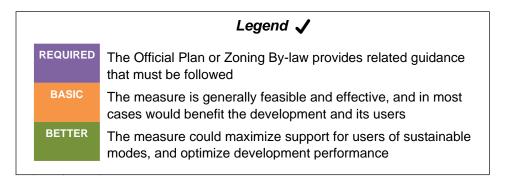




TDM PROGRAM

TDM-Supportive Development Design and Infrastructure Checklist:

Residential Developments (multi-family or condominium)



| | TDM-s | supportive design & infrastructure measures: Residential developments | Check if completed & add descriptions, explanations or plan/drawing references |
|----------|-------|--|--|
| | 1. | WALKING & CYCLING: ROUTES | |
| | 1.1 | Building location & access points | |
| BASIC | 1.1.1 | Locate building close to the street, and do not locate parking areas between the street and building entrances | ✓ parking located in the back |
| BASIC | 1.1.2 | Locate building entrances in order to minimize walking distances to sidewalks and transit stops/stations | ☑ building abutting Teron Road |
| BASIC | 1.1.3 | Locate building doors and windows to ensure visibility of pedestrians from the building, for their security and comfort | ✓ Modern design building |
| | 1.2 | Facilities for walking & cycling | |
| REQUIRED | 1.2.1 | Provide convenient, direct access to stations or major stops along rapid transit routes within 600 metres; minimize walking distances from buildings to rapid transit; provide pedestrian-friendly, weather-protected (where possible) environment between rapid transit accesses and building entrances; ensure quality linkages from sidewalks through building entrances to integrated stops/stations (see Official Plan policy 4.3.3) | A landscaped and enhanced pedestrian pathway proposed through the parking lot to March/Teron intersection. |
| REQUIRED | 1.2.2 | Provide safe, direct and attractive pedestrian access from public sidewalks to building entrances through such measures as: reducing distances between public sidewalks and major building entrances; providing walkways from public streets to major building entrances; within a site, providing walkways along the front of adjoining buildings, between adjacent buildings, and connecting areas where people may congregate, such as courtyards and transit stops; and providing weather protection through canopies, colonnades, and other design elements wherever possible (see Official Plan policy 4.3.12) | Internal pathways to connect to proposed Teron sidewalk and existing March sidewalk |

| | TDM-s | supportive design & infrastructure measures: Residential developments | Check if completed & add descriptions, explanations or plan/drawing references |
|----------|-------|--|--|
| REQUIRED | 1.2.3 | Provide sidewalks of smooth, well-drained walking surfaces of contrasting materials or treatments to differentiate pedestrian areas from vehicle areas, and provide marked pedestrian crosswalks at intersection sidewalks (see Official Plan policy 4.3.10) | Sidewalks to be built to city standard |
| REQUIRED | 1.2.4 | Make sidewalks and open space areas easily accessible through features such as gradual grade transition, depressed curbs at street corners and convenient access to extra-wide parking spaces and ramps (see Official Plan policy 4.3.10) | Sidewalks to be built to city standard |
| REQUIRED | 1.2.5 | Include adequately spaced inter-block/street cycling and pedestrian connections to facilitate travel by active transportation. Provide links to the existing or planned network of public sidewalks, multi-use pathways and onroad cycle routes. Where public sidewalks and multi-use pathways intersect with roads, consider providing traffic control devices to give priority to cyclists and pedestrians (see Official Plan policy 4.3.11) | A MUP connection is proposed on the north side of the property parcel which would connect the current MUP located on the south side of March Road to the MUP located on the south side of Steacie Drive. |
| BASIC | 1.2.6 | Provide safe, direct and attractive walking routes from building entrances to nearby transit stops | ✓ Transit stop located adjacent to site on Teron Road |
| BASIC | 1.2.7 | Ensure that walking routes to transit stops are secure, visible, lighted, shaded and wind-protected wherever possible | ✓ Street lighting provided on March Road and west side of Teron Road |
| BASIC | 1.2.8 | Design roads used for access or circulation by cyclists using a target operating speed of no more than 30 km/h, or provide a separated cycling facility | MUP proposed on north side of development |
| | 1.3 | Amenities for walking & cycling | |
| BASIC | 1.3.1 | Provide lighting, landscaping and benches along walking and cycling routes between building entrances and streets, sidewalks and trails | ☑ Landscaping proposed |
| BASIC | 1.3.2 | Provide wayfinding signage for site access (where required, e.g. when multiple buildings or entrances exist) and egress (where warranted, such as when directions to reach transit stops/stations, trails or other common destinations are not obvious) | |

| | TDM-s | supportive design & infrastructure measures: Residential developments | Check if completed & add descriptions, explanations or plan/drawing references |
|----------|-------|--|--|
| | 2. | WALKING & CYCLING: END-OF-TRIP FACILITY | TIES |
| | 2.1 | Bicycle parking | |
| REQUIRED | 2.1.1 | Provide bicycle parking in highly visible and lighted areas, sheltered from the weather wherever possible (see Official Plan policy 4.3.6) | ☑ Bike parking proposed predominantly within the underground parking structure |
| REQUIRED | 2.1.2 | Provide the number of bicycle parking spaces specified for various land uses in different parts of Ottawa; provide convenient access to main entrances or well-used areas (see Zoning By-law Section 111) | ✓ Exceeds minimum parking, rate of approximately 0.69 spots per units |
| REQUIRED | 2.1.3 | Ensure that bicycle parking spaces and access aisles meet minimum dimensions; that no more than 50% of spaces are vertical spaces; and that parking racks are securely anchored (see Zoning By-law Section 111) | ☑ Majority of spots are horizontal |
| BASIC | 2.1.4 | Provide bicycle parking spaces equivalent to the expected number of resident-owned bicycles, plus the expected peak number of visitor cyclists | |
| | 2.2 | Secure bicycle parking | |
| REQUIRED | 2.2.1 | Where more than 50 bicycle parking spaces are provided for a single residential building, locate at least 25% of spaces within a building/structure, a secure area (e.g. supervised parking lot or enclosure) or bicycle lockers (see Zoning By-law Section 111) | ☑ Bike parking proposed predominantly within the underground parking structure |
| BETTER | 2.2.2 | Provide secure bicycle parking spaces equivalent to at least the number of units at condominiums or multifamily residential developments | |
| | 2.3 | Bicycle repair station | |
| BETTER | 2.3.1 | Provide a permanent bike repair station, with commonly used tools and an air pump, adjacent to the main bicycle parking area (or secure bicycle parking area, if provided) | |
| | 3. | TRANSIT | |
| | 3.1 | Customer amenities | |
| BASIC | 3.1.1 | Provide shelters, lighting and benches at any on-site transit stops | |
| BASIC | 3.1.2 | Where the site abuts an off-site transit stop and insufficient space exists for a transit shelter in the public right-of-way, protect land for a shelter and/or install a shelter | |
| BETTER | 3.1.3 | Provide a secure and comfortable interior waiting area by integrating any on-site transit stops into the building | |

| | TDM-s | supportive design & infrastructure measures: Residential developments | Check if completed & add descriptions, explanations or plan/drawing references |
|----------|-------|--|--|
| | 4. | RIDESHARING | |
| | 4.1 | Pick-up & drop-off facilities | |
| BASIC | 4.1.1 | Provide a designated area for carpool drivers (plus taxis and ride-hailing services) to drop off or pick up passengers without using fire lanes or other no-stopping zones | |
| | 5. | CARSHARING & BIKESHARING | |
| | 5.1 | Carshare parking spaces | |
| BETTER | 5.1.1 | Provide up to three carshare parking spaces in an R3, R4 or R5 Zone for specified residential uses (see Zoning By-law Section 94) | |
| | 5.2 | Bikeshare station location | |
| BETTER | 5.2.1 | Provide a designated bikeshare station area near a major building entrance, preferably lighted and sheltered with a direct walkway connection | |
| | 6. | PARKING | |
| | 6.1 | Number of parking spaces | |
| REQUIRED | 6.1.1 | Do not provide more parking than permitted by zoning, nor less than required by zoning, unless a variance is being applied for | ✓ Meets parking by-laws |
| BASIC | 6.1.2 | Provide parking for long-term and short-term users that is consistent with mode share targets, considering the potential for visitors to use off-site public parking | ✓ Proposed parking for visitors and long-term residents |
| BASIC | 6.1.3 | Where a site features more than one use, provide shared parking and reduce the cumulative number of parking spaces accordingly (see Zoning By-law Section 104) | |
| BETTER | 6.1.4 | Reduce the minimum number of parking spaces required by zoning by one space for each 13 square metres of gross floor area provided as shower rooms, change rooms, locker rooms and other facilities for cyclists in conjunction with bicycle parking (see Zoning By-law Section 111) | |
| | 6.2 | Separate long-term & short-term parking areas | |
| BETTER | 6.2.1 | Provide separate areas for short-term and long-term parking (using signage or physical barriers) to permit access controls and simplify enforcement (i.e. to discourage residents from parking in visitor spaces, and vice versa) | |

APPENDIX H

MMLOS: INTERSECTIONS

Multi-Modal Level of Service - Intersections Form

| Consultant |
|------------|
| Scenario |
| Comments |

| arsons | Project | 113 |
|--------------------------|---------|-----|
| larch/Teron Intersection | Date | 31 |
| | | |
| | | |

| | 1131 Teron | | | | | | | | | |
|---|------------|--|--|--|--|--|--|--|--|--|
| | 31-Jul-19 | | | | | | | | | |
| | | | | | | | | | | |
| ı | | | | | | | | | | |

Unlocked Rows for Replicating

| Proceedings Side North South | | | | | | Unlocked Rows for Replicating | | | | | | | | | |
|--|--------------|--------------------------------------|-------------------|-------------------|-------------------|-------------------------------|-------------------|-------------------|-------------------|-------------------|----------------|-------|------|------|--|
| Crossing Study | | INTERSECTIONS | | | /Teron | | | Beaverbr | ook/Teron | | Intersection C | | | | |
| Decided Continue | | Crossing Side | NORTH | | | WEST | NORTH | | | WEST | NORTH | | | WEST | |
| Carbony Late Turns Processed Proce | | | 5 | | | 7 | 5 | 4 | 4 | 4 | | | | | |
| Part | | Median | No Median - 2.4 m | No Median - 2.4 m | No Median - 2.4 m | No Median - 2.4 m | No Median - 2.4 m | | | | | |
| Part March March | | Conflicting Left Turns | | | | | Permissive | Permissive | Permissive | | | | | | |
| Post September Control Contr | | Conflicting Right Turns | - | • | • | • | _ | | | - | | | | | |
| Committee with Comm | | Right Turns on Red (RToR) ? | RTOR allowed | RTOR allowed | RTOR allowed | RTOR allowed | RTOR allowed | RTOR allowed | RTOR allowed | RTOR allowed | | | | | |
| Page Control Label Contr | | Ped Signal Leading Interval? | No | No | No | No | No | No | No | No | | | | | |
| PETS Score 15 15 15 15 15 15 15 1 | ian | Right Turn Channel | | | | | No Channel | No Channel | No Channel | No Channel | | | | | |
| PETS Score 33 33 3 3 3 3 3 3 3 | str | Corner Radius | >25m | >25m | 15-25m | 15-25m | 5-10m | 5-10m | 5-10m | 10-15m | | | | | |
| PETS Score to Traffic Cols E E F F E D D D D D D D D D | ede | Crosswalk Type | | | | | | | | | | | | | |
| System Large 10 | | PETSI Score | 35 | 35 | 3 | 3 | 38 | | 54 | 53 | | | | | |
| Electric Value Time 26 28 19 15 17 13 19 19 19 19 19 19 19 | | Ped. Exposure to Traffic LoS | E | E | F | F | E | - | D | D | - | - | - | - | |
| Average Pedestrian Delay 1 1 17 17 5 10 10 10 10 10 10 10 | | Cycle Length | 35 | 35 | 66 | 66 | 36 | | 51 | 51 | | | | | |
| Pedestrian Delay LoS | | Effective Walk Time | 28 | 28 | 19 | 19 | 17 | | 19 | 19 | | | | | |
| E E F F E D D D D D D D D D | | | 1 | 1 | 17 | 17 | 5 | | 10 | 10 | | | | | |
| Approach From Noisth South East West Noisth East West Noisth South East West Noisth East West Noisth East West Noisth South East West Noisth East West Med Tarlic Noisth East West Midd Tarlic Noisth East West East West Midd Tarlic Noisth East West East West East West East West East West East West East E | | Pedestrian Delay LoS | Α | Α | В | В | A | - | В | В | - | | - | - | |
| Approach From North South East West North South Ea | | | Е | Е | F | F | E | - | D | D | - | - | - | - | |
| Boycle Lane Arrangement on Approach Mixed Traffic Mixed Traffic Approach Appro | | Level of Service | | | F | | | | E | | | | - | | |
| Right Turn Lane Configuration | | Approach From NORTH | | SOUTH | EAST | WEST | NORTH | SOUTH | EAST | WEST | NORTH | SOUTH | EAST | WEST | |
| Right Turning Speed | | Bicycle Lane Arrangement on Approach | Mixed Traffic | Mixed Traffic | Pocket Bike Lane | Pocket Bike Lane | Mixed Traffic | Mixed Traffic | Mixed Traffic | Mixed Traffic | | | | | |
| Cyclist relative to RT motorists D | | Right Turn Lane Configuration | ≤ 50 m | ≤ 50 m | | | ≤ 50 m | ≤ 50 m | ≤ 50 m | ≤ 50 m | | | | | |
| Separated or Mixed Traffic | | Right Turning Speed | ≤ 25 km/h | ≤ 25 km/h | >25 to 30 km/h | >25 to 30 km/h | ≤ 25 km/h | ≤ 25 km/h | ≤ 25 km/h | ≤ 25 km/h | | | | | |
| Operating Speed | O | Cyclist relative to RT motorists | D | D | D | D | D | D | D | D | - | - | - | - | |
| Operating Speed |) C | Separated or Mixed Traffic | Mixed Traffic | Mixed Traffic | Separated | Separated | Mixed Traffic | Mixed Traffic | Mixed Traffic | Mixed Traffic | - | - | - | - | |
| Left Turning Cyclist | Bicy | Left Turn Approach | One lane crossed | One lane crossed | ≥ 2 lanes crossed | ≥ 2 lanes crossed | One lane crossed | One lane crossed | One lane crossed | One lane crossed | | | | | |
| Level of Service | | | > 40 to ≤ 50 km/h | > 40 to ≤ 50 km/h | ≥ 60 km/h | ≥ 60 km/h | ≤ 40 km/h | ≤ 40 km/h | ≤ 40 km/h | ≤ 40 km/h | | | | | |
| Level of Service | | Left Turning Cyclist | D | D | F | F | В | В | В | В | - | - | - | - | |
| Average Signal Delay | | | D | D | F | F | D | D | D | D | - | - | - | - | |
| F D F C B D E E | | Level of Service | | | F | | | | D | | | | - | | |
| Effective Corner Radius | <u> </u> | Average Signal Delay | > 40 sec | ≤ 30 sec | > 40 sec | ≤ 20 sec | ≤ 10 sec | ≤ 30 sec | ≤ 40 sec | ≤ 40 sec | | | | | |
| Effective Corner Radius | nsi | | F | D | F | С | В | D | E | E | - | - | - | - | |
| Number of Receiving Lanes on Departure from Intersection A A A A A | Tra | Level of Service | | | F | | | | E | | | | - | | |
| From Intersection | | Effective Corner Radius | > 15 m | > 15 m | > 15 m | > 15 m | | | | | | | | | |
| Level of Service A Volume to Capacity Ratio - Capacity Ratio | \ | | ≥2 | ≥2 | ≥2 | ≥ 2 | | | | | | | | | |
| Volume to Capacity Ratio Polume to Capacity Ratio | Tru | | Α | Α | Α | Α | - | - | - | - | - | - | - | - | |
| Š | | Level of Service | | | 4 | | | | - | | | | | | |
| Level of Service - | 0 | Volume to Capacity Ratio | | | | | | | | | | | | | |
| | Aut | Level of Service | | | | | | | - | | | | - | | |



SYNCHRO ANALYSIS: EXISTING CONDITIONS

| | ٠ | → | • | • | ← | • | 4 | † | <i>></i> | > | ļ | 4 |
|------------------------|--------|----------|-------|-------|----------|-------|-------|----------|-------------|-------------|-------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | † | 7 | 7 | ^ | 7 | Ĭ | ^ | 7 | Ĭ | 44 | 7 |
| Traffic Volume (vph) | 475 | 263 | 13 | 23 | 38 | 34 | 36 | 1631 | 199 | 49 | 681 | 180 |
| Future Volume (vph) | 475 | 263 | 13 | 23 | 38 | 34 | 36 | 1631 | 199 | 49 | 681 | 180 |
| Satd. Flow (prot) | 1695 | 1784 | 1517 | 1695 | 1784 | 1517 | 1695 | 3390 | 1517 | 1695 | 3390 | 1517 |
| Flt Permitted | 0.588 | | | 0.342 | | | 0.309 | | | 0.057 | | |
| Satd. Flow (perm) | 1045 | 1784 | 1498 | 610 | 1784 | 1497 | 551 | 3390 | 1498 | 102 | 3390 | 1517 |
| Satd. Flow (RTOR) | | | 188 | | | 188 | | | 188 | | | 188 |
| Lane Group Flow (vph) | 528 | 292 | 14 | 26 | 42 | 38 | 40 | 1812 | 221 | 54 | 757 | 200 |
| Turn Type | pm+pt | NA | Free | pm+pt | NA | Free | pm+pt | NA | Free | pm+pt | NA | Free |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | Free | 8 | | Free | 2 | | Free | 6 | | Free |
| Detector Phase | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 10.0 | | 5.0 | 10.0 | | 5.0 | 10.0 | | 5.0 | 10.0 | |
| Minimum Split (s) | 11.1 | 34.6 | | 11.1 | 34.6 | | 11.4 | 25.3 | | 11.4 | 25.3 | |
| Total Split (s) | 12.0 | 38.0 | | 12.0 | 38.0 | | 12.0 | 68.0 | | 12.0 | 68.0 | |
| Total Split (%) | 9.2% | 29.2% | | 9.2% | 29.2% | | 9.2% | 52.3% | | 9.2% | 52.3% | |
| Yellow Time (s) | 3.3 | 3.3 | | 3.3 | 3.3 | | 4.6 | 4.6 | | 4.6 | 4.6 | |
| All-Red Time (s) | 2.8 | 3.3 | | 2.8 | 3.3 | | 1.8 | 1.7 | | 1.8 | 1.7 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | 6.1 | 6.6 | | 6.1 | 6.6 | | 6.4 | 6.3 | | 6.4 | 6.3 | |
| Lead/Lag | Lead | Lag | | Lead | Lag | | Lead | Lag | | Lead | Lag | |
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | | Yes | Yes | | Yes | Yes | |
| Recall Mode | None | None | | None | None | | None | C-Min | | None | C-Min | |
| Act Effct Green (s) | 29.8 | 25.8 | 130.0 | 25.9 | 21.7 | 130.0 | 78.8 | 73.8 | 130.0 | 79.1 | 73.9 | 130.0 |
| Actuated g/C Ratio | 0.23 | 0.20 | 1.00 | 0.20 | 0.17 | 1.00 | 0.61 | 0.57 | 1.00 | 0.61 | 0.57 | 1.00 |
| v/c Ratio | 1.88 | 0.83 | 0.01 | 0.15 | 0.14 | 0.03 | 0.10 | 0.94 | 0.15 | 0.39 | 0.39 | 0.13 |
| Control Delay | 436.0 | 69.0 | 0.0 | 33.6 | 42.8 | 0.0 | 11.9 | 39.6 | 0.2 | 22.0 | 18.8 | 0.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 436.0 | 69.0 | 0.0 | 33.6 | 42.8 | 0.0 | 11.9 | 39.6 | 0.2 | 22.0 | 18.8 | 0.2 |
| LOS | F | E | Α | С | D | Α | В | D | Α | С | В | Α |
| Approach Delay | | 300.2 | | | 25.2 | | | 34.9 | | | 15.3 | |
| Approach LOS | | F | | | С | | | С | | | В | |
| Queue Length 50th (m) | ~203.0 | 71.9 | 0.0 | 4.8 | 8.9 | 0.0 | 3.9 | ~269.4 | 0.0 | 5.3 | 63.3 | 0.0 |
| Queue Length 95th (m) | #259.4 | 99.5 | 0.0 | 11.1 | 18.1 | 0.0 | 9.7 | #324.2 | 0.0 | 14.1 | 84.3 | 0.0 |
| Internal Link Dist (m) | | 42.6 | | | 349.6 | | | 93.8 | | | 234.3 | |
| Turn Bay Length (m) | 66.0 | | 66.0 | | | 80.0 | 80.0 | | 90.0 | 80.0 | | 85.0 |
| Base Capacity (vph) | 281 | 430 | 1498 | 171 | 430 | 1497 | 388 | 1923 | 1498 | 139 | 1927 | 1517 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 1.88 | 0.68 | 0.01 | 0.15 | 0.10 | 0.03 | 0.10 | 0.94 | 0.15 | 0.39 | 0.39 | 0.13 |

Intersection Summary

Cycle Length: 130

Actuated Cycle Length: 130
Offset: 36 (28%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green

Natural Cycle: 115

Control Type: Actuated-Coordinated

Synchro 10 Report Parsons

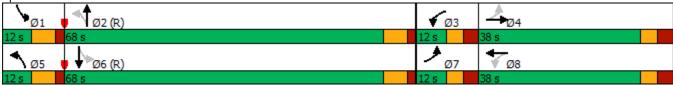
Maximum v/c Ratio: 1.88
Intersection Signal Delay: 84.7
Intersection Capacity Utilization 92.8%
ICU Level of Service F

Analysis Period (min) 15
Description: NOTE: March Road treated as north-south

Volume exceeds capacity, queue is theoretically infinite.
Queue shown is maximum after two cycles.

