

Servicing and Stormwater Management Brief

Rear Building Replacement Revisions to Site Plan Control Application 1871 Merivale Road Nepean, Ontario K2G 1E3

Prepared for:

Benson Auto Parts 700 Education Road Cornwall, Ontario K6H 6B8

Attention: Mr. Marty Benson

Revised September 22, 2020 January 13, 2020

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1 Introduction

LRL Associates Ltd. was retained by Benson Auto Parts. to undertake a Stormwater Management Analysis pertaining to the revisions to the site located at 1871 Merivale Road to accommodate the reconstruction of a building located on the East portion of the existing site. The following brief outlines the proposed development and demonstrates the minor impact the reconstruction of this building has on the previously approved site plan application (Application No. D07-12-17-0054). This brief has been prepared to support the previously completed design and Site Servicing and Stormwater Management Report for the subject property prepared by LRL Associates with a revision date of October 26, 2018.

2 PROJECT OVERVIEW

The subject property is located within the urban boundary of the City of Ottawa; Ward 9 Knoxdale-Merivale, in the Merivale Industrial Park Jamie Sector. The subject property is located at 1871 Merivale Road; East of Merivale Road, and north of Jamie Avenue. The total area of the property measures approximately 0.582 ha.

Currently this site is being redeveloped for a building expansion. The original scope of work that was approved under the previous site plan on November 06, 2018 included demolishing a portion (262 m²) of an existing 1170 m² building on the west half of the site. Once the building was demolished, an expansion of a two-storey warehouse/garage and office space building with a footprint of 1115 m² was erected on the western extent of the site. Refer to Site Development Plan C201 for the permitted phase as per Site Plan Application No. D07-12-17-0054 (#17529).

Initially, it was intended that this new building would be attached to the portion of the existing building which remained after the demolition. However, to improve aesthetics and warehouse conditions, it is proposed to demolish the existing warehouse and construct a new 1-storey building with a similar footprint. Refer to Site Development Plan C201 for the location of proposed building.

The proposed building has a footprint of 835 m² and the existing building which is now proposed to be demolished has a footprint of 917m². Therefore, this project is introducing a reduction of 82 m² of building area and making minor internal site layout changes for vehicular maneuverability and parking. This proposed construction does not increase the impervious area of the original design, as the entire site was hardscape previously.

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3 STORMWATER MANAGEMENT

3.1 Design Criteria

Stormwater quality and quantity control measures are taken into account for this site to reduce post-development stormwater runoff to allowable levels.

For quality control, two oil-grit separators have been proposed through phase 1 which will provide an enhanced level of protection i.e. 80% TSS removal.

For quantity control, all post-development storm events including 100-year event will be controlled to the 5-year pre-development level. The site's major overland route has been designed (through phase 1) to ensure that storm events exceeding 100-year can be conveyed safely towards the Jamie Avenue right of way. The minor system storm sewer within the site is sized to convey the 5-year stormwater flow from the site to the municipal storm sewer on Jamie Avenue.

3.2 Existing Conditions and Stormwater Quantity

As a result of no increase in overall pervious area of the site, the proposed building and minor site changes have been designed to have zero increase on the previously controlled release rate. The extent of the site development is isolated on the east portion which results in only minor updates to the previous stormwater management design. The impact is isolated to the controlled post-development catchment area CA-01. Refer to C702 for the post development catchment plan.

As per the original design, for each of the site's catchment areas, post-development runoff generated by minor and major storm events will be equal or less than the runoff generated during pre-development conditions. Table 1 below summarizes the characteristics for each catchment in the original approved design, as well as the catchments as a result of this proposed development.

Table 1: SWM Catchment Runoff Coefficient Calculations

SWM		roved Site F nt Character		Proposed SWM Catchments				
Catchment Name	Controlled/ Uncontrolled	Runoff Coefficie nt	Area (ha)	Controlled/ Uncontrolled	Runoff Coefficient	Area (ha)		
CA-01	Controlled	0.85	0.140	Controlled	0.81	0.161		
CA-02	Controlled	0.87	0.137	Controlled	0.87	0.144		
CA-03	Controlled	0.88	0.125	Controlled	0.88	0.139		
CA-04	Controlled	0.84	0.135	Controlled	0.84	0.135		
CA-05	Uncontrolled	0.70	0.044	N/A	-	-		
	Total	0.85	0.58	Total	0.85	0.58		

As demonstrated in the table above, the overall area and runoff coefficient for the site remains unchanged. These values ensure that there will be no surplus runoff generated leaving the site; therefore, additional on-site stormwater management quantity control detention measures are not required. Refer to Appendix A for the Pre and Post Development Catchments Plans, C701 and C702 in the design drawings. Refer to Appendix B for the pre and post development runoff coefficients calculations.

3.3 Stormwater Management Concept

The information below should be read in conjunction with Section 5.2 of phase 1 Site Servicing and Stormwater Management Report (Appendix H) and drawing C702. Table 2 shows the summary of release rate.

Table 2- Release Rate Summary (modified from a Table in Section 5.2 of Phase 1 Report)

Outlet	Uncontrolled Release (L/s)	Controlled Release (L/s)	Total Release (L/s)	Remarks
Storm System/Site Outlet #2	5.47	29.52	34.99	Phase 2
Storm System/Site Outlet #3	N/A	14.99	14.99	Phase 1

To restrict flows from phase 2 to the established release rate of 29.52 L/s, a VHV Vertical Vortex Flow Regulator model 150VHV-2 is proposed at STM MH2, refer to C.401 for details. For additional detail of Hydrovex VHV, refer to Appendix D of Phase 1 report.

Refer to Storm Design Sheet included in Appendix B for the calculations of proposed storm sewer network capacity.

3.4 Water Quality

The original design proposed two Stormceptor STC 300 oil/grit separators (one for each storm connection) which provided water quality treatment; where the enhanced 80% TSS removals requirement is met. The Stormceptor proposed originally will remain in the same location on site. Refer to Stormceptor sizing report included within the appendices of the *Phase 1 Site Servicing and Stormwater Management Report* (Appendix H) for details on OGS model and performance.

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4 WATER SUPPLY AND FIRE PROTECTION

4.1 Water Supply Demand and Fire Flow

As per the AWWA Standards and the City of Ottawa Design Guidelines, the average water demand for industrial developments was calculated using an average water demand per fixture unit of 3.33 L/min and a daily and hourly peak factor of 1.5 and 1.8, respectively.

For the proposed building, it was assumed that future use could lead to additional bathrooms. Therefore, it has been assumed that there would be 8 water closets, and 8 lavatories. The peak water demand for the proposed building was calculated for the 33.6 fixtures units (as per Hydraulic Load Table 7.6.3.A O.B.C).

The average daily water demand for the new building is 1.86 L/s, maximum daily is 2.80 L/s, and maximum hourly is 5.03 L/s. Please refer to Appendix C for the water demand calculation sheet. The proposed building has an approximately 20% smaller gross floor area than previously contemplated in approved *Phase 1 Site Servicing and Stormwater Management Report* (Appendix H). Therefore, it is anticipated that pressures received from boundary conditions in Phase 1 for all scenarios would still be above minimum required pressures stated in the City Water Design guidelines.

The fire flow demand was estimated in accordance with the Fire Underwriters Survey (FUS). This method is based on the floor area of the building to be protected, type and combustibility of the structural frame and the separation distances with adjoining buildings. The fire flow demand was calculated to be 133.3 L/s.

There are two fire hydrants, one within 45 m and another within 150 m from the building, that are available to supply the required fire flow demand. Please refer to Appendix D for the fire flow calculation sheet and fire hydrant locations.

4.2 Water Service Design

As per the approved site servicing plan in 2018, there was a 50 mm dia. service connection to the building which was proposed to be demolished. This connection was to be removed, with one new connection to the entire building. However, now that this proposal is to construct a new building, which is to be no longer connected to the west service garage building, it is proposed to re-install a 100mm service to the watermain along Jamie Avenue to feed the proposed new building as shown on Site Servicing Plan C401.



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5 SANITARY SERVICE

5.1 Existing Sanitary Sewer Services

The site is currently being serviced by a 150 mm dia. ABS service, located at the south-east corner of the existing building. The sewage is currently conveyed from this 100mm dia. Service easterly through a 250mm dia. sanitary sewer on Jamie Avenue, then southerly through a 450mm dia. sanitary sewer on Sunderland Street, easterly to a 675 mm dia. sanitary sewer on Bentley Avenue, crossing the train tracks and making its way to the lift station located at 8 Antares Drive in Ottawa.

Please refer to Appendix E for the Jamie Avenue As-Built Drawings, as well as the sanitary sewer distribution maps.

5.2 Sanitary Sewer Servicing Design

As per the approved site servicing plan in 2018, a monitoring manhole (SAN MH2) was installed along the existing 100 mm dia. service, which is located in the east end of the proposed building. It is proposed to remove the existing 100 mm dia. sanitary service and install a new 150 mm dia. PVC pipe for the proposed building as shown on Site Servicing Plan C401.

6 CONCLUSION

This Servicing and Stormwater Management Brief for the building replacement proposed at 1871 Merivale Road presents the details for the servicing requirements for the subject building. In accordance with the report objectives, the servicing requirements for the development are summarized below:

Stormwater

- The proposed building is located on the east portion of the site. Therefore, the existing 250
 mm storm service connecting to Jamie avenue at the east outlet will remain to collect and
 convey runoff generated.
- The remainder of the site will remain as per the original design.
- Stormwater quality objectives will be met with the use of an oil/grit separator.

Domestic Water

• The anticipated water demand for the site is 1.86 L/s (average daily), 2.80 L/s (maximum daily), and 5.03 L/s (maximum hourly).

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- The maximum required fire flow was calculated to be 133.3 L/s using the FUS method.
- Two fire hydrants, one within 45 m and another within 150 m from the building exterior, are located along Jamie Avenue and are available to service the proposed building.
- The new building will be serviced with a 100 mm dia. service lateral connected to the existing 300 mm watermain on Jamie Avenue.

Sanitary

• The new building will be serviced with a 150 mm dia. sanitary servicing to be connected to the monitoring sanitary manhole (SAN MH2) as per the approved site plan (Phase 1).

7 REPORT CONDITIONS AND LIMITATIONS

The report conclusions are applicable only to this specific project described in the preceding pages. Any changes, modifications or additions will require a subsequent review by LRL Associates Ltd. to ensure the compatibility with the recommendations contained in this document.

If you have any questions or comments, please contact the undersigned.

Prepared by:

LRL Associates Ltd.

Amr Salem

Civil Designer

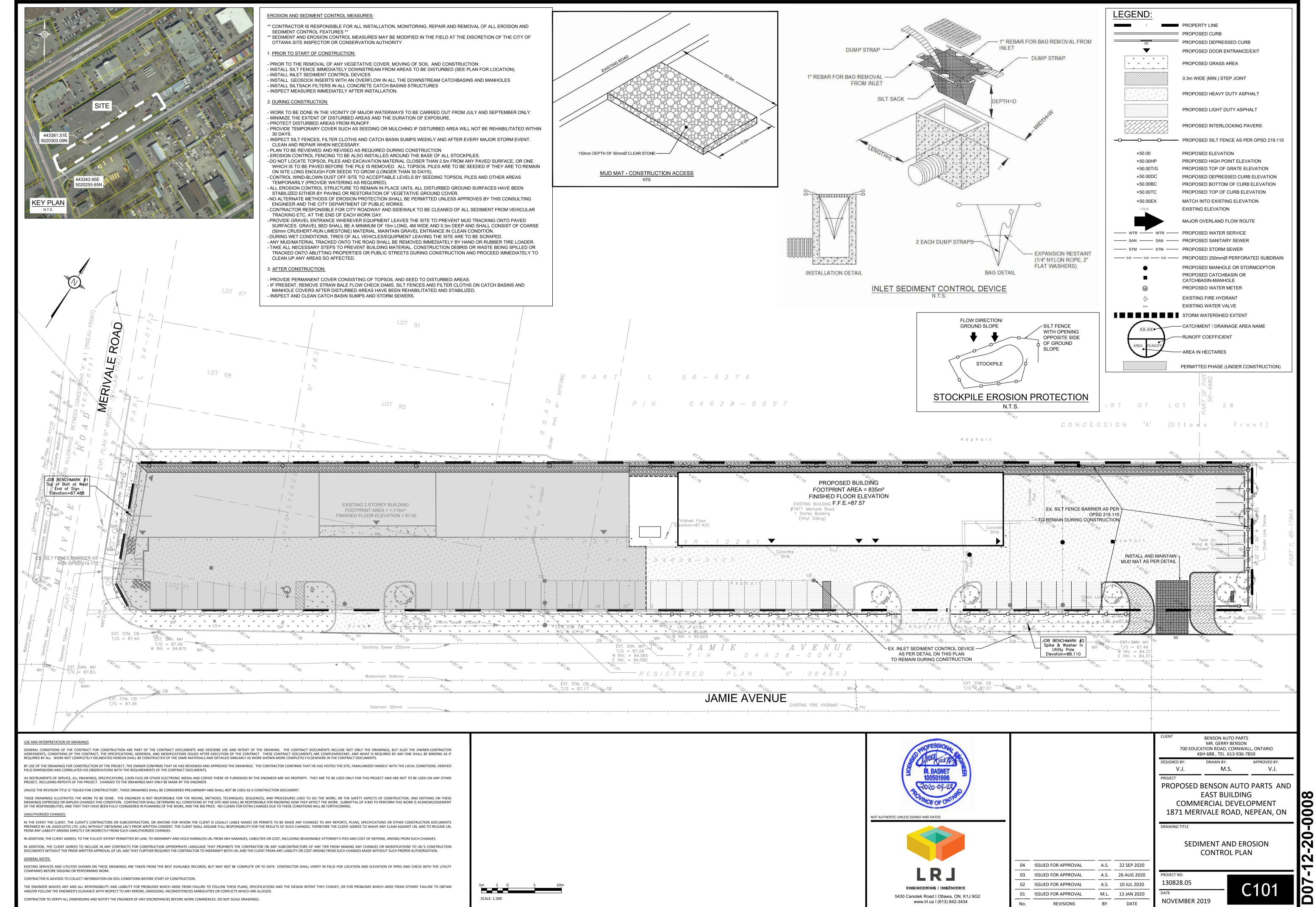
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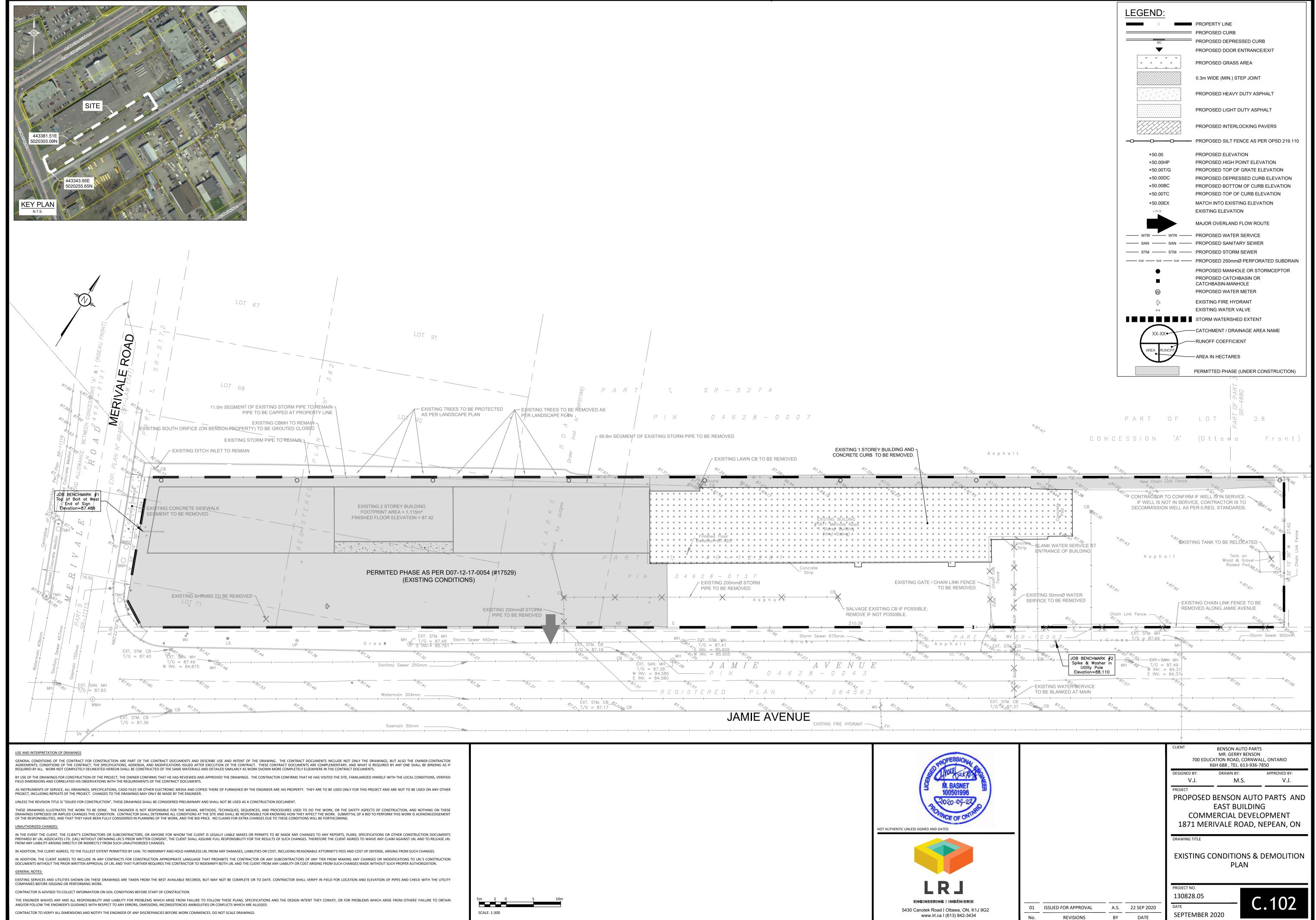
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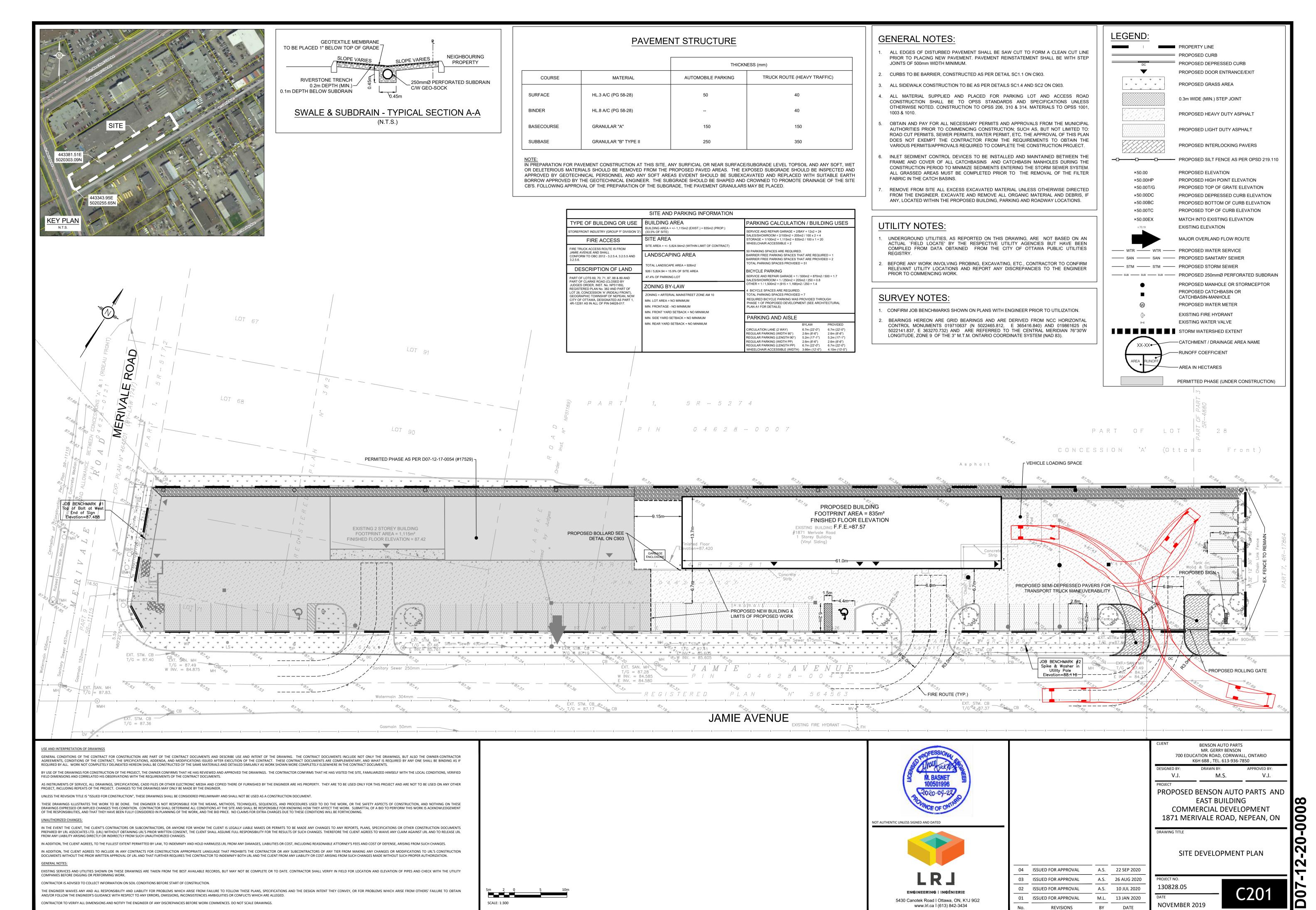
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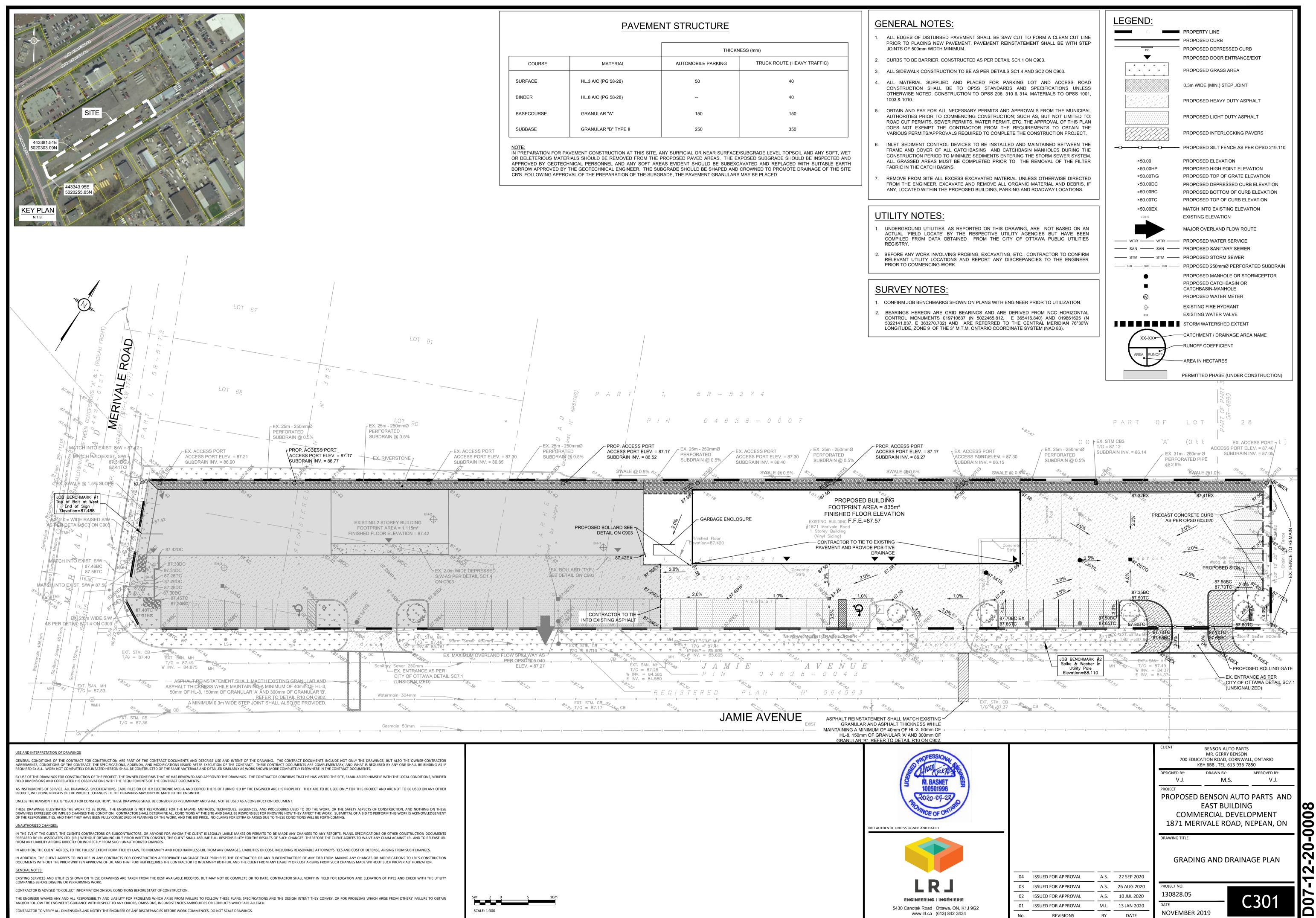
APPENDIX A