95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

Splits and Phases: 1: March & Teron



Parsons Synchro 10 Report

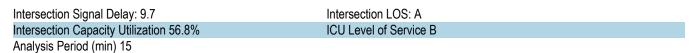
| | • | - | \rightarrow | • | ← | • | • | † | / | > | ļ | 4 |
|------------------------|-------|-------|---------------|-------|----------|-----|-------|----------|-----|-------------|-------|-----|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | Ť | £ | | * | f. | | 7 | £ | | ሻ | ĵ. | |
| Traffic Volume (vph) | 146 | 4 | 180 | 22 | 2 | 34 | 96 | 266 | 4 | 15 | 140 | 38 |
| Future Volume (vph) | 146 | 4 | 180 | 22 | 2 | 34 | 96 | 266 | 4 | 15 | 140 | 38 |
| Satd. Flow (prot) | 1695 | 1522 | 0 | 1695 | 1450 | 0 | 1695 | 1781 | 0 | 1695 | 1717 | 0 |
| Flt Permitted | 0.731 | | | 0.630 | | | 0.633 | | | 0.577 | | |
| Satd. Flow (perm) | 1263 | 1522 | 0 | 1124 | 1450 | 0 | 1127 | 1781 | 0 | 1030 | 1717 | 0 |
| Satd. Flow (RTOR) | | 200 | | | 38 | | | 1 | | | 27 | |
| Lane Group Flow (vph) | 162 | 204 | 0 | 24 | 40 | 0 | 107 | 300 | 0 | 17 | 198 | 0 |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Detector Phase | 4 | 4 | | 8 | 8 | | 2 | 2 | | 6 | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 10.0 | 10.0 | | 10.0 | 10.0 | | 10.0 | 10.0 | | 10.0 | 10.0 | |
| Minimum Split (s) | 22.8 | 22.8 | | 22.8 | 22.8 | | 65.6 | 65.6 | | 65.6 | 65.6 | |
| Total Split (s) | 29.8 | 29.8 | | 29.8 | 29.8 | | 65.6 | 65.6 | | 65.6 | 65.6 | |
| Total Split (%) | 31.2% | 31.2% | | 31.2% | 31.2% | | 68.8% | 68.8% | | 68.8% | 68.8% | |
| Yellow Time (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.3 | 3.3 | | 3.3 | 3.3 | |
| All-Red Time (s) | 2.8 | 2.8 | | 2.8 | 2.8 | | 2.3 | 2.3 | | 2.3 | 2.3 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | 5.8 | 5.8 | | 5.8 | 5.8 | | 5.6 | 5.6 | | 5.6 | 5.6 | |
| Lead/Lag | | | | | | | | | | | | |
| Lead-Lag Optimize? | | | | | | | | | | | | |
| Recall Mode | None | None | | None | None | | Min | Min | | Min | Min | |
| Act Effct Green (s) | 11.7 | 11.7 | | 11.7 | 11.7 | | 12.9 | 12.9 | | 12.9 | 12.9 | |
| Actuated g/C Ratio | 0.32 | 0.32 | | 0.32 | 0.32 | | 0.36 | 0.36 | | 0.36 | 0.36 | |
| v/c Ratio | 0.40 | 0.33 | | 0.07 | 0.08 | | 0.27 | 0.47 | | 0.05 | 0.32 | |
| Control Delay | 13.8 | 3.9 | | 10.1 | 4.9 | | 10.7 | 12.2 | | 8.5 | 9.1 | |
| Queue Delay | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Delay | 13.8 | 3.9 | | 10.1 | 4.9 | | 10.7 | 12.2 | | 8.5 | 9.1 | |
| LOS | В | Α | | В | Α | | В | В | | Α | Α | |
| Approach Delay | | 8.3 | | | 6.9 | | | 11.8 | | | 9.1 | |
| Approach LOS | | Α | | | Α | | | В | | | Α | |
| Queue Length 50th (m) | 6.6 | 0.2 | | 0.9 | 0.1 | | 3.9 | 11.7 | | 0.6 | 6.2 | |
| Queue Length 95th (m) | 21.2 | 9.7 | | 4.7 | 4.4 | | 13.7 | 32.2 | | 3.5 | 19.5 | |
| Internal Link Dist (m) | | 594.0 | | | 268.4 | | | 124.5 | | | 613.0 | |
| Turn Bay Length (m) | 60.0 | | | 15.0 | | | 40.0 | | | 45.0 | | |
| Base Capacity (vph) | 855 | 1095 | | 761 | 994 | | 1127 | 1781 | | 1030 | 1717 | |
| Starvation Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Reduced v/c Ratio | 0.19 | 0.19 | | 0.03 | 0.04 | | 0.09 | 0.17 | | 0.02 | 0.12 | |
| | | | | | | | | | | | | |

Intersection Summary

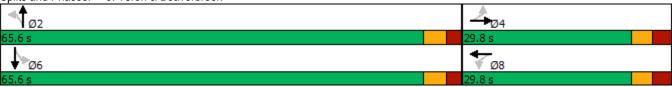
Cycle Length: 95.4

Actuated Cycle Length: 36.3
Natural Cycle: 90
Control Type: Semi Act-Uncoord Maximum v/c Ratio: 0.47

Synchro 10 Report Parsons







Parsons Synchro 10 Report

| Intersection | | | | | | |
|-----------------------------|----------------|---------------|----------|------------|------------|----------------|
| Int Delay, s/veh | 2 | | | | | |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| | | | INDL | | | |
| Lane Configurations | ኝ 87 | 7 | 26 | 4†† | 140 | 7 97 |
| Traffic Vol, veh/h | 87 | 37 37 | 36 36 | 509 509 | 149 149 | 97 |
| Future Vol, veh/h | 4 | 4 | 0 | 509 | 149 | 97 |
| Conflicting Peds, #/hr | | | Free | Free | Free | Free |
| Sign Control RT Channelized | Stop | Stop Yield | | | | |
| | - | | - | Free | - | Yield |
| Storage Length | 50 | 0 | - | - | - | 0 |
| Veh in Median Storage | | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 97 | 41 | 40 | 566 | 166 | 108 |
| | | | | | | |
| Major/Minor | Minor2 | | Major1 | N | Major2 | |
| Conflicting Flow All | 476 | 170 | 166 | 0 | | 0 |
| Stage 1 | 166 | - | - | - | _ | _ |
| Stage 2 | 310 | _ | _ | _ | _ | _ |
| Critical Hdwy | 6.08 | 6.23 | 4.13 | _ | _ | _ |
| Critical Hdwy Stg 1 | 5.43 | - | - | _ | _ | _ |
| Critical Hdwy Stg 2 | 6.03 | _ | _ | _ | _ | _ |
| Follow-up Hdwy | 3.669 | 3.319 | 2.219 | _ | _ | _ |
| Pot Cap-1 Maneuver | 554 | 873 | 1411 | _ | _ | _ |
| Stage 1 | 830 | - | 1711 | _ | _ | _ |
| Stage 2 | 681 | _ | _ | _ | _ | _ |
| Platoon blocked, % | 001 | _ | _ | _ | _ | _ |
| Mov Cap-1 Maneuver | 531 | 870 | 1411 | _ | _ | |
| Mov Cap-1 Maneuver | 531 | 070 | 1411 | _ | _ | - |
| | | | - | - | | - |
| Stage 1 | 796 | - | - | - | - | - |
| Stage 2 | 681 | - | - | - | - | - |
| | | | | | | |
| Approach | EB | | NB | | SB | |
| HCM Control Delay, s | 12.1 | | 0.6 | | 0 | |
| HCM LOS | В | | | | | |
| | | | | | | |
| NA: 1 /NA: NA | | NDI | NDT | EDI 4. | -DI 0 | ODT |
| Minor Lane/Major Mvm | nt | NBL | NRI | EBLn1 E | | SBT |
| Capacity (veh/h) | | 1411 | - | 001 | 870 | - |
| HCM Lane V/C Ratio | | 0.028 | | 0.182 | | - |
| HCM Control Delay (s) | | 7.6 | 0.1 | 13.3 | 9.3 | - |
| HCM Lane LOS | | Α | Α | В | Α | - |
| HCM 95th %tile Q(veh | | 0.1 | - | 0.7 | 0.1 | - |
| | | | | | | |

Parsons Synchro 10 Report

| | ٠ | → | \rightarrow | • | ← | • | • | † | <i>></i> | > | ļ | 4 |
|------------------------|-------|----------|---------------|-------|----------|-------|-------|----------|-------------|-------------|--------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | † | 7 | 7 | ^ | 7 | 7 | ^ | 7 | 7 | 44 | 7 |
| Traffic Volume (vph) | 224 | 50 | 40 | 153 | 167 | 50 | 51 | 1014 | 20 | 11 | 1669 | 455 |
| Future Volume (vph) | 224 | 50 | 40 | 153 | 167 | 50 | 51 | 1014 | 20 | 11 | 1669 | 455 |
| Satd. Flow (prot) | 1695 | 1784 | 1517 | 1695 | 1784 | 1517 | 1695 | 3390 | 1517 | 1695 | 3390 | 1517 |
| Flt Permitted | 0.557 | | | 0.588 | | | 0.057 | | | 0.178 | | |
| Satd. Flow (perm) | 984 | 1784 | 1498 | 1048 | 1784 | 1493 | 102 | 3390 | 1498 | 318 | 3390 | 1517 |
| Satd. Flow (RTOR) | | | 188 | | | 188 | | | 188 | | | 188 |
| Lane Group Flow (vph) | 249 | 56 | 44 | 170 | 186 | 56 | 57 | 1127 | 22 | 12 | 1854 | 506 |
| Turn Type | pm+pt | NA | Free | pm+pt | NA | Free | pm+pt | NA | Free | pm+pt | NA | Free |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | Free | 8 | | Free | 2 | | Free | 6 | | Free |
| Detector Phase | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 10.0 | | 5.0 | 10.0 | | 5.0 | 10.0 | | 5.0 | 10.0 | |
| Minimum Split (s) | 11.1 | 34.6 | | 11.1 | 34.6 | | 11.4 | 25.3 | | 11.4 | 25.3 | |
| Total Split (s) | 17.0 | 35.0 | | 17.0 | 35.0 | | 12.0 | 66.0 | | 12.0 | 66.0 | |
| Total Split (%) | 13.1% | 26.9% | | 13.1% | 26.9% | | 9.2% | 50.8% | | 9.2% | 50.8% | |
| Yellow Time (s) | 3.3 | 3.3 | | 3.3 | 3.3 | | 4.6 | 4.6 | | 4.6 | 4.6 | |
| All-Red Time (s) | 2.8 | 3.3 | | 2.8 | 3.3 | | 1.8 | 1.7 | | 1.8 | 1.7 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | 6.1 | 6.6 | | 6.1 | 6.6 | | 6.4 | 6.3 | | 6.4 | 6.3 | |
| Lead/Lag | Lead | Lag | | Lead | Lag | | Lead | Lag | | Lead | Lag | |
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | | Yes | Yes | | Yes | Yes | |
| Recall Mode | None | None | | None | None | | None | C-Min | | None | C-Min | |
| Act Effct Green (s) | 28.2 | 18.9 | 130.0 | 31.9 | 19.3 | 130.0 | 78.5 | 75.8 | 130.0 | 74.7 | 70.2 | 130.0 |
| Actuated g/C Ratio | 0.22 | 0.15 | 1.00 | 0.25 | 0.15 | 1.00 | 0.60 | 0.58 | 1.00 | 0.57 | 0.54 | 1.00 |
| v/c Ratio | 0.92 | 0.22 | 0.03 | 0.52 | 0.70 | 0.04 | 0.40 | 0.57 | 0.01 | 0.05 | 1.01 | 0.33 |
| Control Delay | 80.0 | 48.4 | 0.0 | 42.7 | 66.1 | 0.0 | 22.8 | 20.5 | 0.0 | 12.1 | 55.3 | 0.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 80.0 | 48.4 | 0.0 | 42.7 | 66.1 | 0.0 | 22.8 | 20.5 | 0.0 | 12.1 | 55.3 | 0.6 |
| LOS | Е | D | Α | D | Е | Α | С | С | Α | В | Е | Α |
| Approach Delay | | 64.8 | | | 47.5 | | | 20.2 | | | 43.4 | |
| Approach LOS | | Е | | | D | | | С | | | D | |
| Queue Length 50th (m) | 54.1 | 12.9 | 0.0 | 35.0 | 46.1 | 0.0 | 5.3 | 80.2 | 0.0 | 1.1 | ~271.6 | 0.0 |
| Queue Length 95th (m) | 72.3 | 23.5 | 0.0 | 49.8 | 65.6 | 0.0 | 15.6 | 146.2 | 0.0 | 4.3 | #343.3 | 0.0 |
| Internal Link Dist (m) | | 42.6 | | | 349.6 | | | 93.8 | | | 234.3 | |
| Turn Bay Length (m) | 66.0 | | 66.0 | | | 80.0 | 80.0 | | 90.0 | 80.0 | | 85.0 |
| Base Capacity (vph) | 272 | 389 | 1498 | 330 | 389 | 1493 | 142 | 1976 | 1498 | 244 | 1829 | 1517 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.92 | 0.14 | 0.03 | 0.52 | 0.48 | 0.04 | 0.40 | 0.57 | 0.01 | 0.05 | 1.01 | 0.33 |

Intersection Summary

Cycle Length: 130

Actuated Cycle Length: 130
Offset: 121 (93%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green

Natural Cycle: 115

Control Type: Actuated-Coordinated

Synchro 10 Report Parsons

| _ | | | | | | | | |
|--|---|---------------------|--|--|--|--|--|--|
| IVI | aximum v/c Ratio: 1.01 | | | | | | | |
| In | tersection Signal Delay: 39.1 | Intersection LOS: D | | | | | | |
| Intersection Capacity Utilization 90.9% ICU Level of Service E | | | | | | | | |
| Ar | Analysis Period (min) 15 | | | | | | | |
| De | Description: NOTE: March Road Treated as north-south | | | | | | | |
| ~ | Volume exceeds capacity, queue is theoretically infinite. | | | | | | | |
| | Queue shown is maximum after two cycles. | | | | | | | |
| # | # 95th percentile volume exceeds capacity, queue may be longer. | | | | | | | |
| | Queue shown is maximum after two cycles. | | | | | | | |

Splits and Phases: 1: March & Teron



Parsons Synchro 10 Report

| | • | → | \rightarrow | • | ← | • | • | † | / | > | ļ | 4 |
|------------------------|-------|----------|---------------|-------|----------|-----|-------|----------|----------|-------------|-------|-----|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | f) | | 7 | f) | | 7 | f) | | 7 | £ | |
| Traffic Volume (vph) | 65 | 6 | 131 | 22 | 11 | 16 | 194 | 153 | 30 | 31 | 405 | 125 |
| Future Volume (vph) | 65 | 6 | 131 | 22 | 11 | 16 | 194 | 153 | 30 | 31 | 405 | 125 |
| Satd. Flow (prot) | 1695 | 1496 | 0 | 1695 | 1584 | 0 | 1695 | 1731 | 0 | 1695 | 1697 | 0 |
| Flt Permitted | 0.738 | | | 0.660 | | | 0.185 | | | 0.630 | | |
| Satd. Flow (perm) | 1293 | 1496 | 0 | 1178 | 1584 | 0 | 330 | 1731 | 0 | 1115 | 1697 | 0 |
| Satd. Flow (RTOR) | | 146 | | | 18 | | | 17 | | | 18 | |
| Lane Group Flow (vph) | 72 | 153 | 0 | 24 | 30 | 0 | 216 | 203 | 0 | 34 | 589 | 0 |
| Turn Type | Perm | NA | | Perm | NA | | pm+pt | NA | | Perm | NA | |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Detector Phase | 4 | 4 | | 8 | 8 | | 5 | 2 | | 6 | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 10.0 | 10.0 | | 10.0 | 10.0 | | 5.0 | 10.0 | | 10.0 | 10.0 | |
| Minimum Split (s) | 22.8 | 22.8 | | 22.8 | 22.8 | | 11.0 | 71.2 | | 50.6 | 50.6 | |
| Total Split (s) | 35.8 | 35.8 | | 35.8 | 35.8 | | 20.6 | 71.2 | | 50.6 | 50.6 | |
| Total Split (%) | 33.5% | 33.5% | | 33.5% | 33.5% | | 19.3% | 66.5% | | 47.3% | 47.3% | |
| Yellow Time (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 4.0 | 3.3 | | 3.3 | 3.3 | |
| All-Red Time (s) | 2.8 | 2.8 | | 2.8 | 2.8 | | 2.0 | 2.3 | | 2.3 | 2.3 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | 5.8 | 5.8 | | 5.8 | 5.8 | | 6.0 | 5.6 | | 5.6 | 5.6 | |
| Lead/Lag | | | | | | | Lead | | | Lag | Lag | |
| Lead-Lag Optimize? | | | | | | | Yes | | | Yes | Yes | |
| Recall Mode | None | None | | None | None | | None | Min | | Min | Min | |
| Act Effct Green (s) | 11.8 | 11.8 | | 11.8 | 11.8 | | 48.8 | 49.2 | | 29.9 | 29.9 | |
| Actuated g/C Ratio | 0.16 | 0.16 | | 0.16 | 0.16 | | 0.67 | 0.68 | | 0.41 | 0.41 | |
| v/c Ratio | 0.35 | 0.42 | | 0.13 | 0.11 | | 0.46 | 0.17 | | 0.07 | 0.83 | |
| Control Delay | 35.9 | 10.8 | | 32.2 | 19.9 | | 7.9 | 4.2 | | 13.4 | 30.1 | |
| Queue Delay | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Delay | 35.9 | 10.8 | | 32.2 | 19.9 | | 7.9 | 4.2 | | 13.4 | 30.1 | |
| LOS | D | В | | С | В | | Α | Α | | В | С | |
| Approach Delay | | 18.8 | | | 25.3 | | | 6.1 | | | 29.1 | |
| Approach LOS | | В | | | С | | | Α | | | С | |
| Queue Length 50th (m) | 8.9 | 0.8 | | 2.9 | 1.4 | | 8.3 | 6.8 | | 2.7 | 66.2 | |
| Queue Length 95th (m) | 23.9 | 16.9 | | 10.7 | 9.2 | | 19.7 | 16.9 | | 8.2 | 119.4 | |
| Internal Link Dist (m) | | 594.0 | | | 268.4 | | | 124.5 | | | 613.0 | |
| Turn Bay Length (m) | 60.0 | | | 15.0 | | | 40.0 | | | 45.0 | | |
| Base Capacity (vph) | 551 | 721 | | 502 | 685 | | 504 | 1538 | | 713 | 1092 | |
| Starvation Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Reduced v/c Ratio | 0.13 | 0.21 | | 0.05 | 0.04 | | 0.43 | 0.13 | | 0.05 | 0.54 | |

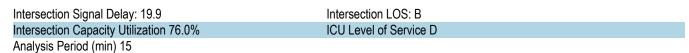
Cycle Length: 107

Actuated Cycle Length: 72.8

Natural Cycle: 95

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.83



Splits and Phases: 3: Teron & Beaverbrook



| Intersection | | | | | | |
|------------------------|--------|-------|--------|----------|----------|-------|
| Int Delay, s/veh | 3.5 | | | | | |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Ť | T T | NUL | 414 | <u> </u> | 7 T |
| Traffic Vol, veh/h | 138 | 87 | 21 | 195 | 506 | 181 |
| Future Vol, veh/h | 138 | 87 | 21 | 195 | 506 | 181 |
| Conflicting Peds, #/hr | 7 | 7 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - - | Yield | - | Free | - | Yield |
| Storage Length | 50 | 0 | _ | - | <u>-</u> | 0 |
| Veh in Median Storage | | - | _ | 0 | 0 | - |
| Grade, % | 0 | _ | _ | 0 | 0 | _ |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| | 2 | 2 | 2 | 2 | 2 | 2 |
| Heavy Vehicles, % | 153 | | 23 | 217 | 562 | 201 |
| Mvmt Flow | 153 | 97 | 23 | 217 | 502 | 201 |
| | | | | | | |
| Major/Minor | Minor2 | | Major1 | | Major2 | |
| Conflicting Flow All | 702 | 569 | 562 | 0 | <u> </u> | 0 |
| Stage 1 | 562 | _ | - | _ | - | _ |
| Stage 2 | 140 | _ | _ | _ | _ | _ |
| Critical Hdwy | 6.08 | 6.23 | 4.13 | - | - | - |
| Critical Hdwy Stg 1 | 5.43 | - | - | _ | _ | _ |
| Critical Hdwy Stg 2 | 6.03 | _ | _ | _ | _ | _ |
| Follow-up Hdwy | 3.669 | 3.319 | 2.219 | _ | _ | _ |
| Pot Cap-1 Maneuver | 420 | 521 | 1007 | _ | _ | _ |
| Stage 1 | 552 | - | - | _ | <u>-</u> | _ |
| Stage 2 | 833 | _ | _ | _ | _ | _ |
| Platoon blocked, % | 000 | | | _ | _ | _ |
| Mov Cap-1 Maneuver | 409 | 518 | 1007 | _ | _ | |
| Mov Cap-1 Maneuver | 409 | - | 1007 | _ | _ | _ |
| Stage 1 | 538 | - | - | <u>-</u> | <u>-</u> | - |
| | | - | - | - | - | - |
| Stage 2 | 833 | _ | - | - | - | - |
| | | | | | | |
| Approach | EB | | NB | | SB | |
| HCM Control Delay, s | 16.9 | | 0.9 | | 0 | |
| HCM LOS | С | | 0.0 | | | |
| | | | | | | |
| | | | | | | |
| Minor Lane/Major Mvn | nt | NBL | NBT | EBLn1 I | | SBT |
| Capacity (veh/h) | | 1007 | - | | 518 | - |
| HCM Lane V/C Ratio | | 0.023 | - | 0.375 | | - |
| HCM Control Delay (s | | 8.7 | 0.1 | 19 | 13.5 | - |
| HCM Lane LOS | | Α | Α | С | В | - |
| HCM 95th %tile Q(veh | 1) | 0.1 | - | 1.7 | 0.7 | - |
| • | | | | | | |



SYNCHRO ANALYSIS: BACKGROUND CONDITIONS

| | ۶ | → | \rightarrow | • | ← | • | 4 | † | <i>></i> | > | ļ | 4 |
|------------------------|--------|----------|---------------|-------|----------|-------|-------|----------|-------------|-------------|-------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | † | 7 | 7 | ^ | 7 | Ĭ | 44 | 7 | 7 | 44 | 7 |
| Traffic Volume (vph) | 493 | 316 | 38 | 23 | 46 | 34 | 44 | 1991 | 199 | 49 | 905 | 186 |
| Future Volume (vph) | 493 | 316 | 38 | 23 | 46 | 34 | 44 | 1991 | 199 | 49 | 905 | 186 |
| Satd. Flow (prot) | 1695 | 1784 | 1517 | 1695 | 1784 | 1517 | 1695 | 3390 | 1517 | 1695 | 3390 | 1517 |
| Flt Permitted | 0.585 | | | 0.308 | | | 0.244 | | | 0.058 | | |
| Satd. Flow (perm) | 1040 | 1784 | 1498 | 549 | 1784 | 1497 | 435 | 3390 | 1498 | 103 | 3390 | 1517 |
| Satd. Flow (RTOR) | | | 188 | | | 188 | | | 188 | | | 188 |
| Lane Group Flow (vph) | 493 | 316 | 38 | 23 | 46 | 34 | 44 | 1991 | 199 | 49 | 905 | 186 |
| Turn Type | pm+pt | NA | Free | pm+pt | NA | Free | pm+pt | NA | Free | pm+pt | NA | Free |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | Free | 8 | | Free | 2 | | Free | 6 | | Free |
| Detector Phase | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 10.0 | | 5.0 | 10.0 | | 5.0 | 10.0 | | 5.0 | 10.0 | |
| Minimum Split (s) | 11.1 | 34.6 | | 11.1 | 34.6 | | 11.4 | 25.3 | | 11.4 | 25.3 | |
| Total Split (s) | 12.0 | 38.0 | | 12.0 | 38.0 | | 12.0 | 68.0 | | 12.0 | 68.0 | |
| Total Split (%) | 9.2% | 29.2% | | 9.2% | 29.2% | | 9.2% | 52.3% | | 9.2% | 52.3% | |
| Yellow Time (s) | 3.3 | 3.3 | | 3.3 | 3.3 | | 4.6 | 4.6 | | 4.6 | 4.6 | |
| All-Red Time (s) | 2.8 | 3.3 | | 2.8 | 3.3 | | 1.8 | 1.7 | | 1.8 | 1.7 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | 6.1 | 6.6 | | 6.1 | 6.6 | | 6.4 | 6.3 | | 6.4 | 6.3 | |
| Lead/Lag | Lead | Lag | | Lead | Lag | | Lead | Lag | | Lead | Lag | |
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | | Yes | Yes | | Yes | Yes | |
| Recall Mode | None | None | | None | None | | None | C-Min | | None | C-Min | |
| Act Effct Green (s) | 31.1 | 27.1 | 130.0 | 27.0 | 22.8 | 130.0 | 77.5 | 72.8 | 130.0 | 77.6 | 72.9 | 130.0 |
| Actuated g/C Ratio | 0.24 | 0.21 | 1.00 | 0.21 | 0.18 | 1.00 | 0.60 | 0.56 | 1.00 | 0.60 | 0.56 | 1.00 |
| v/c Ratio | 1.68 | 0.85 | 0.03 | 0.14 | 0.15 | 0.02 | 0.14 | 1.05 | 0.13 | 0.37 | 0.48 | 0.12 |
| Control Delay | 352.7 | 70.3 | 0.0 | 32.6 | 42.2 | 0.0 | 12.7 | 64.6 | 0.2 | 20.5 | 20.6 | 0.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 352.7 | 70.3 | 0.0 | 32.6 | 42.2 | 0.0 | 12.7 | 64.6 | 0.2 | 20.5 | 20.6 | 0.2 |
| LOS | F | Е | Α | С | D | Α | В | Е | Α | С | С | Α |
| Approach Delay | | 231.5 | | | 26.1 | | | 57.8 | | | 17.3 | |
| Approach LOS | | F | | | С | | | Е | | | В | |
| Queue Length 50th (m) | ~180.8 | 77.7 | 0.0 | 4.1 | 9.5 | 0.0 | 4.5 | ~325.7 | 0.0 | 5.0 | 82.8 | 0.0 |
| Queue Length 95th (m) | #240.0 | 108.5 | 0.0 | 10.3 | 19.6 | 0.0 | 10.2 | #373.8 | 0.0 | 12.0 | 105.2 | 0.0 |
| Internal Link Dist (m) | | 42.6 | | | 349.6 | | | 93.8 | | | 234.3 | |
| Turn Bay Length (m) | 66.0 | | 66.0 | | | 80.0 | 80.0 | | 90.0 | 80.0 | | 85.0 |
| Base Capacity (vph) | 293 | 430 | 1498 | 166 | 430 | 1497 | 317 | 1898 | 1498 | 134 | 1899 | 1517 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 1.68 | 0.73 | 0.03 | 0.14 | 0.11 | 0.02 | 0.14 | 1.05 | 0.13 | 0.37 | 0.48 | 0.12 |

Cycle Length: 130

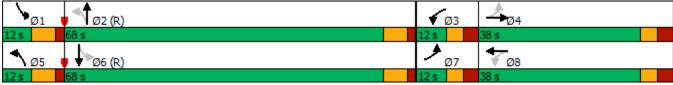
Actuated Cycle Length: 130
Offset: 36 (28%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green

Natural Cycle: 115

Control Type: Actuated-Coordinated

| Maximum v/c Ratio: 1.68 | |
|---|------------------------|
| Intersection Signal Delay: 80.4 | Intersection LOS: F |
| Intersection Capacity Utilization 104.3% | ICU Level of Service G |
| Analysis Period (min) 15 | |
| Description: NOTE: March Road treated as north-south | |
| Volume exceeds capacity, queue is theoretically infinite. | |
| Queue shown is maximum after two cycles. | |
| # 95th percentile volume exceeds capacity, queue may be lo | onger. |
| Queue shown is maximum after two cycles. | |

Splits and Phases: 1: March & Teron



| | • | - | \rightarrow | • | ← | • | • | † | / | > | ļ | 4 |
|------------------------|-------|-------|---------------|-------|----------|-----|-------|----------|-----|-------------|-------|-----|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | Ĭ | £ | | 7 | £ | | , A | f) | | J. | f) | |
| Traffic Volume (vph) | 146 | 4 | 180 | 22 | 2 | 34 | 96 | 334 | 4 | 15 | 200 | 38 |
| Future Volume (vph) | 146 | 4 | 180 | 22 | 2 | 34 | 96 | 334 | 4 | 15 | 200 | 38 |
| Satd. Flow (prot) | 1695 | 1522 | 0 | 1695 | 1452 | 0 | 1695 | 1781 | 0 | 1695 | 1734 | 0 |
| Flt Permitted | 0.734 | | | 0.641 | | | 0.611 | | | 0.557 | | |
| Satd. Flow (perm) | 1268 | 1522 | 0 | 1144 | 1452 | 0 | 1088 | 1781 | 0 | 994 | 1734 | 0 |
| Satd. Flow (RTOR) | | 180 | | | 34 | | | 1 | | | 19 | |
| Lane Group Flow (vph) | 146 | 184 | 0 | 22 | 36 | 0 | 96 | 338 | 0 | 15 | 238 | 0 |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Detector Phase | 4 | 4 | | 8 | 8 | | 2 | 2 | | 6 | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 10.0 | 10.0 | | 10.0 | 10.0 | | 10.0 | 10.0 | | 10.0 | 10.0 | |
| Minimum Split (s) | 22.8 | 22.8 | | 22.8 | 22.8 | | 65.6 | 65.6 | | 65.6 | 65.6 | |
| Total Split (s) | 29.8 | 29.8 | | 29.8 | 29.8 | | 65.6 | 65.6 | | 65.6 | 65.6 | |
| Total Split (%) | 31.2% | 31.2% | | 31.2% | 31.2% | | 68.8% | 68.8% | | 68.8% | 68.8% | |
| Yellow Time (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.3 | 3.3 | | 3.3 | 3.3 | |
| All-Red Time (s) | 2.8 | 2.8 | | 2.8 | 2.8 | | 2.3 | 2.3 | | 2.3 | 2.3 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | 5.8 | 5.8 | | 5.8 | 5.8 | | 5.6 | 5.6 | | 5.6 | 5.6 | |
| Lead/Lag | | | | | | | | | | | | |
| Lead-Lag Optimize? | | | | | | | | | | | | |
| Recall Mode | None | None | | None | None | | Min | Min | | Min | Min | |
| Act Effct Green (s) | 11.5 | 11.5 | | 11.5 | 11.5 | | 14.0 | 14.0 | | 14.0 | 14.0 | |
| Actuated g/C Ratio | 0.31 | 0.31 | | 0.31 | 0.31 | | 0.38 | 0.38 | | 0.38 | 0.38 | |
| v/c Ratio | 0.37 | 0.31 | | 0.06 | 0.08 | | 0.23 | 0.50 | | 0.04 | 0.36 | |
| Control Delay | 14.3 | 4.2 | | 10.9 | 5.5 | | 9.9 | 12.1 | | 7.9 | 9.5 | |
| Queue Delay | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Delay | 14.3 | 4.2 | | 10.9 | 5.5 | | 9.9 | 12.1 | | 7.9 | 9.5 | |
| LOS | В | Α | | В | Α | | Α | В | | Α | Α | |
| Approach Delay | | 8.7 | | | 7.6 | | | 11.6 | | | 9.5 | |
| Approach LOS | | Α | | | Α | | | В | | | Α | |
| Queue Length 50th (m) | 6.1 | 0.2 | | 0.8 | 0.1 | | 3.4 | 13.5 | | 0.5 | 8.2 | |
| Queue Length 95th (m) | 20.7 | 9.9 | | 4.8 | 4.4 | | 12.3 | 36.2 | | 3.1 | 23.9 | |
| Internal Link Dist (m) | | 594.0 | | | 268.4 | | | 124.5 | | | 613.0 | |
| Turn Bay Length (m) | 60.0 | | | 15.0 | | | 40.0 | | | 45.0 | | |
| Base Capacity (vph) | 840 | 1069 | | 758 | 973 | | 1088 | 1781 | | 994 | 1734 | |
| Starvation Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Reduced v/c Ratio | 0.17 | 0.17 | | 0.03 | 0.04 | | 0.09 | 0.19 | | 0.02 | 0.14 | |

Cycle Length: 95.4

Actuated Cycle Length: 37.2 Natural Cycle: 90

Control Type: Semi Act-Uncoord Maximum v/c Ratio: 0.50

| Intersection Signal Delay: 10.0 | Intersection LOS: A |
|---|------------------------|
| Intersection Capacity Utilization 60.6% | ICU Level of Service B |
| Analysis Period (min) 15 | |

Splits and Phases: 3: Teron & Beaverbrook



| Intersection | | | | | | | |
|-------------------------------|--------|----------|--------|-----------|----------|-------|---|
| Intersection Int Delay, s/veh | 2.6 | | | | | | |
| - | | | | | | | , |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR | ı |
| Lane Configurations | | 7 | | ተተኩ | | 7 | |
| Traffic Vol, veh/h | 129 | 66 | 45 | 580 | 170 | 97 | |
| Future Vol, veh/h | 129 | 66 | 45 | 580 | 170 | 97 | |
| Conflicting Peds, #/hr | 4 | 4 | 0 | 0 | 0 | 0 | |
| Sign Control | Stop | Stop | Free | Free | Free | Free | |
| RT Channelized | - | Yield | - | Free | - | Yield | |
| Storage Length | 50 | 0 | - | - | - | 0 | |
| Veh in Median Storage | e, # 0 | - | - | 0 | 0 | - | |
| Grade, % | 0 | - | - | 0 | 0 | - | |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | |
| Mvmt Flow | 129 | 66 | 45 | 580 | 170 | 97 | |
| | | | | | | | |
| Maior/Minor | Minar | | \ | | Maisir | | |
| | Minor2 | | Major1 | | Major2 | ^ | |
| Conflicting Flow All | 496 | 174 | 170 | 0 | - | 0 | |
| Stage 1 | 170 | - | - | - | - | - | |
| Stage 2 | 326 | - | - | - | - | - | |
| Critical Hdwy | 6.08 | 6.23 | 4.13 | - | - | - | |
| Critical Hdwy Stg 1 | 5.43 | - | - | - | - | - | |
| Critical Hdwy Stg 2 | 6.03 | - | - | - | - | - | |
| Follow-up Hdwy | | 3.319 | | - | - | - | |
| Pot Cap-1 Maneuver | 541 | 869 | 1406 | - | - | - | |
| Stage 1 | 827 | - | - | - | - | - | |
| Stage 2 | 668 | - | - | - | - | - | |
| Platoon blocked, % | | | | - | - | - | |
| Mov Cap-1 Maneuver | 516 | 866 | 1406 | - | - | - | |
| Mov Cap-2 Maneuver | 516 | - | - | - | - | - | |
| Stage 1 | 788 | _ | _ | - | - | - | |
| Stage 2 | 668 | - | _ | _ | _ | - | |
| | 300 | | | | | | |
| Ammanah | ED | | ND | | CD | | |
| Approach | EB | | NB | | SB | | |
| HCM Control Delay, s | 12.7 | | 0.6 | | 0 | | |
| HCM LOS | В | | | | | | |
| | | | | | | | |
| Minor Lane/Major Mvn | nt | NBL | NBT | EBLn1 | EBLn2 | SBT | |
| Capacity (veh/h) | | 1406 | - | 516 | 866 | - | |
| HCM Lane V/C Ratio | | 0.032 | _ | | 0.076 | _ | |
| HCM Control Delay (s |) | 7.6 | 0.1 | 14.3 | 9.5 | _ | |
| HCM Lane LOS |) | 7.0 A | Α | 14.3 B | 9.5 A | _ | |
| HCM 95th %tile Q(veh | .) | 0.1 | - - | 1 | 0.2 | | |
| | 11 | U. I | - | 1 | 0.2 | - | |

| | • | → | \rightarrow | • | ← | • | 4 | † | <i>></i> | > | ļ | 4 |
|------------------------|-------|----------|---------------|-------|----------|-------|-------|----------|-------------|-------------|----------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | † | 7 | ሻ | † | 7 | * | ^ | 7 | ሻ | ^ | 7 |
| Traffic Volume (vph) | 236 | 60 | 56 | 153 | 200 | 50 | 77 | 1281 | 20 | 11 | 2019 | 473 |
| Future Volume (vph) | 236 | 60 | 56 | 153 | 200 | 50 | 77 | 1281 | 20 | 11 | 2019 | 473 |
| Satd. Flow (prot) | 1695 | 1784 | 1517 | 1695 | 1784 | 1517 | 1695 | 3390 | 1517 | 1695 | 3390 | 1517 |
| Flt Permitted | 0.521 | | | 0.587 | | | 0.057 | | | 0.134 | | |
| Satd. Flow (perm) | 921 | 1784 | 1498 | 1046 | 1784 | 1493 | 102 | 3390 | 1498 | 239 | 3390 | 1517 |
| Satd. Flow (RTOR) | | | 188 | | | 188 | | | 188 | | | 188 |
| Lane Group Flow (vph) | 236 | 60 | 56 | 153 | 200 | 50 | 77 | 1281 | 20 | 11 | 2019 | 473 |
| Turn Type | pm+pt | NA | Free | pm+pt | NA | Free | pm+pt | NA | Free | pm+pt | NA | Free |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | Free | 8 | | Free | 2 | | Free | 6 | | Free |
| Detector Phase | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 10.0 | | 5.0 | 10.0 | | 5.0 | 10.0 | | 5.0 | 10.0 | |
| Minimum Split (s) | 11.1 | 34.6 | | 11.1 | 34.6 | | 11.4 | 25.3 | | 11.4 | 25.3 | |
| Total Split (s) | 17.0 | 35.0 | | 17.0 | 35.0 | | 12.0 | 66.0 | | 12.0 | 66.0 | |
| Total Split (%) | 13.1% | 26.9% | | 13.1% | 26.9% | | 9.2% | 50.8% | | 9.2% | 50.8% | |
| Yellow Time (s) | 3.3 | 3.3 | | 3.3 | 3.3 | | 4.6 | 4.6 | | 4.6 | 4.6 | |
| All-Red Time (s) | 2.8 | 3.3 | | 2.8 | 3.3 | | 1.8 | 1.7 | | 1.8 | 1.7 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | 6.1 | 6.6 | | 6.1 | 6.6 | | 6.4 | 6.3 | | 6.4 | 6.3 | |
| Lead/Lag | Lead | Lag | | Lead | Lag | | Lead | Lag | | Lead | Lag | |
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | | Yes | Yes | | Yes | Yes | |
| Recall Mode | None | None | | None | None | | None | C-Min | | None | C-Min | |
| Act Effct Green (s) | 28.8 | 19.5 | 130.0 | 32.7 | 20.1 | 130.0 | 77.9 | 75.0 | 130.0 | 72.1 | 66.4 | 130.0 |
| Actuated g/C Ratio | 0.22 | 0.15 | 1.00 | 0.25 | 0.15 | 1.00 | 0.60 | 0.58 | 1.00 | 0.55 | 0.51 | 1.00 |
| v/c Ratio | 0.88 | 0.22 | 0.04 | 0.46 | 0.73 | 0.03 | 0.52 | 0.65 | 0.01 | 0.06 | 1.17 | 0.31 |
| Control Delay | 73.5 | 48.1 | 0.1 | 40.1 | 66.9 | 0.0 | 30.3 | 22.9 | 0.0 | 12.5 | 112.2 | 0.5 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 73.5 | 48.1 | 0.1 | 40.1 | 66.9 | 0.0 | 30.3 | 22.9 | 0.0 | 12.5 | 112.2 | 0.5 |
| LOS | E | D | Α | D | Е | Α | С | С | Α | В | F | Α |
| Approach Delay | | 57.5 | | | 48.4 | | | 23.0 | | | 90.7 | |
| Approach LOS | | Е | | | D | | | С | | | F | |
| Queue Length 50th (m) | 50.2 | 13.7 | 0.0 | 30.8 | 49.5 | 0.0 | 7.5 | 100.0 | 0.0 | 1.0 | ~324.8 | 0.0 |
| Queue Length 95th (m) | 68.4 | 24.7 | 0.0 | 45.0 | 70.2 | 0.0 | #27.5 | 177.1 | 0.0 | 4.1 | #388.9 | 0.0 |
| Internal Link Dist (m) | | 42.6 | | | 349.6 | | | 93.8 | | | 234.3 | |
| Turn Bay Length (m) | 66.0 | | 66.0 | | | 80.0 | 80.0 | 10-0 | 90.0 | 80.0 | 4=0.4 | 85.0 |
| Base Capacity (vph) | 268 | 389 | 1498 | 336 | 389 | 1493 | 149 | 1956 | 1498 | 197 | 1731 | 1517 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.88 | 0.15 | 0.04 | 0.46 | 0.51 | 0.03 | 0.52 | 0.65 | 0.01 | 0.06 | 1.17 | 0.31 |

Cycle Length: 130

Actuated Cycle Length: 130
Offset: 121 (93%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green

Natural Cycle: 115

Control Type: Actuated-Coordinated

| Maximum v/c Ratio: 1.17 | |
|---|------------------------|
| Intersection Signal Delay: 64.4 | Intersection LOS: E |
| Intersection Capacity Utilization 111.8% | ICU Level of Service H |
| Analysis Period (min) 15 | |
| Description: NOTE: March Road Treated as north-south | |
| Volume exceeds capacity, queue is theoretically infinite. | |
| Queue shown is maximum after two cycles. | |
| # 95th percentile volume exceeds capacity, queue may be lor | nger. |
| Queue shown is maximum after two cycles. | |