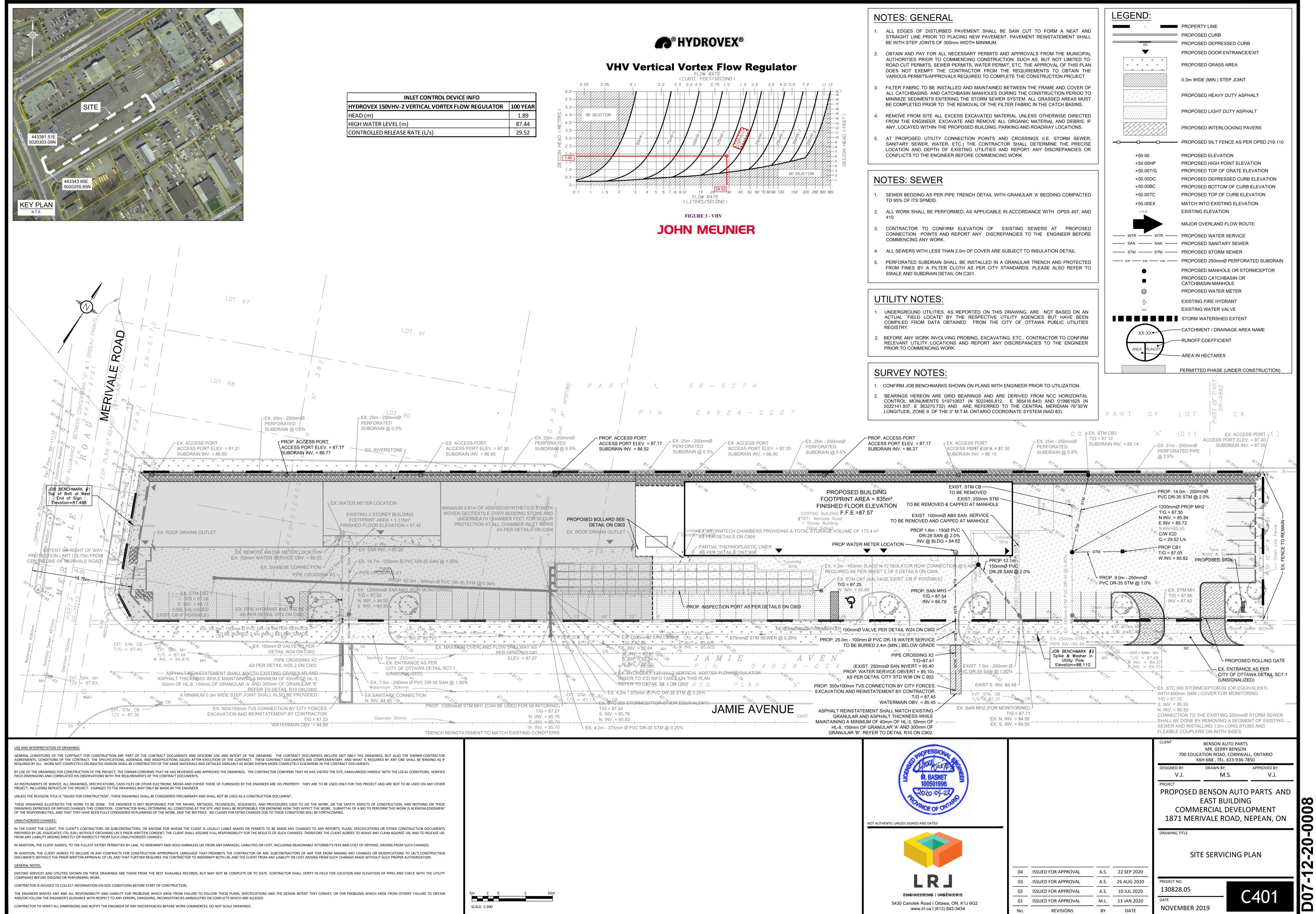
Civil Engineering Design Drawings

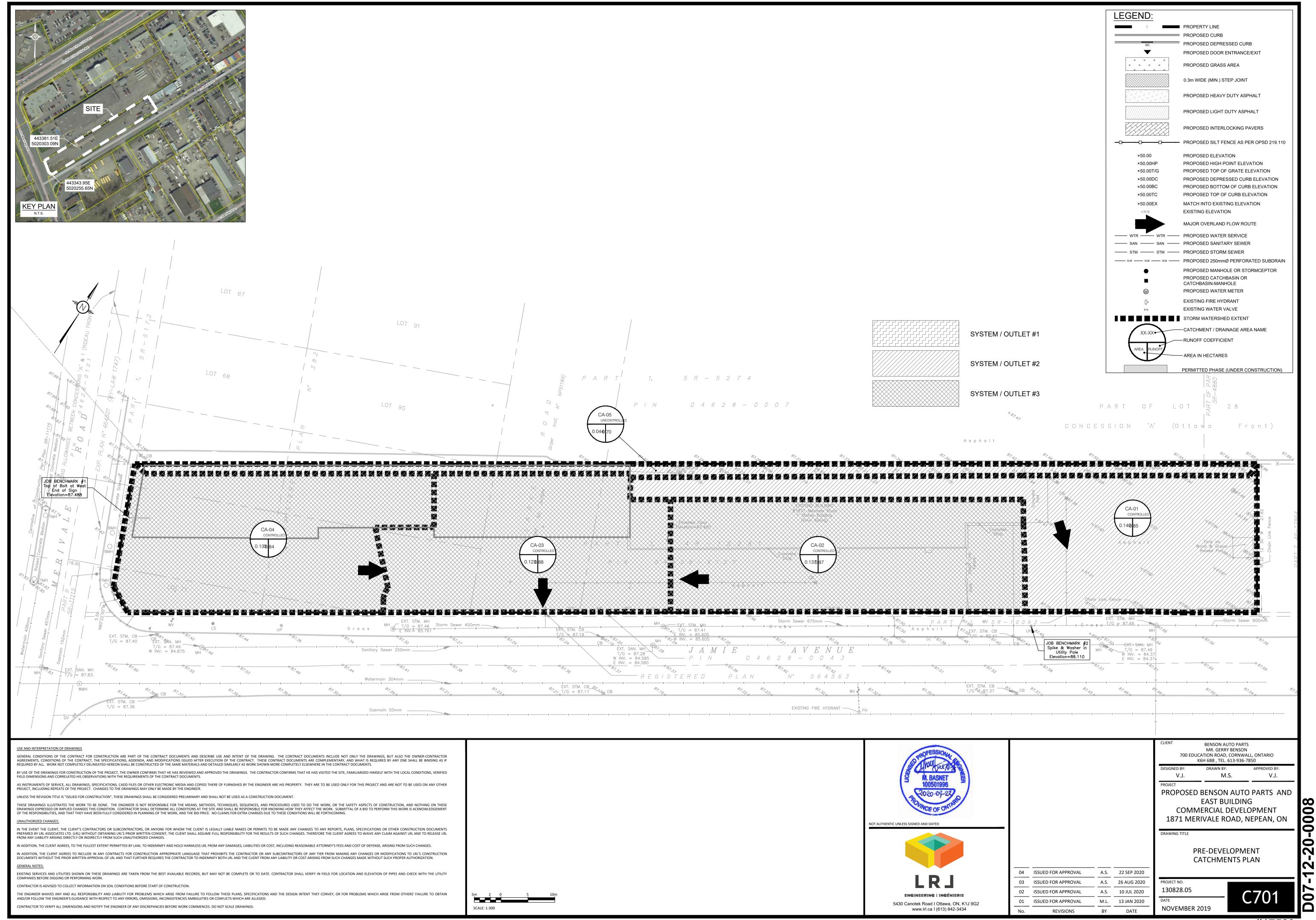


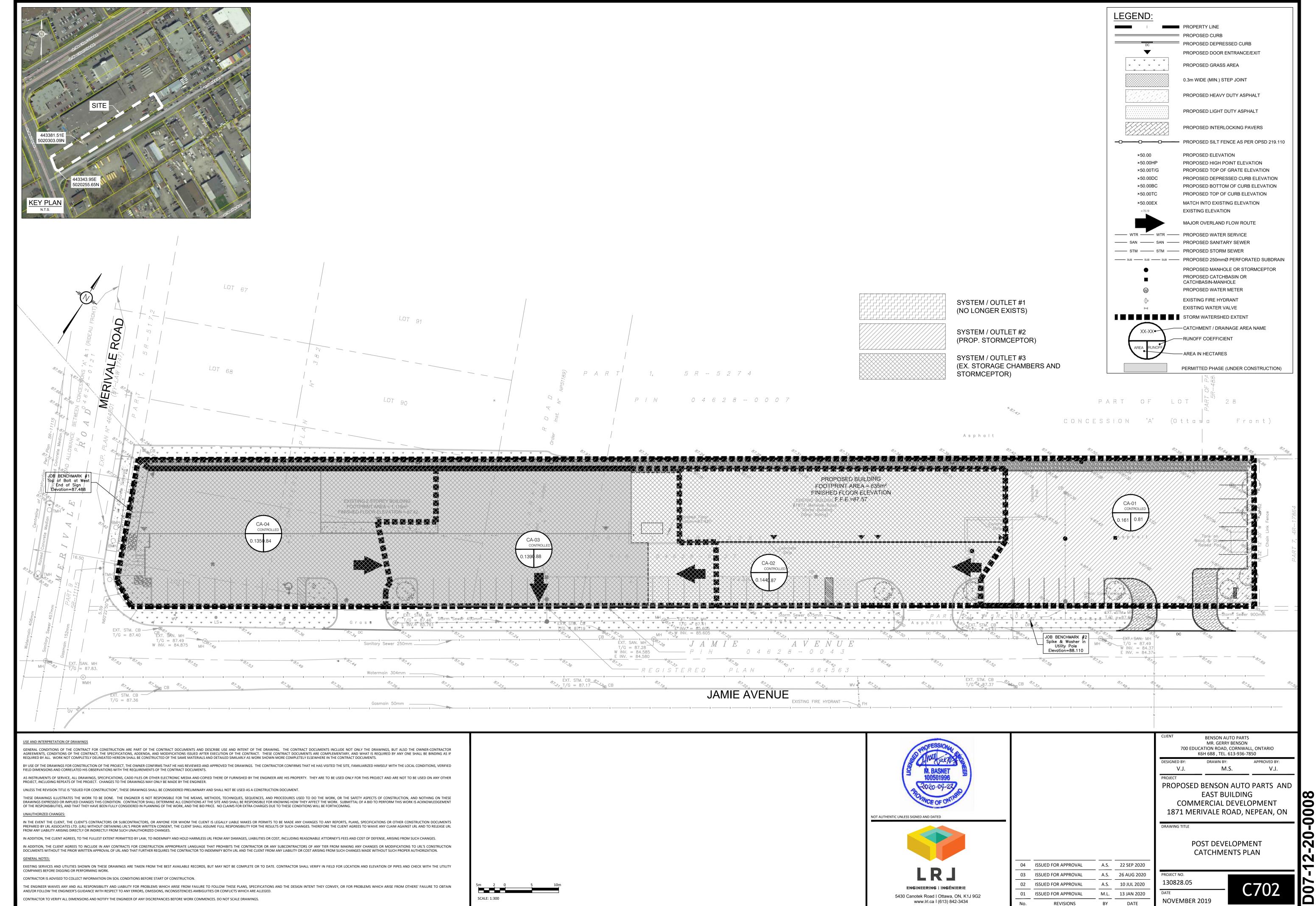


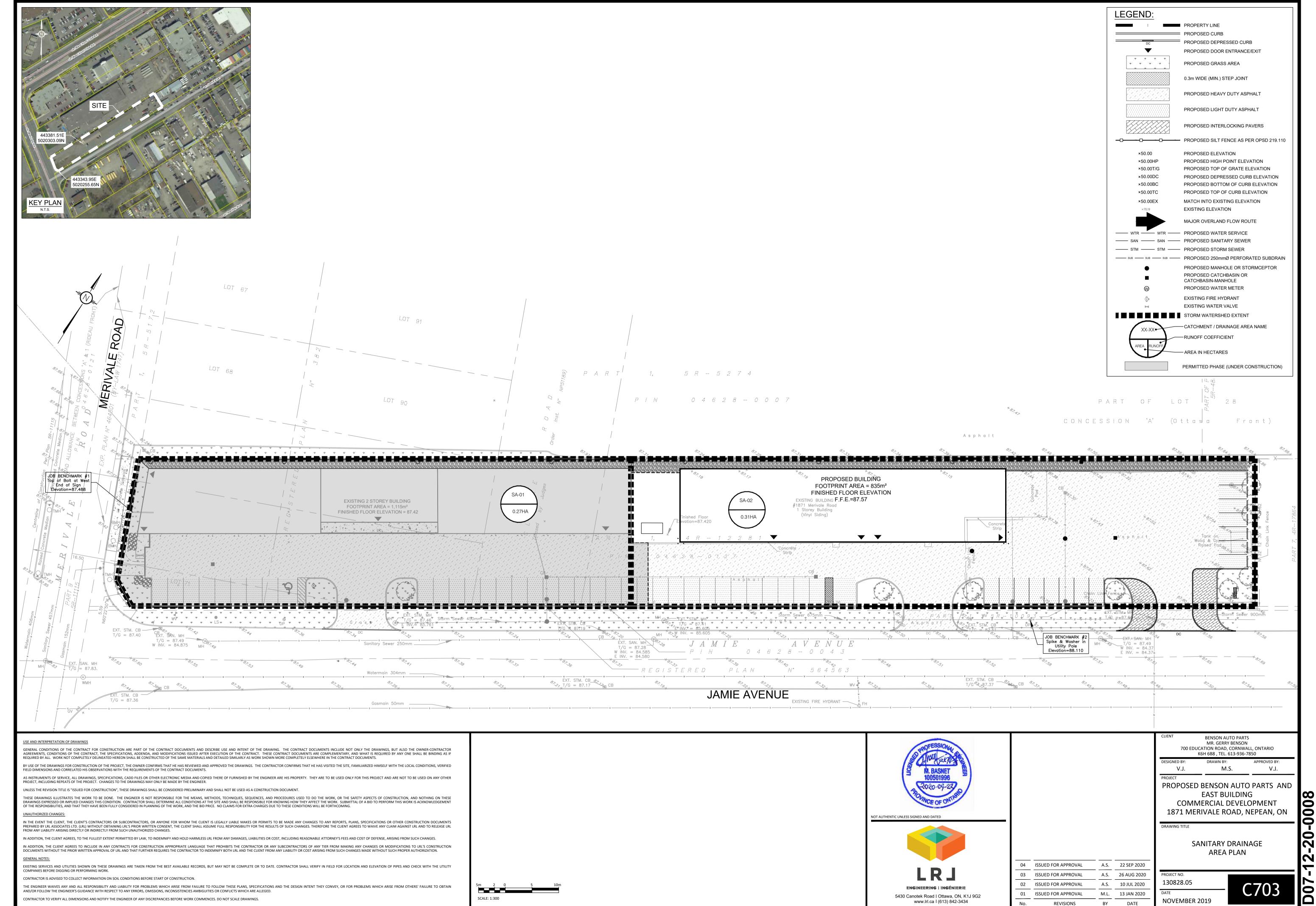


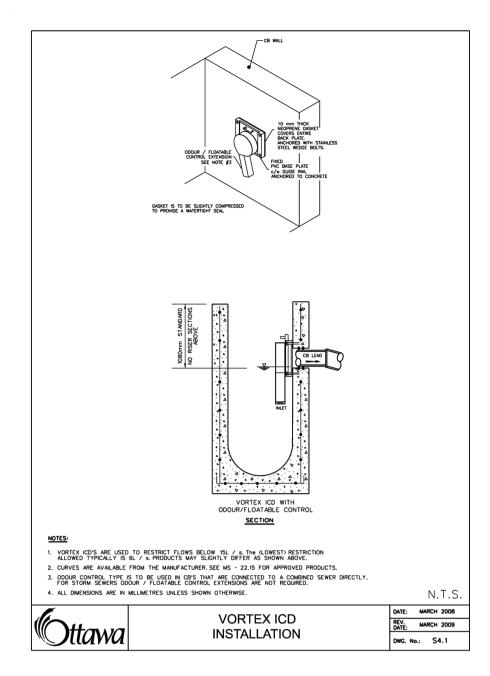


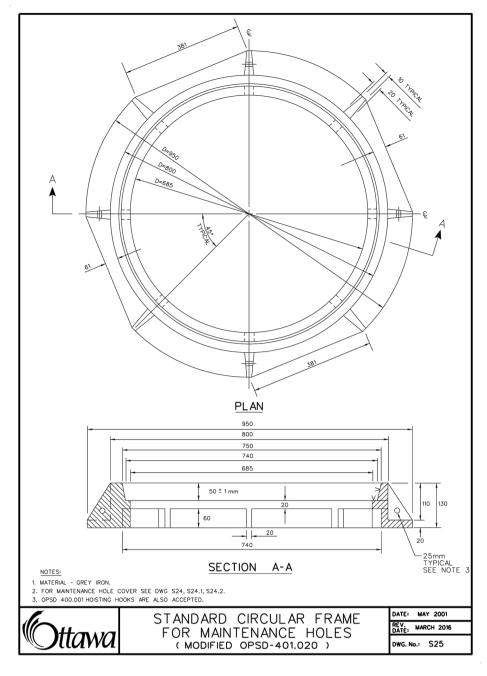


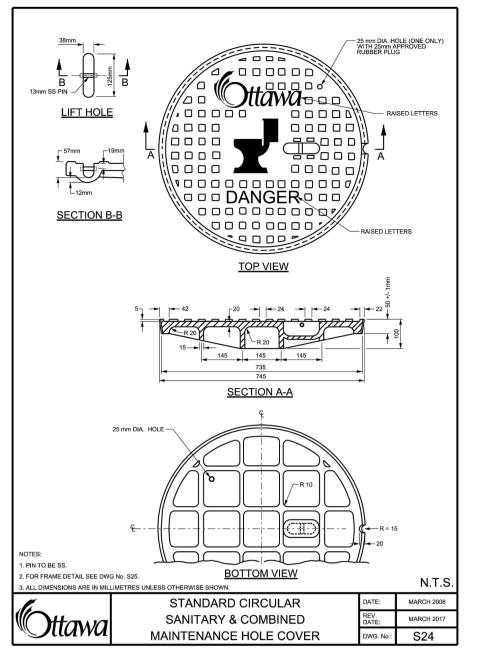


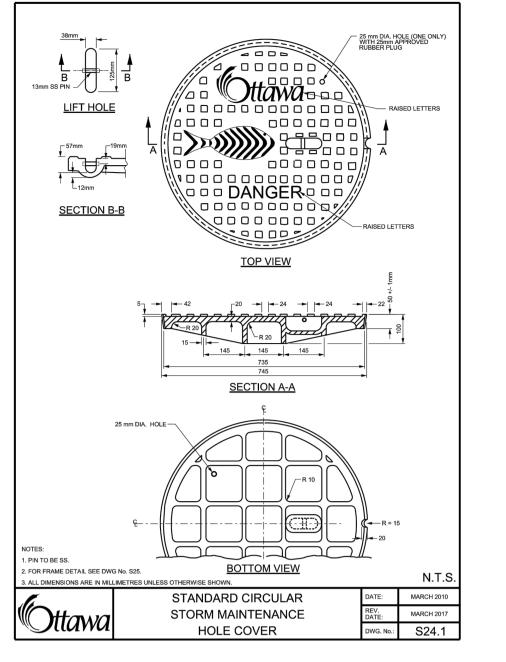


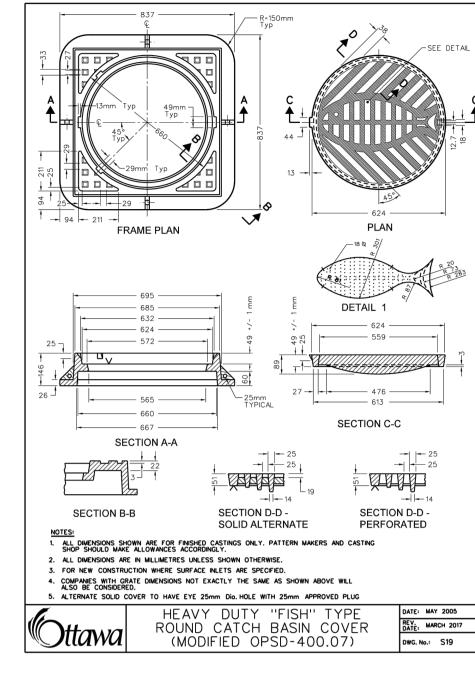


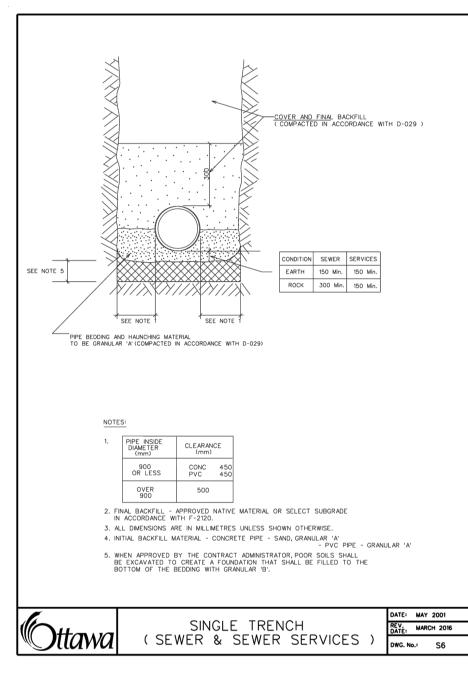


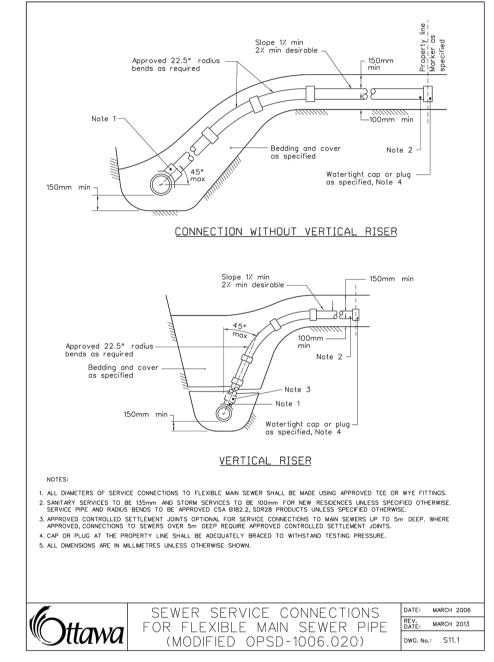


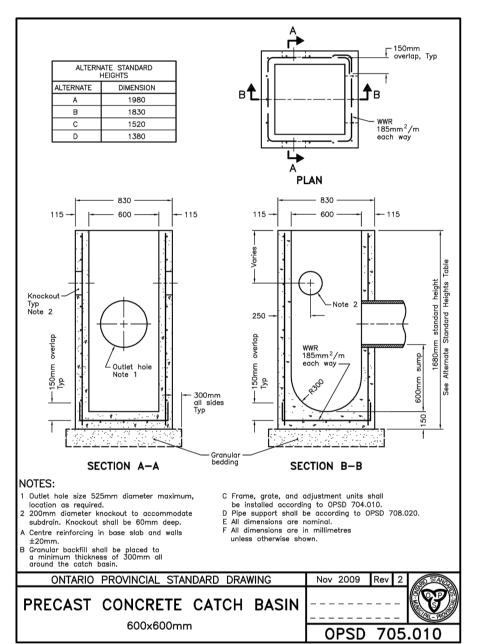


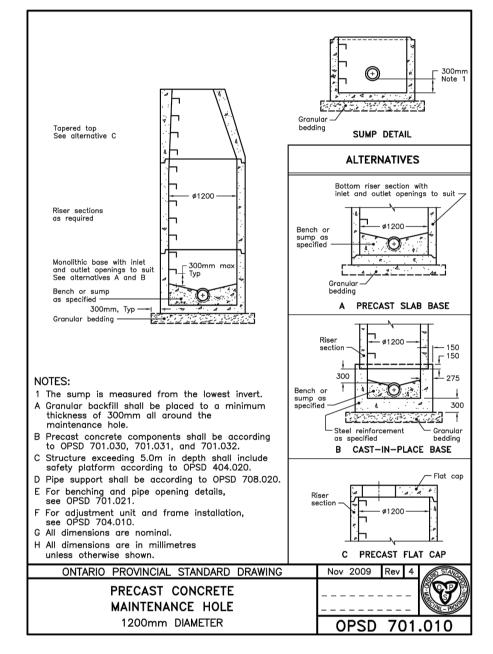


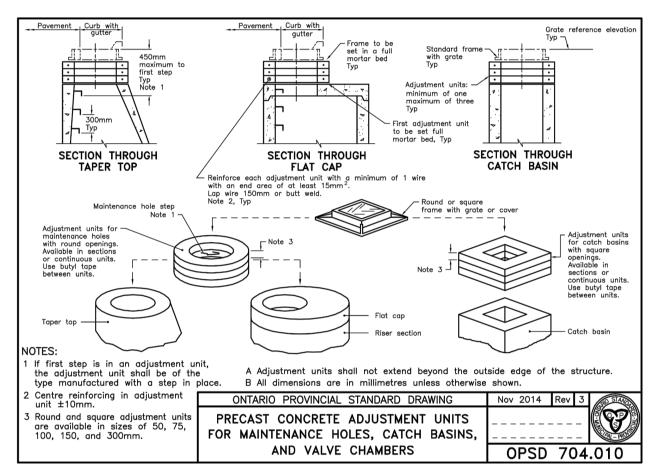


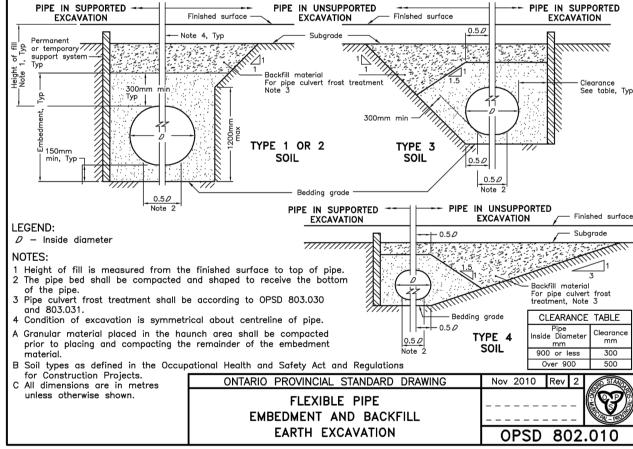












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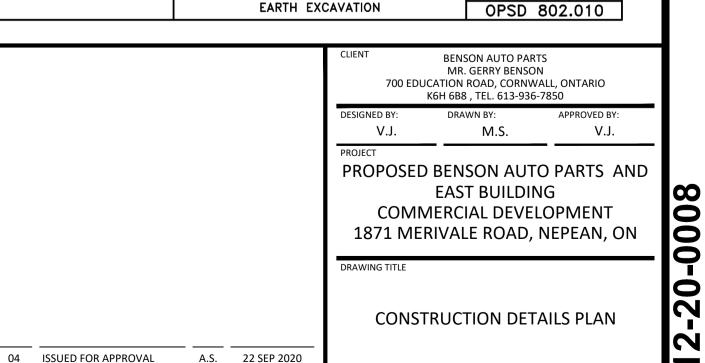
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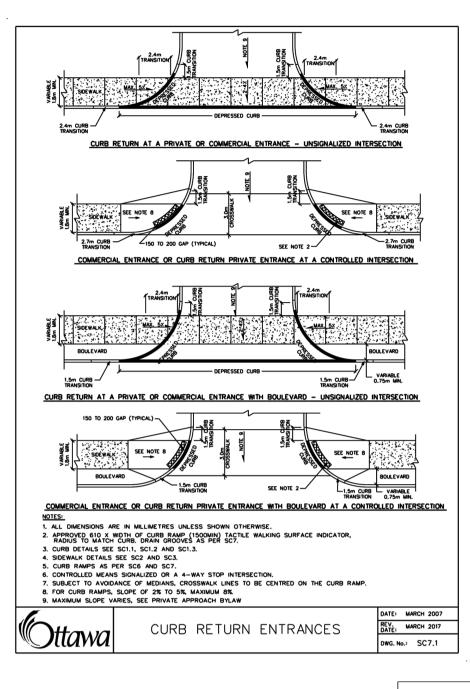
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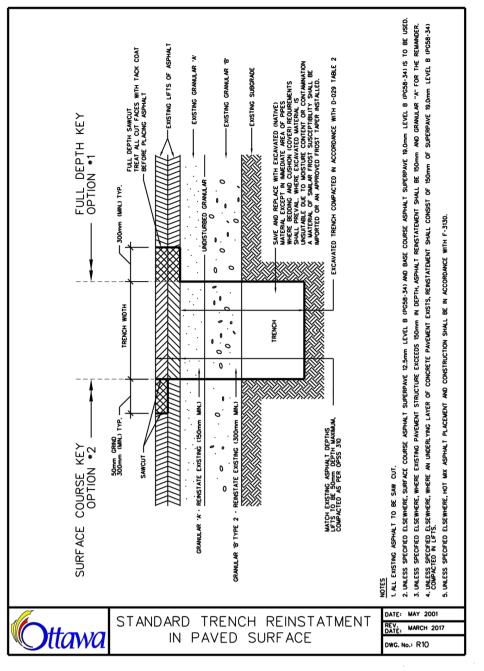
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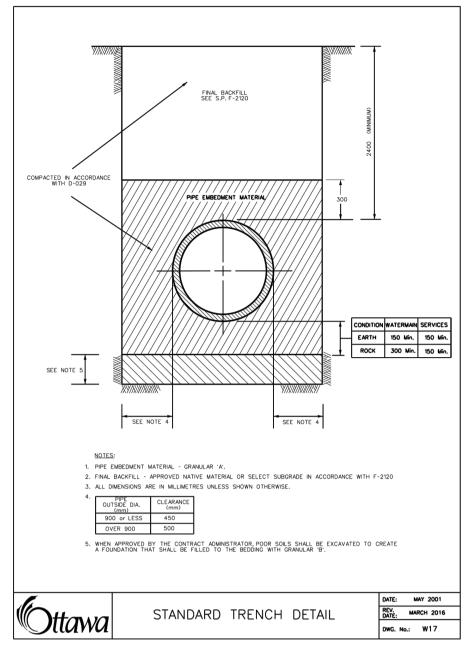
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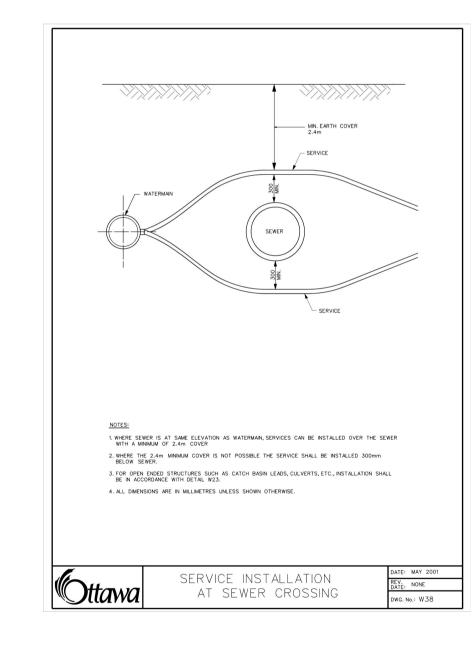
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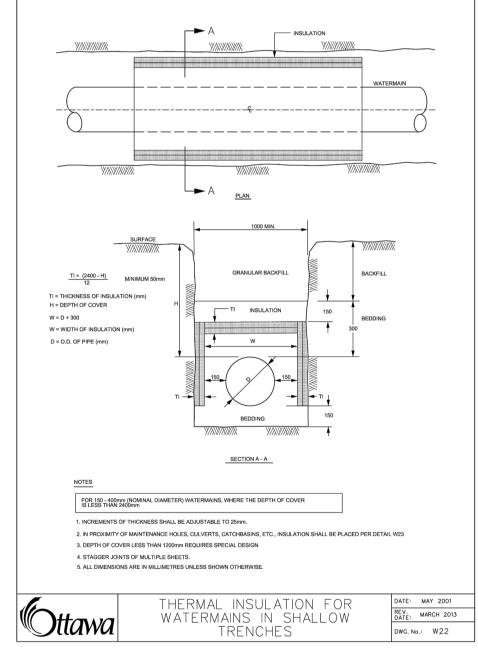
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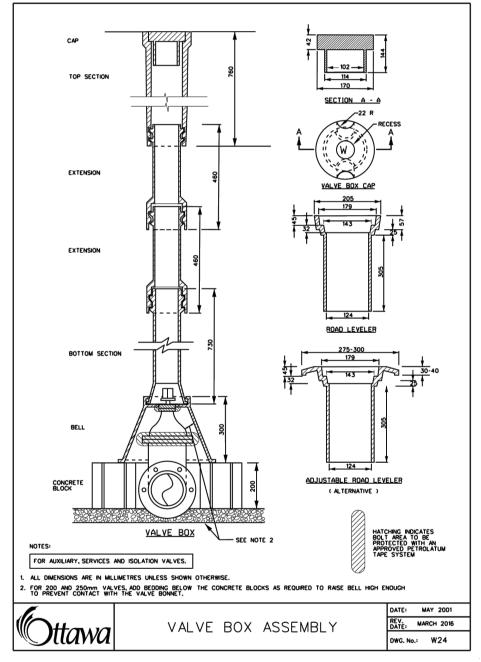












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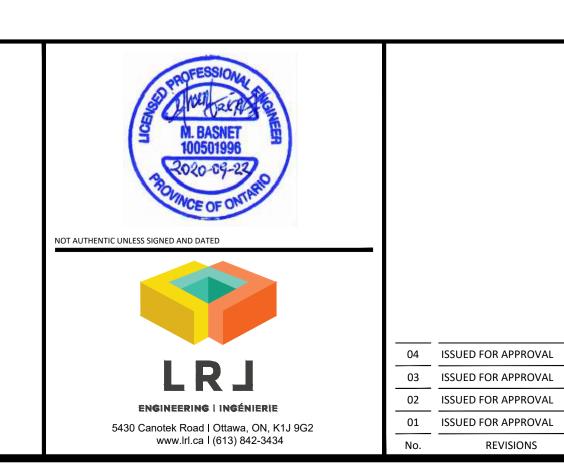
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DRAWING TITLE

CONSTRUCTION DETAILS PLAN

130828.05

A.S. 22 SEP 2020

A.S. 26 AUG 2020

A.S. 10 JUL 2020

M.L. 13 JAN 2020

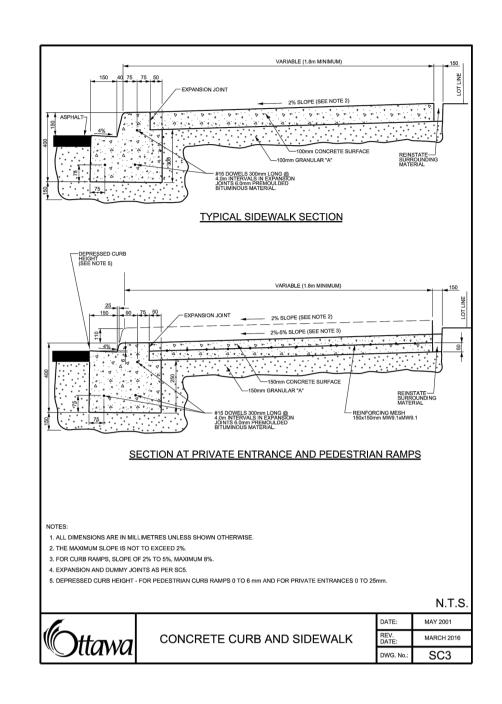
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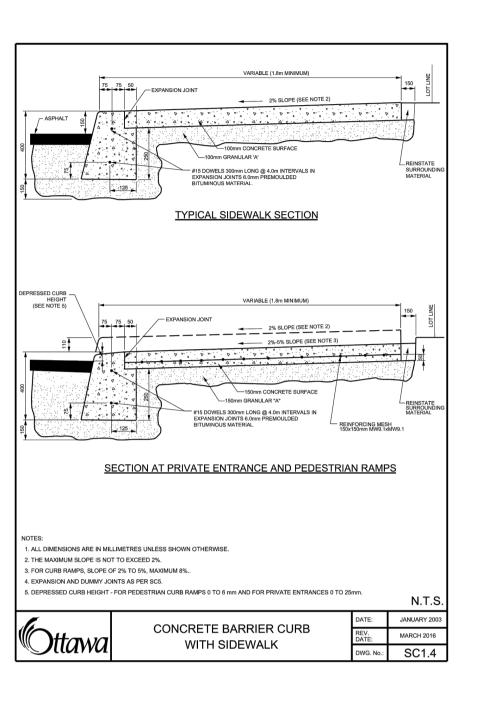
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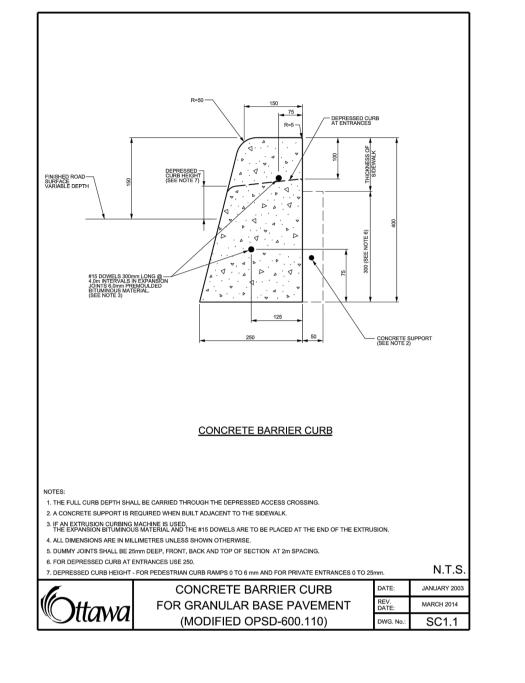
REVISIONS

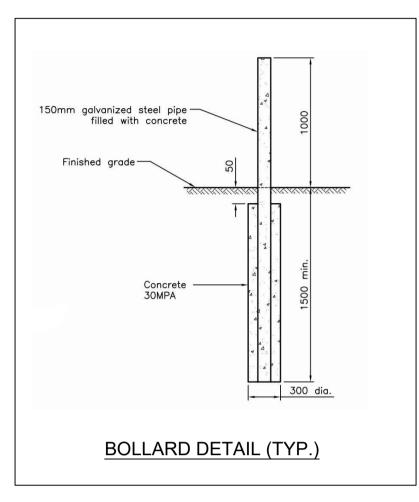
NOVEMBER 2019

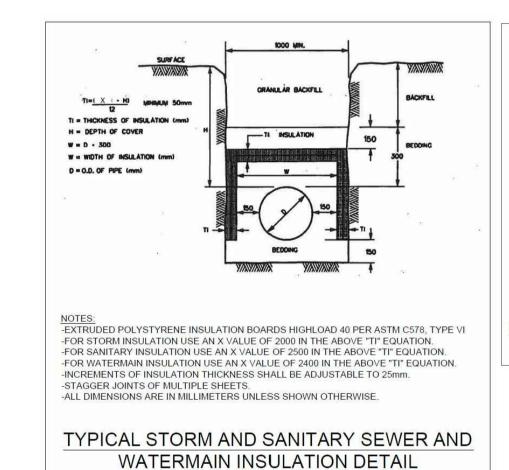
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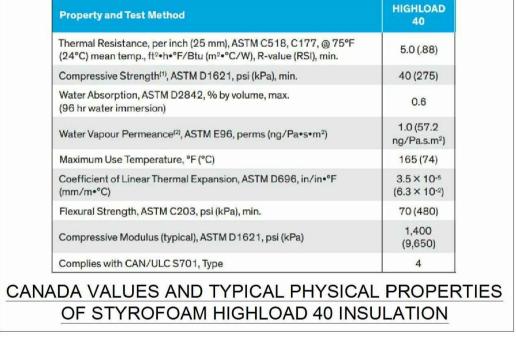


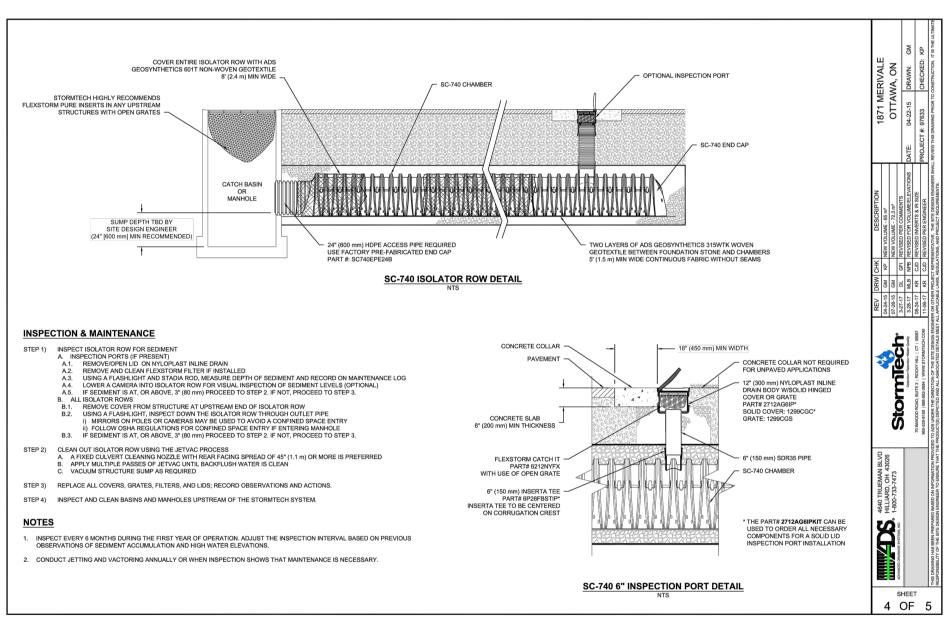


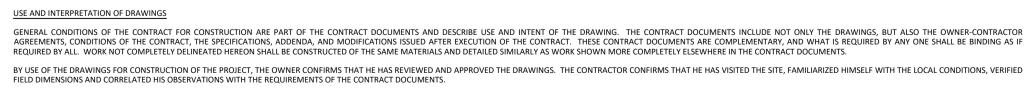




(N.T.S.)







AS INSTRUMENTS OF SERVICE, ALL DRAWINGS, SPECIFICATIONS, CADD FILES OR OTHER ELECTRONIC MEDIA AND COPIED THERE OF FURNISHED BY THE ENGINEER ARE HIS PROPERTY. THEY ARE TO BE USED ONLY FOR THIS PROJECT AND ARE NOT TO BE USED ON ANY OTHER PROJECT, INCLUDING REPEATS OF THE PROJECT. CHANGES TO THE DRAWINGS MAY ONLY BE MADE BY THE ENGINEER. UNLESS THE REVISION TITLE IS "ISSUED FOR CONSTRUCTION", THESE DRAWINGS SHALL BE CONSIDERED PRELIMINARY AND SHALL NOT BE USED AS A CONSTRUCTION DOCUMENT.

THESE DRAWINGS ILLUSTRATES THE WORK TO BE DONE. THE ENGINEER IS NOT RESPONSIBLE FOR THE MEANS, METHODS, TECHNIQUES, SEQUENCES, AND PROCEDURES USED TO DO THE WORK, OR THE SAFETY ASPECTS OF CONSTRUCTION, AND NOTHING ON THESE DRAWINGS EXPRESSED OR IMPLIED CHANGES THIS CONDITION. CONTRACTOR SHALL DETERMINE ALL CONDITIONS AT THE SITE AND SHALL BE RESPONSIBLE FOR KNOWING HOW THEY AFFECT THE WORK. SUBMITTAL OF A BID TO PERFORM THIS WORK IS ACKNOWLEDGEMENT OF THE RESPONSIBILITIES, AND THAT THEY HAVE BEEN FULLY CONSIDERED IN PLANNING OF THE WORK, AND THE BID PRICE. NO CLAIMS FOR EXTRA CHARGES DUE TO THESE CONDITIONS WILL BE FORTHCOMING. UNAUTHORIZED CHANGES:

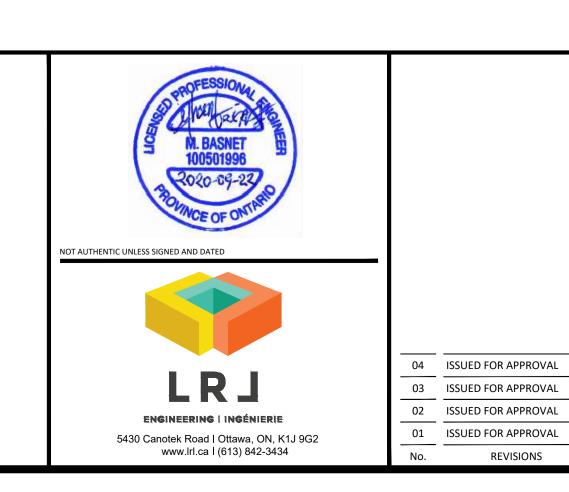
IN THE EVENT THE CLIENT, THE CLIENT, THE CLIENT, SONTRACTORS OR SUBCONTRACTORS, OR ANYONE FOR WHOM THE CLIENT IS LEGALLY LIABLE MAKES OR PERMITS TO BE MADE ANY CHANGES TO ANY REPORTS, PLANS, SPECIFICATIONS OR OTHER CONSTRUCTION DOCUMENTS PREPARED BY LRL ASSOCIATES LTD. (LRL) WITHOUT OBTAINING LRL'S PRIOR WRITTEN CONSENT, THE CLIENT SHALL ASSUME FULL RESPONSIBILITY FOR THE RESULTS OF SUCH CHANGES. THEREFORE THE CLIENT AGREES TO WAIVE ANY CLAIM AGAINST LRL AND TO RELEASE LRL

IN ADDITION, THE CLIENT AGREES, TO THE FULLEST EXTENT PERMITTED BY LAW, TO INDEMNIFY AND HOLD HARMLESS LRL FROM ANY DAMAGES, LIABILITIES OR COST, INCLUDING REASONABLE ATTORNEY'S FEES AND COST OF DEFENSE, ARISING FROM SUCH CHANGES. IN ADDITION, THE CLIENT AGREES TO INCLUDE IN ANY CONTRACTS FOR CONSTRUCTION APPROPRIATE LANGUAGE THAT PROHIBITS THE CONTRACTOR OR ANY SUBCONTRACTORS OF ANY TIER FROM MAKING ANY CHANGES OR MODIFICATIONS TO LRL'S CONSTRUCTION DOCUMENTS WITHOUT THE PRIOR WRITTEN APPROVAL OF LRL AND THAT FURTHER REQUIRES THE CONTRACTOR TO INDEMNIFY BOTH LRL AND THE CLIENT FROM ANY LIABILITY OR COST ARISING FROM SUCH CHANGES MADE WITHOUT SUCH PROPER AUTHORIZATION.

EXISTING SERVICES AND UTILITIES SHOWN ON THESE DRAWINGS ARE TAKEN FROM THE BEST AVAILABLE RECORDS, BUT MAY NOT BE COMPLETE OR TO DATE. CONTRACTOR SHALL VERIFY IN FIELD FOR LOCATION AND ELEVATION OF PIPES AND CHECK WITH THE UTILITY COMPANIES BEFORE DIGGING OR PERFORMING WORK.

CONTRACTOR IS ADVISED TO COLLECT INFORMATION ON SOIL CONDITIONS BEFORE START OF CONSTRUCTION.

THE ENGINEER WAIVES ANY AND ALL RESPONSIBILITY AND LIABILITY FOR PROBLEMS WHICH ARISE FROM FAILURE TO FOLLOW THESE PLANS, SPECIFICATIONS AND THE DESIGN INTENT THEY CONVEY, OR FOR PROBLEMS WHICH ARISE FROM OTHERS' FAILURE TO OBTAIN AND/OR FOLLOW THE ENGINEER'S GUIDANCE WITH RESPECT TO ANY ERRORS, OMISSIONS, INCONSISTENCIES AMBIGUITIES OR CONFLICTS WHICH ARE ALLEGED. CONTRACTOR TO VERIFY ALL DIMENSIONS AND NOTIFY THE ENGINEER OF ANY DISCREPANCIES BEFORE WORK COMMENCES. DO NOT SCALE DRAWINGS.



BENSON AUTO PARTS MR. GERRY BENSON 700 EDUCATION ROAD, CORNWALL, ONTARIO K6H 6B8 . TEL. 613-936-7850 V.J. M.S. V.J.

PROPOSED BENSON AUTO PARTS AND EAST BUILDING COMMERCIAL DEVELOPMENT 1871 MERIVALE ROAD, NEPEAN, ON

DRAWING TITLE

CONSTRUCTION DETAILS PLAN

130828.05

A.S. 22 SEP 2020

A.S. 26 AUG 2020

A.S. 10 JUL 2020

M.L. 13 JAN 2020

DATE

BY

REVISIONS

NOVEMBER 2019

000-

2

APPENDIX B

SWM Catchment Runoff Coefficient Calculations Storm Sewer Design Sheet

LRL Associates Ltd. Storm Design Sheet



LRL File No. 130828.05

Project: Benson Commercial Development- Building Replacement

Location: 1871 Merivale Rd., Nepean, ON

Date:August 2020Designed:Amr SalemDrawing Reference:C.702

SWM Catchment Runoff Coefficient Calculations

As per Original Site Plan Approval											
CATCHMENT	Grass C=0.20	River Stones C=0.70	Bldg. / Asph. / Conc. C=0.90	Total Area (ha)	Combined C						
CA-04	0.012	0.000	0.123	0.135	0.84						

Altered to Account for Proposed Site Changes											
CATCHMENT	Grass C=0.20	River Stones C=0.7	Bldg. / Asph. / Conc. C=0.90	Total Area (ha)	Combined C						
CA-01	0.008	0.045	0.108	0.161	0.81						
CA-02	0.006	0.000	0.138	0.144	0.87						
CA-03	0.003	0.000	0.136	0.139	0.88						

LRL Associates Ltd. Storm Design Sheet



LRL File No. 130828

 Project:
 Benson Auto-Parts

 Location:
 1871 Merivale

 Date:
 September 21, 2020

 Designed:
 Amr Salem

Drawing Reference: C.401

Storm Design Parameters

Rational Method Q = 2.78CIA

Q = Peak flow in litres per second (L/s)
A = Drainage area in hectares (ha)
C = Runoff coefficient

I = Rainfall intensity (mm/hr)

Runoff Coefficient (C)

 Grass
 0.20

 Gravel
 0.80

 Asphalt / rooftop
 0.90

Ottawa Macdonald-Cartier International Airport IDF curve

equation (5 year event, intensity in mm/hr)

 $I = 998.071 / (T_c + 6.053)^{0.814}$ Min. velocity = 0.80 m/s Manning's "n" = 0.013

LC	LOCATION			AREA (ha)		FLOW				STORM SEWER									
WATERSHED / STREET	From MH	То МН	C = 0.20	C = 0.80	C = 0.90	Indiv. 2.78AC	Accum. 2.78AC	Time of Conc. (min.)	Rainfall Intensity (mm/hr)	Peak Flow Q (L/s)	Controlled Flow Q (L/s)	Pipe Diameter (mm)	Туре	Slope (%)	Length (m)	Capacity Full (L/s)	Velocity Full (m/s)	Time of Flow (min.)	Ratio (Q/Q _{FULL})
	EX. ACCESS PORTS	STM CB3	0.000	0.015	0.000	0.034	0.03	10.00	104.2	3.50	2.34	250	HDPE	0.50%	175.0	42.0	0.86	3.40	0.08
CA01	STM CB3	STM MH2	0.000	0.000	0.000	0.000	0.03	13.40	89.1	2.99	1.90	250	PVC	2.00%	14.0	84.1	1.71	0.14	0.04
	CB1	STM MH2	0.01	0.02	0.13	0.375	0.38	10.00	104.2	39.10	4.24	250	PVC	1.00%	9.0	59.5	1.21	0.12	0.66
	STM MH2	EX. STM	0.00	0.02	0.00	0.000	0.41	13.54	88.6	36.22	4.24	250	PVC	0.40%	15.0	37.6	0.77	0.33	0.96

APPENDIX C

Proposed Building Water Demands



Water Supply Calculations LRL File No. 130828

Proposed Benson Commercial Development- Building Replacement Aug, 2020 Mohan Basnet Project

Date Designed:

Domestic Commercial Flow Demand

Total Building Floor Area = Site Total Area =	835 0.58	m² ha			(Proposed Building)
Total Fixture Unit (Hydraulic Load) =	33.6	ea.			(As per OBC, assume 8 water closet, and 8 lavatory sink
Average Demand Per Fixture Unit =	3.33	L/min			
Average Commercial Water Demand =	111.89	L/min	1.86	L/s	
Maximum Daily Peak Factor =	1.5				(As per City of Ottawa)
Maximum Daily Commercial =	167.83	L/d	2.80	L/s	
Maximum Hourly Peak Factor =	1.8				(As per City of Ottawa)
Maximum Hourly Commercial =	302.10	L/d	5.03	L/s	,

Therefore, Total Domestic Flow = Total Fire Flow = 5.03 L/s 133.3 L/s

APPENDIX D

FUS Fire Flow Calculation Fire Hydrant Location Figure



Fire Flow Calculations

LRL File No. 130828.04

Proposed Benson Commercial
Project Development- Building Replacement

Date August, 2020

Method Fire Underwriters Survey (FUS)

Prepared by Mohan Basnet

New Building	835	
	835	m ²

tep	Task	Term	Options	Multiplier	Choose:	Value	unit	Fire Flow
			Structural Framing M	aterial				
			Wood Frame	1.5				
		Coefficient C	Ordinary Construction	1.0			İ	
1	Choose frame used for building	related to the type of	Non-combustible construction	0.8	Ordinary Construction	1	İ	
	building	construction	Fire resistive construction <2 hrs	0.7			İ	
			Fire resistive construction >2 hrs	0.6			ľ	
			Structural Framing Material					
	0, , ,		Single family dwelling	0				
2	Choose type of housing	Type of housing	Townhouse - no. of units	0	Building - no. of units per floor	1	units	
2	liousing		Building - no. of units per floor	1				
	Enter no. of storeys	Number of floors/storey	rs for the building (excluding the basement)			1		
3	Enter area of a unit	Enter floor space area	of one unit	1	835.0	835	sq.m.	
,	Obtain fire flow before	Doguirod fire flow	Fire Fla	220 0	A A0.5		units floor sq.m. L/min L/s L/min L/s L/min L/s L/min L/s	6,000
4	reductions	Required life flow	Fire Fio	W = 220 X C X	Area		L/s	100.0
			Reductions or surcharge due to fact	ors affecting l	burning			
		ilit. Occurrency beyond	Non-combustible	-0.25				
	Choose combustibility		Limited combustible	-0.15				
5	of contents		Combustible	0	Combustible	0		
	or contents	Todaction of surcharge	Free burning	0.15			L/min	6,000
			Rapid burning	0.25			L/s	100.0
				-0.30	False	0	L/min L/s L/min L/s L/min L/s L/min L/s L/min L/s	
6	Choose reduction for sprinklers	Sprinkler reduction		-0.10	False	0	L/min	6,000
			Fully supervised system	-0.10	False	0	L/s	100.0
			North side	20.1 to 30m	0.1			
7	Chassa sonaration	Exposure distance	East side	Over 45m	0			
1	Choose separation	between units	South side	Over 45m	0		L/min	8,000
			West side	3.1 to 10m	0.2	0.3	L/s	133.3
			Net required fire fl	ow				
2 Chh E E E E C C C C C C C C C C C C C C	Obtain fire flow.			Minimum	required fire flow rate (rounded to ne	earest 1000)	L/min	8,000
8	duration, and volume				Minimum required	fire flow rate	L/s	133.3
	daradon, and volume				Required duratio	n of fire flow	hr	2





SCALE: N.T.S.