Splits and Phases: 1: March & Teron



| | ۶ | → | \rightarrow | • | ← | • | 4 | † | / | > | ↓ | 4 |
|------------------------|-------|----------|---------------|-------|----------|-----|-------|----------|----------|-------------|----------|-----|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | f) | | ሻ | ĥ | | ሻ | f) | | ሻ | f) | |
| Traffic Volume (vph) | 65 | 6 | 131 | 22 | 11 | 16 | 194 | 216 | 30 | 31 | 512 | 125 |
| Future Volume (vph) | 65 | 6 | 131 | 22 | 11 | 16 | 194 | 216 | 30 | 31 | 512 | 125 |
| Satd. Flow (prot) | 1695 | 1496 | 0 | 1695 | 1586 | 0 | 1695 | 1744 | 0 | 1695 | 1712 | 0 |
| Flt Permitted | 0.740 | | | 0.669 | | | 0.174 | | | 0.606 | | |
| Satd. Flow (perm) | 1296 | 1496 | 0 | 1194 | 1586 | 0 | 310 | 1744 | 0 | 1073 | 1712 | 0 |
| Satd. Flow (RTOR) | | 131 | | | 16 | | | 12 | | | 14 | |
| Lane Group Flow (vph) | 65 | 137 | 0 | 22 | 27 | 0 | 194 | 246 | 0 | 31 | 637 | 0 |
| Turn Type | Perm | NA | | Perm | NA | | pm+pt | NA | | Perm | NA | |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Detector Phase | 4 | 4 | | 8 | 8 | | 5 | 2 | | 6 | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 10.0 | 10.0 | | 10.0 | 10.0 | | 5.0 | 10.0 | | 10.0 | 10.0 | |
| Minimum Split (s) | 22.8 | 22.8 | | 22.8 | 22.8 | | 11.0 | 71.2 | | 50.6 | 50.6 | |
| Total Split (s) | 35.8 | 35.8 | | 35.8 | 35.8 | | 20.6 | 71.2 | | 50.6 | 50.6 | |
| Total Split (%) | 33.5% | 33.5% | | 33.5% | 33.5% | | 19.3% | 66.5% | | 47.3% | 47.3% | |
| Yellow Time (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 4.0 | 3.3 | | 3.3 | 3.3 | |
| All-Red Time (s) | 2.8 | 2.8 | | 2.8 | 2.8 | | 2.0 | 2.3 | | 2.3 | 2.3 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | 5.8 | 5.8 | | 5.8 | 5.8 | | 6.0 | 5.6 | | 5.6 | 5.6 | |
| Lead/Lag | | | | | | | Lead | | | Lag | Lag | |
| Lead-Lag Optimize? | | | | | | | Yes | | | Yes | Yes | |
| Recall Mode | None | None | | None | None | | None | Min | | Min | Min | |
| Act Effct Green (s) | 11.7 | 11.7 | | 11.7 | 11.7 | | 52.2 | 52.6 | | 33.5 | 33.5 | |
| Actuated g/C Ratio | 0.15 | 0.15 | | 0.15 | 0.15 | | 0.69 | 0.69 | | 0.44 | 0.44 | |
| v/c Ratio | 0.33 | 0.40 | | 0.12 | 0.11 | | 0.43 | 0.20 | | 0.07 | 0.84 | |
| Control Delay | 37.3 | 11.3 | | 33.6 | 21.0 | | 7.3 | 4.4 | | 12.8 | 29.6 | |
| Queue Delay | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Delay | 37.3 | 11.3 | | 33.6 | 21.0 | | 7.3 | 4.4 | | 12.8 | 29.6 | |
| LOS | D | В | | С | С | | Α | Α | | В | С | |
| Approach Delay | | 19.6 | | | 26.7 | | | 5.7 | | | 28.8 | |
| Approach LOS | | В | | | С | | | Α | | | С | |
| Queue Length 50th (m) | 8.8 | 0.8 | | 2.9 | 1.4 | | 7.3 | 8.8 | | 2.4 | 75.2 | |
| Queue Length 95th (m) | 22.0 | 15.9 | | 10.0 | 8.7 | | 17.7 | 20.9 | | 7.7 | 135.3 | |
| Internal Link Dist (m) | | 594.0 | | | 268.4 | | | 124.5 | | | 613.0 | |
| Turn Bay Length (m) | 60.0 | | | 15.0 | | | 40.0 | | | 45.0 | | |
| Base Capacity (vph) | 527 | 686 | | 485 | 654 | | 487 | 1499 | | 654 | 1050 | |
| Starvation Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Reduced v/c Ratio | 0.12 | 0.20 | | 0.05 | 0.04 | | 0.40 | 0.16 | | 0.05 | 0.61 | |

Cycle Length: 107

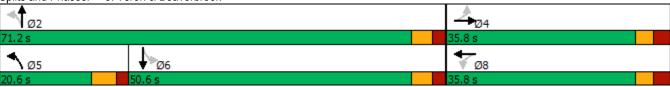
Actuated Cycle Length: 76.1 Natural Cycle: 95

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.84

| Intersection Signal Delay: 19.9 | Intersection LOS: B |
|---|------------------------|
| Intersection Capacity Utilization 81.9% | ICU Level of Service D |
| Analysis Period (min) 15 | |

Splits and Phases: 3: Teron & Beaverbrook



| Intersection | | | | | | | |
|-----------------------------|--------|-------|--------|-------|----------|-------|--|
| Int Delay, s/veh | 4.4 | | | | | | |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR | |
| Lane Configurations | ሻ | 7 | HUL | 414 | <u> </u> | 7 | |
| Traffic Vol, veh/h | 166 | 105 | 50 | 222 | 577 | 181 | |
| Future Vol, veh/h | 166 | 105 | 50 | 222 | 577 | 181 | |
| Conflicting Peds, #/hr | 7 | 7 | 0 | 0 | 0 | 0 | |
| • | | | Free | Free | Free | Free | |
| Sign Control RT Channelized | Stop | Stop | | | | | |
| | - | Yield | - | Free | - | Yield | |
| Storage Length | 50 | 0 | - | - | - | 0 | |
| Veh in Median Storage | | - | - | 0 | 0 | - | |
| Grade, % | 0 | - | - | 0 | 0 | - | |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | |
| Mvmt Flow | 166 | 105 | 50 | 222 | 577 | 181 | |
| | | | | | | | |
| Major/Minor | Minor2 | | Major1 | | Major2 | | |
| | | | | | | | |
| Conflicting Flow All | 773 | 584 | 577 | 0 | - | 0 | |
| Stage 1 | 577 | - | - | - | - | - | |
| Stage 2 | 196 | - | - | - | - | - | |
| Critical Hdwy | 6.08 | 6.23 | 4.13 | - | - | - | |
| Critical Hdwy Stg 1 | 5.43 | - | - | - | - | - | |
| Critical Hdwy Stg 2 | 6.03 | - | - | - | - | - | |
| Follow-up Hdwy | 3.669 | 3.319 | | - | - | - | |
| Pot Cap-1 Maneuver | 384 | 511 | 995 | - | - | - | |
| Stage 1 | 544 | - | - | - | - | - | |
| Stage 2 | 780 | - | - | - | - | - | |
| Platoon blocked, % | | | | - | - | - | |
| Mov Cap-1 Maneuver | 362 | 508 | 995 | - | - | | |
| Mov Cap-2 Maneuver | | - | - | _ | _ | - | |
| Stage 1 | 513 | _ | _ | _ | _ | _ | |
| Stage 2 | 780 | _ | _ | _ | _ | _ | |
| Olugo Z | 700 | | | | | | |
| | | | | | | | |
| Approach | EB | | NB | | SB | | |
| HCM Control Delay, s | 19.5 | | 1.7 | | 0 | | |
| HCM LOS | С | | | | | | |
| | | | | | | | |
| N. 1 (N. 1) | | ND | NDT | EDI 4 | EDI C | ODT | |
| Minor Lane/Major Mvr | nt | NBL | NBI | EBLn1 | | SBT | |
| Capacity (veh/h) | | 995 | - | 362 | 508 | - | |
| HCM Lane V/C Ratio | | 0.05 | | 0.459 | | - | |
| HCM Control Delay (s |) | 8.8 | 0.1 | 23.1 | 13.9 | - | |
| HCM Lane LOS | | Α | Α | С | В | - | |
| HCM 95th %tile Q(veh | 1) | 0.2 | _ | 2.3 | 0.8 | - | |



SYNCHRO ANALYSIS: FUTURE CONDITIONS

| | ٠ | → | • | • | ← | • | 4 | † | <i>></i> | > | ļ | 4 |
|------------------------|--------|----------|-------|-------|----------|-------|-------|----------|-------------|-------------|-------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | † | 7 | 7 | ^ | 7 | Ĭ | 44 | 7 | 7 | 44 | 7 |
| Traffic Volume (vph) | 498 | 289 | 51 | 23 | 42 | 34 | 47 | 1828 | 199 | 49 | 837 | 188 |
| Future Volume (vph) | 498 | 289 | 51 | 23 | 42 | 34 | 47 | 1828 | 199 | 49 | 837 | 188 |
| Satd. Flow (prot) | 1695 | 1784 | 1517 | 1695 | 1784 | 1517 | 1695 | 3390 | 1517 | 1695 | 3390 | 1517 |
| Flt Permitted | 0.590 | | | 0.344 | | | 0.274 | | | 0.057 | | |
| Satd. Flow (perm) | 1049 | 1784 | 1498 | 613 | 1784 | 1497 | 489 | 3390 | 1498 | 102 | 3390 | 1517 |
| Satd. Flow (RTOR) | | | 188 | | | 188 | | | 188 | | | 188 |
| Lane Group Flow (vph) | 498 | 289 | 51 | 23 | 42 | 34 | 47 | 1828 | 199 | 49 | 837 | 188 |
| Turn Type | pm+pt | NA | Free | pm+pt | NA | Free | pm+pt | NA | Free | pm+pt | NA | Free |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | Free | 8 | | Free | 2 | | Free | 6 | | Free |
| Detector Phase | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 10.0 | | 5.0 | 10.0 | | 5.0 | 10.0 | | 5.0 | 10.0 | |
| Minimum Split (s) | 11.1 | 34.6 | | 11.1 | 34.6 | | 11.4 | 25.3 | | 11.4 | 25.3 | |
| Total Split (s) | 12.0 | 38.0 | | 12.0 | 38.0 | | 12.0 | 68.0 | | 12.0 | 68.0 | |
| Total Split (%) | 9.2% | 29.2% | | 9.2% | 29.2% | | 9.2% | 52.3% | | 9.2% | 52.3% | |
| Yellow Time (s) | 3.3 | 3.3 | | 3.3 | 3.3 | | 4.6 | 4.6 | | 4.6 | 4.6 | |
| All-Red Time (s) | 2.8 | 3.3 | | 2.8 | 3.3 | | 1.8 | 1.7 | | 1.8 | 1.7 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | 6.1 | 6.6 | | 6.1 | 6.6 | | 6.4 | 6.3 | | 6.4 | 6.3 | |
| Lead/Lag | Lead | Lag | | Lead | Lag | | Lead | Lag | | Lead | Lag | |
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | | Yes | Yes | | Yes | Yes | |
| Recall Mode | None | None | | None | None | | None | C-Min | | None | C-Min | |
| Act Effct Green (s) | 29.6 | 25.6 | 130.0 | 25.8 | 21.6 | 130.0 | 79.1 | 73.9 | 130.0 | 79.1 | 74.0 | 130.0 |
| Actuated g/C Ratio | 0.23 | 0.20 | 1.00 | 0.20 | 0.17 | 1.00 | 0.61 | 0.57 | 1.00 | 0.61 | 0.57 | 1.00 |
| v/c Ratio | 1.77 | 0.82 | 0.03 | 0.14 | 0.14 | 0.02 | 0.13 | 0.95 | 0.13 | 0.35 | 0.43 | 0.12 |
| Control Delay | 392.1 | 68.8 | 0.0 | 33.3 | 43.0 | 0.0 | 12.1 | 40.4 | 0.2 | 19.5 | 19.5 | 0.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 392.1 | 68.8 | 0.0 | 33.3 | 43.0 | 0.0 | 12.1 | 40.4 | 0.2 | 19.5 | 19.5 | 0.2 |
| LOS | F | E | Α | С | D | Α | В | D | Α | В | В | Α |
| Approach Delay | | 256.7 | | | 26.0 | | | 35.9 | | | 16.1 | |
| Approach LOS | | F | | | С | | | D | | | В | |
| Queue Length 50th (m) | ~187.3 | 71.2 | 0.0 | 4.2 | 8.9 | 0.0 | 4.6 | ~272.8 | 0.0 | 4.8 | 72.2 | 0.0 |
| Queue Length 95th (m) | #242.1 | 98.2 | 0.0 | 10.3 | 18.1 | 0.0 | 10.7 | #328.7 | 0.0 | 12.1 | 95.1 | 0.0 |
| Internal Link Dist (m) | | 42.6 | | | 349.6 | | | 93.8 | | | 234.3 | |
| Turn Bay Length (m) | 66.0 | | 66.0 | | | 80.0 | 80.0 | | 90.0 | 80.0 | | 85.0 |
| Base Capacity (vph) | 281 | 430 | 1498 | 171 | 430 | 1497 | 356 | 1928 | 1498 | 140 | 1928 | 1517 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 1.77 | 0.67 | 0.03 | 0.13 | 0.10 | 0.02 | 0.13 | 0.95 | 0.13 | 0.35 | 0.43 | 0.12 |

Cycle Length: 130

Actuated Cycle Length: 130
Offset: 36 (28%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green

Natural Cycle: 115

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 1.77
Intersection Signal Delay: 75.7
Intersection Capacity Utilization 99.9%
ICU Level of Service F

Analysis Period (min) 15
Description: NOTE: March Road treated as north-south

Volume exceeds capacity, queue is theoretically infinite.
Queue shown is maximum after two cycles.

95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

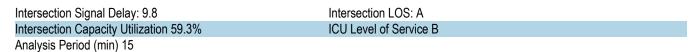
Splits and Phases: 1: March & Teron



| | ۶ | - | • | • | ← | • | • | † | <i>></i> | / | ļ | 1 |
|------------------------|-------|-------|-----|-------|----------|-----|-------|----------|-------------|----------|-------|-----|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | ₽ | | ሻ | f) | | 7 | ₽ | | 7 | 1> | |
| Traffic Volume (vph) | 146 | 4 | 180 | 22 | 2 | 34 | 96 | 310 | 4 | 15 | 190 | 39 |
| Future Volume (vph) | 146 | 4 | 180 | 22 | 2 | 34 | 96 | 310 | 4 | 15 | 190 | 39 |
| Satd. Flow (prot) | 1695 | 1522 | 0 | 1695 | 1452 | 0 | 1695 | 1781 | 0 | 1695 | 1730 | 0 |
| Flt Permitted | 0.734 | | | 0.641 | | | 0.616 | | | 0.570 | | |
| Satd. Flow (perm) | 1268 | 1522 | 0 | 1144 | 1452 | 0 | 1097 | 1781 | 0 | 1017 | 1730 | 0 |
| Satd. Flow (RTOR) | | 180 | | | 34 | | | 1 | | | 21 | |
| Lane Group Flow (vph) | 146 | 184 | 0 | 22 | 36 | 0 | 96 | 314 | 0 | 15 | 229 | 0 |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Detector Phase | 4 | 4 | | 8 | 8 | | 2 | 2 | | 6 | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 10.0 | 10.0 | | 10.0 | 10.0 | | 10.0 | 10.0 | | 10.0 | 10.0 | |
| Minimum Split (s) | 22.8 | 22.8 | | 22.8 | 22.8 | | 65.6 | 65.6 | | 65.6 | 65.6 | |
| Total Split (s) | 29.8 | 29.8 | | 29.8 | 29.8 | | 65.6 | 65.6 | | 65.6 | 65.6 | |
| Total Split (%) | 31.2% | 31.2% | | 31.2% | 31.2% | | 68.8% | 68.8% | | 68.8% | 68.8% | |
| Yellow Time (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.3 | 3.3 | | 3.3 | 3.3 | |
| All-Red Time (s) | 2.8 | 2.8 | | 2.8 | 2.8 | | 2.3 | 2.3 | | 2.3 | 2.3 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | 5.8 | 5.8 | | 5.8 | 5.8 | | 5.6 | 5.6 | | 5.6 | 5.6 | |
| Lead/Lag | | | | | | | | | | | | |
| Lead-Lag Optimize? | | | | | | | | | | | | |
| Recall Mode | None | None | | None | None | | Min | Min | | Min | Min | |
| Act Effct Green (s) | 11.4 | 11.4 | | 11.4 | 11.4 | | 13.3 | 13.3 | | 13.3 | 13.3 | |
| Actuated g/C Ratio | 0.31 | 0.31 | | 0.31 | 0.31 | | 0.37 | 0.37 | | 0.37 | 0.37 | |
| v/c Ratio | 0.37 | 0.31 | | 0.06 | 0.08 | | 0.24 | 0.48 | | 0.04 | 0.35 | |
| Control Delay | 13.5 | 4.0 | | 10.2 | 5.2 | | 10.2 | 12.0 | | 8.2 | 9.6 | |
| Queue Delay | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Delay | 13.5 | 4.0 | | 10.2 | 5.2 | | 10.2 | 12.0 | | 8.2 | 9.6 | |
| LOS | В | Α | | В | Α | | В | В | | Α | Α | |
| Approach Delay | | 8.2 | | | 7.1 | | | 11.6 | | | 9.5 | |
| Approach LOS | | Α | | | Α | | | В | | | Α | |
| Queue Length 50th (m) | 5.9 | 0.2 | | 0.8 | 0.1 | | 3.4 | 12.4 | | 0.5 | 7.7 | |
| Queue Length 95th (m) | 19.4 | 9.3 | | 4.5 | 4.2 | | 12.5 | 33.7 | | 3.2 | 23.1 | |
| Internal Link Dist (m) | | 594.0 | | | 268.4 | | | 124.5 | | | 518.6 | |
| Turn Bay Length (m) | 60.0 | | | 15.0 | | | 40.0 | | | 45.0 | | |
| Base Capacity (vph) | 855 | 1085 | | 771 | 990 | | 1097 | 1781 | | 1017 | 1730 | |
| Starvation Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Reduced v/c Ratio | 0.17 | 0.17 | | 0.03 | 0.04 | | 0.09 | 0.18 | | 0.01 | 0.13 | |

Cycle Length: 95.4

Actuated Cycle Length: 36.4
Natural Cycle: 90
Control Type: Semi Act-Uncoord Maximum v/c Ratio: 0.48







| Intersection | | | | | | |
|------------------------|----------|-------|--------|---------|--------|-------|
| Int Delay, s/veh | 2.7 | | | | | |
| | | EDD | NDI | NDT | CDT | CDD |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | \ | 7 | 4- | ተተኩ | 100 | 7 |
| Traffic Vol, veh/h | 129 | 66 | 45 | 547 | 160 | 97 |
| Future Vol, veh/h | 129 | 66 | 45 | 547 | 160 | 97 |
| Conflicting Peds, #/hr | | 4 | _ 0 | _ 0 | _ 0 | _ 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | Yield | - | Free | - | Yield |
| Storage Length | 50 | 0 | - | - | - | 0 |
| Veh in Median Storage | e, # 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 129 | 66 | 45 | 547 | 160 | 97 |
| | | | | | | |
| | 0 | | | | | |
| | Minor2 | | Major1 | | Major2 | |
| Conflicting Flow All | 473 | 164 | 160 | 0 | - | 0 |
| Stage 1 | 160 | - | - | - | - | - |
| Stage 2 | 313 | - | - | - | - | - |
| Critical Hdwy | 6.08 | 6.23 | 4.13 | - | - | - |
| Critical Hdwy Stg 1 | 5.43 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.03 | - | - | - | - | - |
| Follow-up Hdwy | 3.669 | 3.319 | 2.219 | - | - | - |
| Pot Cap-1 Maneuver | 556 | 880 | 1418 | - | - | - |
| Stage 1 | 835 | - | - | - | - | - |
| Stage 2 | 678 | - | - | - | - | - |
| Platoon blocked, % | | | | _ | - | - |
| Mov Cap-1 Maneuver | 530 | 877 | 1418 | _ | _ | _ |
| Mov Cap-2 Maneuver | | - | - | _ | _ | - |
| Stage 1 | 797 | _ | _ | _ | _ | _ |
| Stage 2 | 678 | _ | _ | _ | _ | _ |
| Olago Z | 0,0 | | | | _ | |
| | | | | | | |
| Approach | EB | | NB | | SB | |
| HCM Control Delay, s | 12.4 | | 0.7 | | 0 | |
| HCM LOS | В | | | | | |
| | | | | | | |
| Minor Long/Major Mar | mt | NDI | NDT | EDI 511 | EDI 52 | CDT |
| Minor Lane/Major Mvr | III | NBL | MRT | EBLn1 I | | SBT |
| Capacity (veh/h) | | 1418 | - | 530 | 877 | - |
| HCM Lane V/C Ratio | | 0.032 | | 0.243 | | - |
| HCM Control Delay (s | 5) | 7.6 | 0.1 | 14 | 9.4 | - |
| HCM Lane LOS | | Α | Α | В | Α | - |
| HCM 95th %tile Q(veh | 1) | 0.1 | _ | 0.9 | 0.2 | _ |

| Intersection | | | | | | |
|------------------------|--------|----------|--------|-------|--------|------|
| Int Delay, s/veh | 0.4 | | | | | |
| | | 14/5-5 | | | 0-1 | 05= |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | ¥ | | f) | | | 4 |
| Traffic Vol, veh/h | 5 | 18 | 576 | 3 | 5 | 223 |
| Future Vol, veh/h | 5 | 18 | 576 | 3 | 5 | 223 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage | e,# 0 | _ | 0 | - | - | 0 |
| Grade, % | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mymt Flow | 5 | 18 | 576 | 3 | 5 | 223 |
| IVIVIII(I IOVV | 0 | 10 | 310 | 3 | 3 | 220 |
| | | | | | | |
| Major/Minor | Minor1 | N | Major1 | 1 | Major2 | |
| Conflicting Flow All | 811 | 578 | 0 | 0 | 579 | 0 |
| Stage 1 | 578 | - | - | - | - | - |
| Stage 2 | 233 | _ | _ | _ | _ | _ |
| Critical Hdwy | 6.42 | 6.22 | _ | _ | 4.12 | _ |
| Critical Hdwy Stg 1 | 5.42 | - | _ | _ | | _ |
| Critical Hdwy Stg 2 | 5.42 | _ | _ | _ | _ | _ |
| Follow-up Hdwy | | 3.318 | _ | _ | 2.218 | _ |
| Pot Cap-1 Maneuver | 349 | 516 | _ | _ | 995 | _ |
| • | 561 | - | _ | _ | - | _ |
| Stage 1 | | | | _ | | |
| Stage 2 | 806 | - | - | - | - | - |
| Platoon blocked, % | 0.47 | 540 | - | - | 005 | - |
| Mov Cap-1 Maneuver | | 516 | - | - | 995 | - |
| Mov Cap-2 Maneuver | | - | - | - | - | - |
| Stage 1 | 561 | - | - | - | - | - |
| Stage 2 | 801 | - | - | - | - | - |
| | | | | | | |
| Approach | WB | | NB | | SB | |
| | | | | | 0.2 | |
| HCM Control Delay, s | 13.1 | | 0 | | 0.2 | |
| HCM LOS | В | | | | | |
| | | | | | | |
| Minor Lane/Major Mvn | nt | NBT | NBRV | VBLn1 | SBL | SBT |
| Capacity (veh/h) | | | | 467 | 995 | |
| HCM Lane V/C Ratio | | <u>-</u> | | 0.049 | | _ |
| HCM Control Delay (s) | ١ | | | 13.1 | 8.6 | 0 |
| |) | - | - | | | |
| HCM Lane LOS | .) | - | - | В | A | Α |
| HCM 95th %tile Q(veh | 1) | - | - | 0.2 | 0 | - |

| | ۶ | → | • | • | ← | • | 4 | † | <i>></i> | > | ļ | 4 |
|------------------------|-------|----------|-------|-------|----------|-------|-------|----------|-------------|-------------|----------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | † | 7 | 7 | † | 7 | * | ^ | 7 | 7 | ^ | 7 |
| Traffic Volume (vph) | 240 | 55 | 64 | 153 | 184 | 50 | 85 | 1179 | 20 | 11 | 1852 | 479 |
| Future Volume (vph) | 240 | 55 | 64 | 153 | 184 | 50 | 85 | 1179 | 20 | 11 | 1852 | 479 |
| Satd. Flow (prot) | 1695 | 1784 | 1517 | 1695 | 1784 | 1517 | 1695 | 3390 | 1517 | 1695 | 3390 | 1517 |
| Flt Permitted | 0.559 | | | 0.591 | | | 0.056 | | | 0.168 | | |
| Satd. Flow (perm) | 988 | 1784 | 1498 | 1053 | 1784 | 1493 | 100 | 3390 | 1498 | 300 | 3390 | 1517 |
| Satd. Flow (RTOR) | | | 188 | | | 188 | | | 188 | | | 188 |
| Lane Group Flow (vph) | 240 | 55 | 64 | 153 | 184 | 50 | 85 | 1179 | 20 | 11 | 1852 | 479 |
| Turn Type | pm+pt | NA | Free | pm+pt | NA | Free | pm+pt | NA | Free | pm+pt | NA | Free |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | Free | 8 | | Free | 2 | | Free | 6 | | Free |
| Detector Phase | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 10.0 | | 5.0 | 10.0 | | 5.0 | 10.0 | | 5.0 | 10.0 | |
| Minimum Split (s) | 11.1 | 34.6 | | 11.1 | 34.6 | | 11.4 | 25.3 | | 11.4 | 25.3 | |
| Total Split (s) | 17.0 | 35.0 | | 17.0 | 35.0 | | 12.0 | 66.0 | | 12.0 | 66.0 | |
| Total Split (%) | 13.1% | 26.9% | | 13.1% | 26.9% | | 9.2% | 50.8% | | 9.2% | 50.8% | |
| Yellow Time (s) | 3.3 | 3.3 | | 3.3 | 3.3 | | 4.6 | 4.6 | | 4.6 | 4.6 | |
| All-Red Time (s) | 2.8 | 3.3 | | 2.8 | 3.3 | | 1.8 | 1.7 | | 1.8 | 1.7 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | 6.1 | 6.6 | | 6.1 | 6.6 | | 6.4 | 6.3 | | 6.4 | 6.3 | |
| Lead/Lag | Lead | Lag | | Lead | Lag | | Lead | Lag | | Lead | Lag | |
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | | Yes | Yes | | Yes | Yes | |
| Recall Mode | None | None | | None | None | | None | C-Min | | None | C-Min | |
| Act Effct Green (s) | 28.1 | 18.8 | 130.0 | 31.8 | 19.2 | 130.0 | 78.9 | 75.9 | 130.0 | 72.6 | 66.9 | 130.0 |
| Actuated g/C Ratio | 0.22 | 0.14 | 1.00 | 0.24 | 0.15 | 1.00 | 0.61 | 0.58 | 1.00 | 0.56 | 0.51 | 1.00 |
| v/c Ratio | 0.88 | 0.21 | 0.04 | 0.47 | 0.70 | 0.03 | 0.56 | 0.60 | 0.01 | 0.05 | 1.06 | 0.32 |
| Control Delay | 74.2 | 48.4 | 0.0 | 41.0 | 65.9 | 0.0 | 33.4 | 21.0 | 0.0 | 12.1 | 71.4 | 0.5 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 74.2 | 48.4 | 0.0 | 41.0 | 65.9 | 0.0 | 33.4 | 21.0 | 0.0 | 12.1 | 71.4 | 0.5 |
| LOS | Е | D | Α | D | Е | Α | С | С | Α | В | Е | Α |
| Approach Delay | | 57.0 | | | 47.5 | | | 21.5 | | | 56.6 | |
| Approach LOS | | Е | | | D | | | С | | | Е | |
| Queue Length 50th (m) | 51.8 | 12.6 | 0.0 | 31.2 | 45.6 | 0.0 | 8.1 | 85.6 | 0.0 | 1.0 | ~275.5 | 0.0 |
| Queue Length 95th (m) | 69.7 | 23.1 | 0.0 | 45.0 | 64.7 | 0.0 | #33.9 | 156.0 | 0.0 | 4.1 | #343.0 | 0.0 |
| Internal Link Dist (m) | | 42.6 | | | 349.6 | | | 93.8 | | | 234.3 | |
| Turn Bay Length (m) | 66.0 | | 66.0 | | | 80.0 | 80.0 | | 90.0 | 80.0 | | 85.0 |
| Base Capacity (vph) | 272 | 389 | 1498 | 329 | 389 | 1493 | 153 | 1979 | 1498 | 230 | 1745 | 1517 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.88 | 0.14 | 0.04 | 0.47 | 0.47 | 0.03 | 0.56 | 0.60 | 0.01 | 0.05 | 1.06 | 0.32 |

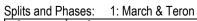
Cycle Length: 130

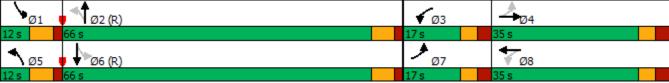
Actuated Cycle Length: 130
Offset: 121 (93%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green

Natural Cycle: 115

Control Type: Actuated-Coordinated

| M | aximum v/c Ratio: 1.06 | | | | | | | |
|----|---|------------------------|--|--|--|--|--|--|
| In | tersection Signal Delay: 45.5 | Intersection LOS: D | | | | | | |
| In | tersection Capacity Utilization 108.1% | ICU Level of Service G | | | | | | |
| Ar | nalysis Period (min) 15 | | | | | | | |
| De | escription: NOTE: March Road Treated as north-south | | | | | | | |
| ~ | Volume exceeds capacity, queue is theoretically infinite. | | | | | | | |
| | Queue shown is maximum after two cycles. | | | | | | | |
| # | # 95th percentile volume exceeds capacity, queue may be longer. | | | | | | | |
| | Queue shown is maximum after two cycles | | | | | | | |





| | • | → | \rightarrow | • | ← | • | 4 | † | <i>></i> | > | ļ | 4 |
|------------------------|-------|----------|---------------|-------|----------|-----|-------|----------|-------------|-------------|-------|-----|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | f) | | ¥ | f) | | * | f) | | J. | f) | |
| Traffic Volume (vph) | 65 | 6 | 131 | 22 | 11 | 16 | 194 | 209 | 30 | 31 | 475 | 125 |
| Future Volume (vph) | 65 | 6 | 131 | 22 | 11 | 16 | 194 | 209 | 30 | 31 | 475 | 125 |
| Satd. Flow (prot) | 1695 | 1496 | 0 | 1695 | 1586 | 0 | 1695 | 1742 | 0 | 1695 | 1707 | 0 |
| Flt Permitted | 0.740 | | | 0.669 | | | 0.181 | | | 0.610 | | |
| Satd. Flow (perm) | 1296 | 1496 | 0 | 1194 | 1586 | 0 | 323 | 1742 | 0 | 1080 | 1707 | 0 |
| Satd. Flow (RTOR) | | 131 | | | 16 | | | 12 | | | 15 | |
| Lane Group Flow (vph) | 65 | 137 | 0 | 22 | 27 | 0 | 194 | 239 | 0 | 31 | 600 | 0 |
| Turn Type | Perm | NA | | Perm | NA | | pm+pt | NA | | Perm | NA | |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Detector Phase | 4 | 4 | | 8 | 8 | | 5 | 2 | | 6 | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 10.0 | 10.0 | | 10.0 | 10.0 | | 5.0 | 10.0 | | 10.0 | 10.0 | |
| Minimum Split (s) | 22.8 | 22.8 | | 22.8 | 22.8 | | 11.0 | 71.2 | | 50.6 | 50.6 | |
| Total Split (s) | 35.8 | 35.8 | | 35.8 | 35.8 | | 20.6 | 71.2 | | 50.6 | 50.6 | |
| Total Split (%) | 33.5% | 33.5% | | 33.5% | 33.5% | | 19.3% | 66.5% | | 47.3% | 47.3% | |
| Yellow Time (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 4.0 | 3.3 | | 3.3 | 3.3 | |
| All-Red Time (s) | 2.8 | 2.8 | | 2.8 | 2.8 | | 2.0 | 2.3 | | 2.3 | 2.3 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | 5.8 | 5.8 | | 5.8 | 5.8 | | 6.0 | 5.6 | | 5.6 | 5.6 | |
| Lead/Lag | | | | | | | Lead | | | Lag | Lag | |
| Lead-Lag Optimize? | | | | | | | Yes | | | Yes | Yes | |
| Recall Mode | None | None | | None | None | | None | Min | | Min | Min | |
| Act Effct Green (s) | 11.7 | 11.7 | | 11.7 | 11.7 | | 48.8 | 49.2 | | 30.2 | 30.2 | |
| Actuated g/C Ratio | 0.16 | 0.16 | | 0.16 | 0.16 | | 0.67 | 0.68 | | 0.42 | 0.42 | |
| v/c Ratio | 0.31 | 0.39 | | 0.12 | 0.10 | | 0.42 | 0.20 | | 0.07 | 0.84 | |
| Control Delay | 35.3 | 10.9 | | 32.1 | 20.2 | | 7.3 | 4.5 | | 13.3 | 30.0 | |
| Queue Delay | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Delay | 35.3 | 10.9 | | 32.1 | 20.2 | | 7.3 | 4.5 | | 13.3 | 30.0 | |
| LOS | D | В | | С | С | | Α | Α | | В | С | |
| Approach Delay | | 18.8 | | | 25.5 | | | 5.7 | | | 29.2 | |
| Approach LOS | | В | | | С | | | Α | | | С | |
| Queue Length 50th (m) | 8.0 | 0.7 | | 2.6 | 1.3 | | 7.3 | 8.5 | | 2.4 | 68.3 | |
| Queue Length 95th (m) | 22.0 | 15.9 | | 10.0 | 8.7 | | 17.7 | 20.3 | | 7.7 | 122.9 | |
| Internal Link Dist (m) | | 594.0 | | | 268.4 | | | 124.5 | | | 518.6 | |
| Turn Bay Length (m) | 60.0 | | | 15.0 | | | 40.0 | | | 45.0 | | |
| Base Capacity (vph) | 554 | 714 | | 510 | 687 | | 502 | 1547 | | 692 | 1100 | |
| Starvation Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Reduced v/c Ratio | 0.12 | 0.19 | | 0.04 | 0.04 | | 0.39 | 0.15 | | 0.04 | 0.55 | |

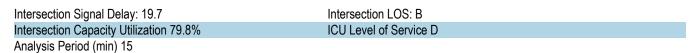
Cycle Length: 107

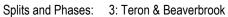
Actuated Cycle Length: 72.7

Natural Cycle: 95

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.84







| Intersection | | | | | | |
|------------------------|--------|-------|---------|----------|---------|-------|
| Int Delay, s/veh | 4.3 | | | | | |
| | | | | | 05= | 055 |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | | 7 | | ተተኩ | | - 7 |
| Traffic Vol, veh/h | 166 | 105 | 50 | 215 | 540 | 181 |
| Future Vol, veh/h | 166 | 105 | 50 | 215 | 540 | 181 |
| Conflicting Peds, #/hr | 7 | 7 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | Yield | - | Free | - | Yield |
| Storage Length | 50 | 0 | - | - | - | 0 |
| Veh in Median Storag | e, # 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 166 | 105 | 50 | 215 | 540 | 181 |
| | | | | | | |
| Maiay/Mina | Mina | | Mais =4 | | Mais =0 | |
| | Minor2 | | Major1 | | Major2 | |
| Conflicting Flow All | 733 | 547 | 540 | 0 | - | 0 |
| Stage 1 | 540 | - | - | - | - | - |
| Stage 2 | 193 | - | - | - | - | - |
| Critical Hdwy | 6.08 | 6.23 | 4.13 | - | - | - |
| Critical Hdwy Stg 1 | 5.43 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.03 | - | - | - | - | - |
| Follow-up Hdwy | 3.669 | 3.319 | 2.219 | - | - | - |
| Pot Cap-1 Maneuver | 404 | 536 | 1027 | - | - | - |
| Stage 1 | 565 | - | - | - | - | - |
| Stage 2 | 782 | - | _ | - | - | - |
| Platoon blocked, % | | | | - | - | - |
| Mov Cap-1 Maneuver | 382 | 533 | 1027 | _ | - | - |
| Mov Cap-2 Maneuver | | - | - | - | - | - |
| Stage 1 | 534 | _ | _ | _ | _ | - |
| Stage 2 | 782 | _ | _ | _ | _ | _ |
| J | . 02 | | | | | |
| | | | | | | |
| Approach | EB | | NB | | SB | |
| HCM Control Delay, s | 18.4 | | 1.7 | | 0 | |
| HCM LOS | С | | | | | |
| | | | | | | |
| Minor Long/Major Myr | mt | NDI | NDT | EDI n1 I | EDI no | CDT |
| Minor Lane/Major Mvr | IIL | NBL | INDI | EBLn1 I | | SBT |
| Capacity (veh/h) | | 1027 | - | 382 | 533 | - |
| HCM Lane V/C Ratio | , | 0.049 | | 0.435 | | - |
| HCM Control Delay (s |) | 8.7 | 0.1 | 21.5 | 13.4 | - |
| HCM Lane LOS | , | Α | Α | С | В | - |
| HCM 95th %tile Q(veh | 1) | 0.2 | - | 2.1 | 0.7 | - |

| Intersection | | | | | | |
|------------------------|--------|-------|-----------|-------|--------|------|
| Int Delay, s/veh | 0.3 | | | | | |
| | | WIDD | NDT | NDD | CDI | CDT |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Å | 40 | ^} | ^ | 4.4 | 4 |
| Traffic Vol, veh/h | 3 | 12 | 254 | 9 | 14 | 635 |
| Future Vol, veh/h | 3 | 12 | 254 | 9 | 14 | 635 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage | e, # 0 | - | 0 | - | - | 0 |
| Grade, % | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 3 | 12 | 254 | 9 | 14 | 635 |
| | | | | | | |
| | | | | | | |
| | Minor1 | | Major1 | | Major2 | |
| Conflicting Flow All | 922 | 259 | 0 | 0 | 263 | 0 |
| Stage 1 | 259 | - | - | - | - | - |
| Stage 2 | 663 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | _ | 2.218 | - |
| Pot Cap-1 Maneuver | 300 | 780 | - | - | 1301 | - |
| Stage 1 | 784 | - | _ | _ | - | _ |
| Stage 2 | 512 | - | _ | _ | - | _ |
| Platoon blocked, % | J12 | | _ | _ | | _ |
| Mov Cap-1 Maneuver | 295 | 780 | | | 1301 | |
| Mov Cap-1 Maneuver | 295 | 700 | | | 1301 | |
| | 784 | - | - | - | - | - |
| Stage 1 | | - | - | - | - | - |
| Stage 2 | 503 | - | _ | - | - | - |
| | | | | | | |
| Approach | WB | | NB | | SB | |
| HCM Control Delay, s | 11.3 | | 0 | | 0.2 | |
| HCM LOS | В | | • | | 0.2 | |
| 110M 200 | | | | | | |
| | | | | | | |
| Minor Lane/Major Mvn | nt | NBT | NBRV | VBLn1 | SBL | SBT |
| Capacity (veh/h) | | - | - | 587 | 1301 | _ |
| HCM Lane V/C Ratio | | - | - | 0.026 | | - |
| HCM Control Delay (s |) | - | - | | 7.8 | 0 |
| HCM Lane LOS | | - | _ | В | A | A |
| HCM 95th %tile Q(veh |) | - | _ | • • | 0 | - |
| TION JOHN JOHN Q(VEI) | 7 | | | 0.1 | U | |

| | ۶ | → | • | • | ← | • | 4 | † | ~ | / | ţ | |
|------------------------|--------|----------|-------|-------|----------|-------|-------|----------|-------|----------|----------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | ^ | 7 | 7 | ^ | 7 | 7 | ^ | 7 | 7 | ^ | 7 |
| Traffic Volume (vph) | 498 | 316 | 51 | 23 | 46 | 34 | 47 | 1991 | 199 | 49 | 905 | 188 |
| Future Volume (vph) | 498 | 316 | 51 | 23 | 46 | 34 | 47 | 1991 | 199 | 49 | 905 | 188 |
| Satd. Flow (prot) | 1695 | 1784 | 1517 | 1695 | 1784 | 1517 | 1695 | 3390 | 1517 | 1695 | 3390 | 1517 |
| Flt Permitted | 0.585 | | | 0.308 | | | 0.244 | | | 0.058 | | |
| Satd. Flow (perm) | 1040 | 1784 | 1498 | 549 | 1784 | 1497 | 435 | 3390 | 1498 | 103 | 3390 | 1517 |
| Satd. Flow (RTOR) | | | 188 | | | 188 | | | 188 | | | 188 |
| Lane Group Flow (vph) | 498 | 316 | 51 | 23 | 46 | 34 | 47 | 1991 | 199 | 49 | 905 | 188 |
| Turn Type | pm+pt | NA | Free | pm+pt | NA | Free | pm+pt | NA | Free | pm+pt | NA | Free |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | Free | 8 | | Free | 2 | | Free | 6 | | Free |
| Detector Phase | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 10.0 | | 5.0 | 10.0 | | 5.0 | 10.0 | | 5.0 | 10.0 | |
| Minimum Split (s) | 11.1 | 34.6 | | 11.1 | 34.6 | | 11.4 | 25.3 | | 11.4 | 25.3 | |
| Total Split (s) | 12.0 | 38.0 | | 12.0 | 38.0 | | 12.0 | 68.0 | | 12.0 | 68.0 | |
| Total Split (%) | 9.2% | 29.2% | | 9.2% | 29.2% | | 9.2% | 52.3% | | 9.2% | 52.3% | |
| Yellow Time (s) | 3.3 | 3.3 | | 3.3 | 3.3 | | 4.6 | 4.6 | | 4.6 | 4.6 | |
| All-Red Time (s) | 2.8 | 3.3 | | 2.8 | 3.3 | | 1.8 | 1.7 | | 1.8 | 1.7 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | 6.1 | 6.6 | | 6.1 | 6.6 | | 6.4 | 6.3 | | 6.4 | 6.3 | |
| Lead/Lag | Lead | Lag | | Lead | Lag | | Lead | Lag | | Lead | Lag | |
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | | Yes | Yes | | Yes | Yes | |
| Recall Mode | None | None | | None | None | | None | C-Min | | None | C-Min | |
| Act Effct Green (s) | 31.1 | 27.1 | 130.0 | 27.0 | 22.8 | 130.0 | 77.6 | 72.8 | 130.0 | 77.6 | 72.8 | 130.0 |
| Actuated g/C Ratio | 0.24 | 0.21 | 1.00 | 0.21 | 0.18 | 1.00 | 0.60 | 0.56 | 1.00 | 0.60 | 0.56 | 1.00 |
| v/c Ratio | 1.70 | 0.85 | 0.03 | 0.14 | 0.15 | 0.02 | 0.15 | 1.05 | 0.13 | 0.37 | 0.48 | 0.12 |
| Control Delay | 359.9 | 70.3 | 0.0 | 32.6 | 42.2 | 0.0 | 12.8 | 64.6 | 0.2 | 20.5 | 20.7 | 0.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 359.9 | 70.3 | 0.0 | 32.6 | 42.2 | 0.0 | 12.8 | 64.6 | 0.2 | 20.5 | 20.7 | 0.2 |
| LOS | F | Е | Α | С | D | Α | В | Е | Α | С | С | Α |
| Approach Delay | | 232.9 | | | 26.1 | | | 57.8 | | | 17.3 | |
| Approach LOS | | F | | | С | | | Е | | | В | |
| Queue Length 50th (m) | ~183.5 | 77.7 | 0.0 | 4.1 | 9.5 | 0.0 | 4.8 | ~325.7 | 0.0 | 5.0 | 83.0 | 0.0 |
| Queue Length 95th (m) | #242.7 | 108.5 | 0.0 | 10.3 | 19.6 | 0.0 | 10.7 | #373.8 | 0.0 | 12.0 | 105.2 | 0.0 |
| Internal Link Dist (m) | | 42.6 | | | 349.6 | | | 93.8 | | | 234.3 | |
| Turn Bay Length (m) | 66.0 | | 66.0 | | | 80.0 | 80.0 | | 90.0 | 80.0 | | 85.0 |
| Base Capacity (vph) | 293 | 430 | 1498 | 166 | 430 | 1497 | 317 | 1898 | 1498 | 134 | 1898 | 1517 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 1.70 | 0.73 | 0.03 | 0.14 | 0.11 | 0.02 | 0.15 | 1.05 | 0.13 | 0.37 | 0.48 | 0.12 |
| | | | | | | | | | | | | |

Cycle Length: 130

Actuated Cycle Length: 130
Offset: 36 (28%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green

Natural Cycle: 115

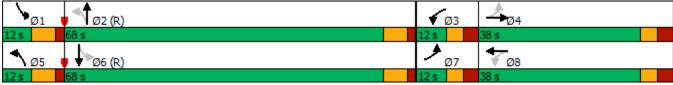
Control Type: Actuated-Coordinated

Maximum v/c Ratio: 1.70
Intersection Signal Delay: 81.2
Intersection Capacity Utilization 104.6%
ICU Level of Service G
Analysis Period (min) 15
Description: NOTE: March Road treated as north-south

Volume exceeds capacity, queue is theoretically infinite.
Queue shown is maximum after two cycles.