CLIENT BENSON COMMERCIAL DEVELOPMENT

DATE PROJECT
MAY 13, 2020

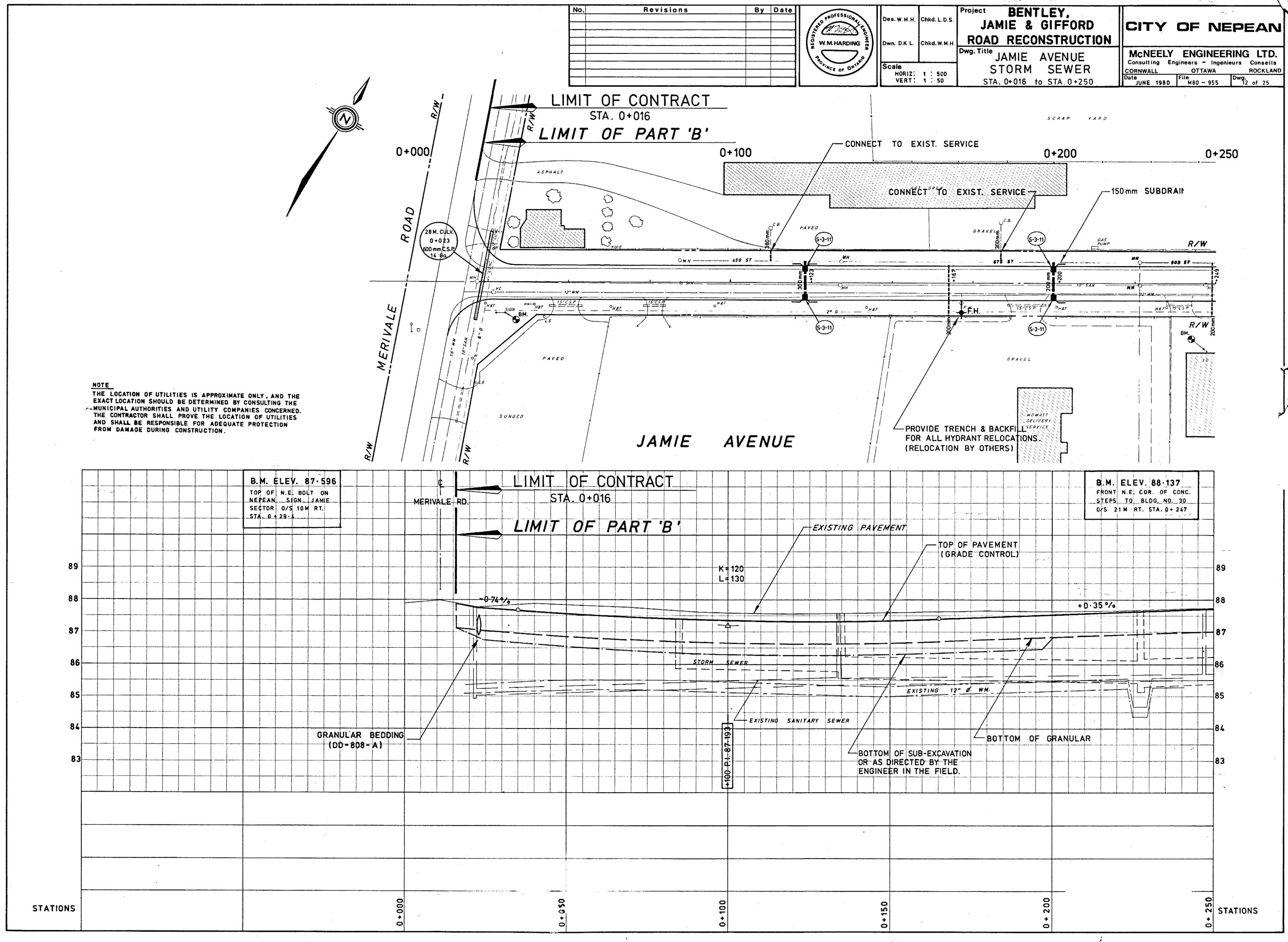
PROJECT
MAY 13, 2020

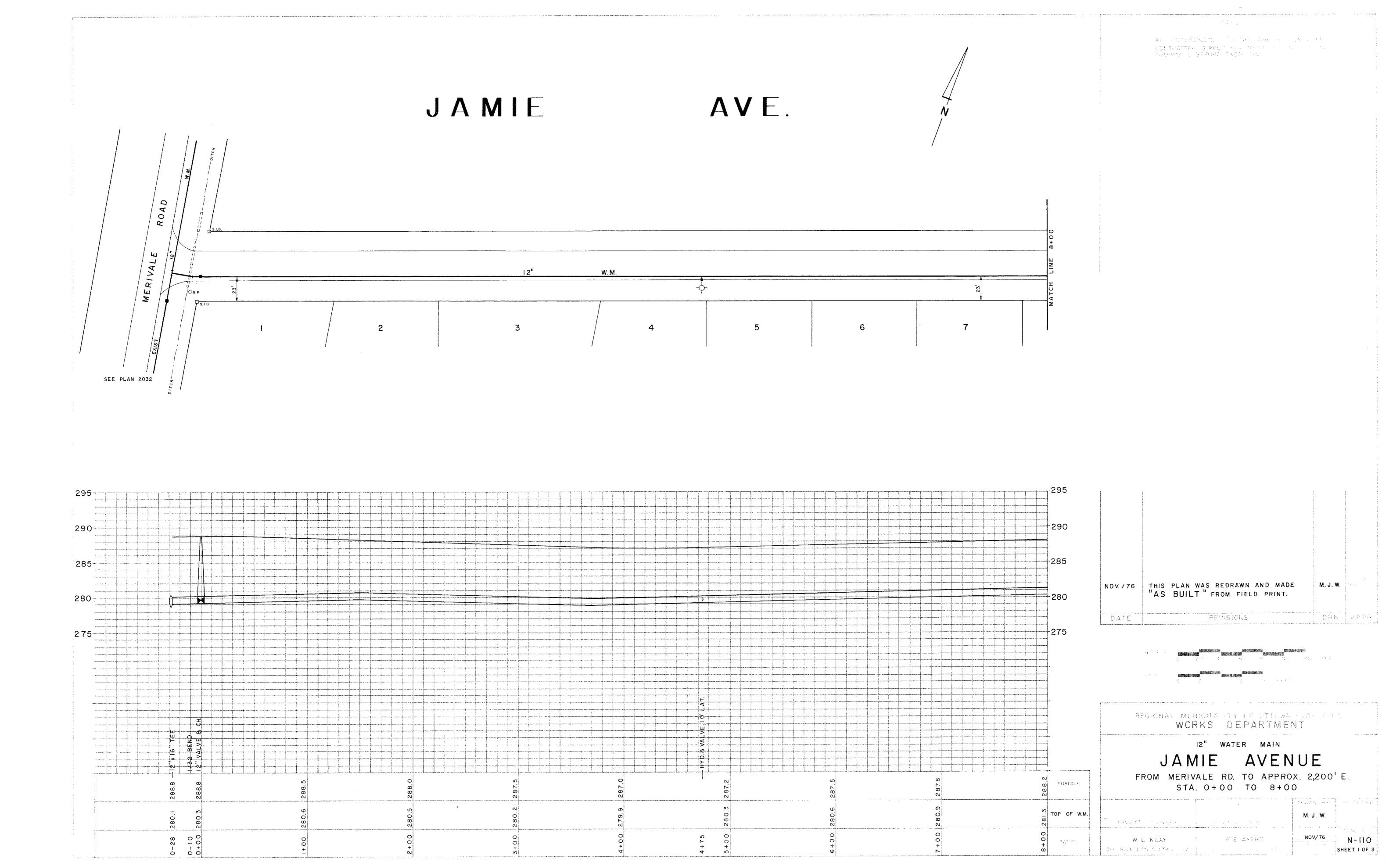
130828

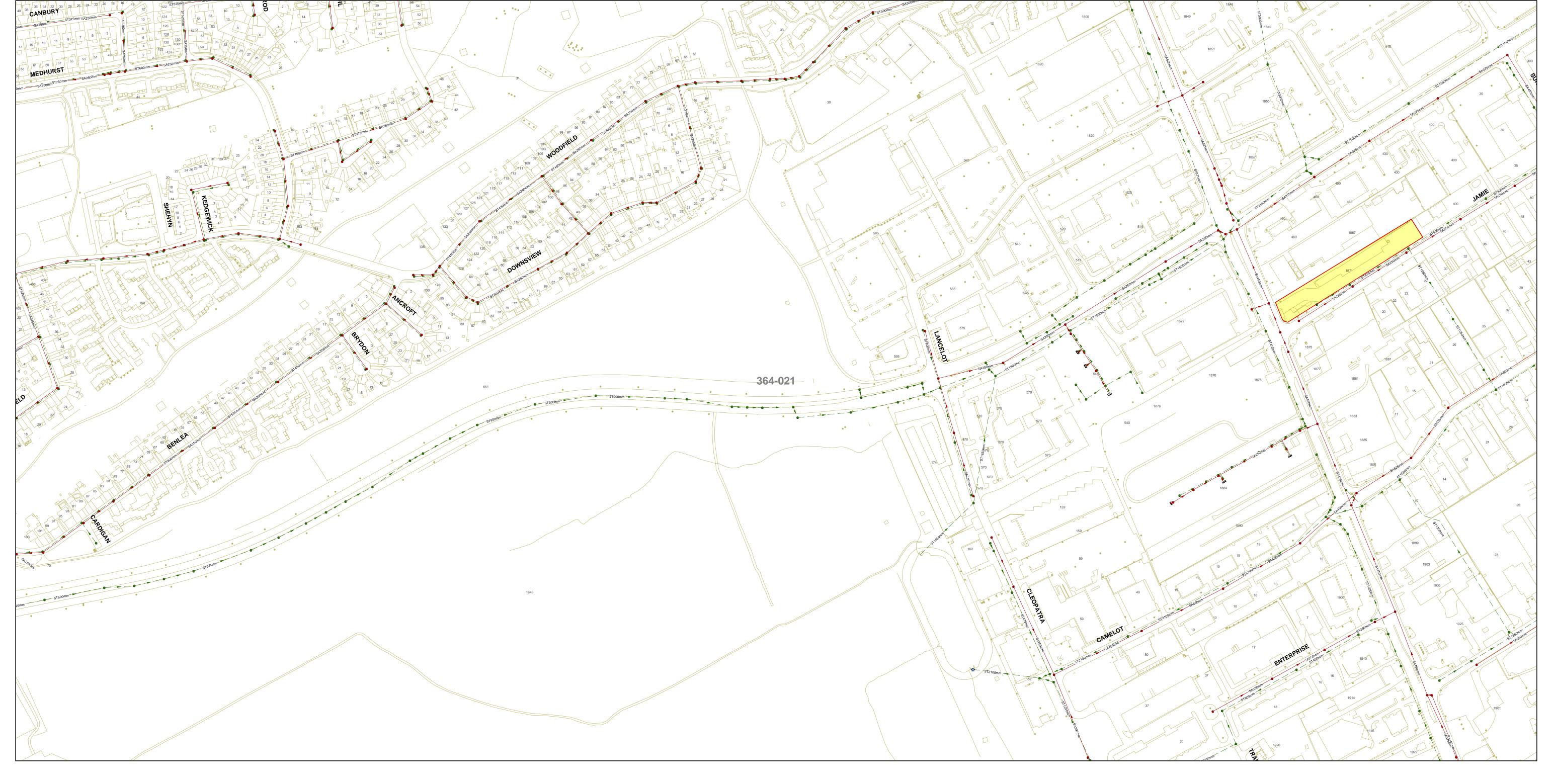


APPENDIX E

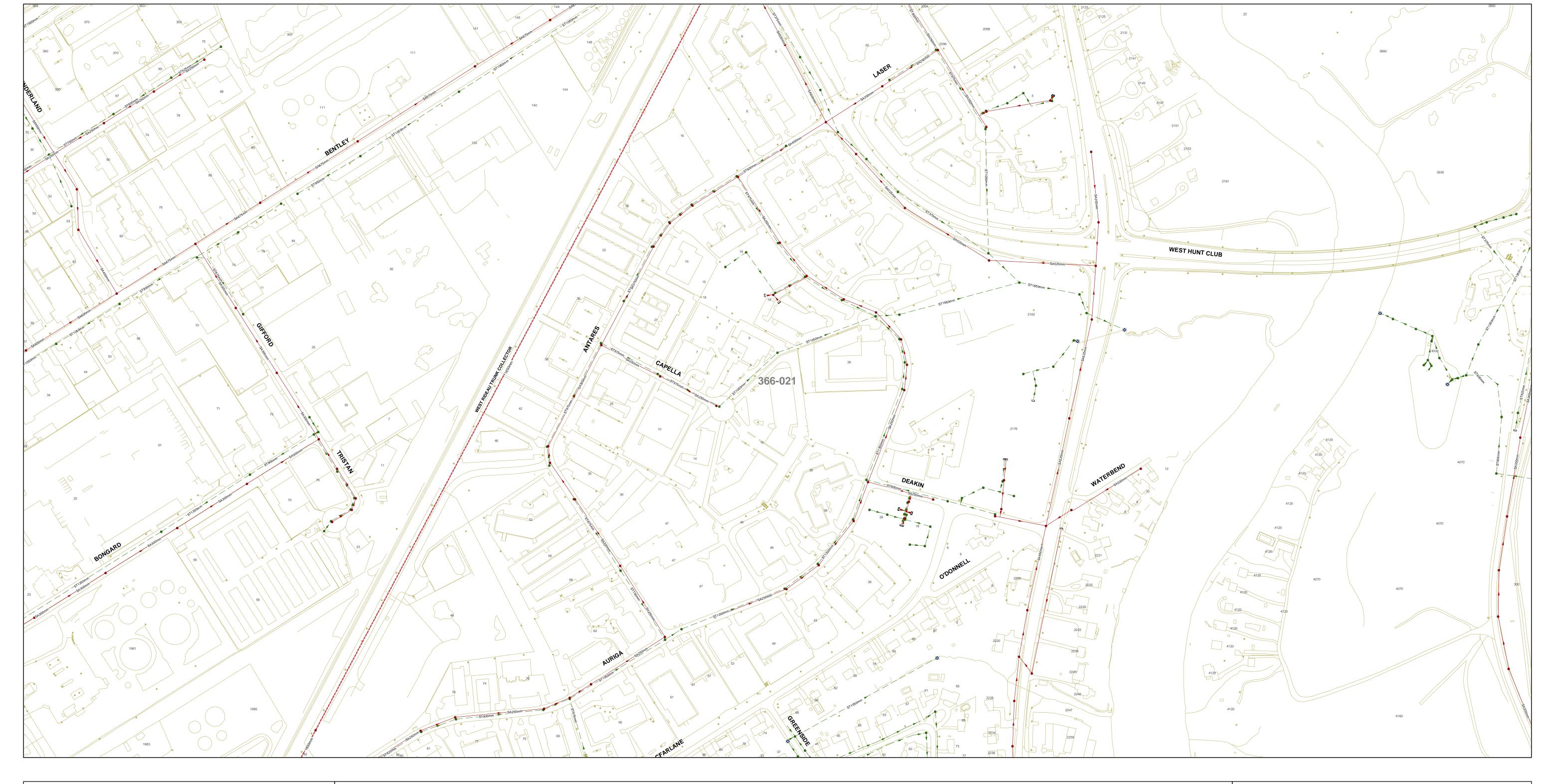
Jamie Avenue As-Builts and Sanitary Mapping







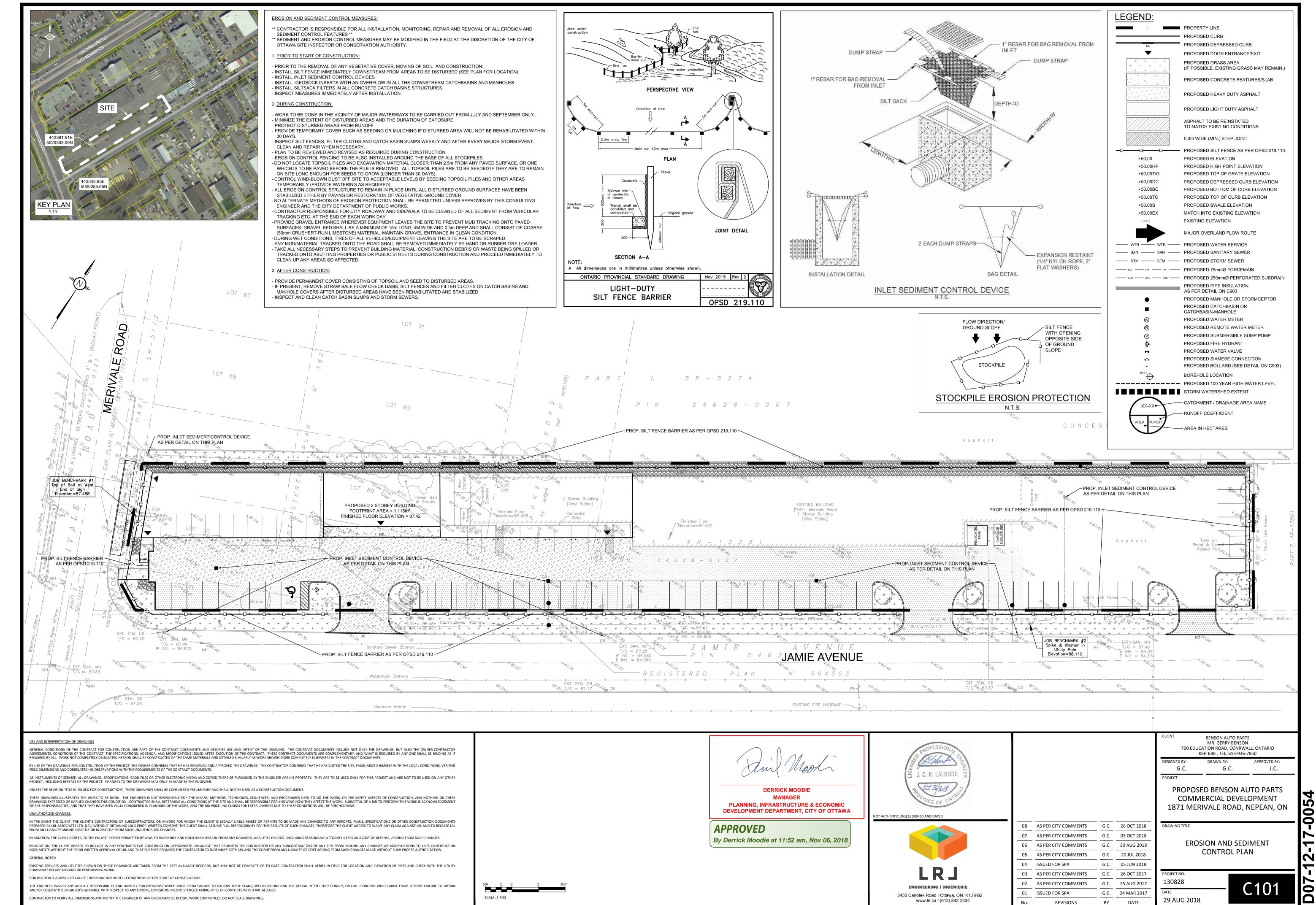


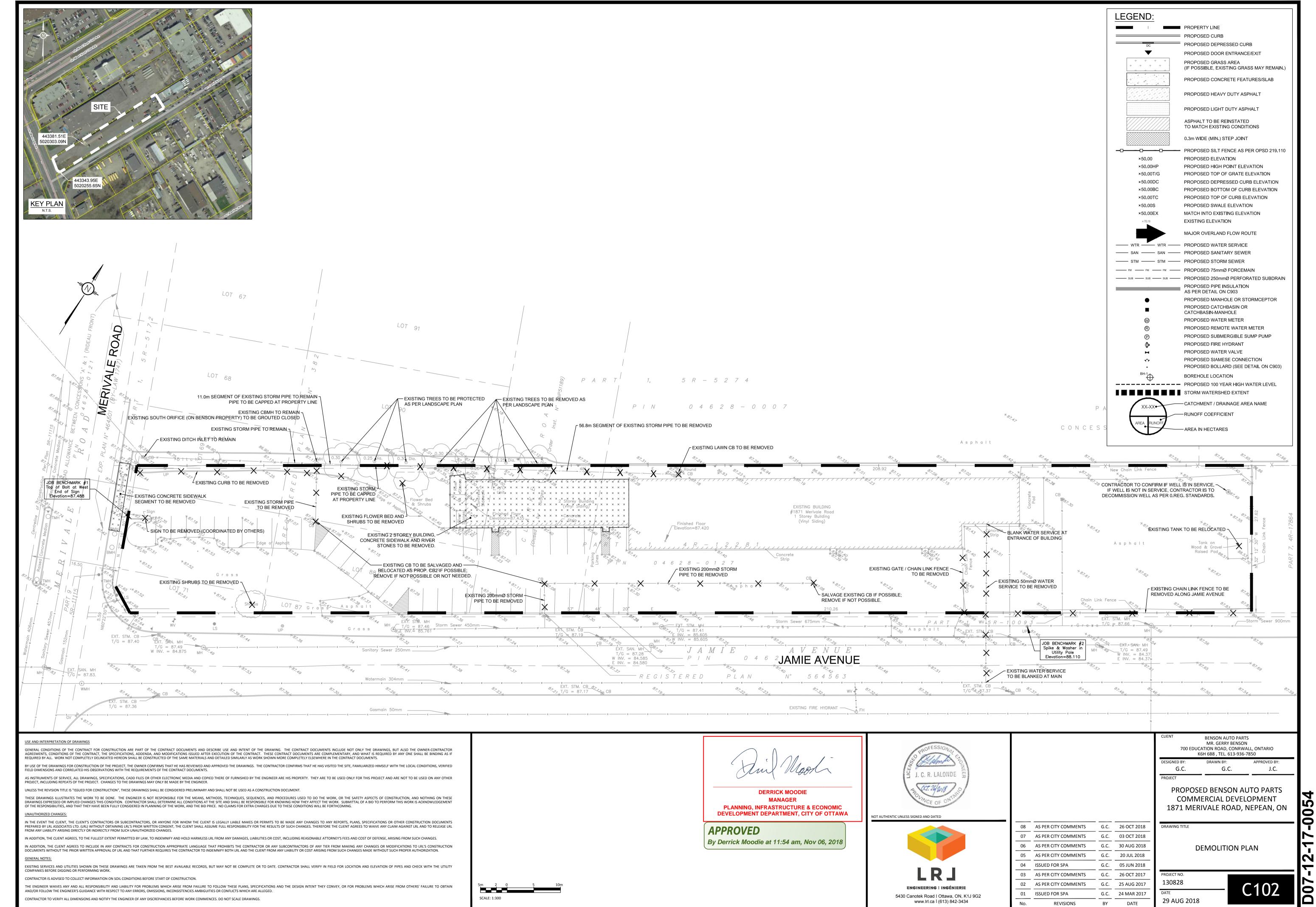




Appendix F

Civil Engineering Drawings (Phase 1)





MATCH INTO EXIST. S/W = 87.42 -

87-31BC

87.41T0

MATCH INTO/EXIST, S/W 1

PROP. SWALE @ 1.5% SLOPE ~

JOB BENCHMARK #1 Top of Bolt at West End of Sign Elevation=87.488

PROP. 2.0m WIDE RAISED S/W

MATCH INTO EXIST. S/W ~

MA#CH,INTO EXIST. S/W |= 87.58 -

AS PER DETAIL SC1.4 ON C903

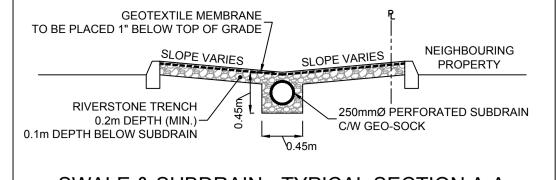
87.46BC

87.56TC

T/G = 87.83.

CONTRACTOR TO VERIFY ALL DIMENSIONS AND NOTIFY THE ENGINEER OF ANY DISCREPANCIES BEFORE WORK COMMENCES. DO NOT SCALE DRAWINGS.

AS PER DETAIL SC3 ON C903



SWALE & SUBDRAIN - TYPICAL SECTION A-A (N.T.S.)

PAVEMENT STRUCTURE

		THICKNESS (mm)		
COURSE	MATERIAL	AUTOMOBILE PARKING	TRUCK ROUTE (HEAVY TRAFFIC)	
SURFACE	HL.3 A/C (PG 58-28)	A/C (PG 58-28) 50 40		
BINDER	HL.8 A/C (PG 58-28)		40	
BASECOURSE	GRANULAR "A"	JULAR "A" 150		
SUBBASE	GRANULAR "B" TYPE II	250	350	

IN PREPARATION FOR PAVEMENT CONSTRUCTION AT THIS SITE, ANY SURFICIAL OR NEAR SURFACE/SUBGRADE LEVEL TOPSOIL AND ANY SOFT, WET OR DELETERIOUS MATERIALS SHOULD BE REMOVED FROM THE PROPOSED PAVED AREAS. THE EXPOSED SUBGRADE SHOULD BE INSPECTED AND APPROVED BY GEOTECHNICAL PERSONNEL AND ANY SOFT AREAS EVIDENT SHOULD BE SUBEXCAVATED AND REPLACED WITH SUITABLE EARTH BORROW APPROVED BY THE GEOTECHNICAL ENGINEER. THE SUBGRADE SHOULD BE SHAPED AND CROWNED TO PROMOTE DRAINAGE OF THE SITE CB'S. FOLLOWING APPROVAL OF THE PREPARATION OF THE SUBGRADE, THE PAVEMENT GRANULARS MAY BE PLACED.

♥PROP. GROUND ELEV. = 87.30 -

(Vinyl Siding)

BROP BOLLARD (TYP.)

SEE DETAIL ON C903 0 4 6 2 8 - 0 1 2 7

REGISTERED

SUBDRAIN INV. = 86.49

5 R - 5 2 7 4

0 4 6 2 8 - 0 0 0 7

GENERAL NOTES:

- ALL EDGES OF DISTURBED PAVEMENT SHALL BE SAW CUT TO FORM A CLEAN CUT LINE PRIOR TO PLACING NEW PAVEMENT. PAVEMENT REINSTATEMENT SHALL BE WITH STEP JOINTS OF 500mm WIDTH MINIMUM.
- CURBS TO BE BARRIER, CONSTRUCTED AS PER DETAIL SC1.1 ON C903.
- ALL SIDEWALK CONSTRUCTION TO BE AS PER DETAILS SC1.4 AND SC2 ON C903.
- ALL MATERIAL SUPPLIED AND PLACED FOR PARKING LOT AND ACCESS ROAD CONSTRUCTION SHALL BE TO OPSS STANDARDS AND SPECIFICATIONS UNLESS OTHERWISE NOTED. CONSTRUCTION TO OPSS 206, 310 & 314. MATERIALS TO OPSS 1001,
- OBTAIN AND PAY FOR ALL NECESSARY PERMITS AND APPROVALS FROM THE MUNICIPAL AUTHORITIES PRIOR TO COMMENCING CONSTRUCTION; SUCH AS, BUT NOT LIMITED TO: ROAD CUT PERMITS, SEWER PERMITS, WATER PERMIT, ETC. THE APPROVAL OF THIS PLAN DOES NOT EXEMPT THE CONTRACTOR FROM THE REQUIREMENTS TO OBTAIN THE VARIOUS PERMITS/APPROVALS REQUIRED TO COMPLETE THE CONSTRUCTION PROJECT.
- INLET SEDIMENT CONTROL DEVICES TO BE INSTALLED AND MAINTAINED BETWEEN THE FRAME AND COVER OF ALL CATCHBASINS AND CATCHBASIN MANHOLES DURING THE CONSTRUCTION PERIOD TO MINIMIZE SEDIMENTS ENTERING THE STORM SEWER SYSTEM. ALL GRASSED AREAS MUST BE COMPLETED PRIOR TO THE REMOVAL OF THE FILTER FABRIC IN THE CATCH BASINS.
- REMOVE FROM SITE ALL EXCESS EXCAVATED MATERIAL UNLESS OTHERWISE DIRECTED FROM THE ENGINEER. EXCAVATE AND REMOVE ALL ORGANIC MATERIAL AND DEBRIS, IF ANY, LOCATED WITHIN THE PROPOSED BUILDING, PARKING AND ROADWAY LOCATIONS.

UTILITY NOTES:

- 1. UNDERGROUND UTILITIES, AS REPORTED ON THIS DRAWING, ARE NOT BASED ON AN ACTUAL 'FIELD LOCATE' BY THE RESPECTIVE UTILITY AGENCIES BUT HAVE BEEN COMPILED FROM DATA OBTAINED FROM THE CITY OF OTTAWA PUBLIC UTILITIES
- BEFORE ANY WORK INVOLVING PROBING, EXCAVATING, ETC., CONTRACTOR TO CONFIRM RELEVANT UTILITY LOCATIONS AND REPORT ANY DISCREPANCIES TO THE ENGINEER PRIOR TO COMMENCING WORK.

SURVEY NOTES:

PROP. 250mmØ PERFORATED SUBDRAIN @ 0.5% -

EXISTING BUILDING

#1871 Merivale Road

564563

EXISTING FIRE HYDRANT -

1 Storey Building

1. CONFIRM JOB BENCHMARKS SHOWN ON PLANS WITH ENGINEER PRIOR TO UTILIZATION.

PROP. RIVERSTONE

BEARINGS HEREON ARE GRID BEARINGS AND ARE DERIVED FROM NCC HORIZONTAL CONTROL MONUMENTS 019710637 (N 5022465.812, E 365416.840) AND 019861625 (N 5022141.837, E 363270.732) AND ARE REFERRED TO THE CENTRAL MERIDIAN 76°30'W LONGITUDE, ZONE 9 OF THE 3° M.T.M. ONTARIO COORDINATE SYSTEM (NAD 83).

Asphalt

PROPERTY LINE PROPOSED CURB PROPOSED DEPRESSED CURB

×50.00S

×50.00EX

LEGEND:

PROPOSED DOOR ENTRANCE/EXIT PROPOSED GRASS AREA (IF POSSIBLE, EXISTING GRASS MAY REMAIN.) PROPOSED CONCRETE FEATURES/SLAB

PROPOSED HEAVY DUTY ASPHALT

PROPOSED LIGHT DUTY ASPHALT

ASPHALT TO BE REINSTATED TO MATCH EXISTING CONDITIONS

0.3m WIDE (MIN.) STEP JOINT --- PROPOSED SILT FENCE AS PER OPSD 219.110 _____

> ×50.00 PROPOSED ELEVATION ×50.00HP PROPOSED HIGH POINT ELEVATION ×50.00T/G PROPOSED TOP OF GRATE ELEVATION ×50.00DC PROPOSED DEPRESSED CURB ELEVATION

> PROPOSED BOTTOM OF CURB ELEVATION ×50.00TC PROPOSED TOP OF CURB ELEVATION

PROPOSED SWALE ELEVATION MATCH INTO EXISTING ELEVATION EXISTING ELEVATION

MAJOR OVERLAND FLOW ROUTE

WTR — PROPOSED WATER SERVICE ---- SAN ----- PROPOSED SANITARY SEWER ----- STM ------ PROPOSED STORM SEWER ---- FM ---- FM ---- PROPOSED 75mmØ FORCEMAIN

PROPOSED PIPE INSULATION AS PER DETAIL ON C903

PROPOSED MANHOLE OR STORMCEPTOR PROPOSED CATCHBASIN OR CATCHBASIN-MANHOLE PROPOSED WATER METER

PROPOSED REMOTE WATER METER PROPOSED SUBMERGIBLE SUMP PUMP PROPOSED FIRE HYDRANT

PROPOSED WATER VALVE PROPOSED SIAMESE CONNECTION PROPOSED BOLLARD (SEE DETAIL ON C903) BOREHOLE LOCATION

PROPOSED 100 YEAR HIGH WATER LEVEL STORM WATERSHED EXTENT - CATCHMENT / DRAINAGE AREA NAME

XX-XX -RUNOFF COEFFICIENT - AREA IN HECTARES

PROP. GOUND ELEV. = 87.40 7 PROP. 250mmØ PERFORATED -SUBDRAIN INV. = 87.05 / SUBDRAIN @ 2.90%

T/G = 87.12 -

JOB BENCHMARK #2

Utility Pole

06 AS PER CITY COMMENTS

05 AS PER CITY COMMENTS

03 AS PER CITY COMMENTS

02 AS PER CITY COMMENTS

REVISIONS

04 ISSUED FOR SPA

01 ISSUED FOR SPA

SUBDRAIN INV. = 86.14

– PROP. 250mmØ NON-PERFORÅTED SUBDRAIN @ 6.00%| — INV.=85.58 TEMPORARY SNOW STORAGE LOCATION -SNOW TO BE REMOVED FROM SITE

> ASPHALT REINSTATEMENT SHALL MATCH EXISTING GRANULAR AND ASPHALT THICKNESS WHILE MAINTAINING A MINIMUM OF 40mm OF HL-3,

50mm OF HL-8, 150mm OF GRANULAR 'A' AND 300mm OF GRANULAR 'B'. REFER TO DETAIL R10 ON C902. A MINIMUM 0.3m WIDE STEP JOINT SHALL ALSO BE PROVIDED.

PROP. ENTRANCE AS PER -

(UNSIGNALIZED)

CITY OF OTTAWA DETAIL SC7.1

J. C. R. LALONDE OCT. 26/2018

NOT AUTHENTIC UNLESS SIGNED AND DATED

5430 Canotek Road | Ottawa, ON, K1J 9G2 www.lrl.ca I (613) 842-3434

PROPOSED BENSON AUTO PARTS COMMERCIAL DEVELOPMENT 1871 MERIVALE ROAD, NEPEAN, ON 08 AS PER CITY COMMENTS G.C. 26 OCT 2018 07 AS PER CITY COMMENTS G.C. 03 OCT 2018

G.C. 30 AUG 2018

G.C. 20 JUL 2018

BY

G.C. 05 JUN 2018

DATE

E INV. = $84.37 \frac{1}{5}$

GRADING AND DRAINAGE PLAN

BENSON AUTO PARTS MR. GERRY BENSON 700 EDUCATION ROAD, CONRWALL, ONTARIO

K6H 6B8, TEL. 613-936-7850

G.C.

G.C. 26 OCT 2017 130828 G.C. 25 AUG 2017 G.C. 24 MAR 2017

29 AUG 2018

PROJEC^{*}

Gasmain 50mm —— GENERAL CONDITIONS OF THE CONTRACT FOR CONSTRUCTION ARE PART OF THE CONTRACT DOCUMENTS AND DESCRIBE USE AND INTENT OF THE DRAWING. THE CONTRACT DOCUMENTS INCLUDE NOT ONLY THE DRAWINGS. BUT ALSO THE OWNER-CONTRACTOR REQUIRED BY ALL. WORK NOT COMPLETELY DELINEATED HEREON SHALL BE CONSTRUCTED OF THE SAME MATERIALS AND DETAILED SIMILARLY AS WORK SHOWN MORE COMPLETELY ELSEWHERE IN THE CONTRACT DOCUMENTS. BY USE OF THE DRAWINGS FOR CONSTRUCTION OF THE PROJECT, THE OWNER CONFIRMS THAT HE HAS REVIEWED AND APPROVED THE DRAWINGS. THE CONTRACTOR CONFIRMS THAT HE HAS VISITED THE SITE, FAMILIARIZED HIMSELF WITH THE LOCAL CONDITIONS, VERIFIED FIELD DIMENSIONS AND CORRELATED HIS OBSERVATIONS WITH THE REQUIREMENTS OF THE CONTRACT DOCUMENTS. AS INSTRUMENTS OF SERVICE, ALL DRAWINGS, SPECIFICATIONS, CADD FILES OR OTHER ELECTRONIC MEDIA AND COPIED THERE OF FURNISHED BY THE ENGINEER ARE HIS PROPERTY. THEY ARE TO BE USED ONLY FOR THIS PROJECT AND ARE NOT TO BE USED ON ANY OTHER PROJECT, INCLUDING REPEATS OF THE PROJECT. CHANGES TO THE DRAWINGS MAY ONLY BE MADE BY THE ENGINEER. UNLESS THE REVISION TITLE IS "ISSUED FOR CONSTRUCTION", THESE DRAWINGS SHALL BE CONSIDERED PRELIMINARY AND SHALL NOT BE USED AS A CONSTRUCTION DOCUMENT DRAWINGS EXPRESSED OR IMPLIED CHANGES THIS CONDITION. CONTRACTOR SHALL DETERMINE ALL CONDITIONS AT THE SITE AND SHALL BE RESPONSIBLE FOR KNOWING HOW THEY AFFECT THE WORK. SUBMITTAL OF A BID TO PERFORM THIS WORK IS ACKNOWLEDGEMENT OF THE RESPONSIBILITIES, AND THAT THEY HAVE BEEN FULLY CONSIDERED IN PLANNING OF THE WORK, AND THE BID PRICE. NO CLAIMS FOR EXTRA CHARGES DUE TO THESE CONDITIONS WILL BE FORTHCOMING. IN THE EVENT THE CLIENT, THE CLIENT, THE CLIENT, SONTRACTORS, OR ANYONE FOR WHOM THE CLIENT IS LEGALLY LIABLE MAKES OR PERMITS TO BE MADE ANY CHANGES TO ANY REPORTS, PLANS, SPECIFICATIONS OR OTHER CONSTRUCTION DOCUMENTS PREPARED BY LRL ASSOCIATES LTD. (LRL) WITHOUT OBTAINING LRL'S PRIOR WRITTEN CONSENT, THE CLIENT SHALL ASSUME FULL RESPONSIBILITY FOR THE RESULTS OF SUCH CHANGES. THEREFORE THE CLIENT AGREES TO WAIVE ANY CLAIM AGAINST LRL AND TO RELEASE LRL IN ADDITION, THE CLIENT AGREES, TO THE FULLEST EXTENT PERMITTED BY LAW, TO INDEMNIFY AND HOLD HARMLESS LRL FROM ANY DAMAGES, LIABILITIES OR COST, INCLUDING REASONABLE ATTORNEY'S FEES AND COST OF DEFENSE, ARISING FROM SUCH CHANGES. IN ADDITION. THE CLIENT AGREES TO INCLUDE IN ANY CONTRACTS FOR CONSTRUCTION APPROPRIATE LANGUAGE THAT PROHIBITS THE CONTRACTOR OR ANY SURCONTRACTORS OF ANY TIER FROM MAKING ANY CHANGES OR MODIFICATIONS TO LRI'S CONSTRUCTION

ASPHALT REINSTATEMENT SHALL MACTH EXISTING GRANULAR AND -

A MINIMUM 0.3m WIDE STEP JOINT SHALL ALSO BE PROVIDED.

REFER TO DETAIL R10 ON C902.

ASPHALT THICKNESS WHILE MAINTAINING A MINIMUM OF 40mm OF HL-3,

50mm OF HL-8, 150mm OF GRANULAR 'A' AND 300mm OF GRANULAR 'B'.

LOT 68

PROP. GOUND ELEV. = 87.21

SUBDRAIN INV = 86.86

87.31DC

W INV. = 84.875

PROP. 250mmØ PERFORATED SUBDRAIN @ 0.5%

PROP. RIVERSTONE

PROP. 2.0m WIDE

- PROP. ENTRANCE AS PER

(UNSIGNALIZED)

CITY OF OTTAWA DETAIL SC7.1

/ DÉPRESSED S/W AS PER [

PROP. MÁXIMUM ÖVERLAND FLOW SPILLWAY

SCALE: 1:300

AS PER OPSD 605.040

DETAIL SC14 ON C903

PROPOSED 2 STOREY BUILDING

FOOTPRINT AREA = 1,115m2

FINISHED FLOOR ELEVATION = 87.42

DOCUMENTS WITHOUT THE PRIOR WRITTEN APPROVAL OF LRL AND THAT FURTHER REQUIRES THE CONTRACTOR TO INDEMNIFY BOTH LRL AND THE CLIENT FROM ANY LIABILITY OR COST ARISING FROM SUCH CHANGES MADE WITHOUT SUCH PROPER AUTHORIZATION. GENERAL NOTES: EXISTING SERVICES AND UTILITIES SHOWN ON THESE DRAWINGS ARE TAKEN FROM THE BEST AVAILABLE RECORDS. BUT MAY NOT BE COMPLETE OR TO DATE. CONTRACTOR SHALL VERIFY IN FIELD FOR LOCATION AND ELEVATION OF PIPES AND CHECK WITH THE UTILITY

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PLANNING, INFRASTRUCTURE & ECONOMIC