95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

Splits and Phases: 1: March & Teron



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|------------------------|-------|----------|-----|-------|----------|-----|-------|-------|----------|----------|-------|-----|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | 1> | | 7 | ₽ | | 7 | 4î | | 7 | 1> | |
| Traffic Volume (vph) | 146 | 4 | 180 | 22 | 2 | 34 | 96 | 337 | 4 | 15 | 204 | 39 |
| Future Volume (vph) | 146 | 4 | 180 | 22 | 2 | 34 | 96 | 337 | 4 | 15 | 204 | 39 |
| Satd. Flow (prot) | 1695 | 1522 | 0 | 1695 | 1452 | 0 | 1695 | 1781 | 0 | 1695 | 1734 | 0 |
| Flt Permitted | 0.734 | | | 0.641 | | | 0.608 | | | 0.556 | | |
| Satd. Flow (perm) | 1268 | 1522 | 0 | 1144 | 1452 | 0 | 1083 | 1781 | 0 | 992 | 1734 | 0 |
| Satd. Flow (RTOR) | | 180 | | | 34 | | | 1 | | | 19 | |
| Lane Group Flow (vph) | 146 | 184 | 0 | 22 | 36 | 0 | 96 | 341 | 0 | 15 | 243 | 0 |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Detector Phase | 4 | 4 | | 8 | 8 | | 2 | 2 | | 6 | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 10.0 | 10.0 | | 10.0 | 10.0 | | 10.0 | 10.0 | | 10.0 | 10.0 | |
| Minimum Split (s) | 22.8 | 22.8 | | 22.8 | 22.8 | | 65.6 | 65.6 | | 65.6 | 65.6 | |
| Total Split (s) | 29.8 | 29.8 | | 29.8 | 29.8 | | 65.6 | 65.6 | | 65.6 | 65.6 | |
| Total Split (%) | 31.2% | 31.2% | | 31.2% | 31.2% | | 68.8% | 68.8% | | 68.8% | 68.8% | |
| Yellow Time (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.3 | 3.3 | | 3.3 | 3.3 | |
| All-Red Time (s) | 2.8 | 2.8 | | 2.8 | 2.8 | | 2.3 | 2.3 | | 2.3 | 2.3 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | 5.8 | 5.8 | | 5.8 | 5.8 | | 5.6 | 5.6 | | 5.6 | 5.6 | |
| Lead/Lag | | | | | | | | | | | | |
| Lead-Lag Optimize? | | | | | | | | | | | | |
| Recall Mode | None | None | | None | None | | Min | Min | | Min | Min | |
| Act Effct Green (s) | 11.5 | 11.5 | | 11.5 | 11.5 | | 14.1 | 14.1 | | 14.1 | 14.1 | |
| Actuated g/C Ratio | 0.31 | 0.31 | | 0.31 | 0.31 | | 0.38 | 0.38 | | 0.38 | 0.38 | |
| v/c Ratio | 0.37 | 0.31 | | 0.06 | 0.08 | | 0.23 | 0.51 | | 0.04 | 0.36 | |
| Control Delay | 14.3 | 4.3 | | 11.0 | 5.6 | | 9.8 | 12.1 | | 7.9 | 9.6 | |
| Queue Delay | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Delay | 14.3 | 4.3 | | 11.0 | 5.6 | | 9.8 | 12.1 | | 7.9 | 9.6 | |
| LOS | В | A | | В | A | | Α | В | | Α | A | |
| Approach Delay | | 8.7 | | | 7.6 | | | 11.6 | | | 9.5 | |
| Approach LOS | | Α | | | Α | | 2.1 | В | | | Α | |
| Queue Length 50th (m) | 6.2 | 0.2 | | 0.8 | 0.1 | | 3.4 | 13.7 | | 0.5 | 8.4 | |
| Queue Length 95th (m) | 20.9 | 9.9 | | 4.8 | 4.4 | | 12.4 | 36.5 | | 3.1 | 24.3 | |
| Internal Link Dist (m) | | 594.0 | | 4-0 | 268.4 | | 40.0 | 124.5 | | 4- 0 | 518.6 | |
| Turn Bay Length (m) | 60.0 | 400= | | 15.0 | 0=4 | | 40.0 | 1=0.1 | | 45.0 | 1=0.1 | |
| Base Capacity (vph) | 838 | 1067 | | 756 | 971 | | 1083 | 1781 | | 992 | 1734 | |
| Starvation Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Reduced v/c Ratio | 0.17 | 0.17 | | 0.03 | 0.04 | | 0.09 | 0.19 | | 0.02 | 0.14 | |
| Internation Comment | | | | | | | | | | | | |

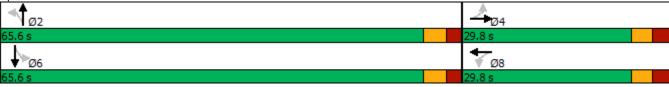
Cycle Length: 95.4

Actuated Cycle Length: 37.3 Natural Cycle: 90

Control Type: Semi Act-Uncoord Maximum v/c Ratio: 0.51

| Intersection Signal Delay: 10.0 | Intersection LOS: B |
|---|------------------------|
| Intersection Capacity Utilization 60.8% | ICU Level of Service B |
| Analysis Period (min) 15 | |





| Intersection | | | | | | |
|------------------------|-----------|-------|--------|---------|-------------------|-------|
| Int Delay, s/veh | 2.6 | | | | | |
| | | EDD | NDI | NDT | CDT | CDD |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ነ | 7 | 45 | 414 | 475 | 7 |
| Traffic Vol, veh/h | 129 | 66 | 45 | 598 | 175 | 97 |
| Future Vol, veh/h | 129 | 66 | 45 | 598 | 175 | 97 |
| Conflicting Peds, #/hr | 4 | 4 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | Yield | - | Free | - | Yield |
| Storage Length | 50 | 0 | - | - | - | 0 |
| Veh in Median Storage | e, # 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 129 | 66 | 45 | 598 | 175 | 97 |
| | | | | | | |
| | | | | | | |
| | Minor2 | | Major1 | | Major2 | |
| Conflicting Flow All | 508 | 179 | 175 | 0 | - | 0 |
| Stage 1 | 175 | - | - | - | - | - |
| Stage 2 | 333 | - | - | - | - | - |
| Critical Hdwy | 6.08 | 6.23 | 4.13 | - | - | - |
| Critical Hdwy Stg 1 | 5.43 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.03 | - | - | - | - | - |
| Follow-up Hdwy | | 3.319 | 2.219 | _ | _ | - |
| Pot Cap-1 Maneuver | 533 | 863 | 1400 | _ | _ | _ |
| Stage 1 | 823 | - | - 100 | _ | _ | - |
| Stage 2 | 662 | _ | _ | _ | _ | _ |
| Platoon blocked, % | 002 | | _ | | _ | |
| Mov Cap-1 Maneuver | 507 | 860 | 1400 | - | <u>-</u> | - |
| | | | 1400 | | - | - |
| Mov Cap-2 Maneuver | 507 | - | - | - | - | - |
| Stage 1 | 783 | - | - | - | - | - |
| Stage 2 | 662 | - | - | - | - | - |
| | | | | | | |
| Approach | EB | | NB | | SB | |
| HCM Control Delay, s | 12.8 | | 0.6 | | 0 | |
| HCM LOS | 12.0 B | | 0.0 | | U | |
| TIOWI LOO | U | | | | | |
| | | | | | | |
| Minor Lane/Major Mvn | nt | NBL | NBT | EBLn1 I | EBL _{n2} | SBT |
| Capacity (veh/h) | | 1400 | - | 507 | 860 | - |
| HCM Lane V/C Ratio | | 0.032 | _ | 0.254 | | _ |
| HCM Control Delay (s |) | 7.7 | 0.1 | 14.5 | 9.5 | - |
| HCM Lane LOS | | Α | Α | В | 3.5 A | _ |
| HCM 95th %tile Q(veh | 1) | 0.1 | - | 1 | 0.2 | _ |
| HOW SOUT WHILE CLANE | ı) | 0.1 | | 1 | U.Z | _ |

| Intersection | | | | | | |
|------------------------|------------|-------|----------|-------|----------|------|
| Int Delay, s/veh | 0.4 | | | | | |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Y | WDIX | 1 | HUIT | ODL | 4 |
| Traffic Vol, veh/h | T 5 | 18 | 635 | 3 | 5 | 243 |
| Future Vol, veh/h | 5 | 18 | 635 | 3 | 5 | 243 |
| | 0 | 0 | | 0 | 0 | |
| Conflicting Peds, #/hr | | | 0 | | | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage | | - | 0 | - | - | 0 |
| Grade, % | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 5 | 18 | 635 | 3 | 5 | 243 |
| | | | | | | |
| Major/Minor Minor1 | | | 1-:1 | | Maia = 0 | |
| | Minor1 | | //ajor1 | | Major2 | |
| Conflicting Flow All | 890 | 637 | 0 | 0 | 638 | 0 |
| Stage 1 | 637 | - | - | - | - | - |
| Stage 2 | 253 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.218 | - |
| Pot Cap-1 Maneuver | 313 | 477 | - | - | 946 | - |
| Stage 1 | 527 | - | _ | - | - | - |
| Stage 2 | 789 | - | _ | _ | - | - |
| Platoon blocked, % | | | _ | _ | | _ |
| Mov Cap-1 Maneuver | 311 | 477 | _ | _ | 946 | _ |
| Mov Cap-1 Maneuver | 311 | 411 | _ | _ | 340 | _ |
| • | 527 | | - | - | - | - |
| Stage 1 | | - | | - | | |
| Stage 2 | 784 | - | - | - | - | - |
| | | | | | | |
| Approach | WB | | NB | | SB | |
| HCM Control Delay, s | 13.9 | | 0 | | 0.2 | |
| HCM LOS | В | | | | 0.2 | |
| 1 JOINI LOO | U | | | | | |
| | | | | | | |
| Minor Lane/Major Mvn | nt | NBT | NBRV | VBLn1 | SBL | SBT |
| Capacity (veh/h) | | - | - | 427 | 946 | - |
| HCM Lane V/C Ratio | | _ | _ | 0.054 | | - |
| HCM Control Delay (s) | | _ | _ | 13.9 | 8.8 | 0 |
| HCM Lane LOS | | _ | _ | В | A | A |
| HCM 95th %tile Q(veh |) | _ | _ | 0.2 | 0 | - |
| HOW SOUL WILLE CALACT |) | _ | _ | 0.2 | U | _ |

| | ٠ | → | • | • | ← | • | • | † | ~ | > | ļ | 4 |
|------------------------|-------|----------|-------|-------|----------|-------|-------|----------|-------|-------------|------------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | † | 7 | 7 | † | 7 | 7 | ^ | 7 | 7 | † † | 7 |
| Traffic Volume (vph) | 240 | 60 | 64 | 153 | 200 | 50 | 85 | 1281 | 20 | 11 | 2019 | 479 |
| Future Volume (vph) | 240 | 60 | 64 | 153 | 200 | 50 | 85 | 1281 | 20 | 11 | 2019 | 479 |
| Satd. Flow (prot) | 1695 | 1784 | 1517 | 1695 | 1784 | 1517 | 1695 | 3390 | 1517 | 1695 | 3390 | 1517 |
| Flt Permitted | 0.521 | | | 0.587 | | | 0.057 | | | 0.134 | | |
| Satd. Flow (perm) | 921 | 1784 | 1498 | 1046 | 1784 | 1493 | 102 | 3390 | 1498 | 239 | 3390 | 1517 |
| Satd. Flow (RTOR) | | | 188 | | | 188 | | | 188 | | | 188 |
| Lane Group Flow (vph) | 240 | 60 | 64 | 153 | 200 | 50 | 85 | 1281 | 20 | 11 | 2019 | 479 |
| Turn Type | pm+pt | NA | Free | pm+pt | NA | Free | pm+pt | NA | Free | pm+pt | NA | Free |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | Free | 8 | | Free | 2 | | Free | 6 | | Free |
| Detector Phase | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 10.0 | | 5.0 | 10.0 | | 5.0 | 10.0 | | 5.0 | 10.0 | |
| Minimum Split (s) | 11.1 | 34.6 | | 11.1 | 34.6 | | 11.4 | 25.3 | | 11.4 | 25.3 | |
| Total Split (s) | 17.0 | 35.0 | | 17.0 | 35.0 | | 12.0 | 66.0 | | 12.0 | 66.0 | |
| Total Split (%) | 13.1% | 26.9% | | 13.1% | 26.9% | | 9.2% | 50.8% | | 9.2% | 50.8% | |
| Yellow Time (s) | 3.3 | 3.3 | | 3.3 | 3.3 | | 4.6 | 4.6 | | 4.6 | 4.6 | |
| All-Red Time (s) | 2.8 | 3.3 | | 2.8 | 3.3 | | 1.8 | 1.7 | | 1.8 | 1.7 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | 6.1 | 6.6 | | 6.1 | 6.6 | | 6.4 | 6.3 | | 6.4 | 6.3 | |
| Lead/Lag | Lead | Lag | | Lead | Lag | | Lead | Lag | | Lead | Lag | |
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | | Yes | Yes | | Yes | Yes | |
| Recall Mode | None | None | | None | None | | None | C-Min | | None | C-Min | |
| Act Effct Green (s) | 28.8 | 19.5 | 130.0 | 32.7 | 20.1 | 130.0 | 78.0 | 75.0 | 130.0 | 71.7 | 66.0 | 130.0 |
| Actuated g/C Ratio | 0.22 | 0.15 | 1.00 | 0.25 | 0.15 | 1.00 | 0.60 | 0.58 | 1.00 | 0.55 | 0.51 | 1.00 |
| v/c Ratio | 0.90 | 0.22 | 0.04 | 0.46 | 0.73 | 0.03 | 0.55 | 0.65 | 0.01 | 0.06 | 1.17 | 0.32 |
| Control Delay | 76.1 | 48.1 | 0.0 | 40.1 | 66.9 | 0.0 | 33.0 | 22.9 | 0.0 | 12.5 | 115.1 | 0.5 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 76.1 | 48.1 | 0.0 | 40.1 | 66.9 | 0.0 | 33.0 | 22.9 | 0.0 | 12.5 | 115.1 | 0.5 |
| LOS | E | D | Α | D | E | Α | С | С | Α | В | F | Α |
| Approach Delay | | 58.1 | | | 48.4 | | | 23.2 | | | 92.8 | |
| Approach LOS | | E | | | D | | | С | | | F | |
| Queue Length 50th (m) | 51.2 | 13.7 | 0.0 | 30.8 | 49.5 | 0.0 | 8.3 | 100.0 | 0.0 | 1.0 | ~326.6 | 0.0 |
| Queue Length 95th (m) | 69.7 | 24.7 | 0.0 | 45.0 | 70.2 | 0.0 | #33.4 | 177.1 | 0.0 | 4.1 | #388.9 | 0.0 |
| Internal Link Dist (m) | | 42.6 | | | 349.6 | | | 93.8 | | | 234.3 | |
| Turn Bay Length (m) | 66.0 | | 66.0 | | | 80.0 | 80.0 | | 90.0 | 80.0 | | 85.0 |
| Base Capacity (vph) | 268 | 389 | 1498 | 336 | 389 | 1493 | 154 | 1956 | 1498 | 196 | 1721 | 1517 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.90 | 0.15 | 0.04 | 0.46 | 0.51 | 0.03 | 0.55 | 0.65 | 0.01 | 0.06 | 1.17 | 0.32 |

Cycle Length: 130

Actuated Cycle Length: 130
Offset: 121 (93%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green

Natural Cycle: 115

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 1.17
Intersection Signal Delay: 65.6 Intersection LOS: E
Intersection Capacity Utilization 113.7% ICU Level of Service H
Analysis Period (min) 15
Description: NOTE: March Road Treated as north-south

Volume exceeds capacity, queue is theoretically infinite.

Queue shown is maximum after two cycles.

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.



| | • | → | \rightarrow | • | ← | • | • | † | / | > | ļ | 4 |
|------------------------|-------|----------|---------------|-------|----------|-----|-------|----------|----------|-------------|-------|-----|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | î, | | ¥ | f) | | ¥ | f) | | ¥ | f) | |
| Traffic Volume (vph) | 65 | 6 | 131 | 22 | 11 | 16 | 194 | 225 | 30 | 31 | 515 | 125 |
| Future Volume (vph) | 65 | 6 | 131 | 22 | 11 | 16 | 194 | 225 | 30 | 31 | 515 | 125 |
| Satd. Flow (prot) | 1695 | 1496 | 0 | 1695 | 1586 | 0 | 1695 | 1745 | 0 | 1695 | 1712 | 0 |
| Flt Permitted | 0.740 | | | 0.669 | | | 0.171 | | | 0.601 | | |
| Satd. Flow (perm) | 1296 | 1496 | 0 | 1194 | 1586 | 0 | 305 | 1745 | 0 | 1064 | 1712 | 0 |
| Satd. Flow (RTOR) | | 131 | | | 16 | | | 12 | | | 14 | |
| Lane Group Flow (vph) | 65 | 137 | 0 | 22 | 27 | 0 | 194 | 255 | 0 | 31 | 640 | 0 |
| Turn Type | Perm | NA | | Perm | NA | | pm+pt | NA | | Perm | NA | |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Detector Phase | 4 | 4 | | 8 | 8 | | 5 | 2 | | 6 | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 10.0 | 10.0 | | 10.0 | 10.0 | | 5.0 | 10.0 | | 10.0 | 10.0 | |
| Minimum Split (s) | 22.8 | 22.8 | | 22.8 | 22.8 | | 11.0 | 71.2 | | 50.6 | 50.6 | |
| Total Split (s) | 35.8 | 35.8 | | 35.8 | 35.8 | | 20.6 | 71.2 | | 50.6 | 50.6 | |
| Total Split (%) | 33.5% | 33.5% | | 33.5% | 33.5% | | 19.3% | 66.5% | | 47.3% | 47.3% | |
| Yellow Time (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 4.0 | 3.3 | | 3.3 | 3.3 | |
| All-Red Time (s) | 2.8 | 2.8 | | 2.8 | 2.8 | | 2.0 | 2.3 | | 2.3 | 2.3 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | 5.8 | 5.8 | | 5.8 | 5.8 | | 6.0 | 5.6 | | 5.6 | 5.6 | |
| Lead/Lag | | | | | | | Lead | | | Lag | Lag | |
| Lead-Lag Optimize? | | | | | | | Yes | | | Yes | Yes | |
| Recall Mode | None | None | | None | None | | None | Min | | Min | Min | |
| Act Effct Green (s) | 11.6 | 11.6 | | 11.6 | 11.6 | | 52.0 | 52.4 | | 33.3 | 33.3 | |
| Actuated g/C Ratio | 0.15 | 0.15 | | 0.15 | 0.15 | | 0.69 | 0.69 | | 0.44 | 0.44 | |
| v/c Ratio | 0.33 | 0.40 | | 0.12 | 0.11 | | 0.44 | 0.21 | | 0.07 | 0.84 | |
| Control Delay | 37.1 | 11.2 | | 33.4 | 20.9 | | 7.3 | 4.4 | | 12.9 | 30.1 | |
| Queue Delay | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Delay | 37.1 | 11.2 | | 33.4 | 20.9 | | 7.3 | 4.4 | | 12.9 | 30.1 | |
| LOS | D | В | | С | С | | Α | Α | | В | С | |
| Approach Delay | | 19.5 | | | 26.5 | | | 5.7 | | | 29.3 | |
| Approach LOS | | В | | | С | | | Α | | | С | |
| Queue Length 50th (m) | 8.7 | 0.8 | | 2.9 | 1.4 | | 7.3 | 9.2 | | 2.4 | 75.9 | |
| Queue Length 95th (m) | 22.0 | 15.9 | | 10.0 | 8.7 | | 17.7 | 21.8 | | 7.8 | 136.3 | |
| Internal Link Dist (m) | | 594.0 | | | 268.4 | | | 124.5 | | | 518.6 | |
| Turn Bay Length (m) | 60.0 | | | 15.0 | | | 40.0 | | | 45.0 | | |
| Base Capacity (vph) | 528 | 687 | | 486 | 656 | | 484 | 1505 | | 650 | 1052 | |
| Starvation Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Reduced v/c Ratio | 0.12 | 0.20 | | 0.05 | 0.04 | | 0.40 | 0.17 | | 0.05 | 0.61 | |

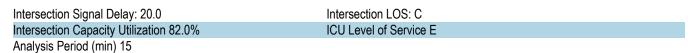
Cycle Length: 107

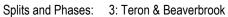
Actuated Cycle Length: 75.8

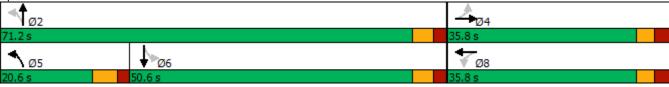
Natural Cycle: 95

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.84







| Intersection | | | | | | | |
|------------------------|--------|-------|--------|---------|----------|-------|--|
| Int Delay, s/veh | 4.4 | | | | | | |
| | | EDD | NDI | NDT | CDT | CDD | |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR | |
| Lane Configurations | 166 | 105 | | 414 | † | 101 | |
| Traffic Vol, veh/h | 166 | 105 | 50 | 234 | 591 | 181 | |
| Future Vol, veh/h | 166 | 105 | 50 | 234 | 591 | 181 | |
| Conflicting Peds, #/hr | 7 | 7 | _ 0 | _ 0 | 0 | _ 0 | |
| Sign Control | Stop | Stop | Free | Free | Free | Free | |
| RT Channelized | - | Yield | - | Free | - | Yield | |
| Storage Length | 50 | 0 | - | - | - | 0 | |
| Veh in Median Storage | | - | - | 0 | 0 | - | |
| Grade, % | 0 | - | - | 0 | 0 | - | |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | |
| Mvmt Flow | 166 | 105 | 50 | 234 | 591 | 181 | |
| | | | | | | | |
| NA - ' /NA' | N 4" O | | M - 1 | | | | |
| | Minor2 | | Major1 | | Major2 | _ | |
| Conflicting Flow All | 792 | 598 | 591 | 0 | - | 0 | |
| Stage 1 | 591 | - | - | - | - | - | |
| Stage 2 | 201 | - | - | - | - | - | |
| Critical Hdwy | 6.08 | 6.23 | 4.13 | - | - | - | |
| Critical Hdwy Stg 1 | 5.43 | - | - | - | - | - | |
| Critical Hdwy Stg 2 | 6.03 | - | - | - | - | - | |
| Follow-up Hdwy | 3.669 | 3.319 | 2.219 | - | - | - | |
| Pot Cap-1 Maneuver | 375 | 501 | 983 | - | - | - | |
| Stage 1 | 536 | - | - | - | - | - | |
| Stage 2 | 775 | _ | - | - | - | - | |
| Platoon blocked, % | | | | _ | _ | _ | |
| Mov Cap-1 Maneuver | 353 | 498 | 983 | _ | _ | _ | |
| Mov Cap-1 Maneuver | | - | - | _ | _ | _ | |
| Stage 1 | 505 | | | | | | |
| Stage 2 | 775 | | | | | | |
| Slaye 2 | 113 | - | - | - | <u>-</u> | - | |
| | | | | | | | |
| Approach | EB | | NB | | SB | | |
| HCM Control Delay, s | 20.1 | | 1.6 | | 0 | | |
| HCM LOS | C | | | | | | |
| | | | | | | | |
| | | | | | | | |
| Minor Lane/Major Mvr | nt | NBL | NBT | EBLn1 I | | SBT | |
| Capacity (veh/h) | | 983 | - | | 498 | - | |
| HCM Lane V/C Ratio | | 0.051 | - | 0.47 | 0.211 | - | |
| HCM Control Delay (s |) | 8.9 | 0.1 | 23.9 | 14.2 | - | |
| HCM Lane LOS | | Α | Α | С | В | - | |
| HCM 95th %tile Q(veh | 1) | 0.2 | - | 2.4 | 0.8 | - | |
| | 7 | 0.2 | | | 3.0 | | |

| Intersection | | | | | | |
|------------------------|--------|-------|---------|-------|--------|------|
| Int Delay, s/veh | 0.3 | | | | | |
| | | WED | NET | NDD | ODI | ODT |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | ¥ | | f) | | | र्स |
| Traffic Vol, veh/h | 3 | 12 | 277 | 9 | 14 | 699 |
| Future Vol, veh/h | 3 | 12 | 277 | 9 | 14 | 699 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | _ | - | - | - | - |
| Veh in Median Storage | e, # 0 | - | 0 | - | - | 0 |
| Grade, % | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 3 | 12 | 277 | 9 | 14 | 699 |
| WWW.CT IOW | Ū | 12 | | U | | 000 |
| | | | | | | |
| | Minor1 | | //ajor1 | | Major2 | |
| Conflicting Flow All | 1009 | 282 | 0 | 0 | 286 | 0 |
| Stage 1 | 282 | - | - | - | - | - |
| Stage 2 | 727 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - |
| Critical Hdwy Stg 1 | 5.42 | _ | - | _ | _ | - |
| Critical Hdwy Stg 2 | 5.42 | _ | _ | _ | - | _ |
| Follow-up Hdwy | 3.518 | 3.318 | - | _ | 2.218 | _ |
| Pot Cap-1 Maneuver | 266 | 757 | _ | _ | 1276 | _ |
| Stage 1 | 766 | - | _ | _ | - | _ |
| Stage 2 | 478 | _ | _ | _ | _ | _ |
| Platoon blocked, % | 470 | | _ | _ | | _ |
| Mov Cap-1 Maneuver | 261 | 757 | _ | _ | 1276 | |
| | 261 | | _ | _ | | - |
| Mov Cap-2 Maneuver | | - | - | _ | - | - |
| Stage 1 | 766 | - | - | - | - | - |
| Stage 2 | 469 | - | - | - | - | - |
| | | | | | | |
| Approach | WB | | NB | | SB | |
| HCM Control Delay, s | 11.7 | | 0 | | 0.2 | |
| HCM LOS | В | | · · | | 0.2 | |
| TIOM LOO | | | | | | |
| | | | | | | |
| Minor Lane/Major Mvr | nt | NBT | NBRV | VBLn1 | SBL | SBT |
| Capacity (veh/h) | | - | - | 549 | 1276 | - |
| HCM Lane V/C Ratio | | - | - | 0.027 | | - |
| HCM Control Delay (s |) | - | _ | | 7.9 | 0 |
| HCM Lane LOS | | _ | _ | В | A | A |
| HCM 95th %tile Q(veh | 1) | _ | _ | • • | 0 | - |
| TOW JOHN JOHN Q(VEI | '/ | | | 0.1 | U | |



SYNCHRO ANALYSIS: TOD NOT MET CONDITIONS

| | ٠ | → | • | • | ← | • | • | † | <i>></i> | > | ļ | 4 |
|------------------------|--------|----------|-------|-------|----------|-------|-------|----------|-------------|-------------|-------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | † | 7 | Ţ | ^ | 7 | 7 | 44 | 7 | 7 | 44 | 7 |
| Traffic Volume (vph) | 503 | 316 | 60 | 23 | 46 | 34 | 48 | 1991 | 199 | 49 | 905 | 189 |
| Future Volume (vph) | 503 | 316 | 60 | 23 | 46 | 34 | 48 | 1991 | 199 | 49 | 905 | 189 |
| Satd. Flow (prot) | 1695 | 1784 | 1517 | 1695 | 1784 | 1517 | 1695 | 3390 | 1517 | 1695 | 3390 | 1517 |
| Flt Permitted | 0.585 | | | 0.308 | | | 0.244 | | | 0.058 | | |
| Satd. Flow (perm) | 1040 | 1784 | 1498 | 549 | 1784 | 1497 | 435 | 3390 | 1498 | 103 | 3390 | 1517 |
| Satd. Flow (RTOR) | | | 188 | | | 188 | | | 188 | | | 188 |
| Lane Group Flow (vph) | 503 | 316 | 60 | 23 | 46 | 34 | 48 | 1991 | 199 | 49 | 905 | 189 |
| Turn Type | pm+pt | NA | Free | pm+pt | NA | Free | pm+pt | NA | Free | pm+pt | NA | Free |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | Free | 8 | | Free | 2 | | Free | 6 | | Free |
| Detector Phase | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 10.0 | | 5.0 | 10.0 | | 5.0 | 10.0 | | 5.0 | 10.0 | |
| Minimum Split (s) | 11.1 | 34.6 | | 11.1 | 34.6 | | 11.4 | 25.3 | | 11.4 | 25.3 | |
| Total Split (s) | 12.0 | 38.0 | | 12.0 | 38.0 | | 12.0 | 68.0 | | 12.0 | 68.0 | |
| Total Split (%) | 9.2% | 29.2% | | 9.2% | 29.2% | | 9.2% | 52.3% | | 9.2% | 52.3% | |
| Yellow Time (s) | 3.3 | 3.3 | | 3.3 | 3.3 | | 4.6 | 4.6 | | 4.6 | 4.6 | |
| All-Red Time (s) | 2.8 | 3.3 | | 2.8 | 3.3 | | 1.8 | 1.7 | | 1.8 | 1.7 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | 6.1 | 6.6 | | 6.1 | 6.6 | | 6.4 | 6.3 | | 6.4 | 6.3 | |
| Lead/Lag | Lead | Lag | | Lead | Lag | | Lead | Lag | | Lead | Lag | |
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | | Yes | Yes | | Yes | Yes | |
| Recall Mode | None | None | | None | None | | None | C-Min | | None | C-Min | |
| Act Effct Green (s) | 31.1 | 27.1 | 130.0 | 27.0 | 22.8 | 130.0 | 77.6 | 72.8 | 130.0 | 77.6 | 72.8 | 130.0 |
| Actuated g/C Ratio | 0.24 | 0.21 | 1.00 | 0.21 | 0.18 | 1.00 | 0.60 | 0.56 | 1.00 | 0.60 | 0.56 | 1.00 |
| v/c Ratio | 1.72 | 0.85 | 0.04 | 0.14 | 0.15 | 0.02 | 0.15 | 1.05 | 0.13 | 0.37 | 0.48 | 0.12 |
| Control Delay | 367.1 | 70.3 | 0.1 | 32.6 | 42.2 | 0.0 | 12.8 | 64.6 | 0.2 | 20.5 | 20.7 | 0.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 367.1 | 70.3 | 0.1 | 32.6 | 42.2 | 0.0 | 12.8 | 64.6 | 0.2 | 20.5 | 20.7 | 0.2 |
| LOS | F | E | Α | С | D | Α | В | Е | Α | С | С | Α |
| Approach Delay | | 235.3 | | | 26.1 | | | 57.8 | | | 17.3 | |
| Approach LOS | | F | | | С | | | Е | | | В | |
| Queue Length 50th (m) | ~186.1 | 77.7 | 0.0 | 4.1 | 9.5 | 0.0 | 4.9 | ~325.7 | 0.0 | 5.0 | 83.0 | 0.0 |
| Queue Length 95th (m) | #245.3 | 108.5 | 0.0 | 10.3 | 19.6 | 0.0 | 11.0 | #373.8 | 0.0 | 12.0 | 105.2 | 0.0 |
| Internal Link Dist (m) | | 42.6 | | | 349.6 | | | 93.8 | | | 234.3 | |
| Turn Bay Length (m) | 66.0 | | 66.0 | | | 80.0 | 80.0 | | 90.0 | 80.0 | | 85.0 |
| Base Capacity (vph) | 293 | 430 | 1498 | 166 | 430 | 1497 | 317 | 1898 | 1498 | 134 | 1898 | 1517 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 1.72 | 0.73 | 0.04 | 0.14 | 0.11 | 0.02 | 0.15 | 1.05 | 0.13 | 0.37 | 0.48 | 0.12 |

Cycle Length: 130

Actuated Cycle Length: 130
Offset: 36 (28%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green

Natural Cycle: 115

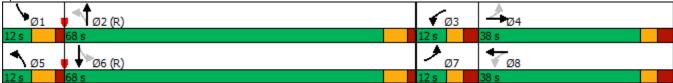
Control Type: Actuated-Coordinated

Maximum v/c Ratio: 1.72
Intersection Signal Delay: 82.2
Intersection Capacity Utilization 104.9%
ICU Level of Service G
Analysis Period (min) 15
Description: NOTE: March Road treated as north-south

Volume exceeds capacity, queue is theoretically infinite.
Queue shown is maximum after two cycles.

95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.





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|------------------------|-------|-------|-----|-------|----------|-----|-------|----------|-------------|----------|-------|-----|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | f) | | ሻ | 4 | | ሻ | 4 | | ሻ | 1> | |
| Traffic Volume (vph) | 146 | 4 | 180 | 22 | 2 | 34 | 96 | 339 | 4 | 15 | 207 | 39 |
| Future Volume (vph) | 146 | 4 | 180 | 22 | 2 | 34 | 96 | 339 | 4 | 15 | 207 | 39 |
| Satd. Flow (prot) | 1695 | 1522 | 0 | 1695 | 1452 | 0 | 1695 | 1781 | 0 | 1695 | 1734 | 0 |
| Flt Permitted | 0.734 | | | 0.641 | | | 0.606 | | | 0.555 | | |
| Satd. Flow (perm) | 1268 | 1522 | 0 | 1144 | 1452 | 0 | 1079 | 1781 | 0 | 990 | 1734 | 0 |
| Satd. Flow (RTOR) | | 180 | | | 34 | | | 1 | | | 19 | |
| Lane Group Flow (vph) | 146 | 184 | 0 | 22 | 36 | 0 | 96 | 343 | 0 | 15 | 246 | 0 |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Detector Phase | 4 | 4 | | 8 | 8 | | 2 | 2 | | 6 | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 10.0 | 10.0 | | 10.0 | 10.0 | | 10.0 | 10.0 | | 10.0 | 10.0 | |
| Minimum Split (s) | 22.8 | 22.8 | | 22.8 | 22.8 | | 65.6 | 65.6 | | 65.6 | 65.6 | |
| Total Split (s) | 29.8 | 29.8 | | 29.8 | 29.8 | | 65.6 | 65.6 | | 65.6 | 65.6 | |
| Total Split (%) | 31.2% | 31.2% | | 31.2% | 31.2% | | 68.8% | 68.8% | | 68.8% | 68.8% | |
| Yellow Time (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.3 | 3.3 | | 3.3 | 3.3 | |
| All-Red Time (s) | 2.8 | 2.8 | | 2.8 | 2.8 | | 2.3 | 2.3 | | 2.3 | 2.3 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | 5.8 | 5.8 | | 5.8 | 5.8 | | 5.6 | 5.6 | | 5.6 | 5.6 | |
| Lead/Lag | | | | | | | | | | | | |
| Lead-Lag Optimize? | | | | | | | | | | | | |
| Recall Mode | None | None | | None | None | | Min | Min | | Min | Min | |
| Act Effct Green (s) | 11.5 | 11.5 | | 11.5 | 11.5 | | 14.1 | 14.1 | | 14.1 | 14.1 | |
| Actuated g/C Ratio | 0.31 | 0.31 | | 0.31 | 0.31 | | 0.38 | 0.38 | | 0.38 | 0.38 | |
| v/c Ratio | 0.38 | 0.31 | | 0.06 | 0.08 | | 0.24 | 0.51 | | 0.04 | 0.37 | |
| Control Delay | 14.4 | 4.3 | | 11.0 | 5.6 | | 9.8 | 12.1 | | 7.9 | 9.6 | |
| Queue Delay | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Delay | 14.4 | 4.3 | | 11.0 | 5.6 | | 9.8 | 12.1 | | 7.9 | 9.6 | |
| LOS | В | Α | | В | Α | | Α | В | | Α | Α | |
| Approach Delay | | 8.7 | | | 7.6 | | | 11.6 | | | 9.5 | |
| Approach LOS | | Α | | | Α | | | В | | | Α | |
| Queue Length 50th (m) | 6.2 | 0.2 | | 0.8 | 0.1 | | 3.4 | 13.8 | | 0.5 | 8.5 | |
| Queue Length 95th (m) | 20.9 | 10.0 | | 4.8 | 4.5 | | 12.4 | 36.7 | | 3.1 | 24.7 | |
| Internal Link Dist (m) | | 594.0 | | | 268.4 | | | 124.5 | | | 518.6 | |
| Turn Bay Length (m) | 60.0 | | | 15.0 | | | 40.0 | | | 45.0 | | |
| Base Capacity (vph) | 837 | 1066 | | 755 | 970 | | 1079 | 1781 | | 990 | 1734 | |
| Starvation Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Reduced v/c Ratio | 0.17 | 0.17 | | 0.03 | 0.04 | | 0.09 | 0.19 | | 0.02 | 0.14 | |
| | | | | | | | | | | | | |

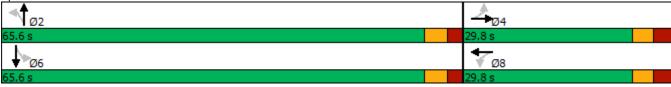
Cycle Length: 95.4

Actuated Cycle Length: 37.3 Natural Cycle: 90

Control Type: Semi Act-Uncoord Maximum v/c Ratio: 0.51

| Intersection Signal Delay: 10.0 | Intersection LOS: B |
|---|------------------------|
| Intersection Capacity Utilization 60.9% | ICU Level of Service B |
| Analysis Period (min) 15 | |

Splits and Phases: 3: Teron & Beaverbrook



| Intersection | | | | | | |
|------------------------|--------|-------|--------------|-------|--------------|-------|
| Int Delay, s/veh | 2.6 | | | | | |
| | | E55 | ND | NST | 007 | 000 |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | | 7 | | ተተኩ | | 7 |
| Traffic Vol, veh/h | 129 | 66 | 45 | 612 | 177 | 97 |
| Future Vol, veh/h | 129 | 66 | 45 | 612 | 177 | 97 |
| Conflicting Peds, #/hr | 4 | 4 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | Yield | - | Free | - | Yield |
| Storage Length | 50 | 0 | - | - | - | 0 |
| Veh in Median Storage | e, # 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 129 | 66 | 45 | 612 | 177 | 97 |
| | | | | | | |
| | | | | | | |
| | Minor2 | | Major1 | | Major2 | |
| Conflicting Flow All | 516 | 181 | 177 | 0 | - | 0 |
| Stage 1 | 177 | - | - | - | - | - |
| Stage 2 | 339 | - | - | - | - | - |
| Critical Hdwy | 6.08 | 6.23 | 4.13 | - | - | - |
| Critical Hdwy Stg 1 | 5.43 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.03 | - | - | - | - | - |
| Follow-up Hdwy | 3.669 | 3.319 | 2.219 | - | _ | _ |
| Pot Cap-1 Maneuver | 528 | 861 | 1398 | _ | - | _ |
| Stage 1 | 821 | | - | _ | _ | _ |
| Stage 2 | 658 | _ | _ | _ | _ | _ |
| Platoon blocked, % | - 000 | | | _ | <u>-</u> | _ |
| Mov Cap-1 Maneuver | 502 | 858 | 1398 | | _ | _ |
| Mov Cap-1 Maneuver | 502 | 000 | 1330 | _ | _ | |
| • | 781 | - | - | - | - | - |
| Stage 1 | 658 | | - | - | = | _ |
| Stage 2 | ბებ | - | - | - | - | - |
| | | | | | | |
| Approach | EB | | NB | | SB | |
| HCM Control Delay, s | 12.9 | | 0.6 | | 0 | |
| HCM LOS | В | | 0.0 | | _ | |
| | | | | | | |
| | | | | | | |
| Minor Lane/Major Mvn | nt | NBL | NBT | EBLn1 | EBLn2 | SBT |
| Capacity (veh/h) | | 1398 | - | 502 | 858 | - |
| HCM Lane V/C Ratio | | 0.032 | - | 0.257 | 0.077 | - |
| HCM Control Delay (s) |) | 7.7 | 0.1 | 14.6 | 9.5 | - |
| HCM Lane LOS | | Α | Α | В | Α | - |
| HCM 95th %tile Q(veh | 1) | 0.1 | - | 1 | 0.2 | - |