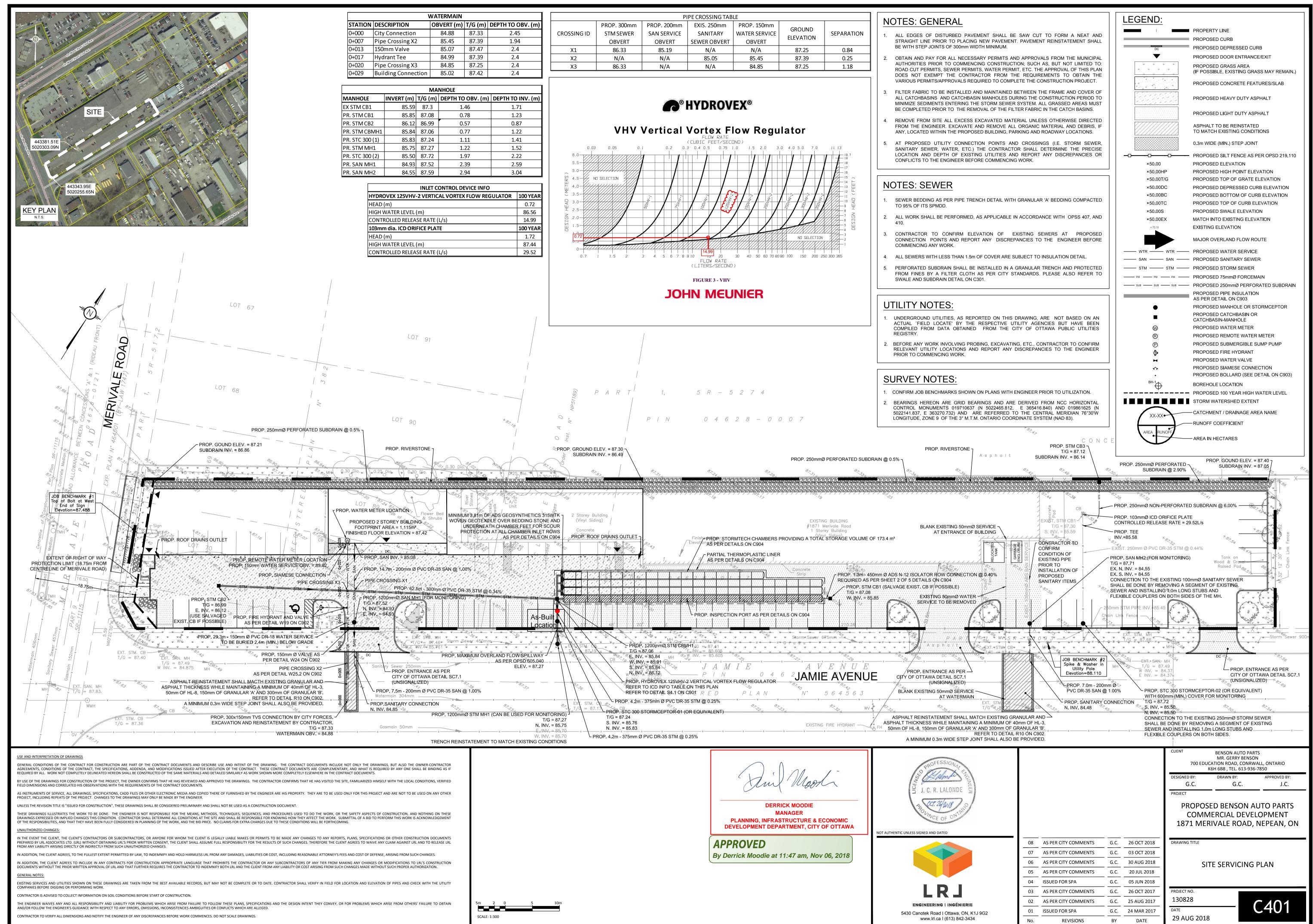
DEVELOPMENT DEPARTMENT, CITY OF OTTAWA

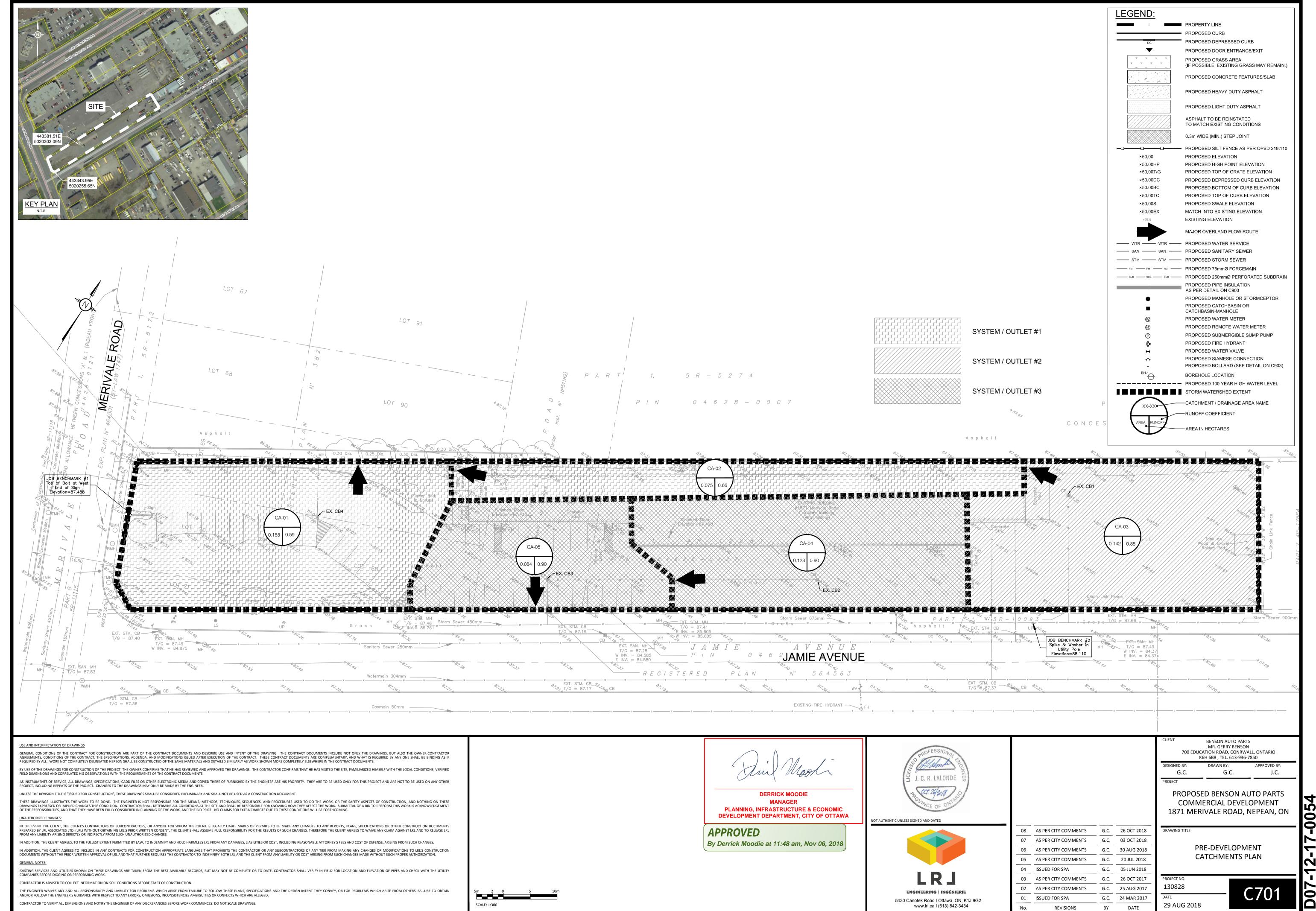
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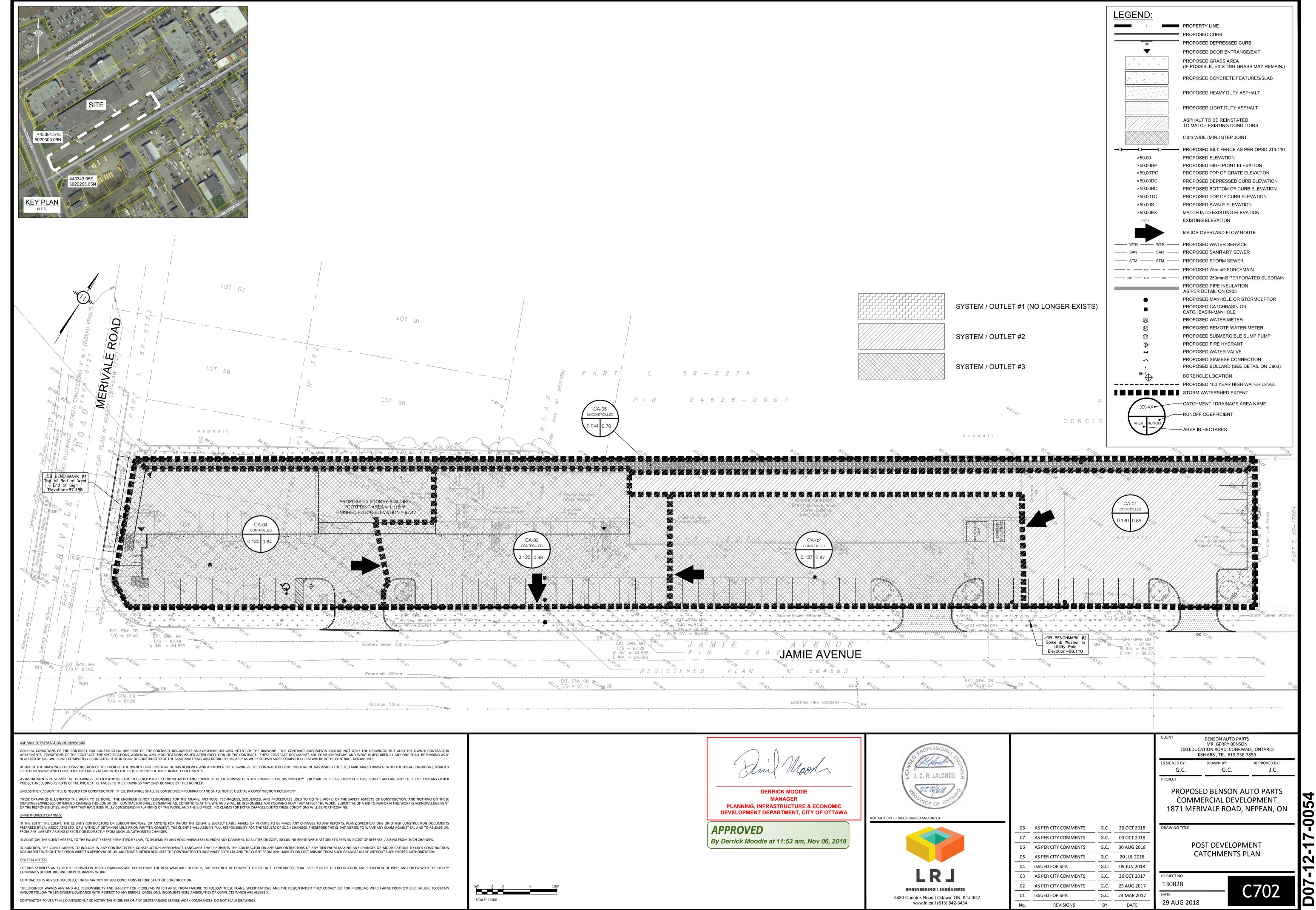
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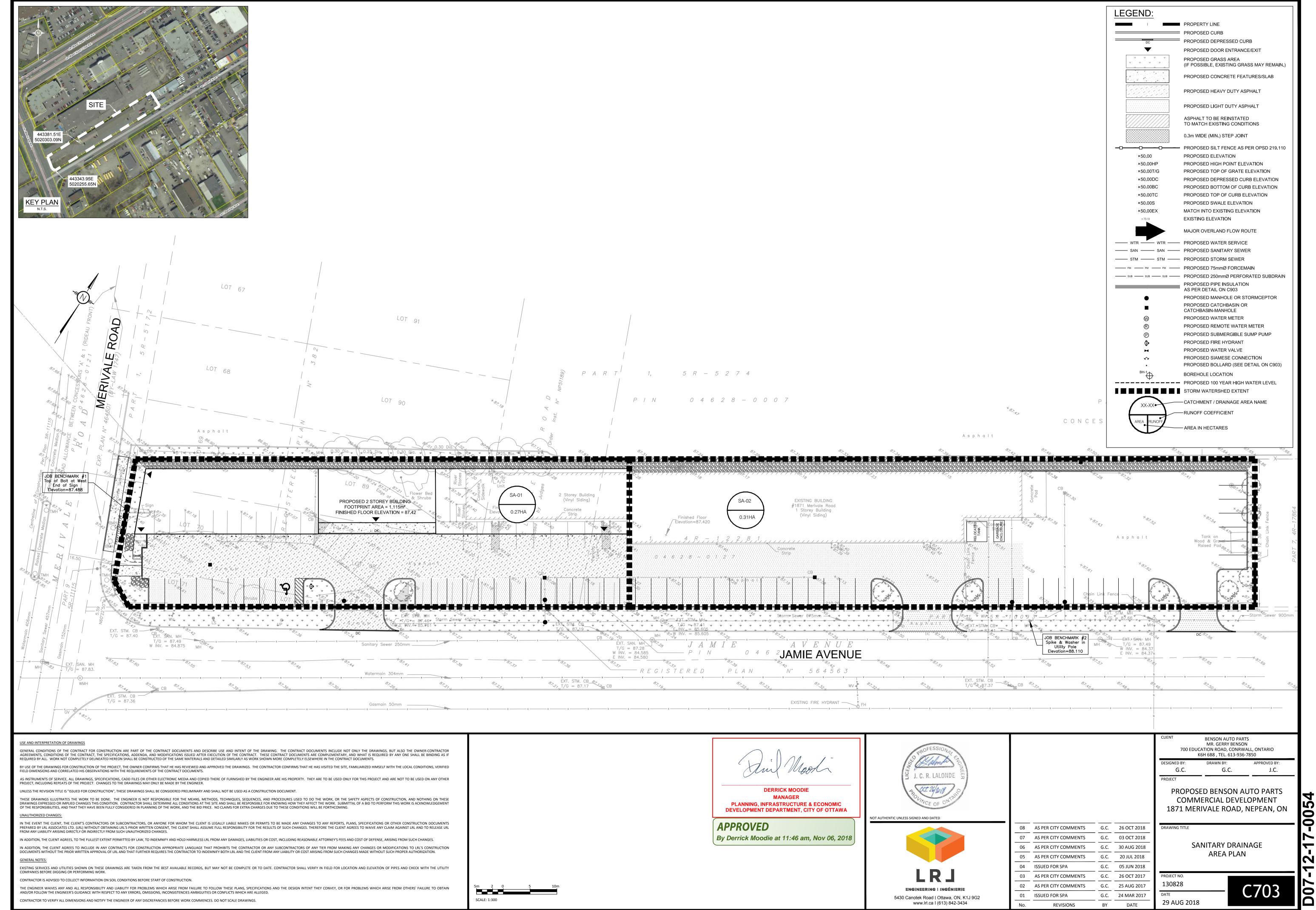
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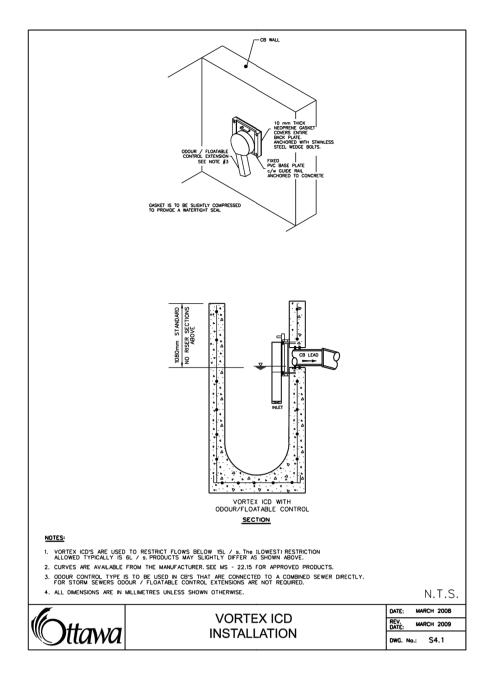
CITY OF OTTAWA DETAIL SC7

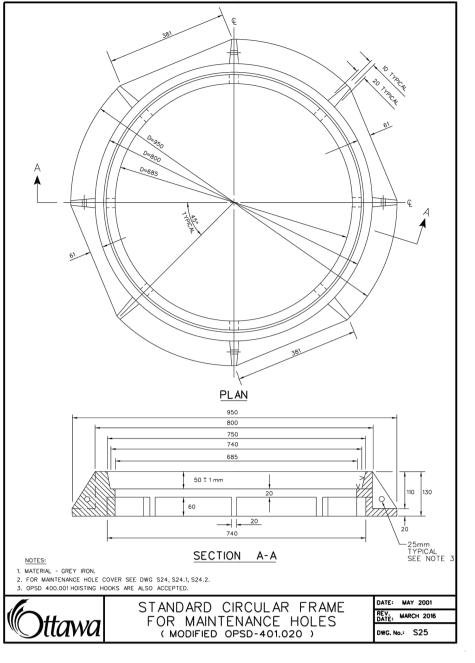


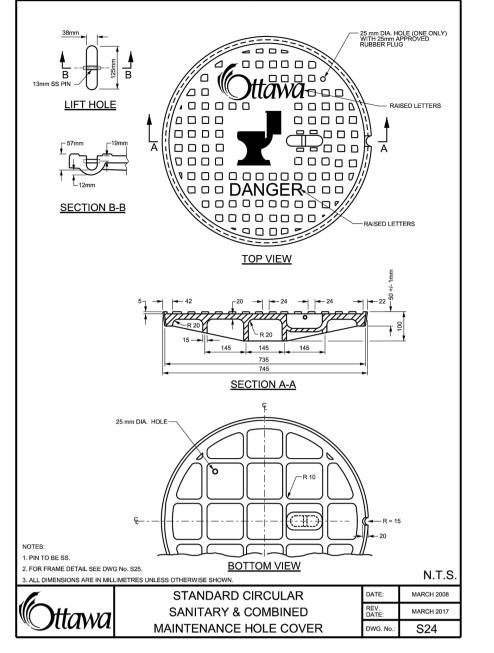


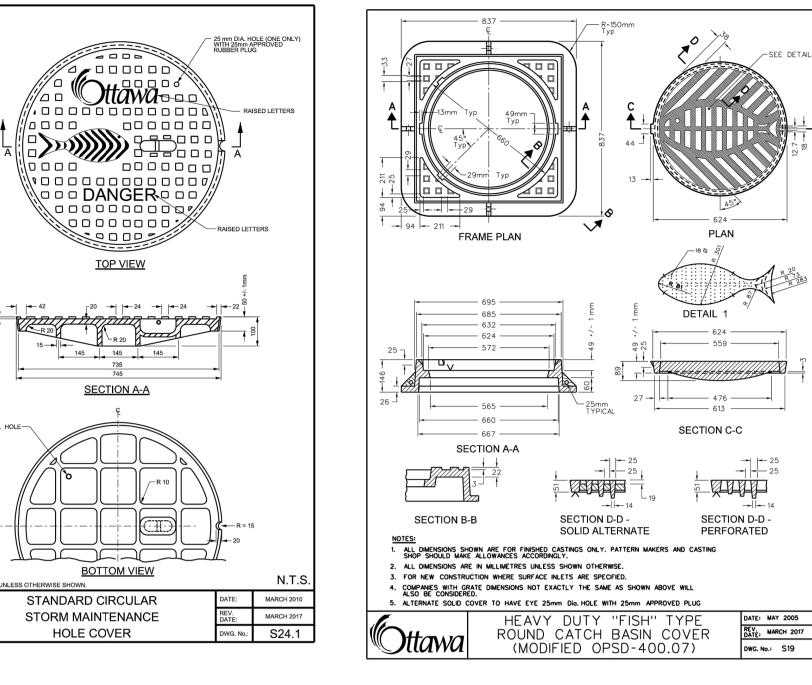


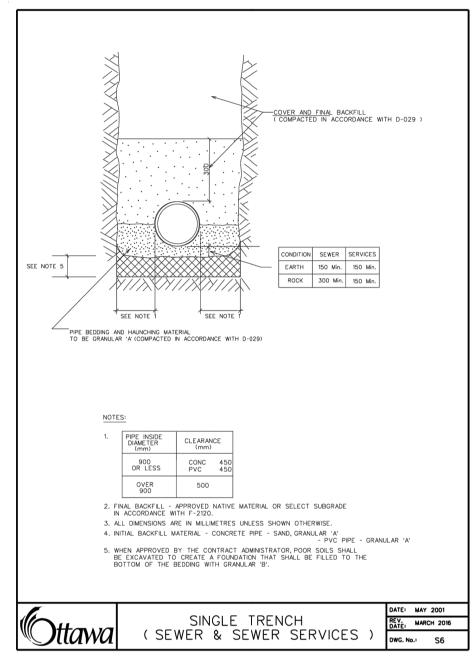


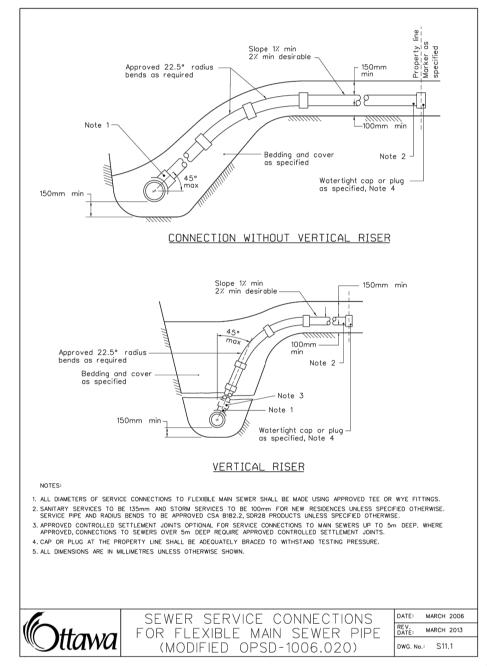


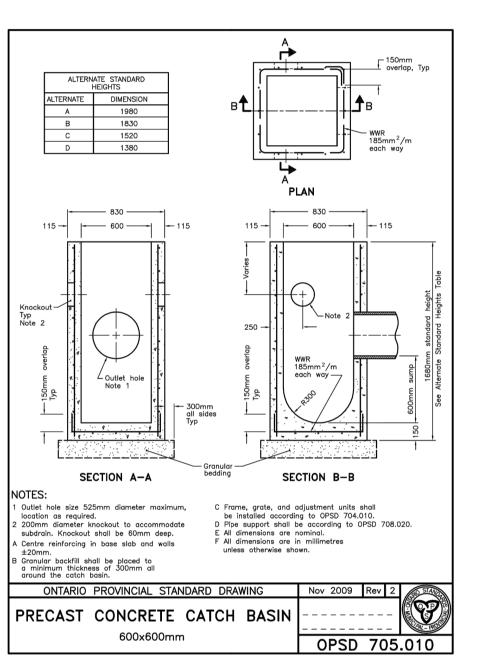


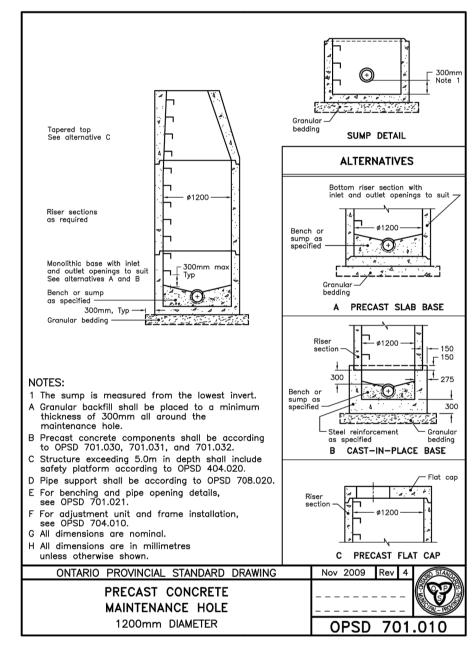












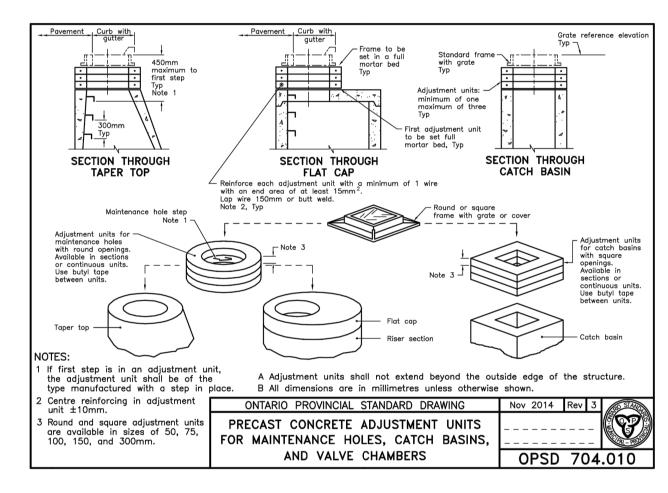
13mm SS PIN —

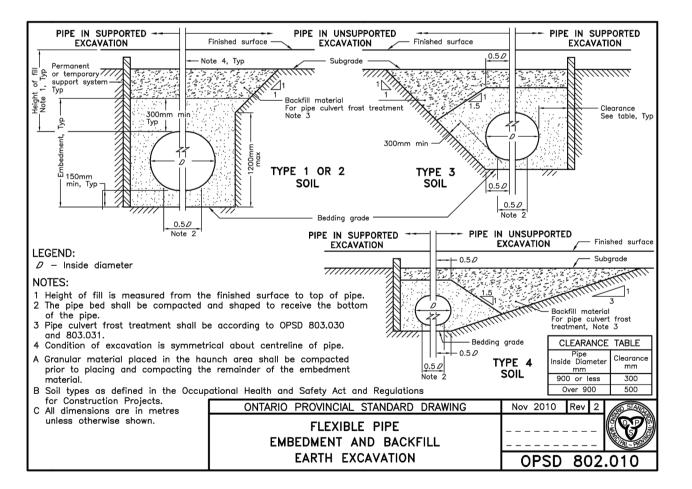
LIFT HOLE

SECTION B-B

1. PIN TO BE SS.

. FOR FRAME DETAIL SEE DWG No. S25.







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PLANNING, INFRASTRUCTURE & ECONOMIC DEVELOPMENT DEPARTMENT, CITY OF OTTAWA

APPROVED By Derrick Moodie at 11:49 am, Nov 06, 2018





5430 Canotek Road | Ottawa, ON, K1J 9G2

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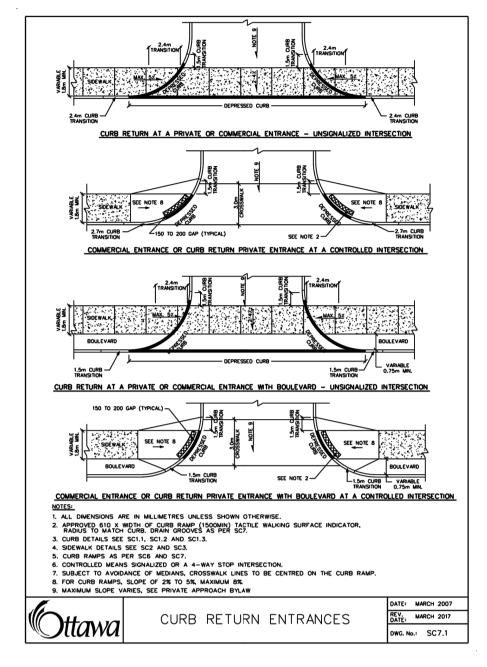
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07	AS PER CITY COMMENTS	G.C.	03 OCT 2018	
06	AS PER CITY COMMENTS	G.C.	30 AUG 2018	CONSTR
05	AS PER CITY COMMENTS	G.C.	20 JUL 2018	
04	ISSUED FOR SPA	G.C.	05 JUN 2018	
03	AS PER CITY COMMENTS	G.C.	26 OCT 2017	PROJECT NO.
02	AS PER CITY COMMENTS	G.C.	25 AUG 2017	130828
01	ISSUED FOR SPA	G.C.	24 MAR 2017	DATE
No.	REVISIONS	BY	DATE	29 AUG 2018

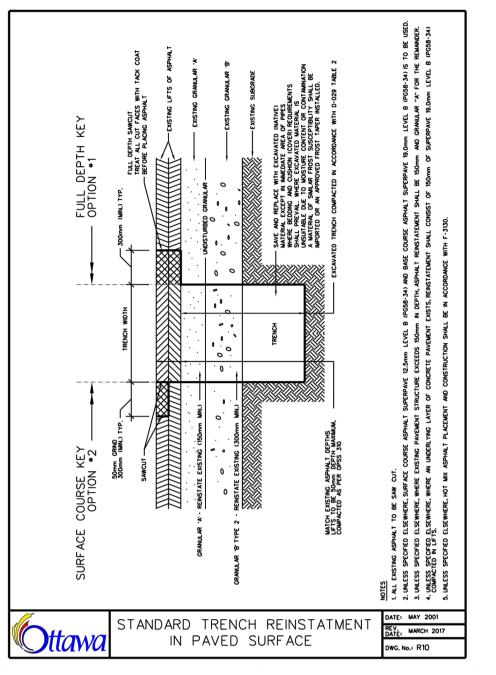
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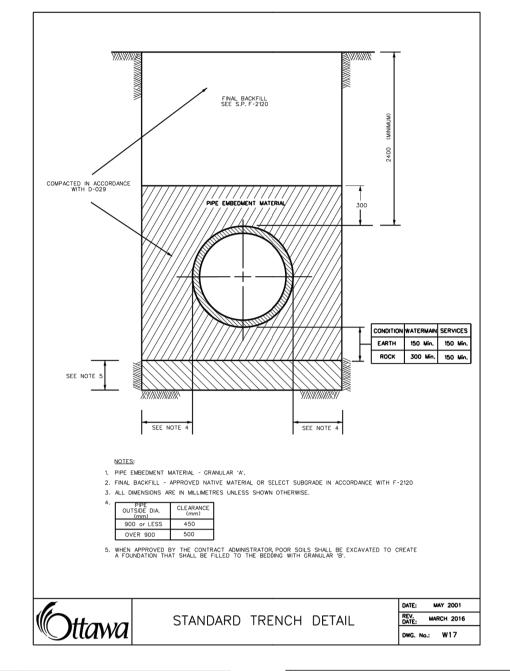
MR. GERRY BENSON 700 EDUCATION ROAD, CONRWALL, ONTARIO

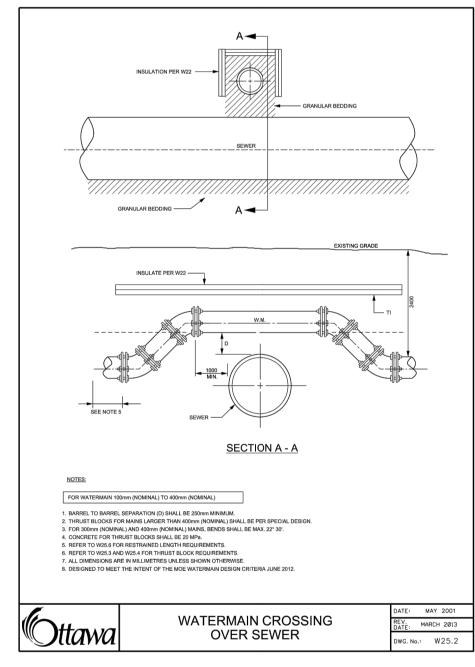
K6H 6B8, TEL. 613-936-7850

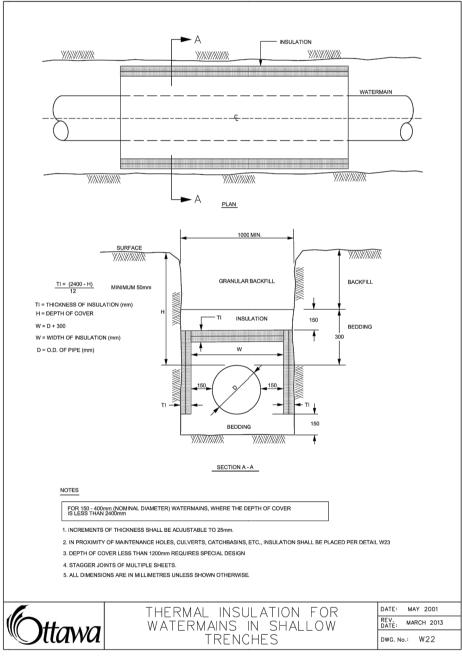
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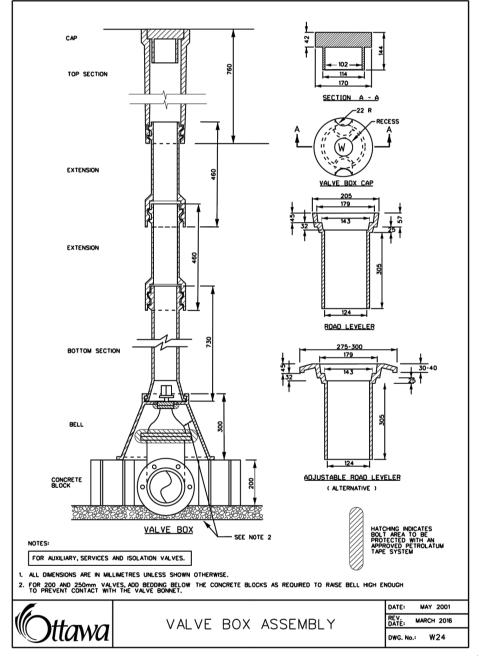


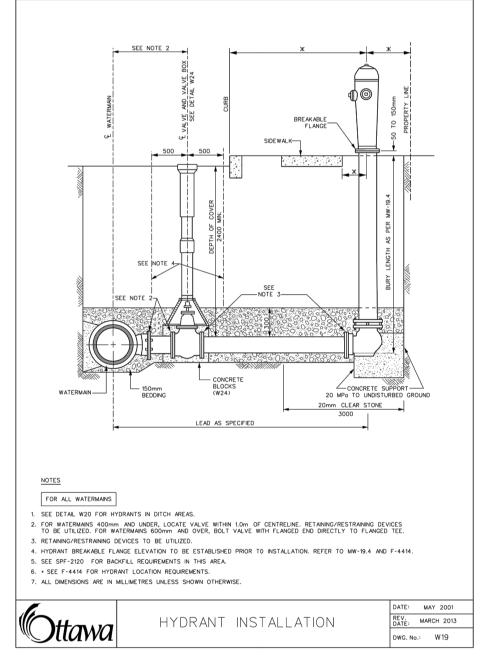












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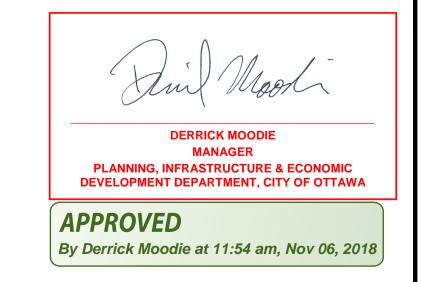
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NOT AUTHENTIC UNLESS SIGNED AND DATED

ENGINEERING | INGÉNIERIE

5430 Canotek Road | Ottawa, ON, K1J 9G2

www.lrl.ca I (613) 842-3434

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	No.	REVISIONS	BY	DATE

CLIENT BENSON AUTO PARTS MR. GERRY BENSON 700 EDUCATION ROAD, CONRWALL, ONTARIO K6H 6B8 , TEL. 613-936-7850					
DESIGNED BY:	DRAWN BY:	APPROVED BY:			
G.C.	G.C.	J.C.			
PROJECT					

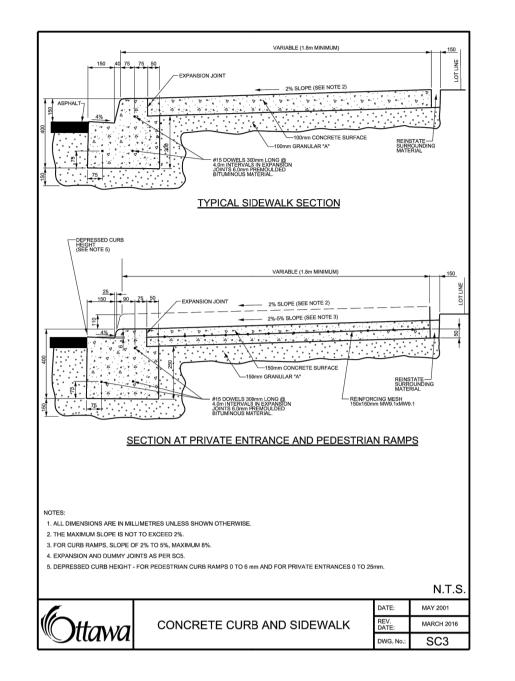
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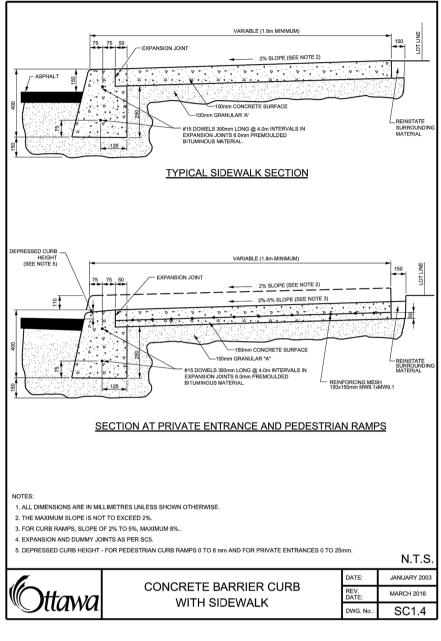
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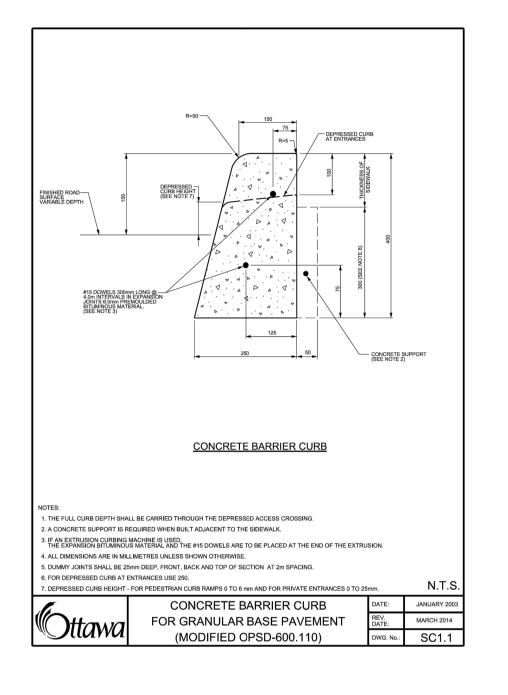
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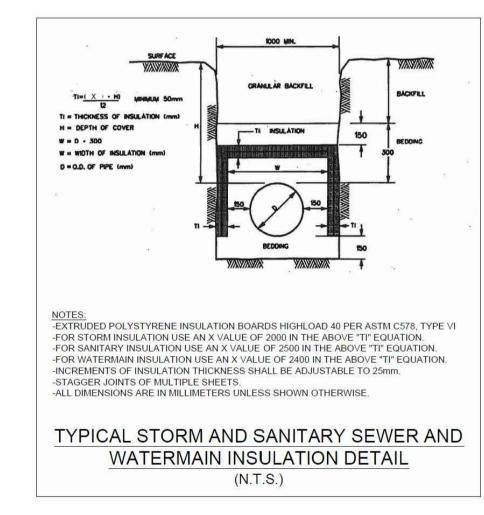
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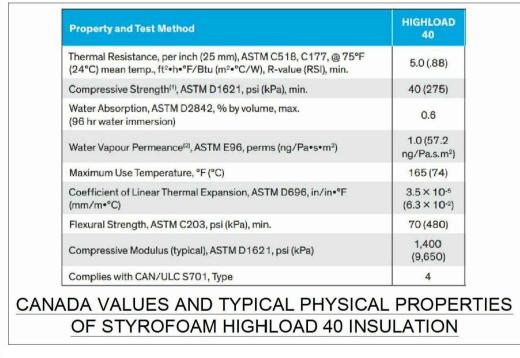
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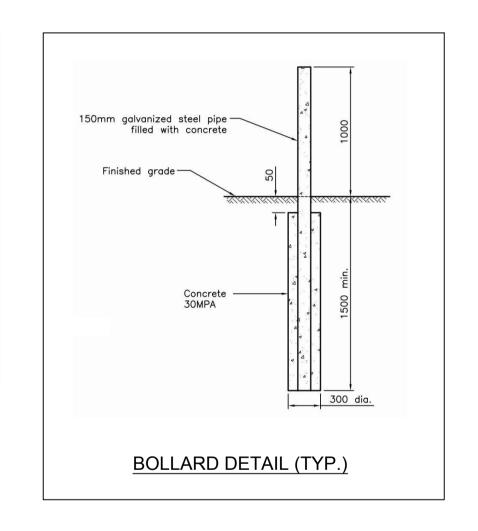












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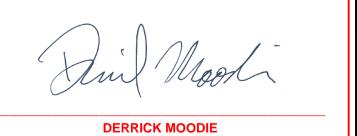
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PLANNING, INFRASTRUCTURE & ECONOMIC DEVELOPMENT DEPARTMENT, CITY OF OTTAWA

APPROVED By Derrick Moodie at 11:53 am, Nov 06, 2018



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	07	AS PER CITY COMMENTS	G.C.	03 OCT 2018
	06	AS PER CITY COMMENTS	G.C.	30 AUG 2018
	05	AS PER CITY COMMENTS	G.C.	20 JUL 2018
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LRJ	03	AS PER CITY COMMENTS	G.C.	26 OCT 2017
ENGINEERING I INGÉNIERIE	02	AS PER CITY COMMENTS	G.C.	25 AUG 2017

01 ISSUED FOR SPA

REVISIONS

BENSON AUTO PARTS MR. GERRY BENSON 700 EDUCATION ROAD, CONRWALL, ONTARIO K6H 6B8 , TEL. 613-936-7850 G.C.

PROJECT PROPOSED BENSON AUTO PARTS COMMERCIAL DEVELOPMENT 1871 MERIVALE ROAD, NEPEAN, ON

CONSTRUCTION DETAILS PLAN

130828

G.C. 24 MAR 2017

DATE

BY

29 AUG 2018





1871 MERIVALE OTTAWA, ON

STORMTECH CHAMBER SPECIFICATIONS

- 1 CHAMBERS SHALL BE STORMTECH SC-740 OR SC-310
- 2. CHAMBERS SHALL BE MANUFACTURED FROM VIRGIN POLYPROPYLENE OR POLYETHYLENE RESINS.
- CHAMBER ROWS SHALL PROVIDE CONTINUOUS, UNOBSTRUCTED INTERNAL SPACE WITH NO INTERNAL SUPPORT PANELS THAT WOULD IMPEDE FLOW OR LIMIT ACCESS FOR INSPECTION.
- THE STRUCTURAL DESIGN OF THE CHAMBERS, THE STRUCTURAL BACKFILL, AND THE INSTALLATION REQUIREMENTS SHALL ENSURE THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, SECTION 12.12, ARE MET FOR: 1) LONG-DURATION DEAD LOADS AND 2, SHORT-DURATION LIVE LOADS, BASED ON THE CSA S6 CL-625 TRUCK AND THE AASHTO DESIGN TRUCK WITH CONSIDERATION FOR IMPACT AND MULTIPLE VEHICLE PRESENCES.

- ONLY CHAMBERS THAT ARE APPROVED BY THE SITE DESIGN ENGINEER WILL BE ALLOWED. THE CHAMBER MANUFACTURER SHALL SUBMIT THE FOLLOWING UPON REQUEST TO THE SITE DESIGN ENGINEER FOR APPROVAL BEFORE DELIVERING CHAMBERS TO THE PROJECT SITE:
- a. A STRUCTURAL EVALUATION SEALED BY A REGISTERED PROFESSIONAL ENGINEER THAT DEMONSTRATES THAT THE SAFETY FACTORS ARE GREATER THAN OR EQUAL TO 1.95 FOR PEAD LOAD AND 1.75 FOR LIVE LOAD, THE MINIMUM REQUIRED BY ASTM F2787 AND BY ASSINTO FOR THERMOPLASTIC PIPE.
- b. A STRUCTURAL EVALUATION SEALED BY A REGISTERED PROFESSIONAL ENGINEER THAT DEMONSTRATES THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, SECTION 12.12, ARE MET, THE 50 YEAR CREEP MODULUS DATA SPECIFIED IN ASTM F2418 OR ASTM F2922 MUST BE USED AS PART OF THE AASHTO STRUCTURAL EVALUATION TO VERIFY LONG-TERM PERFORMANCE.
- c. STRUCTURAL CROSS SECTION DETAIL ON WHICH THE STRUCTURAL EVALUATION IS BASED. 8. CHAMBERS AND END CAPS SHALL BE PRODUCED AT AN ISO 9001 CERTIFIED MANUFACTURING FACILITY.

IMPORTANT - NOTES FOR THE BIDDING AND INSTALLATION OF THE SC-310/SC-740 SYSTEM

- STORMTECH SC-310 & SC-740 CHAMBERS SHALL NOT BE INSTALLED UNTIL THE MANUFACTURER'S REPRESENTATIVE HAS COMPLETED A PRE-CONSTRUCTION MEETING WITH THE INSTALLERS.
- 2. STORMTECH SC-310 & SC-740 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH SC-310/SC-740/SC-780 CONSTRUCTION GUIDE".
- CHAMBERS ARE NOT TO BE BACKFILLED WITH A DOZER OR AN EXCAVATOR SITUATED OVER THE CHAMBERS.
- 4. THE FOUNDATION STONE SHALL BE LEVELED AND COMPACTED PRIOR TO PLACING CHAMBERS.
- 5. JOINTS BETWEEN CHAMBERS SHALL BE PROPERLY SEATED PRIOR TO PLACING STONE.

6. MAINTAIN MINIMUM - 150 mm (6") SPACING BETWEEN THE CHAMBER ROWS.

- EMBEDMENT STONE SURROUNDING CHAMBERS MUST BE A CLEAN, CRUSHED, ANGULAR STONE 20-50 mm (3/4-2").
- 8. THE CONTRACTOR MUST REPORT ANY KNOWN DISCREPANCIES WITH CHAMBER FOUNDATION MATERIALS BEARING CAPACITIES TO THE SITE DESIGN ENGINEER. ADS RECOMMENDS THE USE OF "FLEXSTORM CATCH IT" INSERTS DURING CONSTRUCTION FOR ALL INLETS TO PROTECT THE SUBSURFACE STORMWATER MANAGEMENT SYSTEM FROM CONSTRUCTION SITE RUNOFF.
- NOTES FOR CONSTRUCTION EQUIPMENT STORMTECH SC-310 & SC-740 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE".
- THE USE OF CONSTRUCTION EQUIPMENT OVER SC-310 & SC-740 CHAMBERS IS LIMITED:

 NO EQUIPMENT IS ALLOWED ON BARE CHAMBERS.

 NO RUBBER TIRED LOADERS, DIMP TRUCKS, OR EXCAVATORS ARE ALLOWED UNTIL PROPER FILL DEPTHS ARE REACHED IN ACCORDANCE WITH THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE".

 WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT CAN BE FOUND IN THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE".
- 3. FULL 900 mm (36") OF STABILIZED COVER MATERIALS OVER THE CHAMBERS IS REQUIRED FOR DUMP TRUCK TRAVEL OR DUMPING.

CONTACT STORMTECH AT 1-888-892-2694 WITH ANY QUESTIONS ON INSTALLATION REQUIREMENTS OR WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT

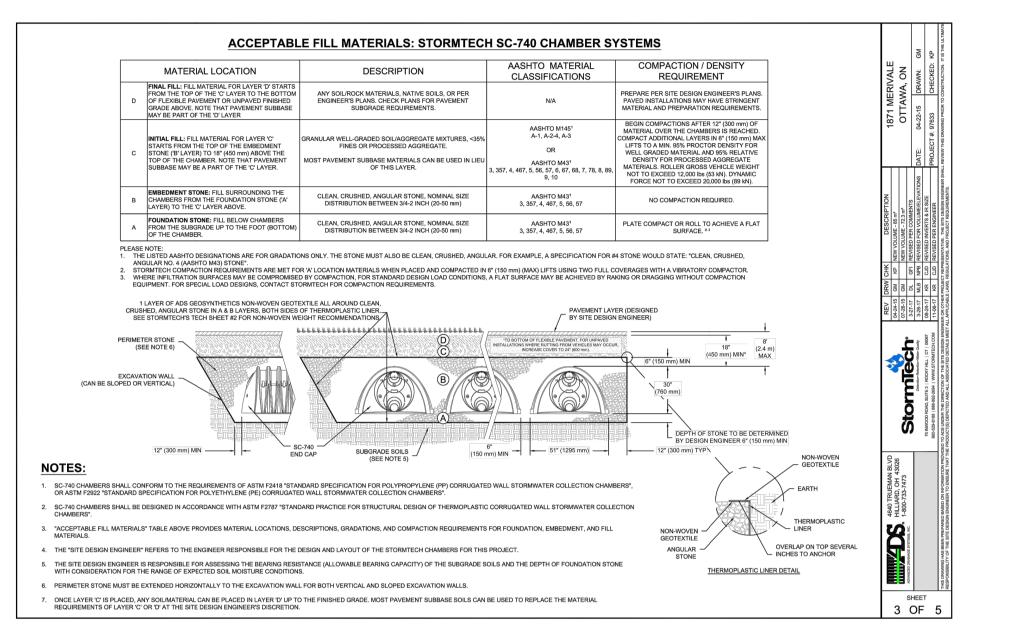
USE OF A DOZER TO PUSH EMBEDMENT STONE BETWEEN THE ROWS OF CHAMBERS MAY CAUSE DAMAGE TO THE CHAMBERS AND IS NOT AN ACCEPTABLE BACKFILL METHOD. ANY CHAMBERS DAMAGED BY THE "DUMP AND PUSH" METHOD ARE NOT COVERED UNDER THE STORMTECH STANDARD WARRANTY.

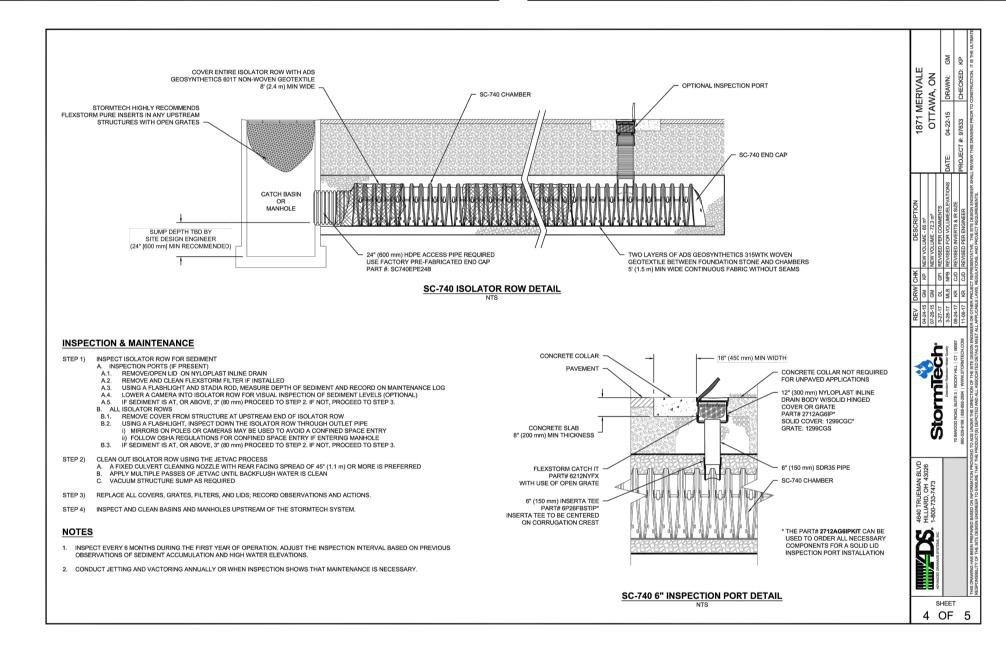
PROPOSED LAYOUT MANIFOLD SIZE TO BE DETERMINED BY SITE DESIGN ENGINEER. SEE TECH SHEET #7 FOR MANIFOLD SIZING GUIDANCE.

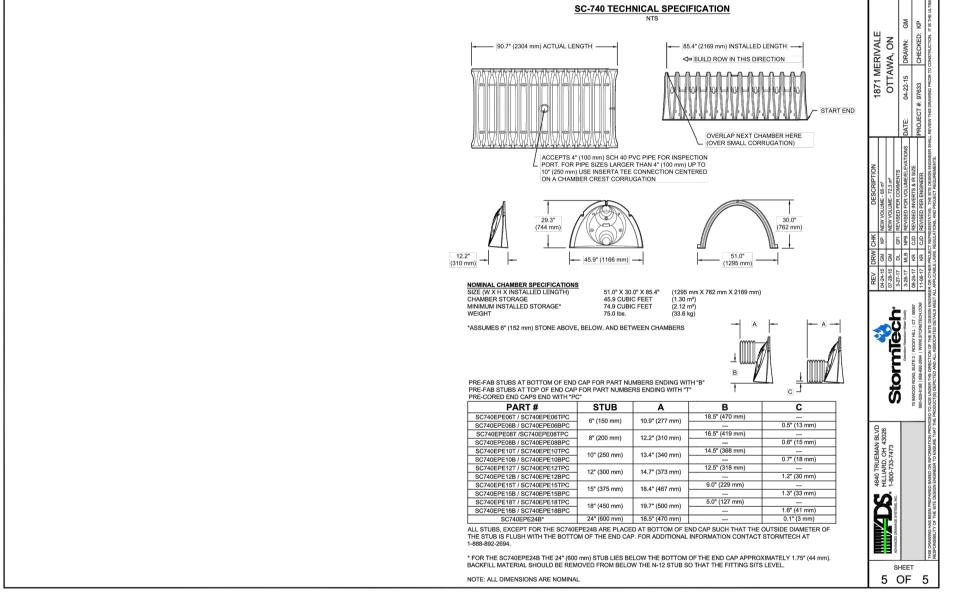
 DUE TO THE ADAPTATION OF THIS CHAMBER SYSTEM TO SPECIFIC SITE AND DESIGN CONSTRAINTS, IT MAY BE NECESSARY TO CUT AND COUPLE ADDITIONAL PIPE TO STANDARD MANIFOLD COMPONENTS IN THE FIELD.

 THE SITE DESIGN ENGINEER MUST REVIEW ELEVATIONS AND IF NECESSARY ADJUST GRADING TO ENSURE THE CHAMBER COVER REQUIREMENTS ARE MET.

 ADS DOES NOT DESIGN OR PROVIDE MEMBRANE LINER SYSTEMS FOR CISTERNS (RAINWATER HARVESTING). TO MINIMIZE STORMTECH SC-740 END CAPS STONE ABOVE (mm) STONE BELOW (mm) 40 % STONE VOID
INSTALLED SYSTEM VOLUME (m²)
(PERIMETER STONE INCLUDED / BASE STONE NOT
INCLUDED)
297 SYSTEM AREA (m²) THE LEAKAGE POTENTIAL OF LINER SYSTEMS, THE MEMBRANE LINER SYSTEM SHOULD BE DESIGNED BY A KNOWLEDGABLE GEOTEXTILE PROFESSIONAL AND INSTALLED BY A QUALIFIED CONTRACTOR. SECTION A-A PROPOSED ELEVATIONS MAXIMUM ALLOWABLE GRADE (TOP OF PAVEMENT/UNPAVED): MINIMUM ALLOWABLE GRADE (UNPAVED WITH TRAFFIC):
MINIMUM ALLOWABLE GRADE (UNPAVED NO TRAFFIC): IIIMUM ALLOWABLE GRADE (ONPAVED NO TRAFFIC):
IIMUM ALLOWABLE GRADE (BASE OF FLEXIBLE PAVEMENT):
IIMUM ALLOWABLE GRADE (TOP OF RIGID PAVEMENT): TOP OF STONE: TOP OF SC-740 CHAMBER 300 mm TOP MANIFOLD INVERT: 450 mm ISOLATOR ROW INVERT: THERMOPLASTIC LINER (DESIGN BY ENGINEER PROVIDED BY OTHERS ISOLATOR ROW







USE AND INTERPRETATION OF DRAWINGS

GENERAL CONDITIONS OF THE CONTRACT FOR CONSTRUCTION ARE PART OF THE CONTRACT DOCUMENTS AND DESCRIBE USE AND INTENT OF THE DRAWING. THE CONTRACT DOCUMENTS INCLUDE NOT ONLY THE DRAWINGS. BUT ALSO THE OWNER-CONTRACTOR REQUIRED BY ALL. WORK NOT COMPLETELY DELINEATED HEREON SHALL BE CONSTRUCTED OF THE SAME MATERIALS AND DETAILED SIMILARLY AS WORK SHOWN MORE COMPLETELY ELSEWHERE IN THE CONTRACT DOCUMENTS.

BY USE OF THE DRAWINGS FOR CONSTRUCTION OF THE PROJECT, THE OWNER CONFIRMS THAT HE HAS REVIEWED AND APPROVED THE DRAWINGS. THE CONTRACTOR CONFIRMS THAT HE HAS VISITED THE SITE, FAMILIARIZED HIMSELF WITH THE LOCAL CONDITIONS, VERIFIED FIELD DIMENSIONS AND CORRELATED HIS OBSERVATIONS WITH THE REQUIREMENTS OF THE CONTRACT DOCUMENTS.

AS INSTRUMENTS OF SERVICE, ALL DRAWINGS, SPECIFICATIONS, CADD FILES OR OTHER ELECTRONIC MEDIA AND COPIED THERE OF FURNISHED BY THE ENGINEER ARE HIS PROPERTY. THEY ARE TO BE USED ONLY FOR THIS PROJECT AND ARE NOT TO BE USED ON ANY OTHER PROJECT, INCLUDING REPEATS OF THE PROJECT. CHANGES TO THE DRAWINGS MAY ONLY BE MADE BY THE ENGINEER. UNLESS THE REVISION TITLE IS "ISSUED FOR CONSTRUCTION", THESE DRAWINGS SHALL BE CONSIDERED PRELIMINARY AND SHALL NOT BE USED AS A CONSTRUCTION DOCUMENT.

THESE DRAWINGS ILLUSTRATES THE WORK TO BE DONE. THE ENGINEER IS NOT RESPONSIBLE FOR THE MEANS, METHODS, TECHNIQUES, SEQUENCES, AND PROCEDURES USED TO DO THE WORK, OR THE SAFETY ASPECTS OF CONSTRUCTION, AND NOTHING ON THESE DRAWINGS EXPRESSED OR IMPLIED CHANGES THIS CONDITION. CONTRACTOR SHALL DETERMINE ALL CONDITIONS AT THE SITE AND SHALL BE RESPONSIBLE FOR KNOWING HOW THEY AFFECT THE WORK. SUBMITTAL OF A BID TO PERFORM THIS WORK IS ACKNOWLEDGEMENT OF THE RESPONSIBILITIES, AND THAT THEY HAVE BEEN FULLY CONSIDERED IN PLANNING OF THE WORK, AND THE BID PRICE. NO CLAIMS FOR EXTRA CHARGES DUE TO THESE CONDITIONS WILL BE FORTHCOMING.

IN THE EVENT THE CLIENT, THE CLIENT, THE CLIENT, PLANS, SPECIFICATIONS OR SUBCONTRACTORS, OR ANYONE FOR WHOM THE CLIENT IS LEGALLY LIABLE MAKES OR PERMITS TO BE MADE ANY CHANGES TO ANY REPORTS, PLANS, SPECIFICATIONS OR OTHER CONSTRUCTION DOCUMENTS PREPARED BY LRL ASSOCIATES LTD. (LRL) WITHOUT OBTAINING LRL'S PRIOR WRITTEN CONSENT, THE CLIENT SHALL ASSUME FULL RESPONSIBILITY FOR THE RESULTS OF SUCH CHANGES. THEREFORE THE CLIENT AGREES TO WAIVE ANY CLAIM AGAINST LRL AND TO RELEASE LRL FROM ANY LIABILITY ARISING DIRECTLY OR INDIRECTLY FROM SUCH UNAUTHORIZED CHANGES. IN ADDITION, THE CLIENT AGREES, TO THE FULLEST EXTENT PERMITTED BY LAW, TO INDEMNIFY AND HOLD HARMLESS LRL FROM ANY DAMAGES, LIABILITIES OR COST, INCLUDING REASONABLE ATTORNEY'S FEES AND COST OF DEFENSE, ARISING FROM SUCH CHANGES.

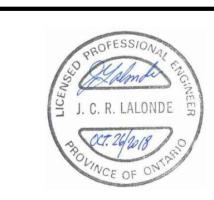
IN ADDITION THE CLIENT AGREES TO INCLUDE IN ANY CONTRACTS FOR CONSTRUCTION APPROPRIATE LANGUAGE THAT PROHIBITS THE CONTRACTOR OR ANY SUBCONTRACTORS OF ANY TIER FROM MAKING ANY CHANGES OR MODIFICATIONS TO LRL'S CONSTRUCTION DOCUMENTS WITHOUT THE PRIOR WRITTEN APPROVAL OF LRL AND THAT FURTHER REQUIRES THE CONTRACTOR TO INDEMNIFY BOTH LRL AND THE CLIENT FROM ANY LIABILITY OR COST ARISING FROM SUCH CHANGES MADE WITHOUT SUCH PROPER AUTHORIZATION. GENERAL NOTES:

EXISTING SERVICES AND UTILITIES SHOWN ON THESE DRAWINGS ARE TAKEN FROM THE BEST AVAILABLE RECORDS, BUT MAY NOT BE COMPLETE OR TO DATE. CONTRACTOR SHALL VERIFY IN FIELD FOR LOCATION AND ELEVATION OF PIPES AND CHECK WITH THE UTILITY COMPANIES BEFORE DIGGING OR PERFORMING WORK. CONTRACTOR IS ADVISED TO COLLECT INFORMATION ON SOIL CONDITIONS BEFORE START OF CONSTRUCTION.

THE ENGINEER WAIVES ANY AND ALL RESPONSIBILITY AND LIABILITY FOR PROBLEMS WHICH ARISE FROM FAILURE TO FOLLOW THESE PLANS, SPECIFICATIONS AND THE DESIGN INTENT THEY CONVEY, OR FOR PROBLEMS WHICH ARISE FROM OTHERS' FAILURE TO OBTAIN AND/OR FOLLOW THE ENGINEER'S GUIDANCE WITH RESPECT TO ANY ERRORS, OMISSIONS, INCONSISTENCIES AMBIGUITIES OR CONFLICTS WHICH ARE ALLEGED. CONTRACTOR TO VERIFY ALL DIMENSIONS AND NOTIFY THE ENGINEER OF ANY DISCREPANCIES BEFORE WORK COMMENCES. DO NOT SCALE DRAWINGS.

DERRICK MOODIE MANAGER PLANNING, INFRASTRUCTURE & ECONOMIC **DEVELOPMENT DEPARTMENT, CITY OF OTTAWA APPROVED**

By Derrick Moodie at 11:51 am, Nov 06, 2018



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REVISIONS

BY

DATE

BENSON AUTO PARTS MR. GERRY BENSON 700 EDUCATION ROAD, CONRWALL, ONTARIO K6H 6B8, TEL. 613-936-7850 G.C. J.C.

PROPOSED BENSON AUTO PARTS COMMERCIAL DEVELOPMENT 1871 MERIVALE ROAD, NEPEAN, ON

PROJECT

CONSTRUCTION DETAILS PLAN

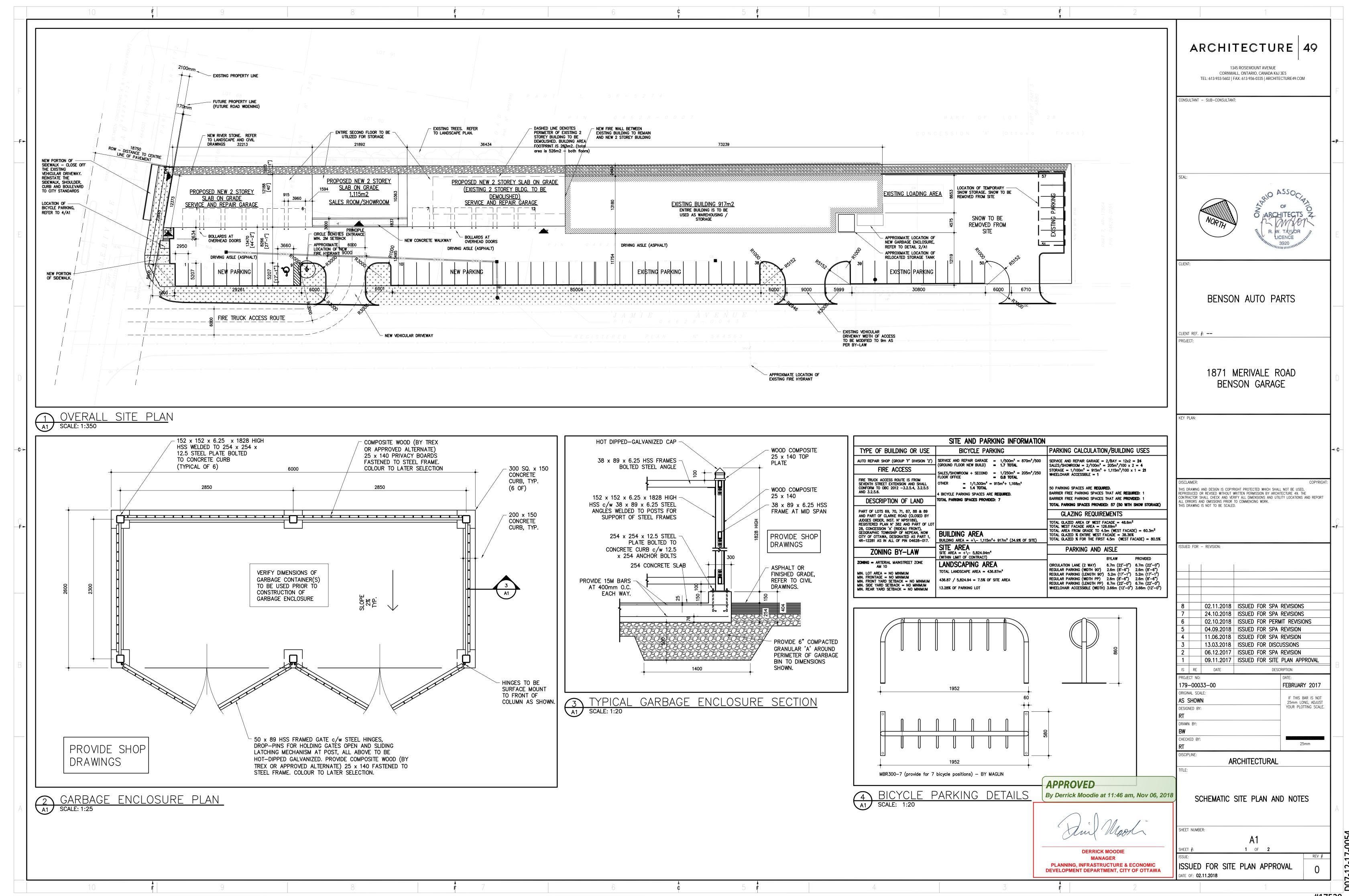
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Appendix G

Architectural Site Plan (Phase 1)



Appendix H

Site Servicing and Stormwater Management Report
(Phase 1)



Site Servicing & Stormwater Management Report

Benson Auto Parts Development 1871 Merivale Road Ottawa, Ontario

Prepared for:

Benson Auto Parts 700 Education Road Cornwall, Ontario K6H 6B8

Attention: Mr. Marty Benson

Application File No.: D07-12-17-0054 August, 25, 2017

LRL File No.: 130828 Rev.4: October 03, 2018

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Appendix A	Water Demand and Fire Flow Calculations
Appendix B	Sanitary Sewer Calculation Sheet
Appendix C	Stormwater Management Design Sheets
Appendix D	Hydrovex Vertical Vortex Flow Regulator Report
Appendix E	StormTech System Design Sheets
Appendix F	Stormceptor Report
Appendix G	Complete Set of Civil Plans
Appendix H	Jamie Avenue As-Built Drawings
Appendix I	Boundary Conditions
Appendix J	RVCA Correspondence



LRL File: 130828

October 03, 2018

LRL Associates Ltd. (LRL) has been retained by Benson Auto Parts to prepare a site servicing and stormwater management report in support of their site plan control application for a proposed expansion of their existing facility. This report presents the proposed servicing plan for the proposed development in regards to water and sanitary services, as well as stormwater management.

This report has been prepared in consideration of the survey carried out by Fairfall Moffatt & Woodland Ltd dated August 9th, 2017. Should there be any discrepancies in the existing infrastructure and/or connections to existing services, which may relate to site servicing considerations, LRL should be advised in order to review the report recommendations. This report should be read in conjunction with the Civil plans prepared by LRL.

1 SITE DESCRIPTION

The subject property is located within the urban boundary of the City of Ottawa; Ward 9 Knoxdale-Merivale, in the Merivale Industrial Park Jamie Sector. As illustrated in Figure 1, the proposed expansion of the development will be part of the Benson Auto Parts property, located at 1871 Merivale Road; East of Merivale Road, and north of Jamie Avenue. The total area of the property measures approximately 0.582 ha.



Figure 1 Aerial view of Benson site at 1871 Merivale Road, Ottawa, ON (via Google Earth, imagery date: September 24, 2014)

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October 03, 2018

The proposed development is located in an industrial area bounded by commercial properties to the north and east of the lot. The site is comprised of an auto parts garage, office and asphalt parking lot.

The proposed expansion of the development will include demolishing a portion (262m²) of the existing 1170m², two-storey, office space. In its place, a two-storey warehouse/garage and office space building (total footprint area of 1185m²) will be built.

2 SCOPE OF WORK

As per applicable guidelines, the scope of work includes the following:

Water services

- Calculate the expected water supply demand at average and peak conditions.
- Calculate the fire flow as per the Fire Underwriter Survey (FUS) method.
- Describe the proposed water distribution network and connection to the existing system.

Sanitary services

- Describe the existing sanitary sewers available to receive wastewater from the building.
- Calculate peak flow rates from the development.
- Describe the proposed sanitary sewer system.
- Verify available capacity in the downstream sanitary sewer.
- Verify the capacity of the existing lateral sanitary sewer

Stormwater management

- Calculate the allowable stormwater release rate.
- Calculate the anticipated post development stormwater release rates.
- Demonstrate how the target quality and quantity objectives will be achieved.
- Verify the capacity of the existing lateral storm sewer

3 WATER SUPPLY AND FIRE PROTECTION

3.1 Existing Water Supply Services

The proposed site is currently being serviced by a 50mm water service that is connected to the existing 300mm dia. PVC watermain extending along Jamie Avenue. There is an existing fire hydrant south of the site on Jamie Avenue and two hydrants west of the site on the east side of Merivale Road. The subject site is located in Pressure Zone 2W. Please refer to Appendix H for the Jamie Avenue As-Built Drawings.

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3.2 Water Supply Demand

As per the AWWA Standards and the City of Ottawa Design Guidelines, the average water demand for industrial developments was calculated using an average water demand per fixture unit of **3.33L/min** and a daily and hourly peak factor of **1.5** and **1.8**, respectively. The peak water demand was calculated for the 50 fixtures units included in the new and existing building. The average daily water demand for the new and existing building is **2.78L/s**, maximum daily is **4.16L/s**, and maximum hourly is **7.49L/s**. Please refer to Appendix A for the water demand calculation sheet.

The fire flow demand was estimated in accordance with the Fire Underwriters Survey (FUS). This method is based on the floor area of the building to be protected, type and combustibility of the structural frame and the separation distances with adjoining buildings. The fire flow demand was calculated to be **183.3L/s**. Please refer to Appendix A for the fire flow calculation sheet.

The City of Ottawa has provided boundary conditions to LRL Associates for this project. Please refer to Appendix I for boundary conditions. Using the provided HGLs, minimum, maximum and maximum day + fire pressures were calculated at the Jamie Avenue connection. Head losses were then calculated from the street connection to the proposed building for the maximum daily demand, maximum hourly demand and maximum daily demand + fire flow. For each of these scenarios, the relevant pressures were determined. Adequate water supply/pressure is available and meets the City of Ottawa standards as per section 4.2.2 of the Ottawa Design Guidelines – Water distribution. For the maximum daily demand, a minimum and maximum pressure of 59.49 and 70.58 psi were calculated; these land within the 50 to 80 psi MOE range. For the maximum hourly demand, a minimum and maximum pressure of 59.43 and 70.52 psi were calculated; these land within the 40 to 80 psi MOE range. For the maximum daily demand + fire flow, a pressure of 25.37 psi was calculated; this is above the minimum 20 psi MOE requirement. A pressure reducing valve is not required based on the above analysis. Please refer to Appendix A for pressure loss calculations.

Summary Table					
Average Water Demand Rate	239760 L/day				
Units	50				
Factors 1.5(max daily) & 1.8(max hourly					
Average Day Demand (L/s)	2.78				
Maximum Daily Demand (L/s)	4.16				
Peak Hour Demand (L/s)	7.49				
FUS Fire Flow Requirement (L/s)	183.3				
Max Day+Fire Flow (L/s)	187.46				

3.3 Water supply servicing design

The existing 50mm water service at the south-east corner of the existing building will be removed during construction to eliminate the use of two separate water meters within the building.

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October 03, 2018

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The proposed building will now be serviced by one new 150mm dia. service. The proposed service will connect to a new fire hydrant (to be located east of the first entrance on Jamie Street) before connecting to the proposed building.

Fire flow protection is to be provided by a proposed sprinkler system, and the proposed fire hydrant. The new hydrant will be located within 45m of the building's siamese connection, as required by the City of Ottawa. The hydrant will be installed on private property. Taking into account the proposed on-site hydrant and the existing hydrant directly across Jamie Avenue, the minimum number of hydrants needed to deliver the required fire flow to the structure is being provided in accordance with Technical Bulletin ISTB-2018-02 dated March 21, 2018. Please refer to table below and dimensions on plan C401.

Required Fire	Hydrants within	Hydrants	Max. Available	Sufficient
Flow Estimate	75m	between 75-	Flow (AA-Rated	Hydrants to
(L/min)		150m	Hydrants)	Provide RFF?
11,000	2	0	11,400	Yes

4 SANITARY DRAINAGE

4.1 Existing Sanitary Sewer Services

The site is currently being serviced by a 100mm dia. ABS service, located at the south-east corner of the existing building. The sewage is currently conveyed from this 100mm dia. Service easterly through a 250mm dia. sanitary sewer on Jamie Avenue, then southerly through a 450mm dia. sanitary sewer on Sunderland Street, easterly to a 675mm dia. sanitary sewer on Bentley Avenue, crossing the train tracks and making its way to the lift station located at 8 Antares Drive in Ottawa. Please refer to Appendix H for the Jamie Avenue As-Built Drawings, as well as the sanitary sewer distribution maps.

4.2 Sanitary Sewer Servicing Design

A monitoring manhole (SAN MH2) is to be installed along the existing 100mm service, located at the south-east corner of the existing building. The segment of pipe from SAN MH2 to Jamie Avenue shall be replaced and upsized with a 200mm PVC pipe.

City of Ottawa Sewer Design Guidelines.

The new building will be serviced with a new 200mm dia. sanitary service, which will connect to the existing 250mm dia. sanitary sewer on Jamie Avenue. A new monitoring manhole (SAN MH1) is to be installed along the proposed 200mm service; near the property line. The new proposed 200mm PVC sanitary service will be installed at a minimum slope of 1.0%, as per the

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October 03, 2018

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The parameters used to calculate the site's allowable sanitary flows are: Commercial average flow demand of 50,000 L/ha/day, a commercial peaking factor of 1.5 and an infiltration rate of 0.28 L/s/ha. Based on these parameters and the total site area of 0.582 ha, the total allowable sanitary flow was estimated to be **0.90 L/s**. Refer to Appendix B for the site sanitary sewer design sheet.

As per Appendix 4-A of the City of Ottawa Sewer Design Guidelines, the site's anticipated sanitary flow is **10,400 L/day (0.12 L/s)**. 30 cars per day are anticipated to be serviced, and from those 30 cars, 75% (23 cars) are anticipated to be washed. Under the "Service Stations" item: 30 cars x 40 L/day = 1200 L/day, under the "(Car) Wash" item: 23 cars x 400 L/day = 9200 L/day; for a total of 10,400 L/day (0.12 L/s). To be on the conservative side, we have assumed all vehicles to be trucks.

5 STORMWATER MANAGEMENT

5.1 Existing Stormwater Infrastructure

The information below should be read in conjunction with LRL drawing C701.

The existing site has three storm service connections. Drainage from existing CA-03 is captured by existing CB1 and is conveyed to the Jamie Street 675mm dia. storm sewer. The south half of the existing rooftops, the asphalt drive aisle and parking lot within existing CA-04 and existing CA-05 are captured by existing CB2 and CB3, respectively. Existing 200mm PVC storm pipes convey the captured drainage through these CBs and to the 450mm dia. storm sewer along Jamie Avenue. Surface runoff from existing CA-01 is captured by CB-4, which is connected to an existing manhole located on the neighboring property. Finally, existing CA-02 includes drainage from the north side of the existing rooftops and some grassed area along the property boundary. Existing CA-02 is captured by a landscaping catchbasin believed to be connected to the existing manhole located on the neighboring property.

Please also refer to Appendix H for the Jamie Avenue As-Built Drawings.

5.2 Stormwater management Concept

The information below should be read in conjunction with LRL drawings C401, C701, C702 and Appendix C (the stormwater management design sheets). The pervious and impervious runoff

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coefficients have been increased by 25% for the 100yr event; as per the Ottawa Sewer Design Guidelines.

The pre and post development catchments are divided in three systems; as the property currently has three outlets.

System #1:

Existing CA-01 and CA-02 currently outlet to an existing manhole and ditch inlet located on the neighboring side of the property line; in a small shared grass ditch. In post-development conditions, no runoff will outlet to this existing manhole.

System #2:

The area of existing CA-03 will remain mostly untouched. Minimal regrading and paving will be done in this location. Existing CA-03 and proposed CA-01 & CA-05 both use the same outlet.

As per City request, the area of CA-05 shall not be controlled due to the potential for contamination; also, surcharging of the perforated pipe may cause disturbance of the storage media.

A proposed 97mm ICD orifice plate is to be installed in existing CB1. This will ensure that the combined post release rate of proposed CA-01(26.07L/s controlled) & CA-05(8.92L/s uncontrolled) match the total existing release rate of **34.99L/s**.

System #3:

In pre-development conditions System #3 is comprised of existing CA-04 and CA-5. In post-development conditions it is comprised of proposed CA-02, CA-03 and CA-04.

The pre-development 5yr allowable release rate has been calculated using the pre-conditions System #3 (existing CA-04 and CA-05) only. The allowable release rate was calculated to be **29.98L/s**.

LRL's analysis determined that the existing 200mm dia. storm sewer does not provide sufficient capacity; even for the minor 5 year storm event. Therefore, LRL proposes to upgrade the on-site storm network to 300mm dia. storm pipes.

The post-development conditions (100 year storm event) were designed using a restricted release flow of **14.99L/s** using a Hydrovex Vertical Vortex Flow Regulator model 125VHV-2 to be installed in proposed CBMH1.

The 100year storm runoff from proposed catchment areas CA-02 to CA-04 will be controlled at proposed CBMH1. Runoff above the 100year will back out of proposed CB1, CB2 and CBMH1 and pond around each drainage structure until it flows overland, making its way to Jamie Avenue through the spill out point located at the property line; just south of proposed CBMH1.

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As underground storage and surface storage is included in the design, an average release rate of 14.99 L/s was assumed to determine the site's storage requirements; this is equal to 50% of the peak allowable rate. The 100yr storage required for this site is **167.00m3**. The 100yr storage provided is **179.05m3**. This is a combination of the StormTech chambers storage of 173.40m3 (refer to Appendix E for StormTech System Design Sheets) and the underground pipes and drainage structures storage of 5.65m3. This storage capacity will be possible using a Hydrovex Vertical Vortex Flow Regulator model 125VHV-2 to be installed in proposed CBMH1 at an allowable release rate of **14.99L/s**. Refer to Appendix D for Hydrovex Vertical Vortex Flow Regulator Report.

Please refer to table below for a summary of the post-development release rates:

Release Rate Summary Table							
Outlet	Uncontrolled Release	Controlled Release	Total Release	ICD			
Storm System / Site Outlet #2	5.47 L/s	29.52 L/s	34.99 L/s	103mm dia. ICD Orifice Plate			
Storm System / Site Outlet #3	N/A	14.99 L/s	14.99 L/s	125VHV-2			

The proposed depths of cover for the proposed storm system are less than the City's Sewer Design Guideline recommendations of 2.0 metres where possible (sections 5.7.1.); due to the required minimum pipe slopes (table 6.1). To rectify this, it is common practice to install insulation where a 2.0 metre depth of cover cannot be met. Where required, and as shown on the Civil plans, the insulation to be installed shall be extruded polystyrene insulation boards highload 40 per ASTM C578, type VI.

The bottom elevation of the proposed StormTech storage chambers is at 85.80m; 2.72m above the groundwater table elevation measured at the time of the subsurface investigation. To account for seasonal fluctuation, 1.5m is added to the groundwater table elevation; still the bottom of the storage chamber will remain a minimum of 1.0m above the high groundwater table.

5.3 Design Criteria

Stormwater quantity and quality control measures are taken into account for this site to reduce post development stormwater runoff to allowable levels.

5.3.1 Water Quality

We have proposed two Stormceptor STC 300 oil/grit separators (one for each storm connection) which provide water quality treatment; where the enhanced 80% TSS removals requirement is met. Please refer to Appendix F – Stormceptor Reports. An isolator row has been incorporated into the StormTech system as well providing additional on-site quality treatment.

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5.3.2 Water Quantity

All storm events up to and including the 100 year event will be controlled to the 5 year predevelopment level. The site's major overland flow route has been designed to ensure that storm events beyond the 100 year design storm can be safely conveyed overland towards the Jamie Avenue right of way. The minor system (storm sewer) within the site is sized to convey the 5 year storm event flows from the site to the municipal storm sewer on Jamie Avenue.

5.4 Method of Analysis

The Rational Method was used to calculate the runoff from the development. The Intensity-Duration-Frequency (IDF) curve formulas of the MacDonald Cartier International Airport, City of Ottawa, were used to calculate the peak storm flows.

5.5 Allowable Release Rate

The 5-year pre-development maximum allowable release rate was calculated from the rational method. Runoff from post-development conditions must be controlled to the pre-development runoff coefficient or a maximum of C=0.5, for both minor and major storms (5 year up to 100 year storms), using a time of concentration not less than 10 minutes. The areas used for the outlets 2 and 3 are 0.142ha and 0.207ha respectively.

6 EROSION AND SEDIMENT CONTROL

During construction, erosion and sediment controls will be provided primarily via a sediment control fence to be erected along the perimeter of the site where runoff has the potential of leaving the site. Inlet sediment control devices are also to be provided in any catchbasin and/or manhole in and around the site that may be impacted by the site construction. Construction and maintenance requirements for erosion and sediment controls are to comply with Ontario Provincial Standard Specification (OPSS) # 577. Refer to LRL drawing C.101 for erosion and sediment control details.

7 Conclusions

In accordance with the report objectives, the analyses of the proposed development can be summarized as follows:



Water Service

- The anticipated maximum domestic water demand of the site is 7.49L/s.
- The maximum required fire flow was calculated at 183.3 L/s using the FUS method.
- There is an existing fire hydrant located south of the building on Jamie Street within the 90m radius. There are also two (2) hydrants located on the east side of Merivale Road that are within 90m radius

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October 03, 2018

Page 9 of 10

- The new hydrant will be located within the 45m radius distance between the fire hydrant and the building Siamese connection.
- The new development/expansion will be serviced with a new 150mm dia. watermain connected to the new 150mm dia. watermain hydrant lead on Jamie Avenue.

Sanitary Service

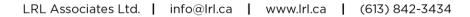
- The sanitary design flow from the proposed development is 2.58 L/s.
- The proposed building will be serviced by a new 200mm sanitary service connection to the existing 250mm dia. sanitary sewer on Jamie Avenue.
- A new monitoring manhole will be installed on the existing 100mm sanitary service that is connected to the existing 250mm dia. sanitary sewer on Jamie Avenue.

Stormwater Management

- In regards to Storm System / Outlet #1, in post-development conditions, a much smaller runoff area will outlet to the existing manhole in the shared ditch (0.017ha post; opposed to 0.233ha pre).
- The Storm System / Outlet #2 post-development release rates of 5.47 L/s (uncontrolled) and 29.52 L/s (controlled) will meet the existing pre-development release rate of 34.99 L/s onto Jamie Avenue.
- The Storm System / Outlet #3 post-development release rate of 14.99 L/s (controlled) will lower than the pre-development maximum allowable release rate of 29.98 L/s onto Jamie Avenue.
- Stormwater quantity control objectives will be met through on site stormwater storage.
- Stormwater quality control objectives will be met on-site through the use of two Stormceptor STC 300 oil/grit separators (one for each storm connection).

8 LIMITATIONS AND USE OF REPORT

The report conclusions are applicable only to the project described in the report. Any changes require a review by LRL Associates Ltd. to insure compatibility with the recommendations contained in this report. We trust the information presented in this report meets your current requirements. Please do not hesitate to contact us should you have any questions or concerns.



Prepared by:

LRL Associates Ltd.

9,

Guillaume Courtois, c.e.t., rcji Civil Engineering Technologist



Jean-Claude Lalonde, P.Eng Senior Project Engineer

APPENDIX A

Water Demand and Fire Flow Calculations



Water Supply Calculations

LRL File No. 130828

Project Proposed Benson Commercial Development

Date October 26, 2017 Designed: Checked: Guillaume Courtois M.Gagnon

Domestic Commercial Flow Demand

Total Building Floor Area = Site Total Area = 3285 ${\rm m}^{\rm 2}$ (Includes existing and proposed building)

0.58 ha

(As per OBC) Total Fixture Unit = 50 ea. Average Demand Per Fixture Unit = 3.33 L/min

Average Commercial Water Demand = 166.50 2.78 (42gpm as per AWWA #M22) L/min L/s

Maximum Daily Peak Factor = Maximum Daily Commercial = (As per City of Ottawa) 1.5

249.75 L/d 4.16

Maximum Hourly Peak Factor = Maximum Hourly Commercial = (As per City of Ottawa) 1.8 449.55 L/d 7.49 L/s

Therefore,

Total Domestic Flow = 7.49 L/s Total Fire Flow = 183.3 L/s





Fire Flow Calculations

LRL File No. 130828

Project Proposed Benson Commercial Development

Date October 26, 2017

Method Fire Underwriters Survey (FUS)

Designed by Guillaume Courtois

New Building	3285	
	3,285	m ²

Step	Task	Term	Options	Multiplier	Choose:	Value	unit	Fire Flow
			Structural Framing Ma	aterial				
			Wood Frame	1.5				
	04	Coefficient C	Ordinary Construction	1.0	1			
1	1 Choose frame used for building	related to the type of	Non-combustible construction	0.8	Ordinary Construction	1		
		construction	Fire resistive construction <2 hrs	0.7	1			
			Fire resistive construction >2 hrs	0.6	1			
			Floor Space Area	a				
			Single family dwelling	0				
2	Choose type of housing	Type of housing	Townhouse - no. of units	0	Building - no. of units per floor	1	units	
*			Building - no. of units per floor	1				
	Enter no. of storeys	Number of floors/storey	s for the building (excluding the basement)			2	floors	
3	Enter area of a unit	Enter floor space area of	of one unit	1	3285.0	1,643	sq.m.	
4	Obtain fire flow before	Required fire flow	Fire Fle	w = 220 v C v	AroaA ^{0.5}		L/min	13,000
	reductions	Trequired line now	File Flo	Fire Flow = 220 x C x Area ^{0.5}				
			Reductions or surcharge due to fact	ors affecting b	ourning			
		, , ,	Non-combustible	-0.25				
			Limited combustible	-0.15				
5			Combustible	0	Combustible	0		
			Free burning	0.15			L/min	13,000
			Rapid burning	0.25			L/s	216.7
			Sprinklers (NFPA13)	-0.30	True	-0.3		
6	Choose reduction for sprinklers	Sprinkler reduction	Water supply is standard for both the system and fire department hose lines	-0.10	False	0	L/min	9,100
			Fully supervised system	-0.10	False	0	L/s	151.7
			North side	10.1 to 20m	0.15			
7	Choose separation	Exposure distance	East side	Over 45m	0			
'	Choose separation	between units	South side	Over 45m	0		L/min	11,000
			West side	Over 45m	0	0.15	L/s	183.3
			Net required fire fl					
	Obtain fire flow,			Minimum	required fire flow rate (rounded to nea		L/min	11,000
8	duration, and volume	Minimum required fire flow rate				L/s	183.3	
		Required duration of fire flow hr 2.25						





Pipe Pressure Losses Calculations

LRL File No. 130828

Project Proposed Benson Commercial Development

Date October 26, 2017
Designed: Guillaume Courtois

Checked: M.Gagnon

Piezometric Head Equation (Derived from Bernoulli's Equation)

$$h = \frac{p}{\gamma} + z$$

Where:

 $_{h\,=\,}\,\text{HGL (m)}$

_{p =} Pressure (Pa)

 $\hat{\gamma}_{=}$ Specific weight (N/m3) = 9810 $z_{=}$ Elevation of centreline of pipe (m) = 84.73

Water Pressure at Jamie Avenue Connection											
HGL (m)		Pressure									
HGL (III)		kPa	psi								
Minimum =	126.7	411.73	59.72								
Maximum =	134.5	488.24	70.81								
Max. Day + Fire =	127.4	418.59	60.71								

Hazen Williams Equation

$$h_f = \frac{10.67 \times Q^{1.95} \times I}{C^{1.95} \times d^{4.97}}$$

Where:

 $h_{\rm f}\!=\!$ Head loss over the length of pipe (m)

Q = Volumetric flow rate (m³/s)

L = Length of pipe (m)

C = Pipe roughness coefficient

d = Pipe diameter (m)



Scenario 1: maximum daily demand

Q (L/s) C L (m.) I.D. (mm) V (m/s) h _f (m) Head Loss (psi) Min. Pressure (psi) Max. Pressure (psi) Service Obv. @ Street Connection (m)	4.16 100 29.3 155 0.22 0.02 0.03 59.69 70.78 84.88	
Service Obv. @ Building Connection (m) Pressure Adjustment (psi)	85.02 -0.20	(due to service elevation difference from street to building)
Adjusted Min. Pressure (psi) Adjusted Max. Pressure (psi)	59.49 70.58	(must not be less than 50psi) (must not be more than 80psi)

Scenario 2: maximum hourly demand

Q (L/s)	7.49	
C	100	
L (m.)	29.3	
I.D. (mm)	155	
V (m/s)	0.40	
h _f (m)	0.06	
Head Loss (psi)	0.09	
Min. Pressure (psi)	59.62	
Max. Pressure (psi)	70.72	
Service Obv. @ Street Connection (m)	84.88	
Service Obv. @ Building Connection (m)	85.02	
Pressure Adjustment (psi)	-0.20	(due to service elevation difference from street to building)
Adjusted Min. Pressure (psi)	59.43	(must not be less than 40psi)
Adjusted Max. Pressure (psi)	70.52	(must not be more than 80psi)

Scenario 3: maximum daily demand + fire flow

Q (L/s) C L (m.) I.D. (mm) V (m/s) h _f (m) Head Loss (psi) Pressure (psi) Service Obv. @ Street Connection (m) Service Obv. @ Building Connection (m)	187.46 100 29.3 155 9.93 24.72 35.15 25.56 84.88 85.02	M. GAGNON AROUNINGE OF OWNER
Pressure Adjustment (psi)	-0.20	(due to service elevation difference from street to building)
Adjusted Pressure (psi)	25.37	(must not be less than 20psi)

APPENDIX B

Sanitary Sewer Calculation Sheet



LRL File No. Project: Location:

Date:

130828

Proposed Benson Commercial Development : 1871 Merivale Road, Nepean, ON

October 26, 2017

Sanitary Design Parameters

Industrial Peak Factor = as per Appendix 4-B = 7 Extraneous Flow = 0.28 L/s/gross ha Pipe Design Parameters

Minimum Velocity = 0.60 m/s Manning's n = 0.013

	LOCATION			RESIDEN	ITIAL ARE	A AND POP	ULATION		COMM	ERCIAL	I.	NDUSTRIA	۱L	INSTITU	JTIONAL	C+I+I	INFILTRATION		TOTAL				MAN		HOLE				
CATCHMENT / STREET	FROM MH	то мн	AREA (Ha)	POP.	CUMM AREA (Ha)	POP.	PEAK FACT.	PEAK FLOW (l/s)	AREA (Ha)	ACCU. AREA (Ha)	AREA (Ha)	ACCU. AREA (Ha)	PEAK FACT.	AREA (Ha)	ACCU. AREA (Ha)	PEAK FLOW (l/s)	TOTAL AREA (Ha)	ACCU. AREA (Ha)	INFILT. FLOW (l/s)		LENGTH (m)	DIA. (mm)	SLOPE (%)	MATERAIL	CAP. (FULL) (l/s)	VEL. (FULL) (m/s)	Ratio (Q/Q _{FULL})	UP INVERT (m)	DOWN INVERT (m)
SA-01	PROP. BLDG	MH01	0.000	0.0	0.0	0.0	4.0	0.00	0.270	0.270	0.00	0.00	0.0	0.0	0.0	0.23	0.27	0.27	0.08	0.31	14.7	200	1.00%	PVC	32.80	1.04	0.01	85.08	84.93
	MH01	TRUNK	0.000	0.0	0.0	0.0	4.0	0.00	0.000	0.270	0.00	0.00	0.0	0.0	0.0	0.23	0.00	0.27	0.08	0.31	7.5	200	1.00%	PVC	32.80	1.04	0.01	84.93	84.85
SA-02	EX. BLDG	MH02	0.000	0.0	0.0	0.0	4.0	0.00	0.310	0.310	0.00	0.00	0.0	0.0	0.0	0.27	0.31	0.31	0.09	0.36	15.6	100	1.00%	ABS	5.17	0.66	0.07	84.69	84.53
	MH02	TRUNK	0.000	0.0	0.0	0.0	4.0	0.00	0.000	0.580	0.00	0.00	0.0	0.0	0.0	0.50	0.00	0.31	0.09	0.59	7.1	200	1.00%	PVC	32.80	1.04	0.02	84.53	84.41
																				0.90									
						NOTES								Designed	Designed: PROJECT:														
	Existing inverts	and slopes a	re estimate	ed. They are	to be confi	irmed on-site).								G.C.						Propo	osed Bens	son Comme	ercial Develo	pment				
														Checked:									LOCATIO	N:					
															M.G.							1817 M	lerivale Ro	ad, Ottawa					
														Dwg. Refe	erence:		File Ref.:				Date:						Sheet No.		
															C.401		130828 October 26, 2017												

Average Daily Flow = 350 L/p/day Commercial & Institutional Flow = 50000 L/ha/day

Light Industrial Flow = 35000 L/ha/day

Heavy Industrial Flow = 55000 L/ha/day

Maximum Residential Peak Factor = 4.0
Commercial & Institutional Peak Factor = 1.5



APPENDIX C

Stormwater Management Design Sheets

LRL Associates Ltd.