| Intersection Int Delay, s/veh |
|---|
| Movement WBL WBR NBT NBR SBL SB Lane Configurations ↑ ↑ ↓ |
| Lane Configurations Y Image: Configuration of the procession o |
| Traffic Vol, veh/h 8 32 635 5 7 24: Future Vol, veh/h 8 32 635 5 7 24: Conflicting Peds, #/hr 0 0 0 0 0 0 Sign Control Stop Stop Free Free <td< td=""></td<> |
| Future Vol, veh/h Conflicting Peds, #/hr O O O O O O O O O O O O O O O O O O O |
| Conflicting Peds, #/hr |
| Sign Control Stop Stop Free Romon Storage Length 0 - 0 - 0 - - 0 - 0 - 0 - 0 - 0 - 0 - 0 <td< td=""></td<> |
| RT Channelized - None - None - None Storage Length 0 |
| Storage Length 0 - - - - Veh in Median Storage, # 0 - 0 - - - Grade, % 0 - 0 - - - - Peak Hour Factor 100 |
| Veh in Median Storage, # 0 - 0 - - - - - - - - - - - - - - - - - |
| Grade, % 0 - 0 - - 0 Peak Hour Factor 100 |
| Peak Hour Factor 100 20 </td |
| Major/Minor Minor1 Major1 Major2 |
| Mvmt Flow 8 32 635 5 7 24 Major/Minor Minor1 Major1 Major2 Conflicting Flow All 895 638 0 0 640 640 Stage 1 638 - |
| Momental Major Major Major Major Major Minor Minor Minor Major Majo |
| Major/Minor Minor1 Major1 Major2 Conflicting Flow All 895 638 0 0 640 Stage 1 638 - - - - Stage 2 257 - - - - Critical Hdwy 6.42 6.22 - 4.12 Critical Hdwy Stg 1 5.42 - - - Critical Hdwy Stg 2 5.42 - - - Follow-up Hdwy 3.518 3.318 - - 2.218 Pot Cap-1 Maneuver 311 477 - 944 Stage 1 526 - - - Stage 2 786 - - - Platoon blocked, % - - - - Mov Cap-1 Maneuver 308 477 - 944 Mov Cap-2 Maneuver 308 - - - Stage 2 779 - - - |
| Conflicting Flow All 895 638 0 0 640 Stage 1 638 - - - - Stage 2 257 - - - - Critical Hdwy 6.42 6.22 - - 4.12 Critical Hdwy Stg 1 5.42 - - - - Critical Hdwy Stg 2 5.42 - - - - Follow-up Hdwy 3.518 3.318 - - 2.218 Pot Cap-1 Maneuver 311 477 - 944 Stage 1 526 - - - - Platoon blocked, % - - - - - - Mov Cap-1 Maneuver 308 477 - 944 Mov Cap-2 Maneuver 308 - - - - Stage 2 779 - - - - Approach WB NB SB |
| Conflicting Flow All 895 638 0 0 640 Stage 1 638 - - - - Stage 2 257 - - - - Critical Hdwy 6.42 6.22 - - 4.12 Critical Hdwy Stg 1 5.42 - - - - Critical Hdwy Stg 2 5.42 - - - - Follow-up Hdwy 3.518 3.318 - - 2.218 Pot Cap-1 Maneuver 311 477 - 944 Stage 1 526 - - - - Platoon blocked, % - - - - - - Mov Cap-1 Maneuver 308 477 - 944 Mov Cap-2 Maneuver 308 - - - - Stage 2 779 - - - - Approach WB NB SB |
| Stage 1 638 - - - - Stage 2 257 - - - - Critical Hdwy 6.42 6.22 - - 4.12 Critical Hdwy Stg 1 5.42 - - - - Critical Hdwy Stg 2 5.42 - - - - Follow-up Hdwy 3.518 3.318 - - 2.218 Pot Cap-1 Maneuver 311 477 - 944 Stage 1 526 - - - - Stage 2 786 - - - - Platoon blocked, % - - - - - Mov Cap-1 Maneuver 308 477 - 944 Mov Cap-2 Maneuver 308 - - - - Stage 1 526 - - - - Stage 2 779 - - - - Approach WB NB SB HCM Control Delay, s 14.2 |
| Stage 2 257 - - - - Critical Hdwy 6.42 6.22 - 4.12 Critical Hdwy Stg 1 5.42 - - - Critical Hdwy Stg 2 5.42 - - - Follow-up Hdwy 3.518 3.318 - 2.218 Pot Cap-1 Maneuver 311 477 - 944 Stage 1 526 - - - Stage 2 786 - - - Platoon blocked, % - - - - Mov Cap-1 Maneuver 308 477 - 944 Mov Cap-2 Maneuver 308 - - - Stage 1 526 - - - Stage 2 779 - - - Approach WB NB SB HCM Control Delay, s 14.2 0 0.2 HCM LOS B Minor Lane/Major Mvmt NBT NBRWBLn1 SBL SB Capacity (veh/h) - 430 944 |
| Critical Hdwy 6.42 6.22 - - 4.12 Critical Hdwy Stg 1 5.42 - - - - Critical Hdwy Stg 2 5.42 - - - - Follow-up Hdwy 3.518 3.318 - - 2.218 Pot Cap-1 Maneuver 311 477 - 944 Stage 1 526 - - - - Stage 2 786 - - - - - Platoon blocked, % - |
| Critical Hdwy Stg 1 5.42 Critical Hdwy Stg 2 5.42 |
| Critical Hdwy Stg 2 5.42 Follow-up Hdwy 3.518 3.318 - 2.218 Pot Cap-1 Maneuver 311 477 - 944 Stage 1 526 Stage 2 786 |
| Critical Hdwy Stg 2 5.42 Follow-up Hdwy 3.518 3.318 2.218 Pot Cap-1 Maneuver 311 477 - 944 Stage 1 526 |
| Follow-up Hdwy 3.518 3.318 2.218 Pot Cap-1 Maneuver 311 477 944 Stage 1 526 Stage 2 786 Platoon blocked, % Mov Cap-1 Maneuver 308 477 - 944 Mov Cap-2 Maneuver 308 Stage 1 526 Stage 2 779 Approach WB NB SB HCM Control Delay, s 14.2 0 0.2 HCM LOS B Minor Lane/Major Mvmt NBT NBRWBLn1 SBL SB Capacity (veh/h) - 430 944 |
| Pot Cap-1 Maneuver 311 477 - - 944 Stage 1 526 - - - - Stage 2 786 - - - - Platoon blocked, % - |
| Stage 1 526 - - - Stage 2 786 - - - Platoon blocked, % - - - - Mov Cap-1 Maneuver 308 477 - 944 Mov Cap-2 Maneuver 308 - - - Stage 1 526 - - - Stage 2 779 - - - Approach WB NB SB HCM Control Delay, s 14.2 0 0.2 HCM LOS B Minor Lane/Major Mvmt NBT NBRWBLn1 SBL SB' Capacity (veh/h) - 430 944 |
| Stage 2 786 - - - - Platoon blocked, % - - - - Mov Cap-1 Maneuver 308 477 - - 944 Mov Cap-2 Maneuver 308 - |
| Platoon blocked, % - - Mov Cap-1 Maneuver 308 477 - 944 Mov Cap-2 Maneuver 308 - - - - Stage 1 526 - - - - Stage 2 779 - - - - Approach WB NB SB HCM Control Delay, s 14.2 0 0.2 HCM LOS B Minor Lane/Major Mvmt NBT NBRWBLn1 SBL SB' Capacity (veh/h) - 430 944 |
| Mov Cap-1 Maneuver 308 477 - - 944 Mov Cap-2 Maneuver 308 - - - - Stage 1 526 - - - - Stage 2 779 - - - - Approach WB NB SB HCM Control Delay, s 14.2 0 0.2 HCM LOS B Minor Lane/Major Mvmt NBT NBRWBLn1 SBL SB' Capacity (veh/h) - 430 944 |
| Mov Cap-2 Maneuver 308 - |
| Stage 1 526 - |
| Stage 2 779 - |
| Approach WB NB SB HCM Control Delay, s 14.2 0 0.2 HCM LOS B Minor Lane/Major Mvmt NBT NBRWBLn1 SBL SB' Capacity (veh/h) - 430 944 |
| HCM Control Delay, s 14.2 0 0.2 |
| HCM Control Delay, s 14.2 0 0.2 |
| HCM Control Delay, s 14.2 0 0.2 HCM LOS B Minor Lane/Major Mvmt NBT NBRWBLn1 SBL SB Capacity (veh/h) - 430 944 |
| HCM LOS B Minor Lane/Major Mvmt NBT NBRWBLn1 SBL SB Capacity (veh/h) - 430 944 |
| Minor Lane/Major Mvmt NBT NBRWBLn1 SBL SB Capacity (veh/h) - 430 944 |
| Capacity (veh/h) 430 944 |
| Capacity (veh/h) 430 944 |
| |
| |
| HCM Lane V/C Ratio 0.093 0.007 |
| HCM Control Delay (s) 14.2 8.8 |
| HCM Lane LOS B A |
| HCM 95th %tile Q(veh) 0.3 0 |

| | ٠ | → | • | • | ← | • | 4 | † | <i>></i> | > | ļ | 4 |
|------------------------|-------|----------|-------|-------|----------|-------|-------|----------|-------------|-------------|----------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | † | 7 | 7 | † | 7 | * | ^ | 7 | 7 | ^ | 7 |
| Traffic Volume (vph) | 242 | 60 | 70 | 153 | 200 | 50 | 91 | 1281 | 20 | 11 | 2019 | 483 |
| Future Volume (vph) | 242 | 60 | 70 | 153 | 200 | 50 | 91 | 1281 | 20 | 11 | 2019 | 483 |
| Satd. Flow (prot) | 1695 | 1784 | 1517 | 1695 | 1784 | 1517 | 1695 | 3390 | 1517 | 1695 | 3390 | 1517 |
| Flt Permitted | 0.521 | | | 0.587 | | | 0.057 | | | 0.135 | | |
| Satd. Flow (perm) | 921 | 1784 | 1498 | 1046 | 1784 | 1493 | 102 | 3390 | 1498 | 241 | 3390 | 1517 |
| Satd. Flow (RTOR) | | | 188 | | | 188 | | | 188 | | | 188 |
| Lane Group Flow (vph) | 242 | 60 | 70 | 153 | 200 | 50 | 91 | 1281 | 20 | 11 | 2019 | 483 |
| Turn Type | pm+pt | NA | Free | pm+pt | NA | Free | pm+pt | NA | Free | pm+pt | NA | Free |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | Free | 8 | | Free | 2 | | Free | 6 | | Free |
| Detector Phase | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 10.0 | | 5.0 | 10.0 | | 5.0 | 10.0 | | 5.0 | 10.0 | |
| Minimum Split (s) | 11.1 | 34.6 | | 11.1 | 34.6 | | 11.4 | 25.3 | | 11.4 | 25.3 | |
| Total Split (s) | 17.0 | 35.0 | | 17.0 | 35.0 | | 12.0 | 66.0 | | 12.0 | 66.0 | |
| Total Split (%) | 13.1% | 26.9% | | 13.1% | 26.9% | | 9.2% | 50.8% | | 9.2% | 50.8% | |
| Yellow Time (s) | 3.3 | 3.3 | | 3.3 | 3.3 | | 4.6 | 4.6 | | 4.6 | 4.6 | |
| All-Red Time (s) | 2.8 | 3.3 | | 2.8 | 3.3 | | 1.8 | 1.7 | | 1.8 | 1.7 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | 6.1 | 6.6 | | 6.1 | 6.6 | | 6.4 | 6.3 | | 6.4 | 6.3 | |
| Lead/Lag | Lead | Lag | | Lead | Lag | | Lead | Lag | | Lead | Lag | |
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | | Yes | Yes | | Yes | Yes | |
| Recall Mode | None | None | | None | None | | None | C-Min | | None | C-Min | |
| Act Effct Green (s) | 28.8 | 19.5 | 130.0 | 32.7 | 20.1 | 130.0 | 78.2 | 75.0 | 130.0 | 71.4 | 65.7 | 130.0 |
| Actuated g/C Ratio | 0.22 | 0.15 | 1.00 | 0.25 | 0.15 | 1.00 | 0.60 | 0.58 | 1.00 | 0.55 | 0.51 | 1.00 |
| v/c Ratio | 0.90 | 0.22 | 0.05 | 0.46 | 0.73 | 0.03 | 0.58 | 0.65 | 0.01 | 0.06 | 1.18 | 0.32 |
| Control Delay | 77.4 | 48.1 | 0.1 | 40.1 | 66.9 | 0.0 | 34.9 | 22.9 | 0.0 | 12.5 | 117.5 | 0.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 77.4 | 48.1 | 0.1 | 40.1 | 66.9 | 0.0 | 34.9 | 22.9 | 0.0 | 12.5 | 117.5 | 0.6 |
| LOS | E | D | Α | D | Е | Α | С | С | Α | В | F | Α |
| Approach Delay | | 58.1 | | | 48.4 | | | 23.4 | | | 94.6 | |
| Approach LOS | | E | | | D | | | С | | | F | |
| Queue Length 50th (m) | 51.7 | 13.7 | 0.0 | 30.8 | 49.5 | 0.0 | 8.9 | 100.0 | 0.0 | 1.0 | ~327.7 | 0.0 |
| Queue Length 95th (m) | 70.2 | 24.7 | 0.0 | 45.0 | 70.2 | 0.0 | #37.7 | 177.1 | 0.0 | 4.1 | #388.9 | 0.0 |
| Internal Link Dist (m) | | 42.6 | | | 349.6 | | | 93.8 | | | 234.3 | |
| Turn Bay Length (m) | 66.0 | | 66.0 | | | 80.0 | 80.0 | 10-0 | 90.0 | 80.0 | 1=10 | 85.0 |
| Base Capacity (vph) | 268 | 389 | 1498 | 336 | 389 | 1493 | 157 | 1956 | 1498 | 197 | 1713 | 1517 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.90 | 0.15 | 0.05 | 0.46 | 0.51 | 0.03 | 0.58 | 0.65 | 0.01 | 0.06 | 1.18 | 0.32 |

Cycle Length: 130

Actuated Cycle Length: 130
Offset: 121 (93%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green

Natural Cycle: 115

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 1.18
Intersection Signal Delay: 66.5
Intersection Capacity Utilization 114.1%
ICU Level of Service H
Analysis Period (min) 15
Description: NOTE: March Road Treated as north-south

Volume exceeds capacity, queue is theoretically infinite.

Queue shown is maximum after two cycles.

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

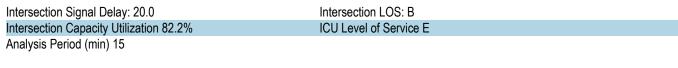


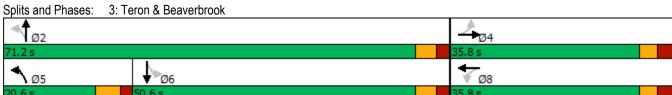


| | ۶ | → | • | • | ← | • | 4 | † | / | / | ţ | 4 |
|------------------------|-------|----------|-----|-------|----------|-----|-------|----------|----------|----------|-------|-----|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | ₽ | | ሻ | ₽ | | ሻ | f) | | ሻ | ₽ | |
| Traffic Volume (vph) | 65 | 6 | 131 | 22 | 11 | 16 | 194 | 232 | 30 | 31 | 517 | 125 |
| Future Volume (vph) | 65 | 6 | 131 | 22 | 11 | 16 | 194 | 232 | 30 | 31 | 517 | 125 |
| Satd. Flow (prot) | 1695 | 1496 | 0 | 1695 | 1586 | 0 | 1695 | 1747 | 0 | 1695 | 1712 | 0 |
| Flt Permitted | 0.740 | | | 0.669 | | | 0.170 | | | 0.597 | | |
| Satd. Flow (perm) | 1296 | 1496 | 0 | 1194 | 1586 | 0 | 303 | 1747 | 0 | 1057 | 1712 | 0 |
| Satd. Flow (RTOR) | | 131 | | | 16 | | | 11 | | | 14 | |
| Lane Group Flow (vph) | 65 | 137 | 0 | 22 | 27 | 0 | 194 | 262 | 0 | 31 | 642 | 0 |
| Turn Type | Perm | NA | | Perm | NA | | pm+pt | NA | | Perm | NA | |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Detector Phase | 4 | 4 | | 8 | 8 | | 5 | 2 | | 6 | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 10.0 | 10.0 | | 10.0 | 10.0 | | 5.0 | 10.0 | | 10.0 | 10.0 | |
| Minimum Split (s) | 22.8 | 22.8 | | 22.8 | 22.8 | | 11.0 | 71.2 | | 50.6 | 50.6 | |
| Total Split (s) | 35.8 | 35.8 | | 35.8 | 35.8 | | 20.6 | 71.2 | | 50.6 | 50.6 | |
| Total Split (%) | 33.5% | 33.5% | | 33.5% | 33.5% | | 19.3% | 66.5% | | 47.3% | 47.3% | |
| Yellow Time (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 4.0 | 3.3 | | 3.3 | 3.3 | |
| All-Red Time (s) | 2.8 | 2.8 | | 2.8 | 2.8 | | 2.0 | 2.3 | | 2.3 | 2.3 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | 5.8 | 5.8 | | 5.8 | 5.8 | | 6.0 | 5.6 | | 5.6 | 5.6 | |
| Lead/Lag | | | | | | | Lead | | | Lag | Lag | |
| Lead-Lag Optimize? | | | | | | | Yes | | | Yes | Yes | |
| Recall Mode | None | None | | None | None | | None | Min | | Min | Min | |
| Act Effct Green (s) | 11.6 | 11.6 | | 11.6 | 11.6 | | 52.2 | 52.6 | | 33.5 | 33.5 | |
| Actuated g/C Ratio | 0.15 | 0.15 | | 0.15 | 0.15 | | 0.69 | 0.69 | | 0.44 | 0.44 | |
| v/c Ratio | 0.33 | 0.40 | | 0.12 | 0.11 | | 0.44 | 0.22 | | 0.07 | 0.84 | |
| Control Delay | 37.2 | 11.2 | | 33.5 | 20.9 | | 7.4 | 4.5 | | 12.9 | 30.1 | |
| Queue Delay | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Delay | 37.2 | 11.2 | | 33.5 | 20.9 | | 7.4 | 4.5 | | 12.9 | 30.1 | |
| LOS | D | В | | С | С | | Α | Α | | В | С | |
| Approach Delay | | 19.6 | | | 26.5 | | | 5.7 | | | 29.3 | |
| Approach LOS | | В | | | С | | | Α | | | С | |
| Queue Length 50th (m) | 8.8 | 8.0 | | 2.9 | 1.4 | | 7.3 | 9.6 | | 2.4 | 76.1 | |
| Queue Length 95th (m) | 22.0 | 15.9 | | 10.0 | 8.7 | | 17.7 | 22.5 | | 7.8 | 137.0 | |
| Internal Link Dist (m) | | 594.0 | | | 268.4 | | | 124.5 | | | 518.6 | |
| Turn Bay Length (m) | 60.0 | | | 15.0 | | | 40.0 | | | 45.0 | | |
| Base Capacity (vph) | 527 | 685 | | 485 | 654 | | 483 | 1504 | | 644 | 1049 | |
| Starvation Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Reduced v/c Ratio | 0.12 | 0.20 | | 0.05 | 0.04 | | 0.40 | 0.17 | | 0.05 | 0.61 | |

Cycle Length: 107 Actuated Cycle Length: 76
Natural Cycle: 95
Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.84





| Intersection | | | | | | |
|------------------------|--------|----------|--------|-----------|-----------|-------|
| Int Delay, s/veh | 4.5 | | | | | |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | * | 7 | | ተተኩ | ↑ | 7 |
| Traffic Vol, veh/h | 166 | 105 | 50 | 242 | 601 | 181 |
| Future Vol, veh/h | 166 | 105 | 50 | 242 | 601 | 181 |
| Conflicting Peds, #/hr | 7 | 7 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | Yield | - | Free | _ | Yield |
| Storage Length | 50 | 0 | _ | _ | _ | 0 |
| Veh in Median Storage | | _ | - | 0 | 0 | _ |
| Grade, % | 0 | _ | _ | 0 | 0 | _ |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mymt Flow | 166 | 105 | 50 | 242 | 601 | 181 |
| WWW. | 100 | 100 | 00 | 272 | 001 | 101 |
| | | | | | | |
| | Minor2 | | Major1 | | Major2 | |
| Conflicting Flow All | 805 | 608 | 601 | 0 | - | 0 |
| Stage 1 | 601 | - | - | - | - | - |
| Stage 2 | 204 | - | - | - | - | - |
| Critical Hdwy | 6.08 | 6.23 | 4.13 | - | - | - |
| Critical Hdwy Stg 1 | 5.43 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.03 | - | - | - | - | - |
| Follow-up Hdwy | 3.669 | 3.319 | 2.219 | - | - | - |
| Pot Cap-1 Maneuver | 369 | 495 | 974 | - | - | - |
| Stage 1 | 530 | - | - | - | - | - |
| Stage 2 | 772 | - | - | - | - | - |
| Platoon blocked, % | | | | - | - | - |
| Mov Cap-1 Maneuver | 347 | 492 | 974 | - | - | - |
| Mov Cap-2 Maneuver | 347 | - | - | - | - | - |
| Stage 1 | 499 | _ | _ | - | - | - |
| Stage 2 | 772 | _ | - | _ | - | - |
| o talgo _ | | | | | | |
| | | | N.D. | | 0.0 | |
| Approach | EB | | NB | | SB | |
| HCM Control Delay, s | | | 1.6 | | 0 | |
| HCM LOS | С | | | | | |
| | | | | | | |
| Minor Lane/Major Mvr | nt | NBL | NBTI | EBLn1 E | -BI n2 | SBT |
| Capacity (veh/h) | | 974 | - 1151 | 347 | 492 | |
| HCM Lane V/C Ratio | | 0.051 | | 0.478 | | _ |
| HCM Control Delay (s | ١ | 8.9 | 0.1 | 24.5 | 14.3 | - |
| HCM Lane LOS | | 0.9 A | Α | 24.5 C | 14.3 B | |
| HCM 95th %tile Q(veh | 1) | 0.2 | Α | 2.5 | 0.8 | - |
| | 1) | 0.2 | | 2.0 | 0.0 | _ |

| Intersection | | | | | | |
|------------------------|----------|-------|--------|-------|--------|------|
| Int Delay, s/veh | 0.5 | | | | | |
| | | | | | | |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | ¥ | | f) | | | 4 |
| Traffic Vol, veh/h | 5 | 20 | 277 | 16 | 24 | 699 |
| Future Vol, veh/h | 5 | 20 | 277 | 16 | 24 | 699 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage | e, # 0 | - | 0 | - | - | 0 |
| Grade, % | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 5 | 20 | 277 | 16 | 24 | 699 |
| | | | | | | 000 |
| | | | | | | |
| | Minor1 | | Major1 | | Major2 | |
| Conflicting Flow All | 1032 | 285 | 0 | 0 | 293 | 0 |
| Stage 1 | 285 | - | - | - | - | - |
| Stage 2 | 747 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - |
| Critical Hdwy Stg 1 | 5.42 | _ | _ | _ | _ | - |
| Critical Hdwy Stg 2 | 5.42 | _ | - | _ | - | _ |
| Follow-up Hdwy | 3.518 | 3.318 | _ | _ | 2.218 | _ |
| Pot Cap-1 Maneuver | 258 | 754 | _ | _ | 1269 | _ |
| Stage 1 | 763 | - | _ | _ | - | _ |
| Stage 2 | 468 | _ | _ | _ | _ | _ |
| Platoon blocked, % | 700 | | _ | _ | | _ |
| Mov Cap-1 Maneuver | 250 | 754 | _ | _ | 1269 | _ |
| | 250 | | | | | |
| Mov Cap-2 Maneuver | | - | - | - | - | - |
| Stage 1 | 763 | - | _ | - | - | - |
| Stage 2 | 453 | - | - | - | - | - |
| | | | | | | |
| Approach | WB | | NB | | SB | |
| HCM Control Delay, s | 12 | | 0 | | 0.3 | |
| HCM LOS | В | | U | | 0.0 | |
| TIOW LOO | <u> </u> | | | | | |
| | | | | | | |
| Minor Lane/Major Mvr | nt | NBT | NBRV | VBLn1 | SBL | SBT |
| Capacity (veh/h) | | - | _ | 537 | 1269 | _ |
| HCM Lane V/C Ratio | | - | _ | 0.047 | | - |
| HCM Control Delay (s |) | _ | _ | 12 | 7.9 | 0 |
| HCM Lane LOS | | _ | _ | В | A | A |
| HCM 95th %tile Q(veh | 1) | _ | _ | 0.1 | 0.1 | - |
| HOW JOHN JOHNE Q(VEI | '/ | | | 0.1 | 0.1 | _ |