Storm Design Sheet



LRL File No. 130828

Project: Benson Commercial Development **Location:** 1871 Merivale Rd., Nepean, ON

Date: 03 Oct 2018

Designed: Guillaume Courtois
Checked: Jean-Claude Lalonde

Drawing Reference: C.702

Storm System / Site Outlet #2

Pre-development Catchments												
CATCHMENT	Grass C=0.20	River Stones C=0.70	Bldg. / Asph. / Conc. C=0.90	Total Area (ha)	Combined C							
CA-03	0.010	0.000	0.132	0.142	0.85							

Post-development Catchments													
CATCHMENT	CHMENT Grass C=0.20 River Stones C=0.7		Bldg. / Asph. / Conc. C=0.90	Total Area (ha)	Combined C								
CA-01	0.011	0.000	0.129	0.140	0.85								
CA-05	0.000	0.044	0.000	0.044	0.70								





LRL File No. 130828

 Project:
 Benson Commercial Development

 Location:
 1871 Merivale Rd., Nepean, ON

 Date:
 03 Oct 2018

 Designed:
 Guillaume Courtois

 Checked:
 Jean-Claude Lalonde

 Drawing Reference:
 C701 & C702

Rational Method Q = 2.78CIA

Q = Peak flow in litres per second (L/s)
A = Drainage area in hectares (ha)
C = Runoff coefficient

I = Rainfall intensity (mm/hr)

Runoff Coefficient (C)

Grass 0.2
Gravel 0.7
Bldg. / Asph. / Conc. 0.9

Storm Design Parameters

Ottawa Macdonald-Cartier International Airport

Storm Event 5 years Formula $I = a / (T_c + b)^c$

IDF Curve

Formula $I = a / (T_c + b)^c$ a = 998.071 b = 6.053 c = 0.814

Pipe Design Parameters

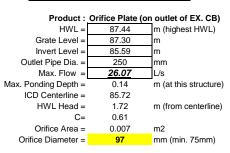
Maximum velocity = 3.00 m/s Minimum velocity = 0.80 m/s Manning's Coeff. "n" = 0.013

Pre and Post-Conditions at Storm System / Site Outlet #2

LOCATION AREA (ha) FLOW									STO	RM SEWER	₹						M	ANHOLE			WATE	RSHED	FLOW CONTROL									
CATCHMENT /STREET	From Structure	To Structure	Grass C=0.20	River Stones C=0.70	Bldg./ Asph./ Conc. C=0.90	Indiv. 2.78AC	Accum. 2.78AC	Conc.			Controlled Peak Flow Q (L/s)	Pipe Diameter (mm)	Туре	Slope (%)	Length (m)	Capacity Full (L/s)	Spar Capa y (L/s	cit Full	Time of Flow (min.)	Ratio (Q/Q _{FULL})	Up Invert (m)	Down Invert (m)	T/G Up Stream (m)	T/G Down Stream (m)	Depth	Down Depth obv (m)	Up Depth inv (m)	Total Area (ha)	Combined C	Controlled / Uncontrolled	Controlled Flow (Max.)	ICD
	PRE-DEVELOPMENT PRE-DEVELOPMENT																															
CA-03	EX. CB	Trunk	0.010	0.000	0.132	0.34	0.34	10.00	104.19	34.99	N/A	250	PVC	0.44%	24.0	39.45	4.46	6 0.80	0.50	0.89	85.59	85.49	87.00	87.60	1.16	1.86	1.41	0.142	0.85	Uncontrolled		
-																																
														POST-D	EVELOF	PMENT																
CA-05 (uncontrolled)	CB3	EX. CB	0.000	0.044	0.000	0.09	0.09	10.00	104.19	8.92	N/A	250	HDPE	6.00%	9.3	145.67	136.7	74 2.97	0.05	0.06	86.14	85.58	87.12	87.30	0.73	1.47	0.98	0.044	0.70	Uncontrolled		
CA-01 (controlled)	EX. CB	MH2	0.011	0.000	0.129	0.33	0.41	10.05	103.92	43.07	26.07	250	PVC	0.44%	20.3	39.67	-3.4	1 0.80	0.42	1.09	85.59	85.50	87.30	87.72	1.46	1.97	1.71	0.140	0.85	Controlled	29.52 L/s	Orifice Plate
	MH2	Trunk	0.000	0.000	0.000	0.00	0.41	10.48	101.75	42.17	26.07	250	PVC	0.44%	3.4	39.45	-2.7	3 0.80	0.07	1.07	85.50	85.49	87.72	87.60	1.97	1.86	2.22	0.000	0.00	Controlled	29.52 L/s	

Note: Post-Development Controlled Peak Flow of 26.07 L/s is the result of the Pre-Development Peak Flow of 34.99 L/s minus the Post-Development Uncontrolled Peak Flow of 5.47 L/s.

Inlet Control Device Parameters





LRL Associates Ltd.

Storm Design Sheet



LRL File No. 130828

Project: Benson Commercial Development **Location:** 1871 Merivale Rd., Nepean, ON

Date: 20 Jul 2018

Designed: Guillaume Courtois

Drawing Reference: C701 & C702

Storm System / Site Outlet #3

	Post-development Catchments												
CATCHMENT	Grass / Permeable Pavers C=0.20	River Stones C=0.70	Bldg. / Asph. / Conc. C=0.90	Total Area (ha)	Combined C								
CA-02	0.005	0.000	0.132	0.137	0.87								
CA-03	0.003	0.000	0.120	0.123	0.88								
CA-04	0.012	0.000	0.123	0.135	0.84								





LRL File No. 130828

Project: Benson Commercial Development **Location:** 1871 Merivale Rd., Nepean, ON

Date:20 Jul 2018Designed:Guillaume CourtoisDrawing Ref.:C701 & C702

Stormwater Management Design Sheet

(Tc shall not be less than 10min; therefore 10min is used for the following calculations.

Storm System / Site Outlet #3

Allowable Release Rate (5 Year Pre-development)

Time of Concentration:

$$Tc = G (1.1 - C) L^{0.5} / (S)^{1/3}$$

where: G = 3.26 Constant C = 0.9 Runoff Coefficient

L = 35.56 Longest flow path lenth in metres

S = 0.93 Slope %
Tc = 3.98 min.

This is also more conservative.)

Intensity:

 $I_5 = 998.071 / (Tc + 6.053)^{0.814}$

as per City of Ottawa Guidelines

where: I = intensity in mm/hr

Tc = Time of Concentration (10min)

 $I_5 = 104.2$

Allowable Release:

0.5 pre condition as per City of Ottawa Guidelines 104.2 mm/hr l = Tc = 10.00 min Total Site Area = 0.207 ha 29.98 2.78 x C x I x A Q = L/s



Catchment Area and Runoff Coeffecient (Post-development)

	Individual Watersheds	Total Area (ha)	Grass / Permeable Pavers Area (ha)	River Stones Area (ha)	Bldg. / Asph. / Conc. Area (ha)	∑C * A	C weighted (1:5 yr)	C weighted (1:100 yr)
p	CA-2	0.137	0.005	0.000	0.132	0.120	0.87	1.00
Controlled	CA-3	0.123	0.003	0.000	0.120	0.109	0.88	1.00
ပိ	CA-4	0.135	0.012	0.000	0.123	0.113	0.84	1.00

					1:5 YEAR	1:100 YEAR
	Total Site Area =	0.395	ha	∑C=	0.86	1.00
_	Bldg. / Asph. / Conc. Area =	0.375	ha	C=	0.90	1.00
Controlled	River Stones Area =	0.000	ha	C=	0.70	0.88
Contr	Grass Area =	0.020	ha	C=	0.20	0.25
	Total Controlled =	0.395	ha	Σc=	0.86	1.00



LRL File No. 130828

Project: Benson Commercial Development **Location:** 1871 Merivale Rd., Nepean, ON

Date:20 Jul 2018Designed:Guillaume CourtoisDrawing Ref.:C701 & C702

Stormwater Management Design Sheet

Post-development Stormwater Management

5 Year Post-development:

 $I_5 = 998.071 / (Tc + 6.053)^{0.814}$

as per City of Ottawa Guidelines

where: I = intensity in mm/hr
Tc = Time of Concentration

		1:5 YEA	R STORM EVENT		
Time	Intensity	Peak Flow	Release Rate	Storage Rate	Storage
(min)	(mm/hr)	(L/s)	(L/s)	(L/s)	Volume (m ³)
10	104.2	98.92	14.99	83.93	50.36
15	83.6	79.33	14.99	64.34	57.90
20	70.3	66.69	14.99	51.70	62.05
25	60.9	57.81	14.99	42.82	64.23
30	53.9	51.20	14.99	36.21	65.17
35	48.5	46.06	14.99	31.07	65.25
40	44.2	41.95	14.99	26.96	64.70
45	40.6	38.57	14.99	23.58	63.67
50	37.7	35.75	14.99	20.76	62.27
55	35.1	33.35	14.99	18.36	60.57
60	32.9	31.28	14.99	16.29	58.63

100 Year Post-development:

Intensity:

 $I_{100} = 1735.688 / (Tc + 6.014)^{0.820}$

as per City of Ottawa Guidelines

where: I = intensity in mm/hr
Tc = Time of Concentration

		1:100 YE	AR STORM EVENT		
Time	Intensity	Peak Flow	Release Rate	Storage Rate	Storage
(min)	(mm/hr)	(L/s)	(L/s)	(L/s)	Volume (m ³)
10	178.6	196.08	14.99	181.09	108.65
20	120.0	131.72	14.99	116.73	140.07
30	91.9	100.88	14.99	85.89	154.60
40	75.1	82.52	14.99	67.53	162.06
50	64.0	70.23	14.99	55.24	165.71
60	55.9	61.38	14.99	46.39	167.00
70	49.8	54.67	14.99	39.68	166.67
80	45.0	49.40	14.99	34.41	165.19
90	41.1	45.14	14.99	30.15	162.83
100	37.9	41.62	14.99	26.63	159.79
110	35.2	38.66	14.99	23.67	156.19





LRL File No. 130828

Project: Benson Commercial Development **Location:** 1871 Merivale Rd., Nepean, ON

Date:20 Jul 2018Designed:Guillaume CourtoisDrawing Ref.:C701 & C702

Stormwater Management Design Sheet

Onsite Stormwater Retention

Total Storage Required =167.00 m³Overland Ponding = 0.00 m^3 Pipe Storage = 4.42 m^3 CB/MH Storage = 1.23 m^3 Stormtech Chambers = 173.40 m^3

Total Available Storage = $\frac{179.05}{m^3}$ m³ Supplementary Storage Required = 0.00 m^3

refer to LRL Plan C.904



LRL Associates Ltd. Storm Design Sheet



LRL File No. 130828 Project: Benson Commercial Development Location: 1871 Merivale Rd., Nepean, ON 20 Jul 2018 Date: Designed: Guillaume Courtois Drawing Reference: C701 & C702

Q = 2.78CIA Rational Method

Q = Peak flow in litres per second (L/s)

A = Drainage area in hectares (ha)

C = Runoff coefficient

I = Rainfall intensity (mm/hr)

Runoff Coefficient (C) Grass / Permeable Pavers 0.2 Storm Event 5 years 0.7

0.9

Storm Design Parameters

IDF Curve Ottawa Macdonald-Cartier International Airport

6.053

c = 0.814

 $I = a / (T_c + b)^c$

b =

a = 998.07

Minimum velocity = 0.80 m/s Manning's Coeff. "n" = 0.013

Pipe Design Parameters

Post-Conditions at Storm System / Site Outlet #3

	LOCATION		AF	REA (ha)					FLOW						STORM SEWER							MANHO	I.F.			WATE	ERSHED		AVAII ABI F	STORAGE	:	FLO	OW CONTROL	
CATCHMENT A	From Structure	To Structure	Grass / Permeable Pavers C=0.20	River	Bldg./ Asph./ Conc. C=0.90	Indiv. 2.78AC	Accum. 2.78AC	Time of Conc. (min.)	Rainfall Intensity (mm/hr)	Peak Flow Q (L/s)	Controlled Peak Flow Q (L/s)	Pipe Diameter (mm)	Type Slope (%)		Capacity Full (L/s)	are Vel	ocity Time of Flow (min.)	i Ratio	Up Invert (m)	Down Invert (m)	T/G Up Stream (m)	T/G	Up Depth obv (m)	I lenth	Jp Depth inv (m)	Total	Combined C	Pipe	Upstream	Water Depth (m)	CB/MH Storage		Controlled Flow (Max.)	ICD
CA-02	PR. CB1	PR. CBMH1	0.005	0.000	0.132	0.33	0.33	10.00	104.19	34.70	N/A	SC-740							85.85	85.84	87.08	87.06			1.23	0.137	0.87		0.60	0.71	0.26	Uncontrolled		
																																i I		
CA-04	PR. CB2	PR. CBMH1	0.012	0.000	0.123	0.31	0.31	10.00	104.19	32.76	N/A	300	PVC 0.34%	62.5	56.39 23	.63 0	.80 1.31	0.58	86.12	85.91	86.99	87.06	0.57	0.85	0.87	0.135	0.84	4.42	0.60	0.44	0.16	Uncontrolled		
																																i I		
CA-03	PR. CBMH1	STC300 Stormceptor-01	0.003	0.000	0.120	0.30	0.95	11.31	97.77	92.82	14.99	375	PVC 0.31%	4.2	97.62 4.	80 0	.88 0.08	0.95	85.84	85.83	87.06	87.24	0.84	1.04	1.22	0.123	0.88		1.20	0.72	0.81	Controlled	29.98 L/s 1	125VHV-2
	STC300 Stormceptor-01	PR. MH1					0.95	11.39	97.41	92.47	14.99	375	PVC 0.31%	4.2	97.62 5.	15 0	.88 0.08	0.95	85.76	85.75	87.24	87.27	1.10	1.15	1.48				1.20	0.80		Controlled	29.98 L/s	
Note: Flow restr	ictor has been incorporated.																											4.42			1.23	i T		

River Stones

Bldg. / Asph. / Conc.

100yr HWL 86.56 Total Storage 5.65



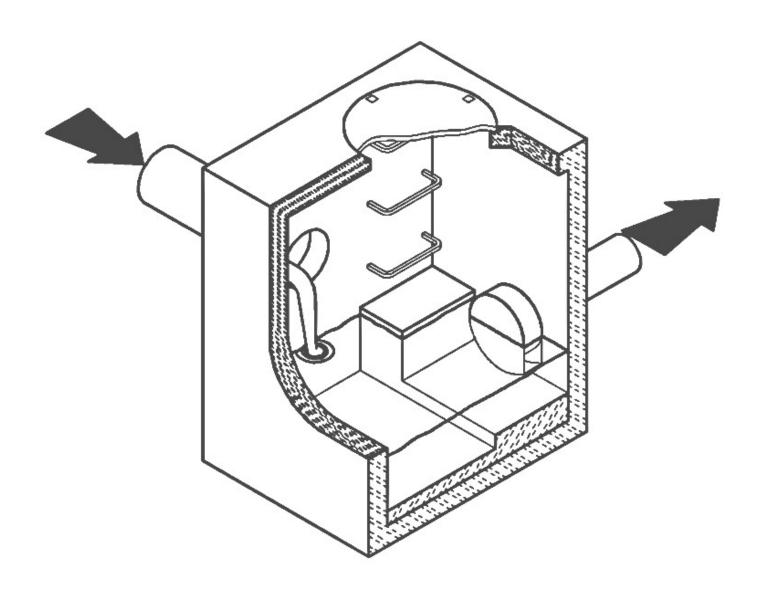
APPENDIX D

Hydrovex Vertical Vortex Flow Regulator Report

CSO/STORMWATER MANAGEMENT



• HYDROVEX® VHV / SVHV Vertical Vortex Flow Regulator



JOHN MEUNIER

HYDROVEX® VHV / SVHV VERTICAL VORTEX FLOW REGULATOR

APPLICATIONS

One of the major problems of urban wet weather flow management is the runoff generated after a heavy rainfall. During a storm, uncontrolled flows may overload the drainage system and cause flooding. Due to increased velocities, sewer pipe wear is increased dramatically and results in network deterioration. In a combined sewer system, the wastewater treatment plant may also experience significant increases in flows during storms, thereby losing its treatment efficiency.

A simple means of controlling excessive water runoff is by controlling excessive flows at their origin (manholes). **John Meunier Inc.** manufactures the **HYDROVEX**[®] **VHV** / **SVHV** line of vortex flow regulators to control stormwater flows in sewer networks, as well as manholes.

The vortex flow regulator design is based on the fluid mechanics principle of the forced vortex. This grants flow regulation without any moving parts, thus reducing maintenance. The operation of the regulator, depending on the upstream head and discharge, switches between orifice flow (gravity flow) and vortex flow. Although the concept is quite simple, over 12 years of research have been carried out in order to get a high performance.

The HYDROVEX® VHV / SVHV Vertical Vortex Flow Regulators (refer to Figure 1) are manufactured entirely of stainless steel, and consist of a hollow body (1) (in which flow control takes place) and an outlet orifice (7). Two rubber "O" rings (3) seal and retain the unit inside the outlet pipe. Two stainless steel retaining rings (4) are welded on the outlet sleeve to ensure that there is no shifting of the "O" rings during installation and use.

- 1. BODY
- 2. SLEEVE
- 3. O-RING
- RETAINING RINGS (SQUARE BAR)
- 5. ANCHOR PLATE
- 6. INLET
- 7. OUTLET ORIFICE

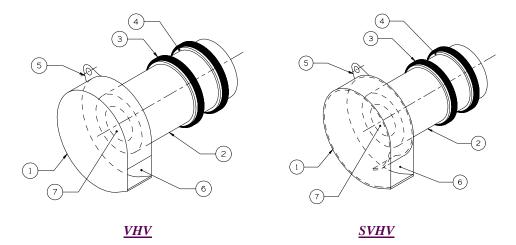


FIGURE 1: HYDROVEX® VHV-SVHV VERTICAL VORTREX FLOW REGULATORS

ADVANTAGES

- The **HYDROVEX**® **VHV** / **SVHV** line of flow regulators are manufactured entirely of stainless steel, making them durable and corrosion resistant.
- Having no moving parts, they require minimal maintenance.
- The geometry of the HYDROVEX® VHV / SVHV flow regulators allows a control equal to an orifice plate, having a cross section area 4 to 6 times smaller. This decreases the chance of blockage of the regulator, due to sediments and debris found in stormwater flows. Figure 2 illustrates the comparison between a regulator model 100 SVHV-2 and an equivalent orifice plate. One can see that for the same height of water, the regulator controls a flow approximately four times smaller than an equivalent orifice plate.
- Installation of the **HYDROVEX**® **VHV** / **SVHV** flow regulators is quick and straightforward and is performed after all civil works are completed.
- Installation requires no special tools or equipment and may be carried out by any contractor.
- Installation may be carried out in existing structures.

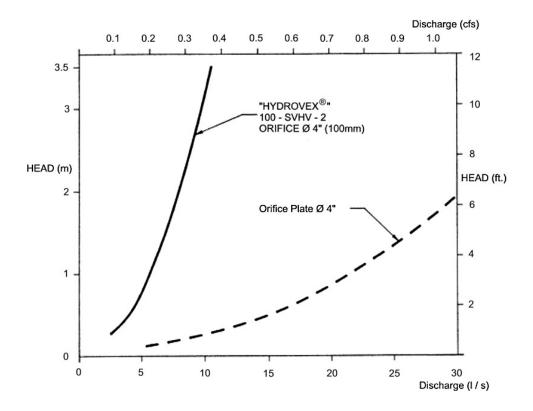


FIGURE 2: DISCHARGE CURVE SHOWING A HYDROVEX® FLOW REGULATOR VS AN ORIFICE PLATE

SELECTION

Selection of a **VHV or SVHV** regulator can be easily made using the selection charts found at the back of this brochure (see **Figure 3**). These charts are a graphical representation of the maximum upstream water pressure (head) and the maximum discharge at the manhole outlet. The maximum design head is the difference between the maximum upstream water level and the invert of the outlet pipe. All selections should be verified by John Meunier Inc. personnel prior to fabrication.

Example:

✓ Maximum design head 2m (6.56 ft.) ✓ Maximum discharge 6 L/s (0.2 cfs)

✓ Using **Figure 3** - VHV model required is a **75 VHV-1**

INSTALLATION REQUIREMENTS

All HYDROVEX® VHV / SVHV flow regulators can be installed in circular or square manholes. Figure 4 gives the various minimum dimensions required for a given regulator. It is imperative to respect the minimum clearances shown to ensure easy installation and proper functioning of the regulator.

SPECIFICATIONS

In order to specify a **HYDROVEX**® regulator, the following parameters must be defined:

- The model number (ex: 75-VHV-1)
- The diameter and type of outlet pipe (ex: 6" diam. SDR 35)
- The desired discharge (ex: 6 l/s or 0.21 CFS)
- The upstream head (ex: 2 m or 6.56 ft.) *
- The manhole diameter (ex: 36" diam.)
- The minimum clearance "H" (ex: 10 inches)
- The material type (ex: 304 s/s, 11 Ga. standard)
- * Upstream head is defined as the difference in elevation between the maximum upstream water level and the invert of the outlet pipe where the HYDROVEX® flow regulator is to be installed.

PLEASE NOTE THAT WHEN REQUESTING A PROPOSAL, WE SIMPLY REQUIRE THAT YOU PROVIDE US WITH THE FOLLOWING:

- project design flow rate
- pressure head
- > chamber's outlet pipe diameter and type



Typical VHV model in factory



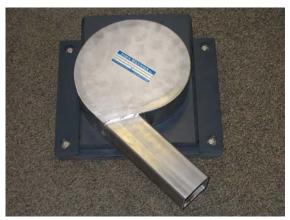
FV – SVHV (mounted on sliding plate)



VHV-1-O (standard model with odour control inlet)



VHV with Gooseneck assembly in existing chamber without minimum release at the bottom



FV – VHV-O (mounted on sliding plate with odour control inlet)



VHV with air vent for minimal slopes



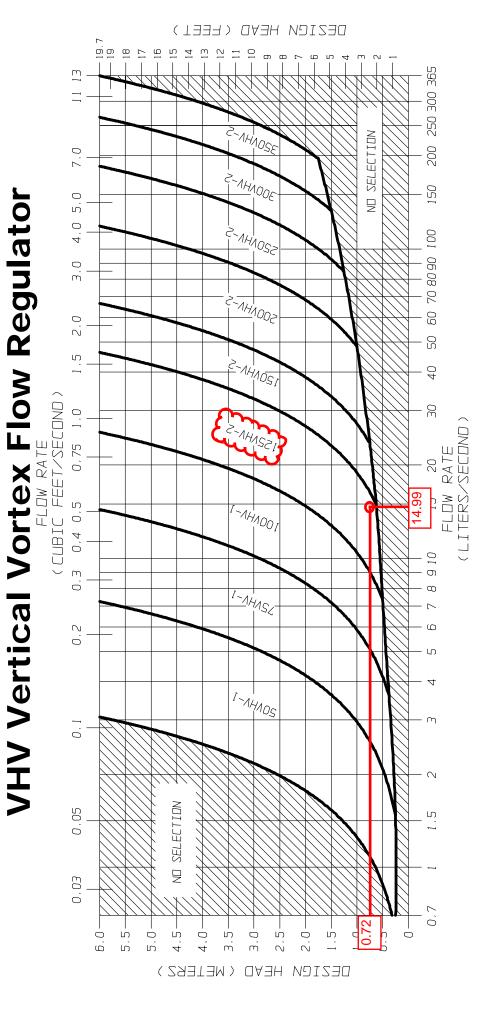
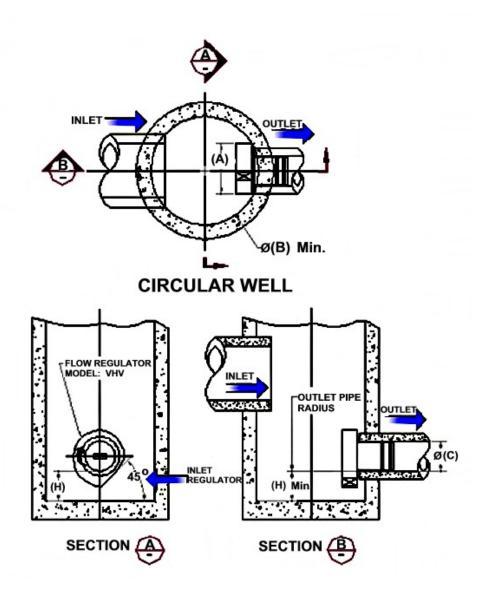


FIGURE 3 - VHV

JOHN MEUNIER

FLOW REGULATOR TYPICAL INSTALLATION IN CIRCULAR MANHOLE FIGURE 4 (MODEL VHV)

Model Number		ılator neter		Manhole neter		n Outlet ameter	Minimum Clearance		
	A (mm)	A (in.)	B (mm)	B (in.)	C (mm)	C (in.)	H (mm)	H (in.)	
50VHV-1	150	6	600	24	150	6	150	6	
75VHV-1	250	10	600	24	150	6	150	6	
100VHV-1	325	13	900	36	150	6	200	8	
125VHV-2	275	11	900	36	150	6	200	8	
150VHV-2	350	14	900	36	150	6	225	9	
200VHV-2	450	18	1200	48	200	8	300	12	
250VHV-2	575	23	1200	48	250	10	350	14	
300VHV-2	675	27	1600	64	250	10	400	16	
350VHV-2	800	32	1800	72	300	12	500	20	



INSTALLATION

The installation of a HYDROVEX® regulator may be undertaken once the manhole and piping is in place. Installation consists of simply fitting the regulator into the outlet pipe of the manhole. **John Meunier Inc.** recommends the use of a lubricant on the outlet pipe, in order to facilitate the insertion and orientation of the flow controller.

MAINTENANCE

HYDROVEX® regulators are manufactured in such a way as to be maintenance free; however, a periodic inspection (every 3-6 months) is suggested in order to ensure that neither the inlet nor the outlet has become blocked with debris. The manhole should undergo periodically, particularly after major storms, inspection and cleaning as established by the municipality

GUARANTY

The HYDROVEX® line of VHV / SVHV regulators are guaranteed against both design and manufacturing defects for a period of 5 years. Should a unit be defective, John Meunier Inc. is solely responsible for either modification or replacement of the unit.

ISO 9001: 2008 **Head Office**

4105 Sartelon

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USA Office

2209 Menlo Avenue Glenside, PA USA 19038

Tel.: 412-417-6614 www.johnmeunier.com



APPENDIX E

StormTech System Design Sheets

PRO	PROJECT INFORMATION							
ENGINEERED PRODUCT MANAGER:	VIVEK SHARMA 647-463-9803 VIVEK.SHARMA@ADS-PIPE.COM							
ADS SALES REP:	HASSAN ELMI 416-985-9757 HASSAN.ELMI@ADS-PIPE.COM							
PROJECT NO:	97633							





1871 MERIVALE

OTTAWA, ON

STORMTECH CHAMBER SPECIFICATIONS

- CHAMBERS SHALL BE STORMTECH SC-740 OR SC-310.
- 2. CHAMBERS SHALL BE MANUFACTURED FROM VIRGIN POLYPROPYLENE OR POLYETHYLENE RESINS.
- 3. CHAMBER ROWS SHALL PROVIDE CONTINUOUS, UNOBSTRUCTED INTERNAL SPACE WITH NO INTERNAL SUPPORT PANELS THAT WOULD IMPEDE FLOW OR LIMIT ACCESS FOR INSPECTION.
- 4. THE STRUCTURAL DESIGN OF THE CHAMBERS, THE STRUCTURAL BACKFILL, AND THE INSTALLATION REQUIREMENTS SHALL ENSURE THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, SECTION 12.12, ARE MET FOR: 1) LONG-DURATION DEAD LOADS AND 2) SHORT-DURATION LIVE LOADS, BASED ON THE CSA S6 CL-625 TRUCK AND THE AASHTO DESIGN TRUCK WITH CONSIDERATION FOR IMPACT AND MULTIPLE VEHICLE PRESENCES.
- 5. CHAMBERS SHALL BE CERTIFIED TO CSA B184, "POLYMERIC SUB-SURFACE STORMWATER MANAGEMENT STRUTURES", AND MEET ASTM F2922 (POLYETHYLENE) OR ASTM F2418-16 (POLYPROPYLENE), "STANDARD SPECIFICATION FOR THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- 6. CHAMBERS SHALL BE DESIGNED AND ALLOWABLE LOADS DETERMINED IN ACCORDANCE WITH ASTM F2787, "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- 7. ONLY CHAMBERS THAT ARE APPROVED BY THE SITE DESIGN ENGINEER WILL BE ALLOWED. THE CHAMBER MANUFACTURER SHALL SUBMIT THE FOLLOWING UPON REQUEST TO THE SITE DESIGN ENGINEER FOR APPROVAL BEFORE DELIVERING CHAMBERS TO THE PROJECT SITE:
 - a. A STRUCTURAL EVALUATION SEALED BY A REGISTERED PROFESSIONAL ENGINEER THAT DEMONSTRATES THAT THE SAFETY FACTORS ARE GREATER THAN OR EQUAL TO 1.95 FOR DEAD LOAD AND 1.75 FOR LIVE LOAD, THE MINIMUM REQUIRED BY ASTM F2787 AND BY AASHTO FOR THERMOPLASTIC PIPE.
 - b. A STRUCTURAL EVALUATION SEALED BY A REGISTERED PROFESSIONAL ENGINEER THAT DEMONSTRATES THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, SECTION 12.12, ARE MET. THE 50 YEAR CREEP MODULUS DATA SPECIFIED IN ASTM F2418 OR ASTM F2922 MUST BE USED AS PART OF THE AASHTO STRUCTURAL EVALUATION TO VERIFY LONG-TERM PERFORMANCE.
 - c. STRUCTURAL CROSS SECTION DETAIL ON WHICH THE STRUCTURAL EVALUATION IS BASED.
- 8. CHAMBERS AND END CAPS SHALL BE PRODUCED AT AN ISO 9001 CERTIFIED MANUFACTURING FACILITY.

IMPORTANT - NOTES FOR THE BIDDING AND INSTALLATION OF THE SC-310/SC-740 SYSTEM

- 1. STORMTECH SC-310 & SC-740 CHAMBERS SHALL NOT BE INSTALLED UNTIL THE MANUFACTURER'S REPRESENTATIVE HAS COMPLETED A PRE-CONSTRUCTION MEETING WITH THE INSTALLERS.
- 2. STORMTECH SC-310 & SC-740 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH SC-310/SC-740/SC-780 CONSTRUCTION GUIDE".
- 3. CHAMBERS ARE NOT TO BE BACKFILLED WITH A DOZER OR AN EXCAVATOR SITUATED OVER THE CHAMBERS. STORMTECH RECOMMENDS 3 BACKFILL METHODS:
 - STONESHOOTER LOCATED OFF THE CHAMBER BED.
 - BACKFILL AS ROWS ARE BUILT USING AN EXCAVATOR ON THE FOUNDATION STONE OR SUBGRADE.
 - BACKFILL FROM OUTSIDE THE EXCAVATION USING A LONG BOOM HOE OR EXCAVATOR.
- 4. THE FOUNDATION STONE SHALL BE LEVELED AND COMPACTED PRIOR TO PLACING CHAMBERS.
- 5. JOINTS BETWEEN CHAMBERS SHALL BE PROPERLY SEATED PRIOR TO PLACING STONE.
- 6. MAINTAIN MINIMUM 150 mm (6") SPACING BETWEEN THE CHAMBER ROWS.
- EMBEDMENT STONE SURROUNDING CHAMBERS MUST BE A CLEAN, CRUSHED, ANGULAR STONE 20-50 mm (3/4-2").
- 8. THE CONTRACTOR MUST REPORT ANY KNOWN DISCREPANCIES WITH CHAMBER FOUNDATION MATERIALS BEARING CAPACITIES TO THE SITE DESIGN ENGINEER.
- ADS RECOMMENDS THE USE OF "FLEXSTORM CATCH IT" INSERTS DURING CONSTRUCTION FOR ALL INLETS TO PROTECT THE SUBSURFACE STORMWATER MANAGEMENT SYSTEM FROM CONSTRUCTION SITE RUNOFF.

NOTES FOR CONSTRUCTION EQUIPMENT

- STORMTECH SC-310 & SC-740 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE".
- 2. THE USE OF CONSTRUCTION EQUIPMENT OVER SC-310 & SC-740 CHAMBERS IS LIMITED:
 - NO EQUIPMENT IS ALLOWED ON BARE CHAMBERS.
 - NO RUBBER TIRED LOADERS, DUMP TRUCKS, OR EXCAVATORS ARE ALLOWED UNTIL PROPER FILL DEPTHS ARE REACHED IN ACCORDANCE WITH THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE".
 - WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT CAN BE FOUND IN THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE".
- 3. FULL 900 mm (36") OF STABILIZED COVER MATERIALS OVER THE CHAMBERS IS REQUIRED FOR DUMP TRUCK TRAVEL OR DUMPING.

USE OF A DOZER TO PUSH EMBEDMENT STONE BETWEEN THE ROWS OF CHAMBERS MAY CAUSE DAMAGE TO THE CHAMBERS AND IS NOT AN ACCEPTABLE BACKFILL METHOD. ANY CHAMBERS DAMAGED BY THE "DUMP AND PUSH" METHOD ARE NOT COVERED UNDER THE STORMTECH STANDARD WARRANTY.

CONTACT STORMTECH AT 1-888-892-2694 WITH ANY QUESTIONS ON INSTALLATION REQUIREMENTS OR WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT.

PROPOSED LAYOUT STORMTECH SC-740 CHAMBERS STORMTECH SC-740 END CAPS STONE ABOVE (mm) 152 STONE BELOW (mm) 152 % STONE VOID 40 **INSTALLED SYSTEM VOLUME (m³)** (PERIMETER STONE INCLUDED / BASE STONE NOT 173.4 SYSTEM AREA (m²) 297 SYSTEM PERIMETER (m) 112

PROPOSED ELEVATIONS

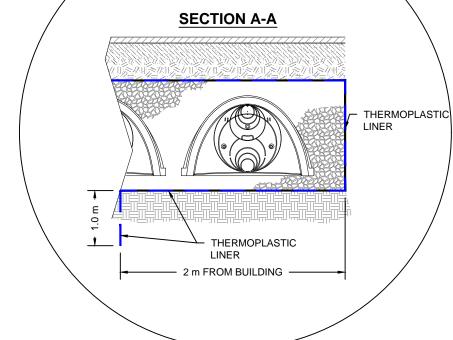
MAXIMUM ALLOWABLE GRADE (TOP OF PAVEMENT/UNPAVED):	89.0020
MINIMUM ALLOWABLE GRADE (UNPAVED WITH TRAFFIC):	87.1740
MINIMUM ALLOWABLE GRADE (UNPAVED NO TRAFFIC):	87.0210
MINIMUM ALLOWABLE GRADE (BASE OF FLEXIBLE PAVEMENT):	87.0210
MINIMUM ALLOWABLE GRADE (TOP OF RIGID PAVEMENT):	87.0210
TOP OF STONE:	86.7160
TOP OF SC-740 CHAMBER:	86.5640
300 mm TOP MANIFOLD INVERT:	86.1190
450 mm ISOLATOR ROW INVERT:	85.8430
BOTTOM OF SC-740 CHAMBER:	85.8020
BOTTOM OF STONE:	85.6500

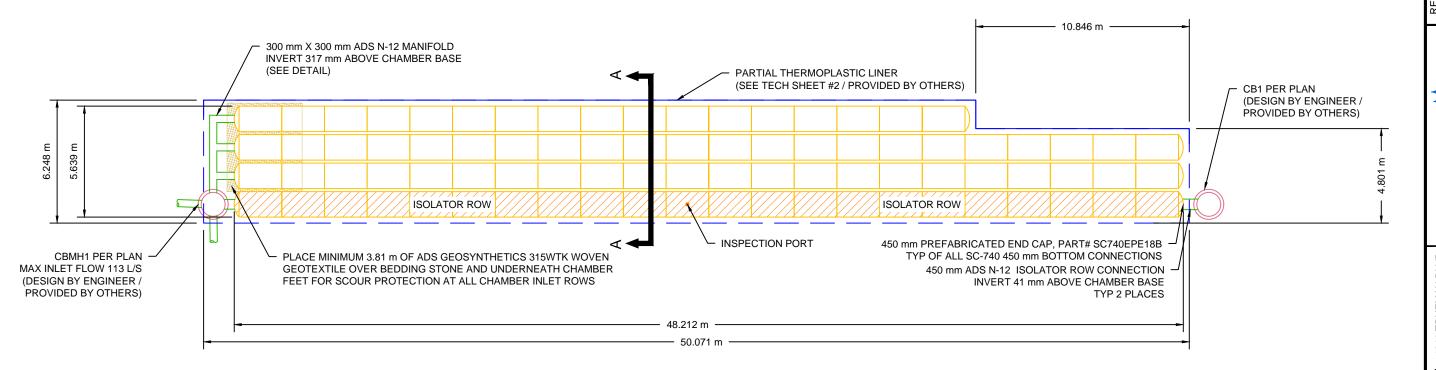
NOTES MANIFOLD SIZE TO BE DETERMINED BY SITE DESIGN ENGINEER. SEE TECH SHEET #7 FOR MANIFOLD SIZING GUIDANCE.

DUE TO THE ADAPTATION OF THIS CHAMBER SYSTEM TO SPECIFIC SITE AND DESIGN CONSTRAINTS, IT MAY BE

NECESSARY TO CUT AND COUPLE ADDITIONAL PIPE TO STANDARD MANIFOLD COMPONENTS IN THE FIELD.

- THE SITE DESIGN ENGINEER MUST REVIEW ELEVATIONS AND IF NECESSARY ADJUST GRADING TO ENSURE THE CHAMBER COVER REQUIREMENTS ARE MET.
- ADS DOES NOT DESIGN OR PROVIDE MEMBRANE LINER SYSTEMS FOR CISTERNS (RAINWATER HARVESTING). TO MINIMIZE
 THE LEAKAGE POTENTIAL OF LINER SYSTEMS, THE MEMBRANE LINER SYSTEM SHOULD BE DESIGNED BY A
 KNOWLEDGABLE GEOTEXTILE PROFESSIONAL AND INSTALLED BY A QUALIFIED CONTRACTOR.





07-28-15 GM NEW VOLUME - 72.3 m³ OTTAWA, ON 03-27-17 DL GFI REVISED PER COMMENTS DATE: 04-22-15 DRAWN: G 06-24-17 KR CJD REVISED INVERTS & IR SIZE PROJECT #: 97633 CHECKED: KI
EVATIONS DATE: ZE PROJECT #:
3-28-17 MLB NPB REVISED FOR VOLUME/ELEVATIONS DATE: 08-24-17 KR CJD REVISED INVERTS & IR SIZE PROJECT #:
08-24-17 KR CJD REVISED INVERTS & IR SIZE 11-06-17 KR CJD REVISED PER ENGINEER PROJECT #: 97633
11-06-17 KR CJD REVISED PER ENGINEER PROJECT #: 97633

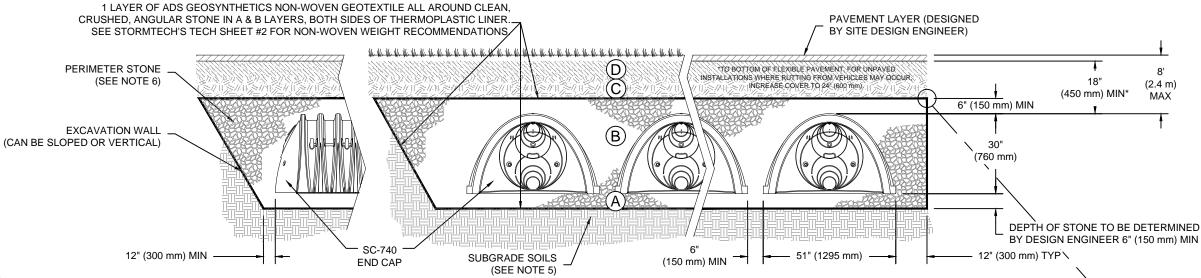
SHEET 2 OF 5

ACCEPTABLE FILL MATERIALS: STORMTECH SC-740 CHAMBER SYSTEMS

	MATERIAL LOCATION	DESCRIPTION	AASHTO MATERIAL CLASSIFICATIONS	COMPACTION / DENSITY REQUIREMENT
D	FINAL FILL: FILL MATERIAL FOR LAYER 'D' STARTS FROM THE TOP OF THE 'C' LAYER TO THE BOTTOM OF FLEXIBLE PAVEMENT OR UNPAVED FINISHED GRADE ABOVE. NOTE THAT PAVEMENT SUBBASE MAY BE PART OF THE 'D' LAYER	ANY SOIL/ROCK MATERIALS, NATIVE SOILS, OR PER ENGINEER'S PLANS. CHECK PLANS FOR PAVEMENT SUBGRADE REQUIREMENTS.	N/A	PREPARE PER SITE DESIGN ENGINEER'S PLANS. PAVED INSTALLATIONS MAY HAVE STRINGENT MATERIAL AND PREPARATION REQUIREMENTS.
С	INITIAL FILL: FILL MATERIAL FOR LAYER 'C' STARTS FROM THE TOP OF THE EMBEDMENT STONE ('B' LAYER) TO 18" (450 mm) ABOVE THE TOP OF THE CHAMBER. NOTE THAT PAVEMENT SUBBASE MAY BE A PART OF THE 'C' LAYER.	GRANULAR WELL-GRADED SOIL/AGGREGATE MIXTURES, <35% FINES OR PROCESSED AGGREGATE. MOST PAVEMENT SUBBASE MATERIALS CAN BE USED IN LIEU OF THIS LAYER.	AASHTO M145 ¹ A-1, A-2-4, A-3 OR AASHTO M43 ¹ 3, 357, 4, 467, 5, 56, 57, 6, 67, 68, 7, 78, 8, 89, 9, 10	BEGIN COMPACTIONS AFTER 12" (300 mm) OF MATERIAL OVER THE CHAMBERS IS REACHED. COMPACT ADDITIONAL LAYERS IN 6" (150 mm) MAX LIFTS TO A MIN. 95% PROCTOR DENSITY FOR WELL GRADED MATERIAL AND 95% RELATIVE DENSITY FOR PROCESSED AGGREGATE MATERIALS. ROLLER GROSS VEHICLE WEIGHT NOT TO EXCEED 12,000 lbs (53 kN). DYNAMIC FORCE NOT TO EXCEED 20,000 lbs (89 kN).
В	EMBEDMENT STONE: FILL SURROUNDING THE CHAMBERS FROM THE FOUNDATION STONE ('A' LAYER) TO THE 'C' LAYER ABOVE.	CLEAN, CRUSHED, ANGULAR STONE, NOMINAL SIZE DISTRIBUTION BETWEEN 3/4-2 INCH (20-50 mm)	AASHTO M43 ¹ 3, 357, 4, 467, 5, 56, 57	NO COMPACTION REQUIRED.
Α	FOUNDATION STONE: FILL BELOW CHAMBERS FROM THE SUBGRADE UP TO THE FOOT (BOTTOM) OF THE CHAMBER.	CLEAN, CRUSHED, ANGULAR STONE, NOMINAL SIZE DISTRIBUTION BETWEEN 3/4-2 INCH (20-50 mm)	AASHTO M43 ¹ 3, 357, 4, 467, 5, 56, 57	PLATE COMPACT OR ROLL TO ACHIEVE A FLAT SURFACE. 23

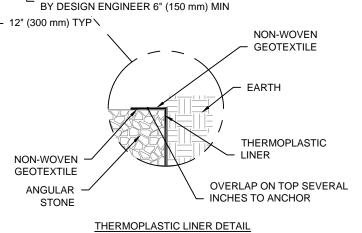
PLEASE NOTE:

- THE LISTED AASHTO DESIGNATIONS ARE FOR GRADATIONS ONLY. THE STONE MUST ALSO BE CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR FOR EXAMPLE, ANGU ANGULAR NO. 4 (AASHTO M43) STONE"
- STORMTECH COMPACTION REQUIREMENTS ARE MET FOR 'A' LOCATION MATERIALS WHEN PLACED AND COMPACTED IN 6" (150 mm) (MAX) LIFTS USING TWO FULL COVERAGES WITH A VIBRATORY COMPACTOR.
- WHERE INFILTRATION SURFACES MAY BE COMPROMISED BY COMPACTION, FOR STANDARD DESIGN LOAD CONDITIONS, A FLAT SURFACE MAY BE ACHIEVED BY RAKING OR DRAGGING WITHOUT COMPACTION EQUIPMENT. FOR SPECIAL LOAD DESIGNS, CONTACT STORMTECH FOR COMPACTION REQUIREMENTS.



NOTES:

- 1. SC-740 CHAMBERS SHALL CONFORM TO THE REQUIREMENTS OF ASTM F2418 "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS", OR ASTM F2922 "STANDARD SPECIFICATION FOR POLYETHYLENE (PE) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- SC-740 CHAMBERS SHALL BE DESIGNED IN ACCORDANCE WITH ASTM F2787 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- "ACCEPTABLE FILL MATERIALS" TABLE ABOVE PROVIDES MATERIAL LOCATIONS, DESCRIPTIONS, GRADATIONS, AND COMPACTION REQUIREMENTS FOR FOUNDATION, EMBEDMENT, AND FILL MATERIALS.
- THE "SITE DESIGN ENGINEER" REFERS TO THE ENGINEER RESPONSIBLE FOR THE DESIGN AND LAYOUT OF THE STORMTECH CHAMBERS FOR THIS PROJECT.
- THE SITE DESIGN ENGINEER IS RESPONSIBLE FOR ASSESSING THE BEARING RESISTANCE (ALLOWABLE BEARING CAPACITY) OF THE SUBGRADE SOILS AND THE DEPTH OF FOUNDATION STONE WITH CONSIDERATION FOR THE RANGE OF EXPECTED SOIL MOISTURE CONDITIONS.
- PERIMETER STONE MUST BE EXTENDED HORIZONTALLY TO THE EXCAVATION WALL FOR BOTH VERTICAL AND SLOPED EXCAVATION WALLS.
- 7. ONCE LAYER 'C' IS PLACED, ANY SOIL/MATERIAL CAN BE PLACED IN LAYER 'D' UP TO THE FINISHED GRADE, MOST PAVEMENT SUBBASE SOILS CAN BE USED TO REPLACE THE MATERIAL REQUIREMENTS OF LAYER 'C' OR 'D' AT THE SITE DESIGN ENGINEER'S DISCRETION.



PROJECT #: 97633 Storm 4640 TRUEMAN BLVD HILLIARD, OH 43026 I-800-733-7473 SHEET 3 OF

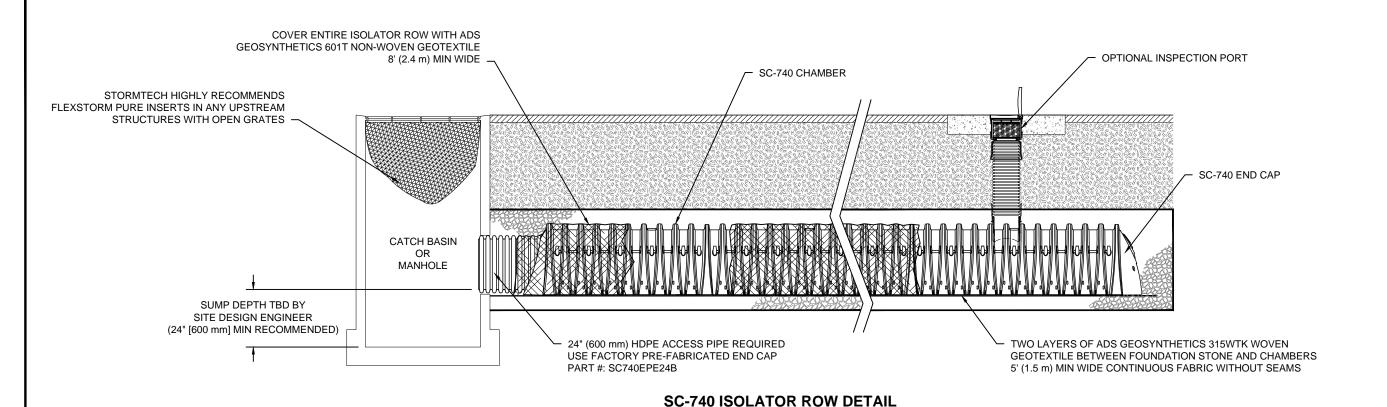
Ω

DRAWN:

04-22-15

OTTAWA, ON

1871 MERIVAL



INSPECTION & MAINTENANCE

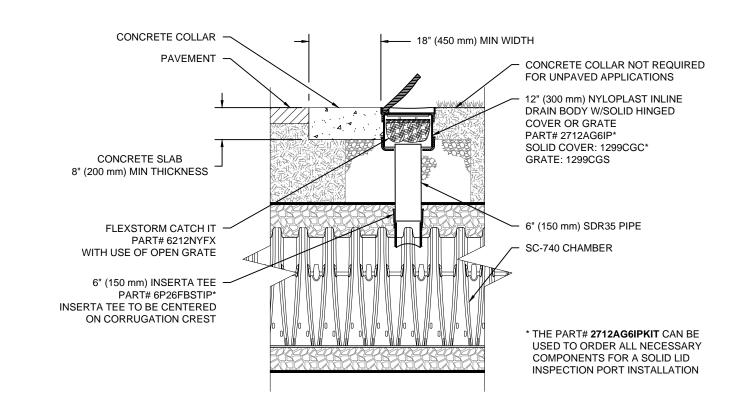
STEP 1) INSPECT ISOLATOR ROW FOR SEDIMENT

A. INSPECTION PORTS (IF PRESENT)

- REMOVE/OPEN LID ON NYLOPLAST INLINE DRAIN
- REMOVE AND CLEAN FLEXSTORM FILTER IF INSTALLED A.2.
- USING A FLASHLIGHT AND STADIA ROD, MEASURE DEPTH OF SEDIMENT AND RECORD ON MAINTENANCE LOG A.3.
- LOWER A CAMERA INTO ISOLATOR ROW FOR VISUAL INSPECTION OF SEDIMENT LEVELS (OPTIONAL)
- IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2. IF NOT, PROCEED TO STEP 3. A.5.
- B. ALL ISOLATOR ROWS
- REMOVE COVER FROM STRUCTURE AT UPSTREAM END OF ISOLATOR ROW USING A FLASHLIGHT, INSPECT DOWN THE ISOLATOR ROW THROUGH OUTLET PIPE
- - i) MIRRORS ON POLES OR CAMERAS MAY BE USED TO AVOID A CONFINED SPACE ENTRY
 - ii) FOLLOW OSHA REGULATIONS FOR CONFINED SPACE ENTRY IF ENTERING MANHOLE IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2. IF NOT, PROCEED TO STEP 3.
- CLEAN OUT ISOLATOR ROW USING THE JETVAC PROCESS
 - A. A FIXED CULVERT CLEANING NOZZLE WITH REAR FACING SPREAD OF 45" (1.1 m) OR MORE IS PREFERRED
 - APPLY MULTIPLE PASSES OF JETVAC UNTIL BACKFLUSH WATER IS CLEAN
 - C. VACUUM STRUCTURE SUMP AS REQUIRED
- REPLACE ALL COVERS, GRATES, FILTERS, AND LIDS; RECORD OBSERVATIONS AND ACTIONS.
- INSPECT AND CLEAN BASINS AND MANHOLES UPSTREAM OF THE STORMTECH SYSTEM.

NOTES

- INSPECT EVERY 6 MONTHS DURING THE FIRST YEAR OF OPERATION. ADJUST THE INSPECTION INTERVAL BASED ON PREVIOUS OBSERVATIONS OF SEDIMENT ACCUMULATION AND HIGH WATER ELEVATIONS.
- 2. CONDUCT JETTING AND VACTORING ANNUALLY OR WHEN INSPECTION SHOWS THAT MAINTENANCE IS NECESSARY.



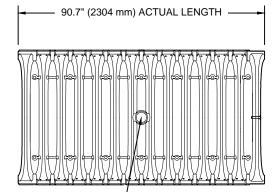
SC-740 6" INSPECTION PORT DETAIL

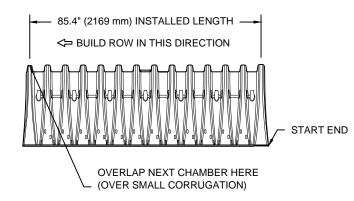
GΜ OTTAWA, ON DRAWN: 1871 MERIVAL 04-22-15 Storm 4640 TRUEMAN BLVD HILLIARD, OH 43026 I-800-733-7473 SHEET

OF

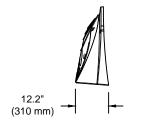
SC-740 TECHNICAL SPECIFICATION

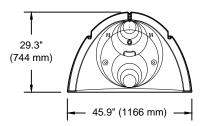
NTS

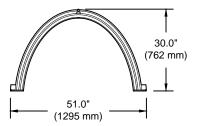




ACCEPTS 4" (100 mm) SCH 40 PVC PIPE FOR INSPECTION PORT. FOR PIPE SIZES LARGER THAN 4" (100 mm) UP TO 10" (250 mm) USE INSERTA TEE CONNECTION CENTERED ON A CHAMBER CREST CORRUGATION





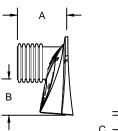


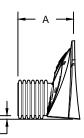
NOMINAL CHAMBER SPECIFICATIONS

SIZE (W X H X INSTALLED LENGTH) CHAMBER STORAGE MINIMUM INSTALLED STORAGE* WEIGHT 51.0" X 30.0" X 85.4" 45.9 CUBIC FEET 74.9 CUBIC FEET 75.0 lbs. (1295 mm X 762 mm X 2169 mm) (1.30 m³) (2.12 m³)

(33.6 kg)

*ASSUMES 6" (152 mm) STONE ABOVE, BELOW, AND BETWEEN CHAMBERS





PRE-FAB STUBS AT BOTTOM OF END CAP FOR PART NUMBERS ENDING WITH "B" PRE-FAB STUBS AT TOP OF END CAP FOR PART NUMBERS ENDING WITH "T" PRE-CORED END CAPS END WITH "PC"

PART#	STUB	Α	В	С
SC740EPE06T / SC740EPE06TPC	6" (150 mm)	10.9" (277 mm)	18.5" (470 mm)	
SC740EPE06B / SC740EPE06BPC	0 (130 11111)	10.9 (277 11111)		0.5" (13 mm)
SC740EPE08T /SC740EPE08TPC	8" (200 mm)	12.2" (310 mm)	16.5" (419 mm)	
SC740EPE08B / SC740EPE08BPC	0 (200 11111)	12.2 (31011111)		0.6" (15 mm)
SC740EPE10T / SC740EPE10TPC	10" (250 mm)	13.4" (340 mm)	14.5" (368 mm)	
SC740EPE10B / SC740EPE10BPC	10 (230 11111)	13.4 (340 11111)		0.7" (18 mm)
SC740EPE12T / SC740EPE12TPC	12" (300 mm)	14.7" (373 mm)	12.5" (318 mm)	
SC740EPE12B / SC740EPE12BPC	12 (300 11111)	14.7 (3/3/11111)		1.2" (30 mm)
SC740EPE15T / SC740EPE15TPC	15" (375 mm)	18.4" (467 mm)	9.0" (229 mm)	
SC740EPE15B / SC740EPE15BPC	13 (3/3 11111)	10.4 (407 11111)		1.3" (33 mm)
SC740EPE18T / SC740EPE18TPC	18" (450 mm)	19.7" (500 mm)	5.0" (127 mm)	
SC740EPE18B / SC740EPE18BPC	10 (430111111)	19.7 (300 11111)		1.6" (41 mm)
SC740EPE24B*	24" (600 mm)	18.5" (470 mm)		0.1" (3 mm)

ALL STUBS, EXCEPT FOR THE SC740EPE24B ARE PLACED AT BOTTOM OF END CAP SUCH THAT THE OUTSIDE DIAMETER OF THE STUB IS FLUSH WITH THE BOTTOM OF THE END CAP. FOR ADDITIONAL INFORMATION CONTACT STORMTECH AT 1-888-892-2694.

* FOR THE SC740EPE24B THE 24" (600 mm) STUB LIES BELOW THE BOTTOM OF THE END CAP APPROXIMATELY 1.75" (44 mm). BACKFILL MATERIAL SHOULD BE REMOVED FROM BELOW THE N-12 STUB SO THAT THE FITTING SITS LEVEL.

NOTE: ALL DIMENSIONS ARE NOMINAL

					ര		Z
= IV/\Id:	RIVALE VA, ON			DRAWN:		CHECKED: KF	
1871 MERIVALE OTTAWA, ON			04-22-15		PROJECT #: 97633		
				L	DATE:		PROJE
DESCRIPTION	04-24-15 GM KP NEW VOLUME - 65 m ³	NEW VOLUME - 72.3 m³	3-27-17 DI GEI REVISED PER COMMENTS	INCAIDED I EN COMMISSINO	3-28-17 MLB NPB REVISED FOR VOLUME/ELEVATIONS DATE:	08-24-17 KR CJD REVISED INVERTS & IR SIZE	11-06-17 KR CJD REVISED PER ENGINEER
хнэ	ΑУ		IJU	5	BdN	aro	CJD
DRW	ВМ	GM	2	7	MLB	KR	Ж
REV DRW CHK	04-24-15	07-28-15 GM	3-27-17	7-17-0	3-28-17	08-24-17	11-06-17
						57	OM



4640 TRUEMAN BLVD HILLIARD, OH 43026 1-800-733-7473



SHEET

5 OF

APPENDIX F
Stormceptor Reports





Brief Stormceptor Sizing Report - Benson Auto Parts - Stormceptor01

Project Information & Location			
Project Name	Name Benson Auto Parts Project Number 130828		130828
City	Ottawa	State/ Province	Ontario
Country	Canada	Date	11/13/2017
Designer Information		EOR Information (optional)	
Name	Guillaume Courtois	Name	
Company	LRL Associates Ltd.	Company	
Phone #	613-842-3434	Phone #	
Email	gcourtois@lrl.ca	Email	

Stormwater Treatment Recommendation

The recommended Stormceptor Model(s) which achieve or exceed the user defined water quality objective for each site within the project are listed in the below Sizing Summary table.

Site Name	Benson Auto Parts - Stormceptor 01	
Target TSS Removal (%)	80	
TSS Removal (%) Provided	84	
Recommended Stormceptor Model	STC 300	

The recommended Stormceptor Model achieves the water quality objectives based on the selected inputs, historical rainfall records and selected particle size distribution.

Stormceptor Sizing Summary			
Stormceptor Model	% TSS Removal Provided		
STC 300	84		
STC 750	90		
STC 1000	90		
STC 1500	90		
STC 2000	91		
STC 3000	92		
STC 4000	93		
STC 5000	94		
STC 6000	95		
STC 9000	96		
STC 10000	96		
STC 14000	97		
StormceptorMAX	Custom		





Sizing Details					
Drainage	Drainage Area		Water Quality Objective		
Total Area (ha)	0.41	TSS Removal (%) 80		80.0	
Imperviousness %	95.0	Runoff Volume Capture (%)			
Rainfa	Rainfall		Oil Spill Capture Volume (L)		
Station Name	OTTAWA MACDONALD- CARTIER INT'L A	Peak Conveyed Flow Rate (L/s)			
State/Province	Ontario	Water Quality Flow Rate (L/s)			
Station ID #	6000	Up Stream Storage			
Years of Records	37	Storage (ha-m) Discharge (cms)		ge (cms)	
Latitude	45°19'N	0.000	0.0	000	
Longitude	75°40'W	0.018	0.	030	

Up Stream Flow Diversion

Max. Flow to Stormceptor (cms)

Particle Size Distribution (PSD) The selected PSD defines TSS removal					
	Fine Distribution				
Particle Diameter Distribution Specific Gravity (microns) %					
20.0	20.0	1.30			
60.0	20.0	1.80			
150.0	20.0	2.20			
400.0	20.0	2.65			
2000.0	20.0	2.65			

Notes

- Stormceptor performance estimates are based on simulations using PCSWMM for Stormceptor, which uses the EPA Rainfall and Runoff modules.
- Design estimates listed are only representative of specific project requirements based on total suspended solids (TSS) removal defined by the selected PSD, and based on stable site conditions only, after construction is completed.
- For submerged applications or sites specific to spill control, please contact your local Stormceptor representative for further design assistance.

For Stormceptor Specifications and Drawings Please Visit: http://www.imbriumsystems.com/technical-specifications





Brief Stormceptor Sizing Report - Benson Auto Parts - Stormceptor02

Project Information & Location				
Project Name	Benson Auto Parts	Project Number	130828	
City	Ottawa	State/ Province	Ontario	
Country	Canada Date 11/13/2017		11/13/2017	
Designer Information		EOR Information (optional)		
Name	Guillaume Courtois	Name		
Company	LRL Associates Ltd.	Company		
Phone #	613-842-3434	Phone #		
Email	gcourtois@lrl.ca	Email		

Stormwater Treatment Recommendation

The recommended Stormceptor Model(s) which achieve or exceed the user defined water quality objective for each site within the project are listed in the below Sizing Summary table.

Site Name	Benson Auto Parts - Stormceptor 02	
Target TSS Removal (%)	80	
TSS Removal (%) Provided	84	
Recommended Stormceptor Model	STC 300	

The recommended Stormceptor Model achieves the water quality objectives based on the selected inputs, historical rainfall records and selected particle size distribution.

Stormceptor Sizing Summary			
Stormceptor Model	% TSS Removal Provided		
STC 300	84		
STC 750	90		
STC 1000	91		
STC 1500	91		
STC 2000	93		
STC 3000	94		
STC 4000	95		
STC 5000	96		
STC 6000	96		
STC 9000	98		
STC 10000	98		
STC 14000	98		
StormceptorMAX	Custom		





Sizing Details				
Drainage	Area	Water Quality Objective		
Total Area (ha)	0.14	TSS Removal (%) 80.0		80.0
Imperviousness %	100.0	Runoff Volume Capture (%)		
Rainfa	all	Oil Spill Capture Volume (L)		
Station Name	OTTAWA MACDONALD- CARTIER INT'L A	Peak Conveyed Flow Rate (L/s)		
State/Province	Ontario	Water Quality Flow Rate (L/s)		
Station ID #	6000	Up Stream Storage		
Years of Records	37	Storage (ha-m) Discharge (cms)		ge (cms)
Latitude	45°19'N	0.000 0.000		000
Longitude	75°40'W	Up Stream Flow Diversion		
		Max. Flow to Stormce	eptor (cms)	

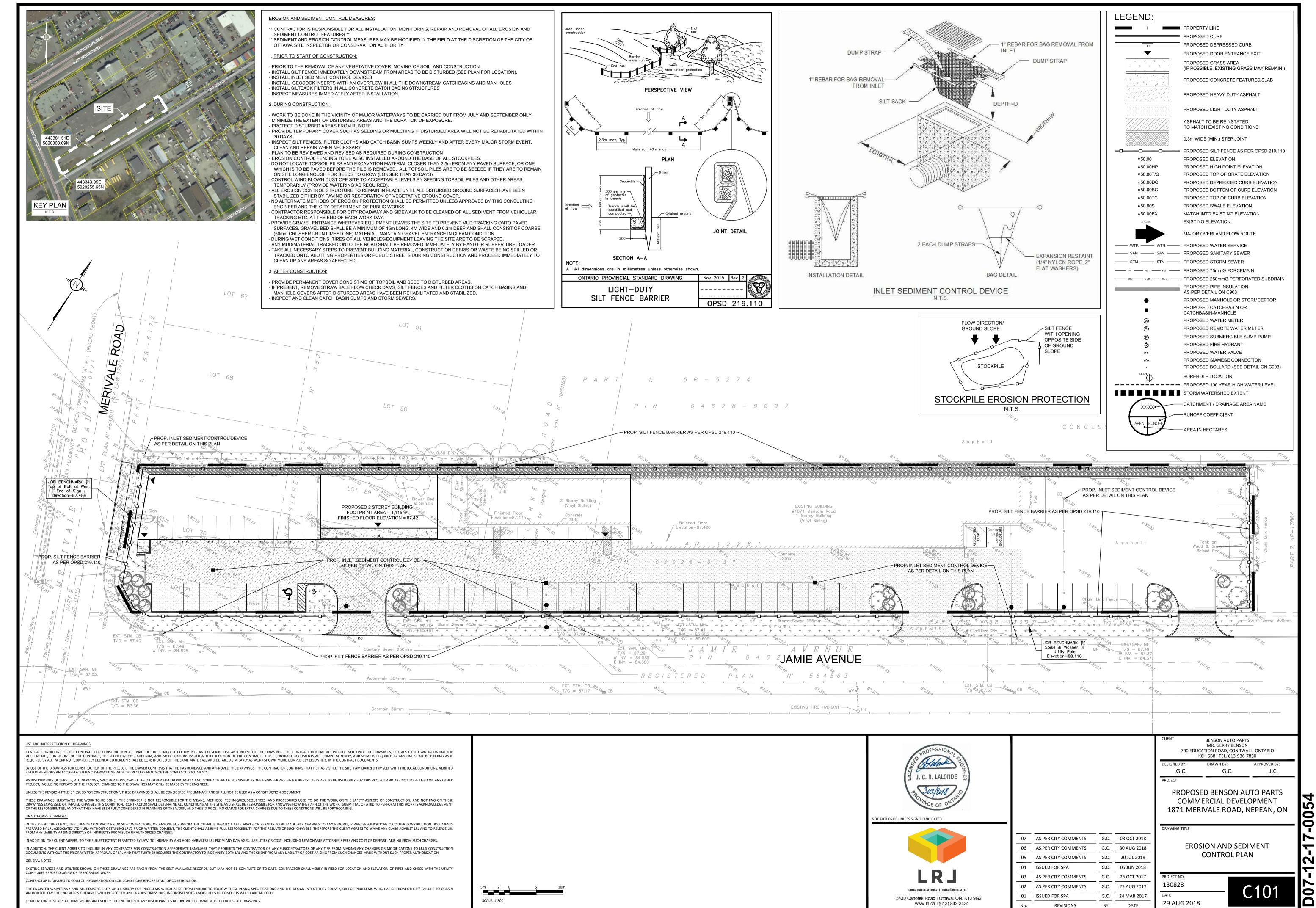
Particle Size Distribution (PSD) The selected PSD defines TSS removal				
	Fine Distribution			
Particle Diameter Distribution Specific Gravity (microns) %				
20.0	20.0	1.30		
60.0	20.0	1.80		
150.0	20.0	2.20		
400.0	20.0	2.65		
2000.0	20.0	2.65		

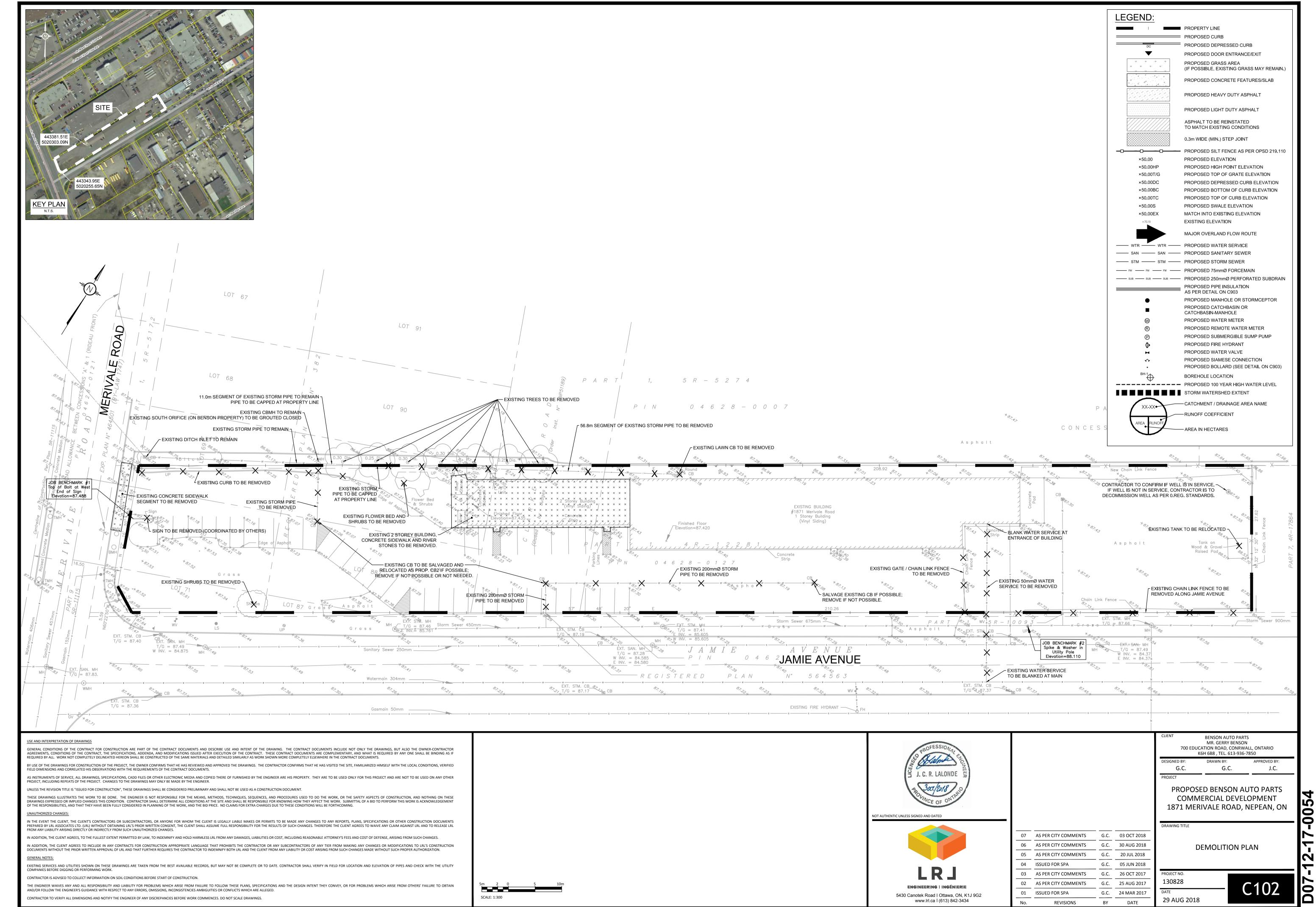
Notes

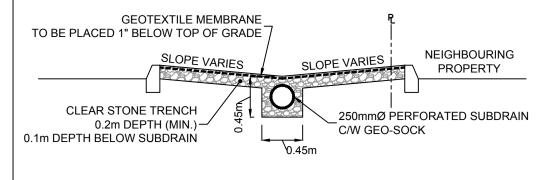
- Stormceptor performance estimates are based on simulations using PCSWMM for Stormceptor, which uses the EPA Rainfall and Runoff modules.
- Design estimates listed are only representative of specific project requirements based on total suspended solids (TSS) removal defined by the selected PSD, and based on stable site conditions only, after construction is completed.
- For submerged applications or sites specific to spill control, please contact your local Stormceptor representative for further design assistance.

For Stormceptor Specifications and Drawings Please Visit: http://www.imbriumsystems.com/technical-specifications APPENDIX G

Complete Set of Civil Plans







SWALE & SUBDRAIN - TYPICAL SECTION A-A (N.T.S.)

PAVEMENT STRUCTURE

		THICKNESS (mm)		
COURSE	MATERIAL	AUTOMOBILE PARKING	TRUCK ROUTE (HEAVY TRAFFIC)	
SURFACE	HL.3 A/C (PG 58-28)	50	40	
BINDER	HL.8 A/C (PG 58-28)		40	
BASECOURSE	GRANULAR "A"	150	150	
SUBBASE	GRANULAR "B" TYPE II	250	350	

IN PREPARATION FOR PAVEMENT CONSTRUCTION AT THIS SITE, ANY SURFICIAL OR NEAR SURFACE/SUBGRADE LEVEL TOPSOIL AND ANY SOFT, WET OR DELETERIOUS MATERIALS SHOULD BE REMOVED FROM THE PROPOSED PAVED AREAS. THE EXPOSED SUBGRADE SHOULD BE INSPECTED AND APPROVED BY GEOTECHNICAL PERSONNEL AND ANY SOFT AREAS EVIDENT SHOULD BE SUBEXCAVATED AND REPLACED WITH SUITABLE EARTH BORROW APPROVED BY THE GEOTECHNICAL ENGINEER. THE SUBGRADE SHOULD BE SHAPED AND CROWNED TO PROMOTE DRAINAGE OF THE SITE CB'S. FOLLOWING APPROVAL OF THE PREPARATION OF THE SUBGRADE, THE PAVEMENT GRANULARS MAY BE PLACED.

♥PROP. GROUND ELEV. = 87.30 -

(Vinyl Siding)

BROP BOLLARD (TYP.)

SEE DETAIL ON C903 0 4 6 2 8 - 0 1 2 7

REGISTERED

SUBDRAIN INV. = 86.49

5 R - 5 2 7 4

0 4 6 2 8 - 0 0 0 7

GENERAL NOTES:

- ALL EDGES OF DISTURBED PAVEMENT SHALL BE SAW CUT TO FORM A CLEAN CUT LINE PRIOR TO PLACING NEW PAVEMENT. PAVEMENT REINSTATEMENT SHALL BE WITH STEP JOINTS OF 500mm WIDTH MINIMUM.
- CURBS TO BE BARRIER, CONSTRUCTED AS PER DETAIL SC1.1 ON C903.
- ALL SIDEWALK CONSTRUCTION TO BE AS PER DETAILS SC1.4 AND SC2 ON C903.
- ALL MATERIAL SUPPLIED AND PLACED FOR PARKING LOT AND ACCESS ROAD CONSTRUCTION SHALL BE TO OPSS STANDARDS AND SPECIFICATIONS UNLESS OTHERWISE NOTED. CONSTRUCTION TO OPSS 206, 310 & 314. MATERIALS TO OPSS 1001,
- OBTAIN AND PAY FOR ALL NECESSARY PERMITS AND APPROVALS FROM THE MUNICIPAL AUTHORITIES PRIOR TO COMMENCING CONSTRUCTION: SUCH AS, BUT NOT LIMITED TO: ROAD CUT PERMITS, SEWER PERMITS, WATER PERMIT, ETC. THE APPROVAL OF THIS PLAN DOES NOT EXEMPT THE CONTRACTOR FROM THE REQUIREMENTS TO OBTAIN THE VARIOUS PERMITS/APPROVALS REQUIRED TO COMPLETE THE CONSTRUCTION PROJECT.
- INLET SEDIMENT CONTROL DEVICES TO BE INSTALLED AND MAINTAINED BETWEEN THE FRAME AND COVER OF ALL CATCHBASINS AND CATCHBASIN MANHOLES DURING THE CONSTRUCTION PERIOD TO MINIMIZE SEDIMENTS ENTERING THE STORM SEWER SYSTEM. ALL GRASSED AREAS MUST BE COMPLETED PRIOR TO THE REMOVAL OF THE FILTER FABRIC IN THE CATCH BASINS.
- REMOVE FROM SITE ALL EXCESS EXCAVATED MATERIAL UNLESS OTHERWISE DIRECTED FROM THE ENGINEER. EXCAVATE AND REMOVE ALL ORGANIC MATERIAL AND DEBRIS, IF ANY, LOCATED WITHIN THE PROPOSED BUILDING, PARKING AND ROADWAY LOCATIONS.

UTILITY NOTES:

- 1. UNDERGROUND UTILITIES, AS REPORTED ON THIS DRAWING, ARE NOT BASED ON AN ACTUAL 'FIELD LOCATE' BY THE RESPECTIVE UTILITY AGENCIES BUT HAVE BEEN COMPILED FROM DATA OBTAINED FROM THE CITY OF OTTAWA PUBLIC UTILITIES
- BEFORE ANY WORK INVOLVING PROBING, EXCAVATING, ETC., CONTRACTOR TO CONFIRM RELEVANT UTILITY LOCATIONS AND REPORT ANY DISCREPANCIES TO THE ENGINEER PRIOR TO COMMENCING WORK.

SURVEY NOTES:

PROP. 250mmØ PERFORATED SUBDRAIN @ 0.5% -

EXISTING BUILDING

→ → → → → → → → Storm→Sewer 6₹5mm → → → → → → → →

564563

EXISTING FIRE HYDRANT -

#1871 Merivale Road

1 Storey Building

1. CONFIRM JOB BENCHMARKS SHOWN ON PLANS WITH ENGINEER PRIOR TO UTILIZATION.

PROP. CLEAR STONE -

BEARINGS HEREON ARE GRID BEARINGS AND ARE DERIVED FROM NCC HORIZONTAL CONTROL MONUMENTS 019710637 (N 5022465.812, E 365416.840) AND 019861625 (N 5022141.837, E 363270.732) AND ARE REFERRED TO THE CENTRAL MERIDIAN 76°30'W LONGITUDE, ZONE 9 OF THE 3° M.T.M. ONTARIO COORDINATE SYSTEM (NAD 83).

Asphalt

×50.00EX

LEGEND:

PROPOSED GRASS AREA (IF POSSIBLE, EXISTING GRASS MAY REMAIN.) PROPOSED CONCRETE FEATURES/SLAB

PROPOSED DEPRESSED CURB PROPOSED DOOR ENTRANCE/EXIT

PROPERTY LINE

PROPOSED CURB

PROPOSED HEAVY DUTY ASPHALT

PROPOSED LIGHT DUTY ASPHALT

ASPHALT TO BE REINSTATED TO MATCH EXISTING CONDITIONS

0.3m WIDE (MIN.) STEP JOINT --- PROPOSED SILT FENCE AS PER OPSD 219.110 _____ ×50.00 PROPOSED ELEVATION ×50.00HP PROPOSED HIGH POINT ELEVATION ×50.00T/G PROPOSED TOP OF GRATE ELEVATION

> ×50.00DC PROPOSED DEPRESSED CURB ELEVATION PROPOSED BOTTOM OF CURB ELEVATION ×50.00TC PROPOSED TOP OF CURB ELEVATION PROPOSED SWALE ELEVATION ×50.00S

MATCH INTO EXISTING ELEVATION EXISTING ELEVATION

MAJOR OVERLAND FLOW ROUTE

WTR — PROPOSED WATER SERVICE ---- SAN ----- PROPOSED SANITARY SEWER ----- STM ------ PROPOSED STORM SEWER ---- FM ---- FM ---- PROPOSED 75mmØ FORCEMAIN

PROPOSED PIPE INSULATION AS PER DETAIL ON C903 PROPOSED MANHOLE OR STORMCEPTOR

PROPOSED CATCHBASIN OR CATCHBASIN-MANHOLE PROPOSED WATER METER PROPOSED REMOTE WATER METER PROPOSED SUBMERGIBLE SUMP PUMP

PROPOSED FIRE HYDRANT PROPOSED WATER VALVE PROPOSED SIAMESE CONNECTION PROPOSED BOLLARD (SEE DETAIL ON C903)

BOREHOLE LOCATION PROPOSED 100 YEAR HIGH WATER LEVEL STORM WATERSHED EXTENT - CATCHMENT / DRAINAGE AREA NAME

XX-XX -RUNOFF COEFFICIENT

- AREA IN HECTARES

PROP. GOUND ELEV. = 87.40 7 PROP. 250mmØ PERFORATED -SUBDRAIN INV. = 87.05 / SUBDRAIN @ 2.90% – PROP. 250mmØ NON-PERFORATED SUBDRAIN @ 6.00%| — INV.=85.58

TEMPORARY SNOW STORAGE LOCATION -

SNOW TO BE REMOVED FROM SITE

E INV. = $84.37 \frac{1}{5}$

Utility Pole

JOB BENCHMARK #2

T/G = 87.12 -

SUBDRAIN INV. = 86.14

CITY OF OTTAWA DETAIL SC7 ♂> (UNSIGNALIZED) →

BENSON AUTO PARTS MR. GERRY BENSON 700 EDUCATION ROAD, CONRWALL, ONTARIO

K6H 6B8, TEL. 613-936-7850

G.C.

- PROP. ENTRANCE AS PER

ASPHALT REINSTATEMENT SHALL MATCH EXISTING GRANULAR AND ASPHALT THICKNESS WHILE MAINTAINING A MINIMUM OF 40mm OF HL-3, 50mm OF HL-8, 150mm OF GRANULAR 'A' AND 300mm OF GRANULAR 'B'. REFER TO DETAIL R10 ON C902.

A MINIMUM 0.3m WIDE STEP JOINT SHALL ALSO BE PROVIDED.

MATCH INTO EXIST. S/W = 87.42 -

87-31BC

87.41T0

MATCH INTO/EXIST, S/W 1

PROP. SWALE @ 1.5% SLOPE ~

PROP. RAISED S/W -

87.46BC

87.56TC

JOB BENCHMARK #1 End of Sign Elevation=87.488

AS PER DETAIL SC3 ON C903

MATCH INTO EXIST. S/W ~

MA#€H,INTO EXIST. S/W = 87.58 ~

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ASPHALT REINSTATEMENT SHALL MACTH EXISTING GRANULAR AND -

A MINIMUM 0.3m WIDE STEP JOINT SHALL ALSO BE PROVIDED.

REFER TO DETAIL R10 ON C902.

ASPHALT THICKNESS WHILE MAINTAINING A MINIMUM OF 40mm OF HL-3,

50mm OF HL-8, 150mm OF GRANULAR 'A' AND 300mm OF GRANULAR 'B'.

LOT 68

PROP. GOUND ELEV. = 87.21

SUBDRAIN INV = 86.86

PROP. 250mmØ PERFORATED SUBDRAIN @ 0.5%

PROP. CLEAR STONE

- PROP. ENTRANCE AS PER

(UNSIGNALIZED)

Gasmain 50mm ——

CITY OF OTTAWA DETAIL SC7.1

> PROP. DÉPRESSED S/WAS

PÉR DETAIL SC1.4 ÓN C903/

PROP. MÁXIMUM ÖVERLAND FLOW SPILLWAY

SCALE: 1:300

AS PER OPSD 605.040

PROPOSED 2 STOREY BUILDING

FOOTPRINT AREA = 1,115m2

FINISHED FLOOR ELEVATION = 87.42

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W $\dot{N}V. = 84.875$

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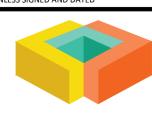
J. C. R. LALONDE

PROP. ENTRANCE AS PER -

(UNSIGNALIZED)

CITY OF OTTAWA DETAIL SC7.1

OT AUTHENTIC UNLESS SIGNED AND DATED



5430 Canotek Road | Ottawa, ON, K1J 9G2 www.lrl.ca I (613) 842-3434

07 AS PER CITY COMMENTS G.C. 03 OCT 2018 06 AS PER CITY COMMENTS G.C. 30 AUG 2018 05 AS PER CITY COMMENTS G.C. 20 JUL 2018 04 ISSUED FOR SPA G.C. 05 JUN 2018 03 AS PER CITY COMMENTS G.C. 26 OCT 2017 02 AS PER CITY COMMENTS G.C. 25 AUG 2017 01 ISSUED FOR SPA G.C. 24 MAR 2017

REVISIONS

BY

DATE

PROPOSED BENSON AUTO PARTS COMMERCIAL DEVELOPMENT 1871 MERIVALE ROAD, NEPEAN, ON

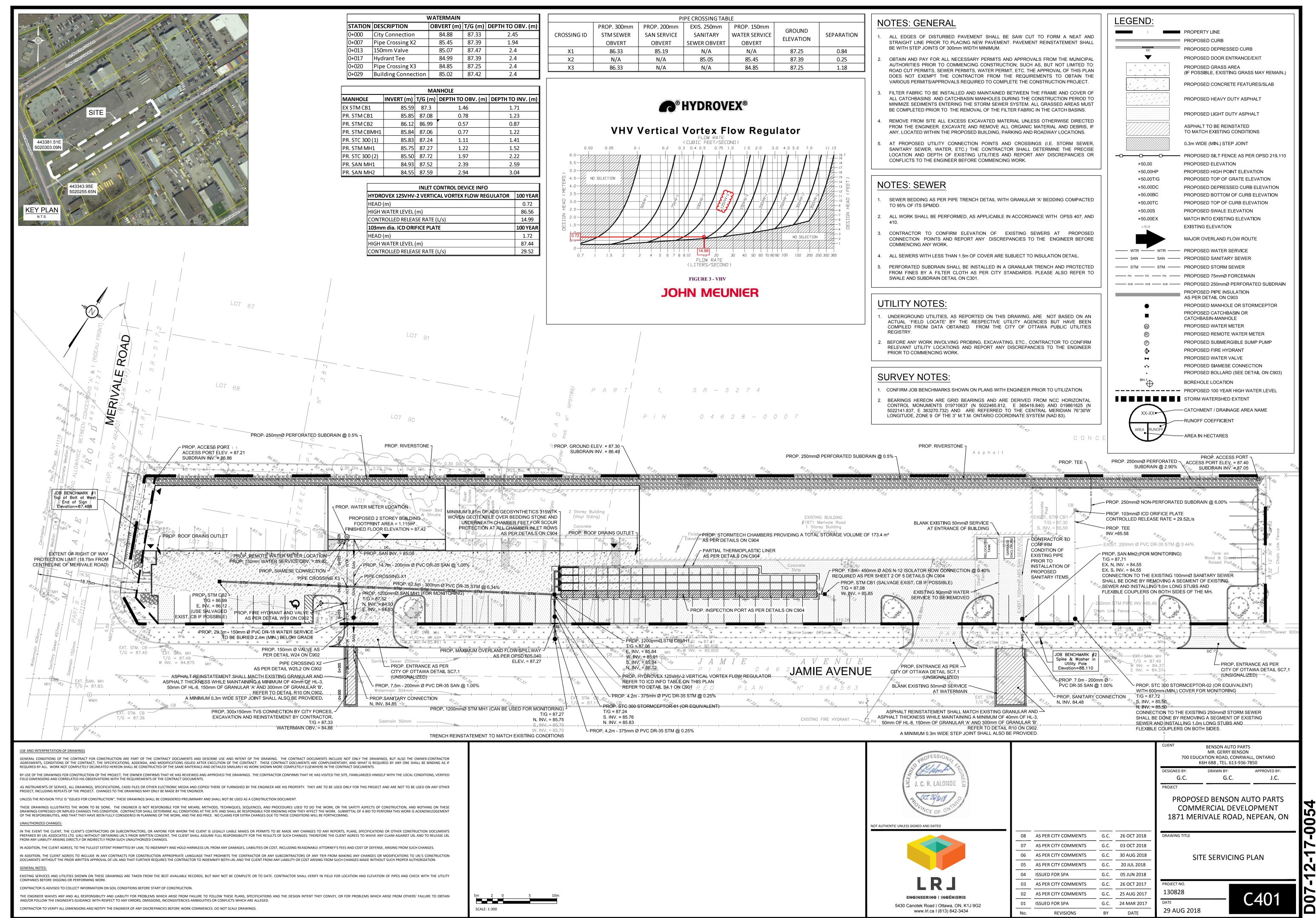
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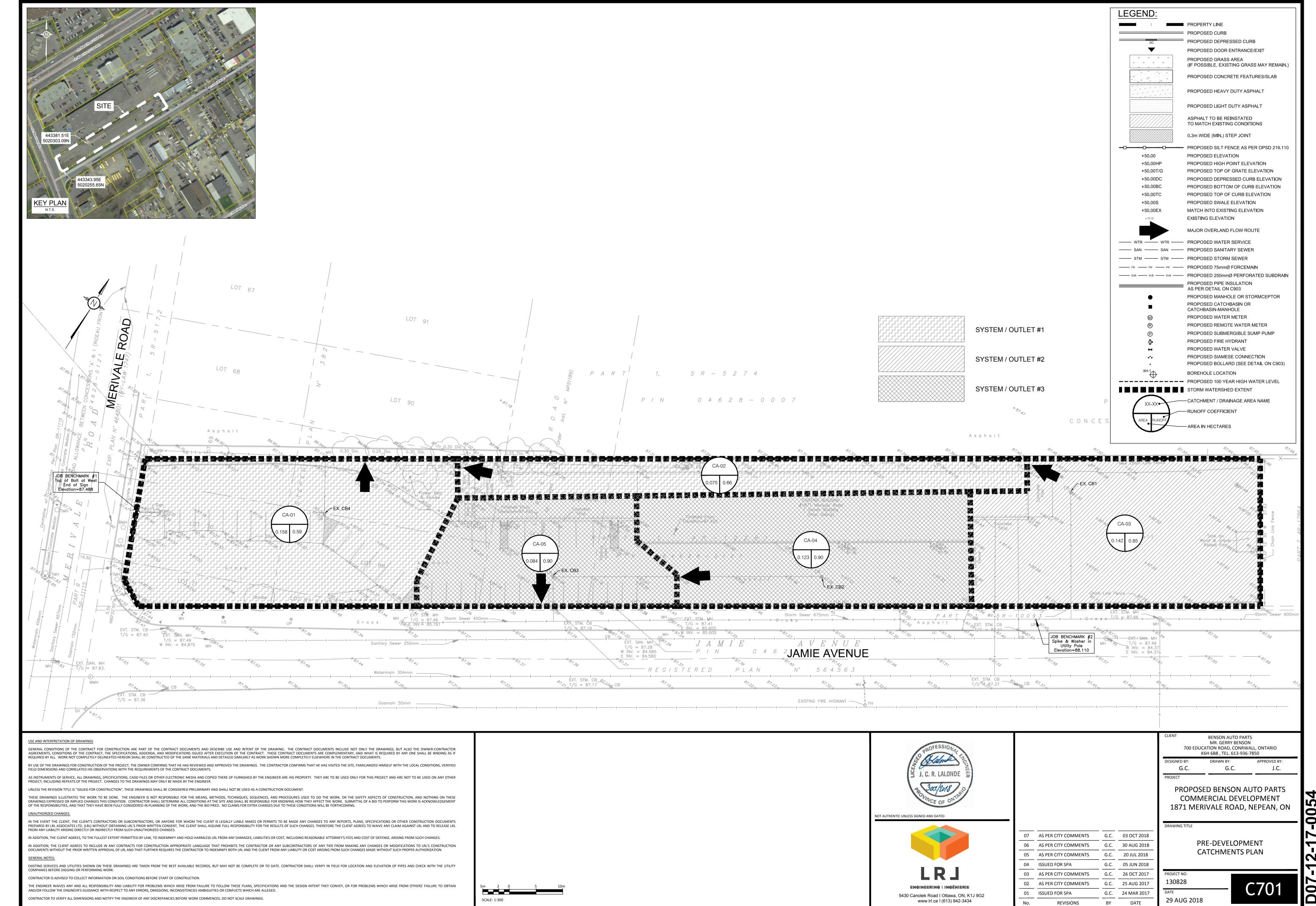
GRADING AND DRAINAGE PLAN

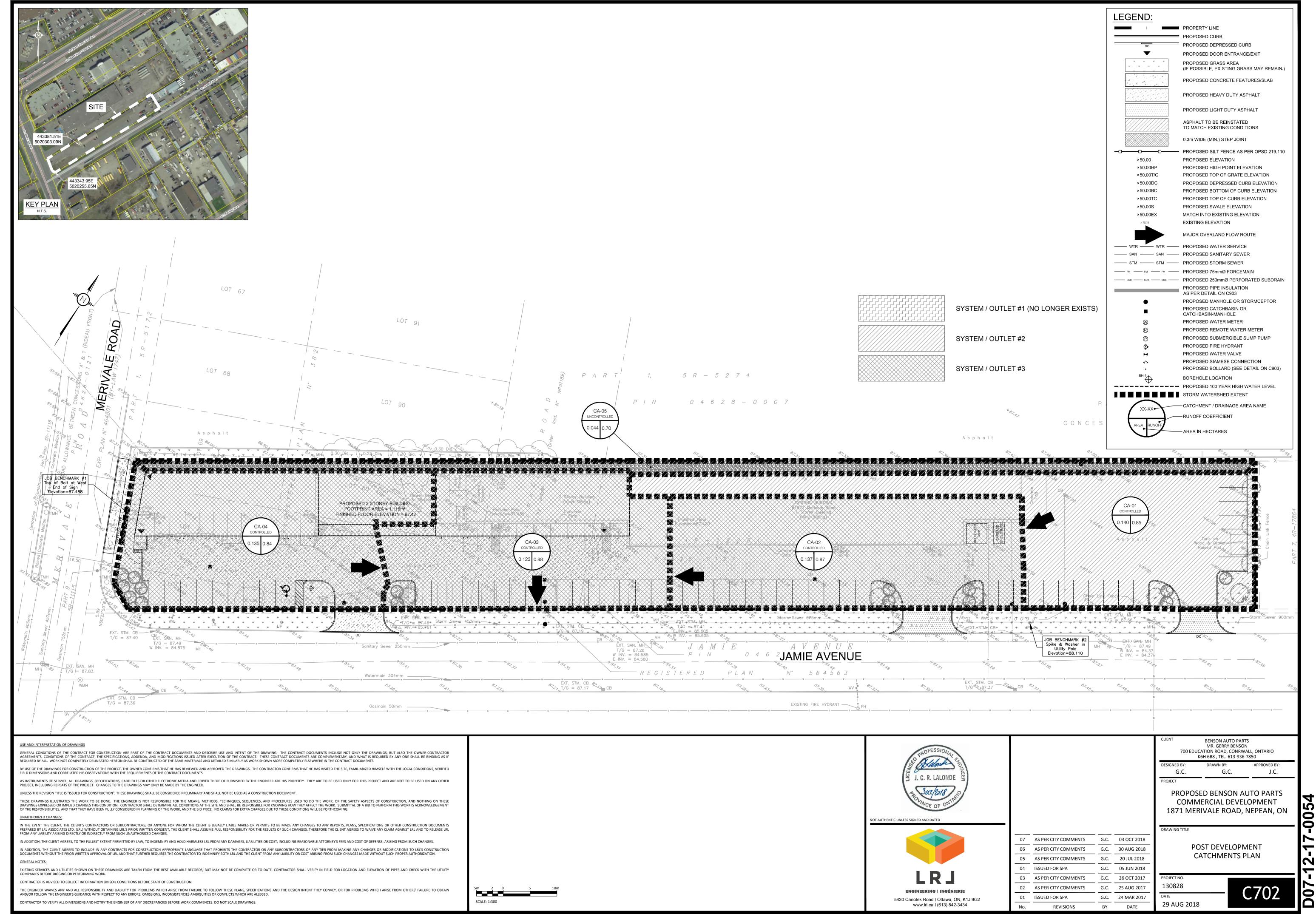
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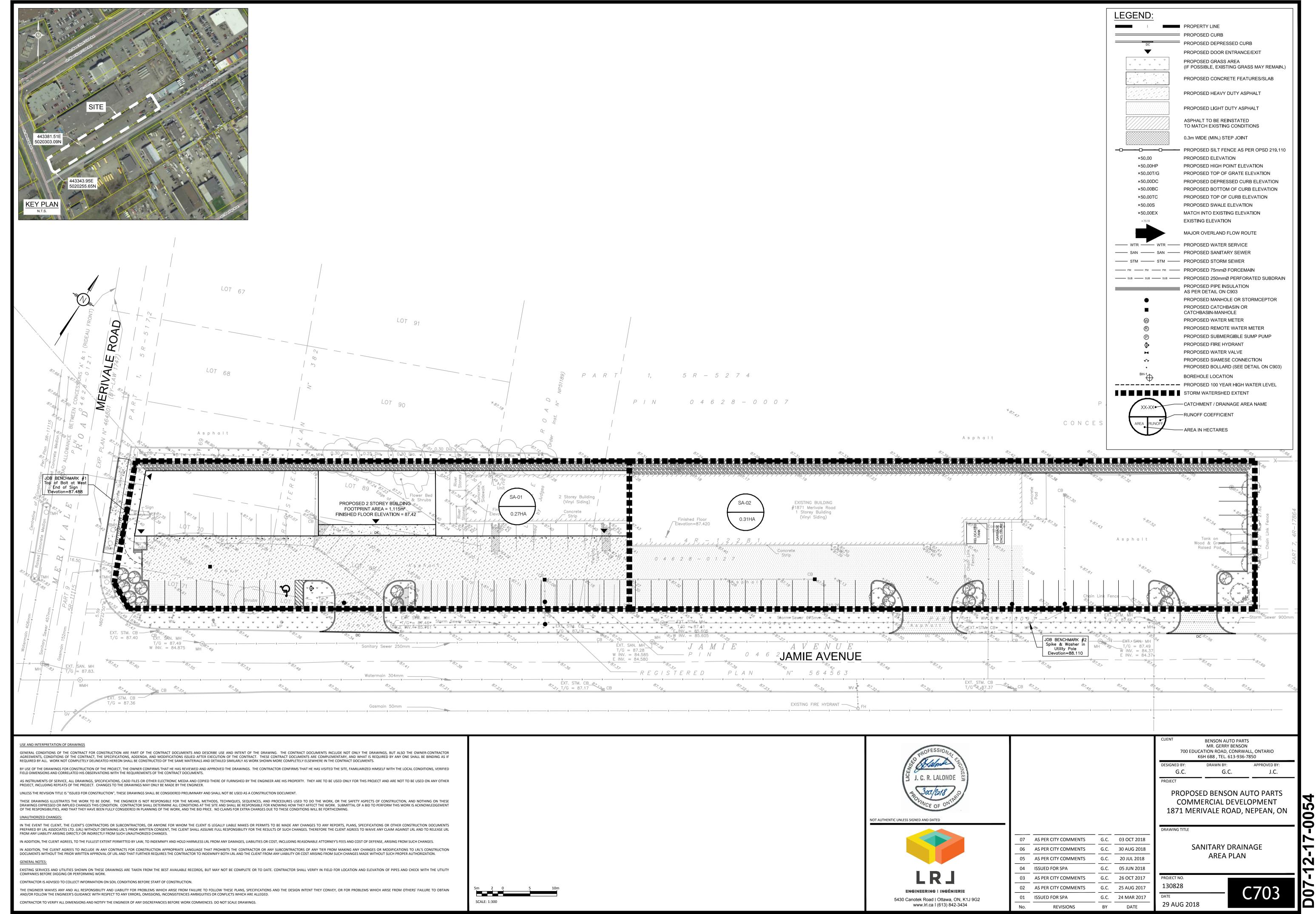
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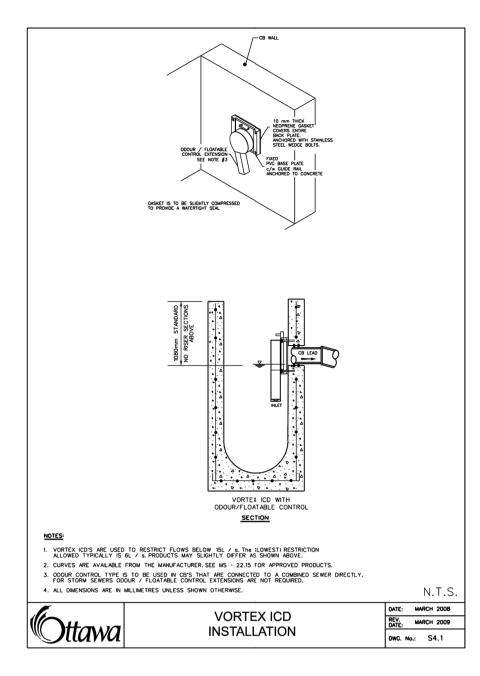
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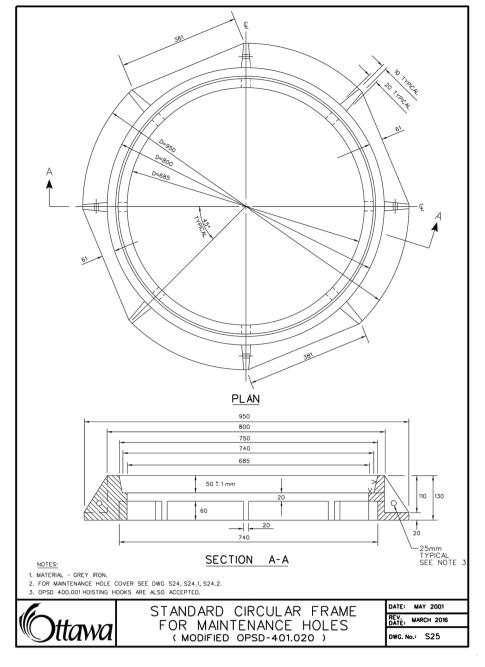


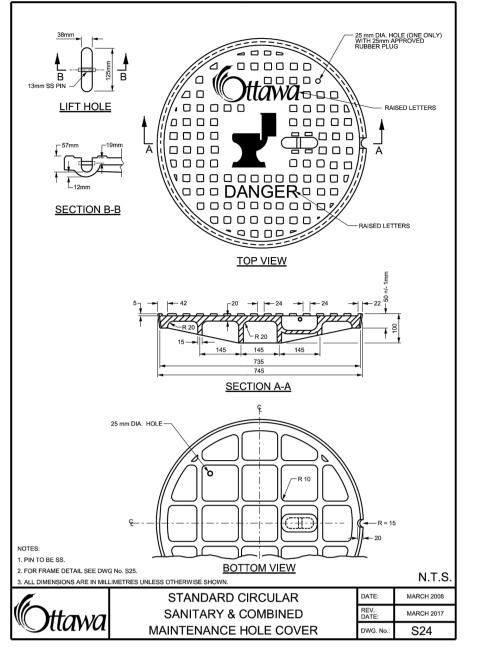


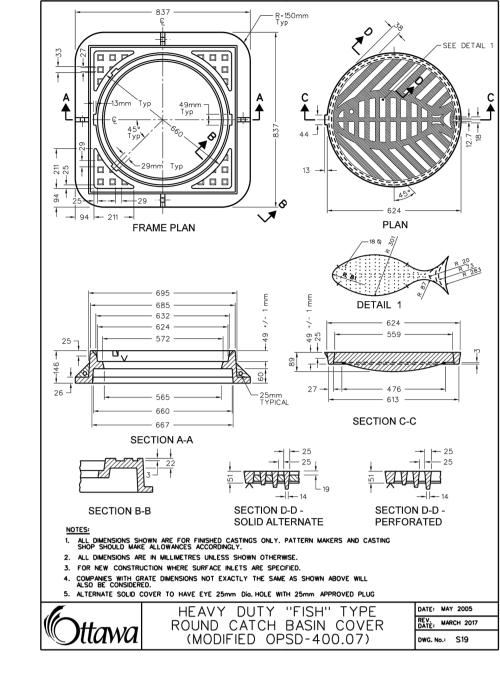


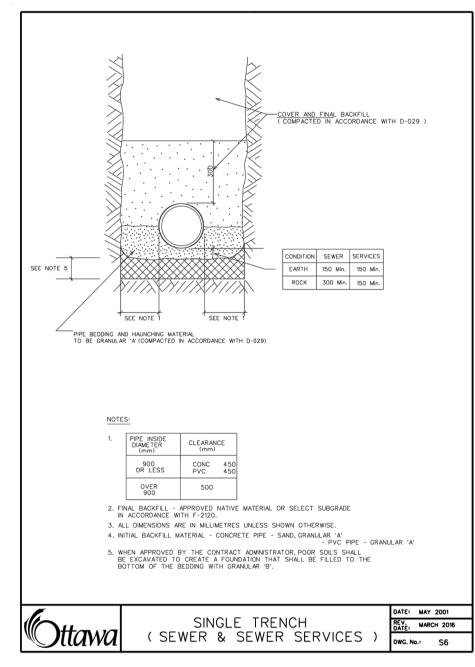


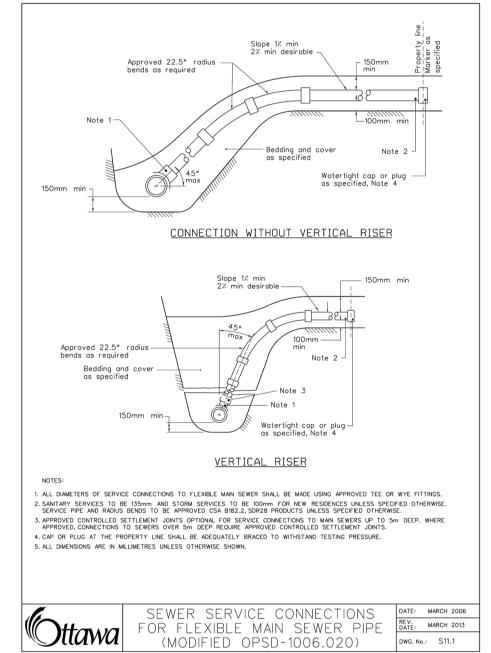


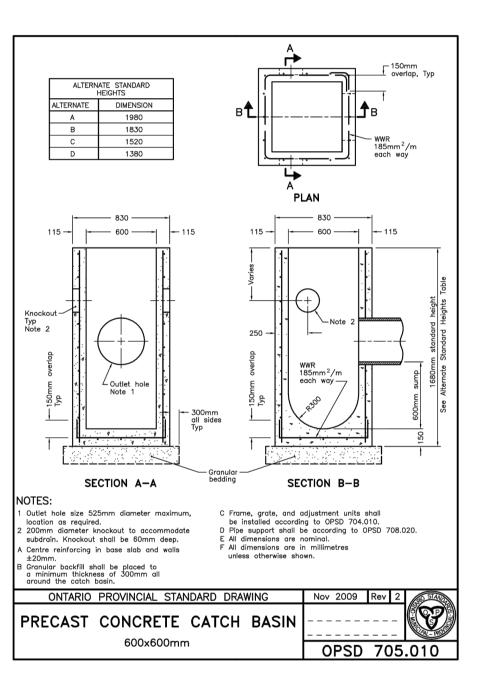


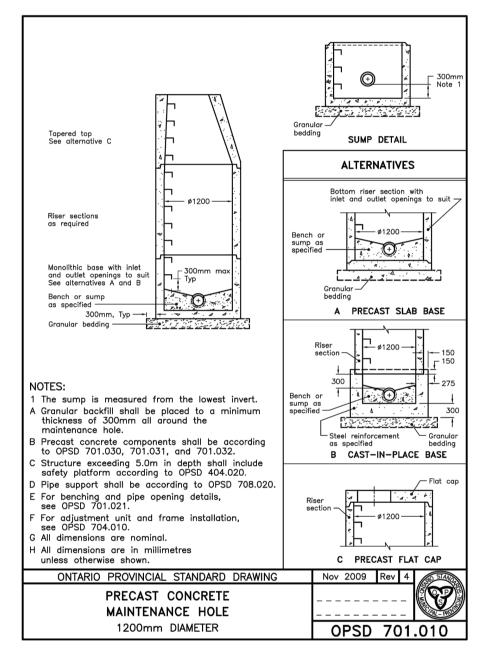












25 mm DIA. HOLE (ONE ONLY)
 WITH 25mm APPROVED
 RUBBER PLUG

DWG. No.: S24.1

OOO DANGEROOO

0000000000000

9000

TOP VIEW

SECTION A-A

BOTTOM VIEW

STANDARD CIRCULAR

STORM MAINTENANCE

HOLE COVER

-20 → | -24 → | -24 → | -21

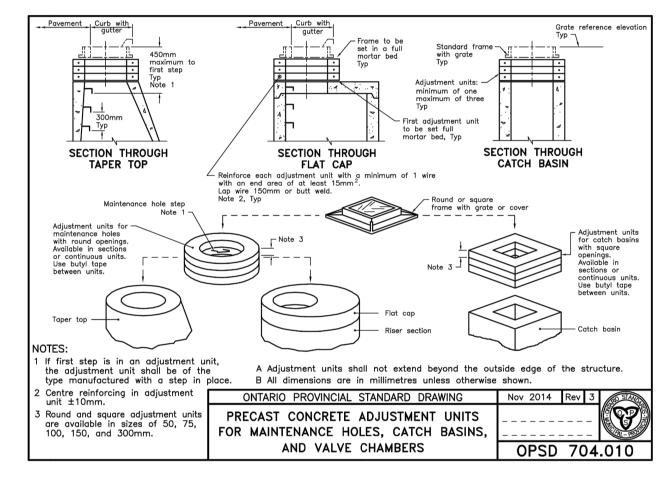
13mm SS PIN —

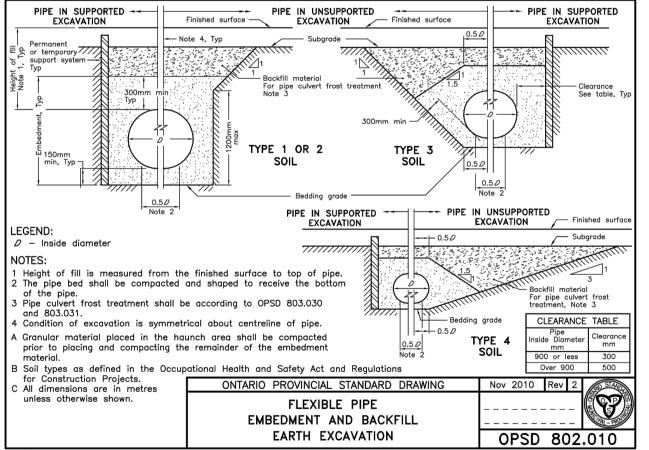
LIFT HOLE

SECTION B-B

1. PIN TO BE SS.

. FOR FRAME DETAIL SEE DWG No. S25.







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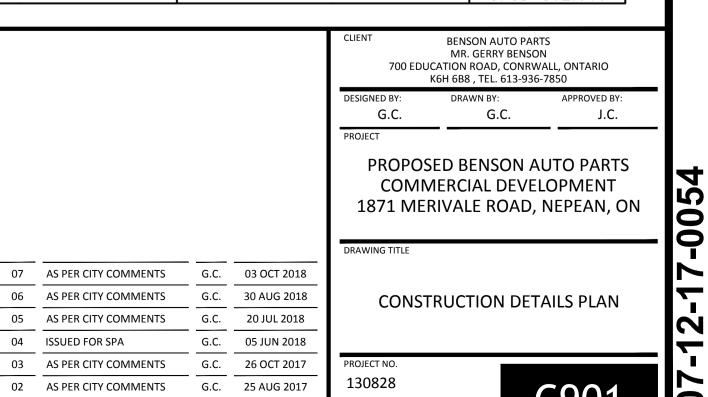
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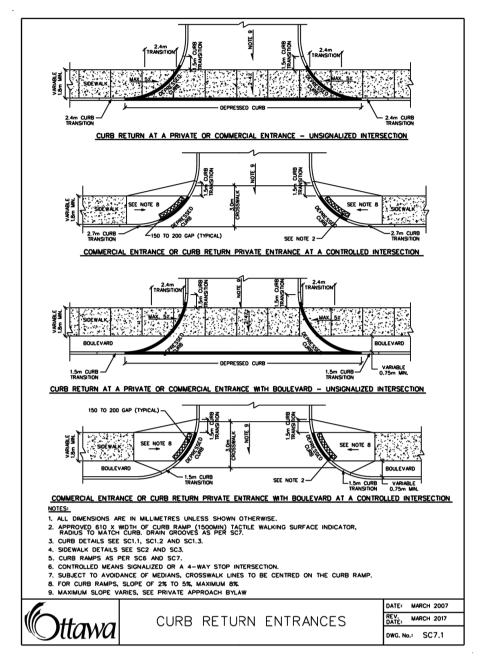
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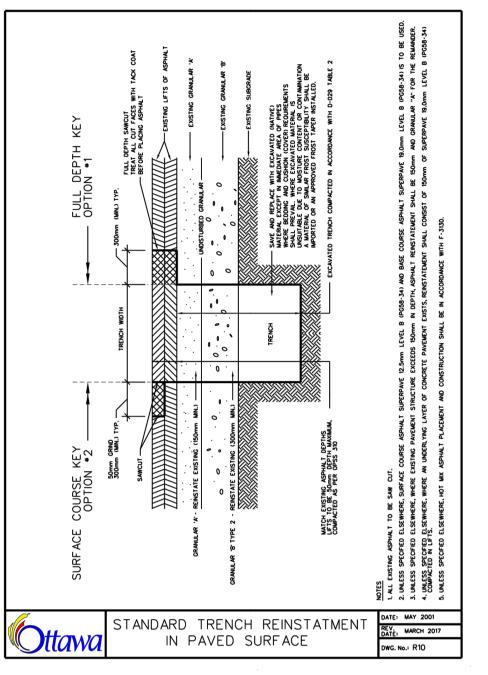
G.C. 24 MAR 2017

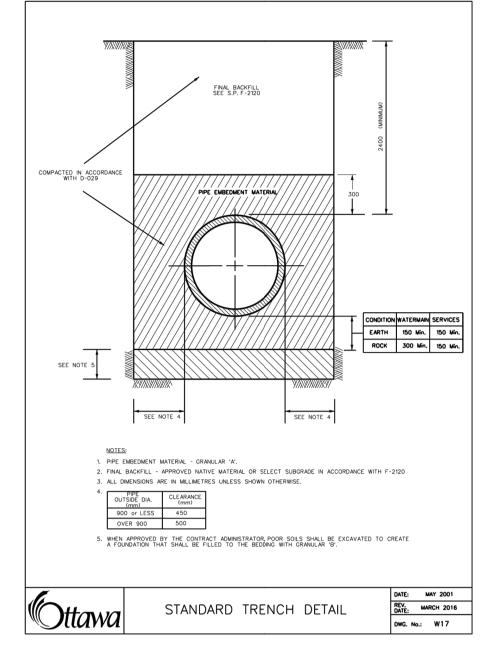
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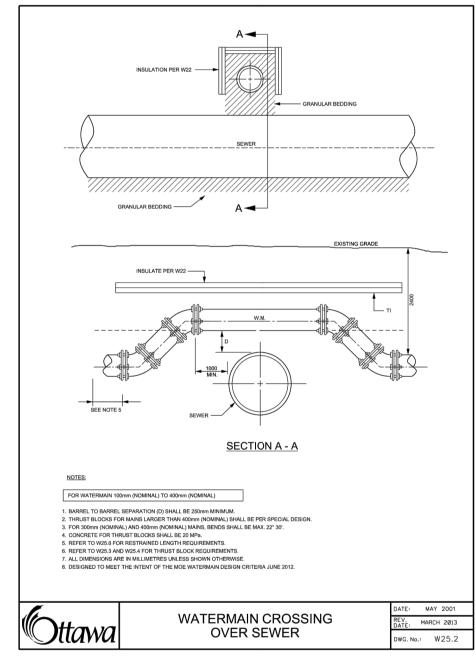
BY

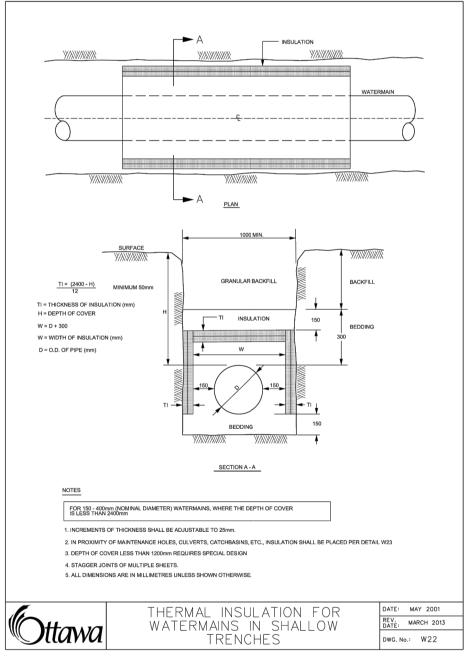
REVISIONS

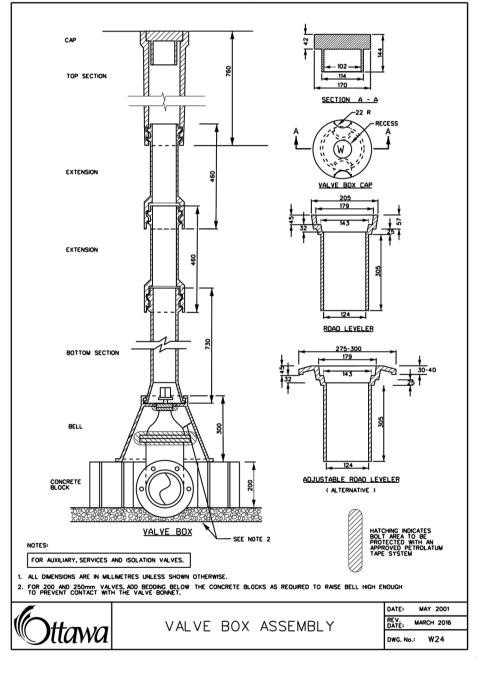


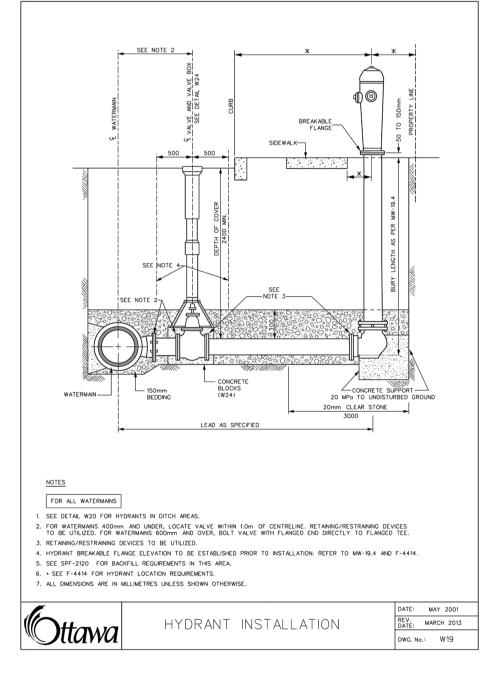












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NOT AUTHENTIC UNLESS SIGNED AND DATED



ENGINEERING | INGÉNIERIE 5430 Canotek Road | Ottawa, ON, K1J 9G2 www.lrl.ca I (613) 842-3434

07	AS PER CITY COMMENTS	G.C.	03 OCT 2018
06	AS PER CITY COMMENTS	G.C.	30 AUG 2018
05	AS PER CITY COMMENTS	G.C.	20 JUL 2018
04	ISSUED FOR SPA	G.C.	05 JUN 2018
03	AS PER CITY COMMENTS	G.C.	26 OCT 2017
02	AS PER CITY COMMENTS	G.C.	25 AUG 2017
01	ISSUED FOR SPA	G.C.	24 MAR 2017
No.	REVISIONS	BY	DATE

BENSON AUTO PARTS MR. GERRY BENSON 700 EDUCATION ROAD, CONRWALL, ONTARIO K6H 6B8 , TEL. 613-936-7850 G.C. J.C.

PROPOSED BENSON AUTO PARTS COMMERCIAL DEVELOPMENT 1871 MERIVALE ROAD, NEPEAN, ON

PROJECT

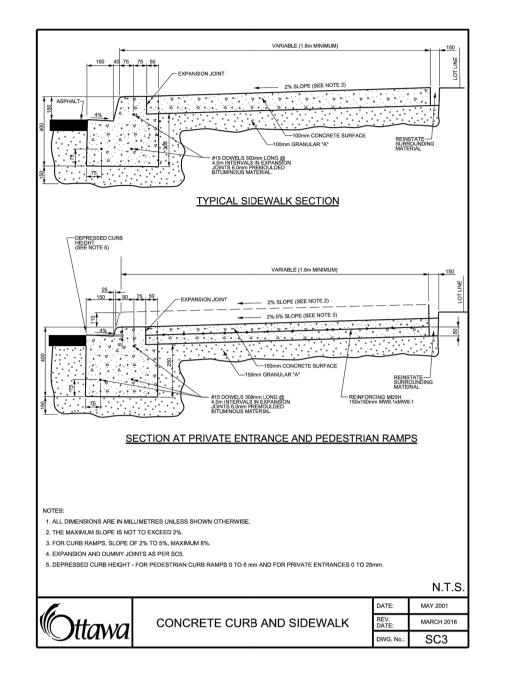
CONSTRUCTION DETAILS PLAN

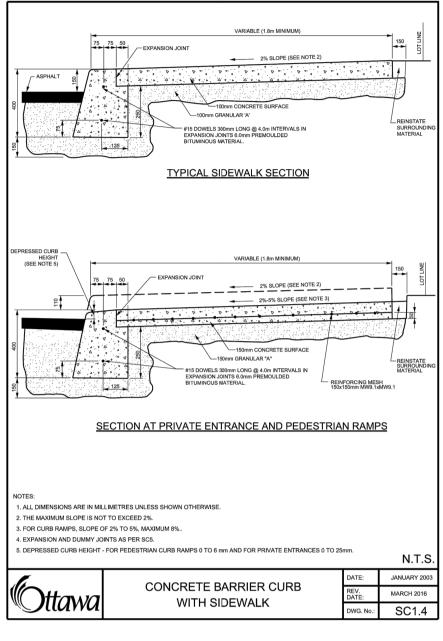
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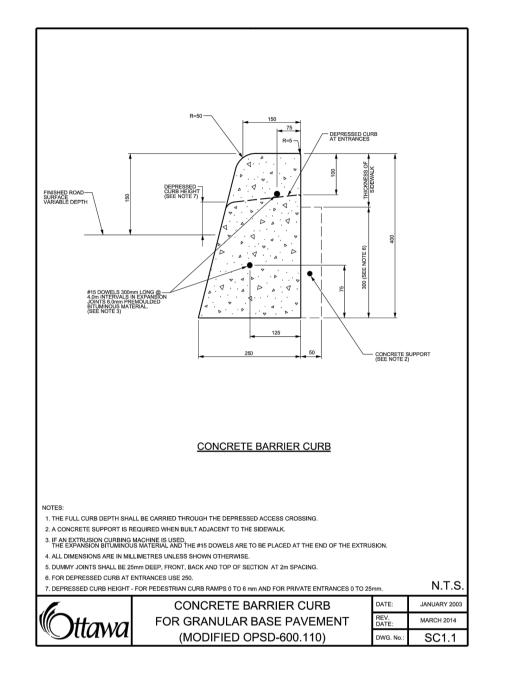
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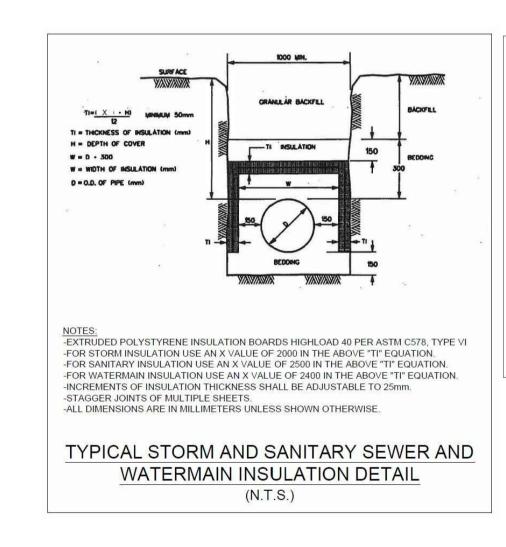
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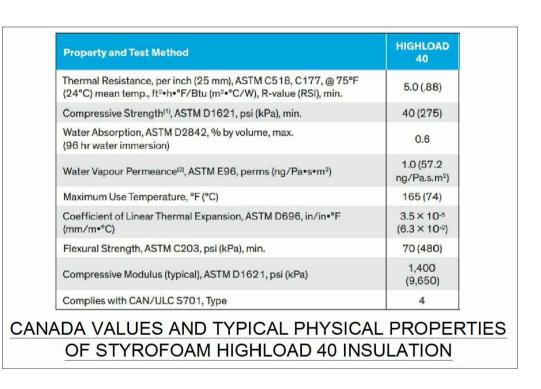
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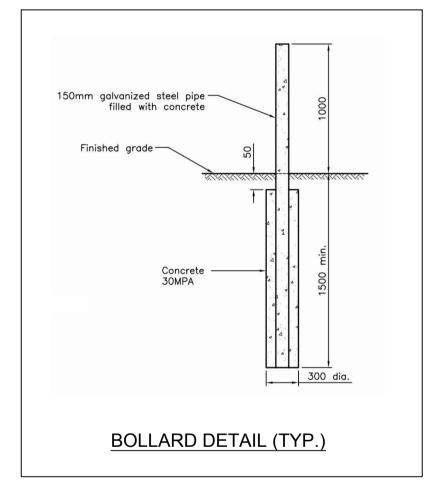












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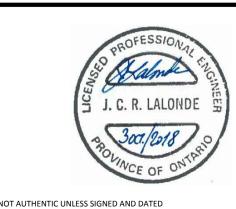
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 ${\tt CONTRACTOR}\ {\tt IS}\ {\tt ADVISED}\ {\tt TO}\ {\tt COLLECT}\ {\tt INFORMATION}\ {\tt ON}\ {\tt SOIL}\ {\tt CONDITIONS}\ {\tt BEFORE}\ {\tt START}\ {\tt OF}\ {\tt CONSTRUCTION}.$

THE ENGINEER WAIVES ANY AND ALL RESPONSIBILITY AND LIABILITY FOR PROBLEMS WHICH ARISE FROM FAILURE TO FOLLOW THESE PLANS, SPECIFICATIONS AND THE DESIGN INTENT THEY CONVEY, OR FOR PROBLEMS WHICH ARISE FROM OTHERS' FAILURE TO OBTAIN $AND/OR\ FOLLOW\ THE\ ENGINEER'S\ GUIDANCE\ WITH\ RESPECT\ TO\ ANY\ ERRORS,\ OMISSIONS,\ INCONSISTENCIES\ AMBIGUITIES\ OR\ CONFLICTS\ WHICH\ ARE\ ALLEGED.$ CONTRACTOR TO VERIFY ALL DIMENSIONS AND NOTIFY THE ENGINEER OF ANY DISCREPANCIES BEFORE WORK COMMENCES. DO NOT SCALE DRAWINGS.





	07	AS PER CITY COMMENTS	G.C.	03 OCT 2018
	06	AS PER CITY COMMENTS	G.C.	30 AUG 2018
	05	AS PER CITY COMMENTS	G.C.	20 JUL 2018
	04	ISSUED FOR SPA	G.C.	05 JUN 2018
LRJ	03	AS PER CITY COMMENTS	G.C.	26 OCT 2017
ENGINEERING INGÉNIERIE	02	AS PER CITY COMMENTS	G.C.	25 AUG 2017
5430 Canotek Road Ottawa, ON, K1J 9G2	01	ISSUED FOR SPA	G.C.	24 MAR 2017
www.lrl.ca I (613) 842-3434	No.	REVISIONS	BY	DATE

BENSON AUTO PARTS MR. GERRY BENSON 700 EDUCATION ROAD, CONRWALL, ONTARIO K6H 6B8 , TEL. 613-936-7850 G.C. PROJECT

PROPOSED BENSON AUTO PARTS COMMERCIAL DEVELOPMENT 1871 MERIVALE ROAD, NEPEAN, ON

CONSTRUCTION DETAILS PLAN

130828

29 AUG 2018

<u>05</u>





1871 MERIVALE OTTAWA, ON

STORMTECH CHAMBER SPECIFICATIONS

- 1 CHAMBERS SHALL BE STORMTECH SC-740 OR SC-310
- 2. CHAMBERS SHALL BE MANUFACTURED FROM VIRGIN POLYPROPYLENE OR POLYETHYLENE RESINS.
- CHAMBER ROWS SHALL PROVIDE CONTINUOUS, UNOBSTRUCTED INTERNAL SPACE WITH NO INTERNAL SUPPORT PANELS THAT WOULD IMPEDE FLOW OR LIMIT ACCESS FOR INSPECTION.
- THE STRUCTURAL DESIGN OF THE CHAMBERS, THE STRUCTURAL BACKFILL, AND THE INSTALLATION REQUIREMENTS SHALL ENSURE THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, SECTION 12.12, ARE MET FOR: 1) LONG-DURATION DEAD LOADS AND 2) SHORT-DURATION LIVE LOADS, BASED ON THE CSA S6 CL-625 TRUCK AND THE AASHTO DESIGN TRUCK WITH CONSIDERATION FOR IMPACT AND MULTIPLE VEHICLE PRESENCES.

- ONLY CHAMBERS THAT ARE APPROVED BY THE SITE DESIGN ENGINEER WILL BE ALLOWED. THE CHAMBER MANUFACTURER SHALL SUBMIT THE FOLLOWING UPON REQUEST TO THE SITE DESIGN ENGINEER FOR APPROVAL BEFORE DELIVERING CHAMBERS TO THE PROJECT SITE:
- a. A STRUCTURAL EVALUATION SEALED BY A REGISTERED PROFESSIONAL ENGINEER THAT DEMONSTRATES THAT THE SAFETY FACTORS ARE GREATER THAN OR EQUAL TO 1.95 FOR PEAD LOAD AND 1.75 FOR LIVE LOAD, THE MINIMUM REQUIRED BY ASTM F2787 AND BY ASSINTO FOR THERMOPLASTIC PIPE.
- b. A STRUCTURAL EVALUATION SEALED BY A REGISTERED PROFESSIONAL ENGINEER THAT DEMONSTRATES THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, SECTION 12.12, ARE MET, THE 50 YEAR CREEP MODULUS DATA SPECIFIED IN ASTM F2418 OR ASTM F2922 MUST BE USED AS PART OF THE AASHTO STRUCTURAL EVALUATION TO VERIFY LONG-TERM PERFORMANCE.
- c. STRUCTURAL CROSS SECTION DETAIL ON WHICH THE STRUCTURAL EVALUATION IS BASED. 8. CHAMBERS AND END CAPS SHALL BE PRODUCED AT AN ISO 9001 CERTIFIED MANUFACTURING FACILITY.

IMPORTANT - NOTES FOR THE BIDDING AND INSTALLATION OF THE SC-310/SC-740 SYSTEM

- STORMTECH SC-310 & SC-740 CHAMBERS SHALL NOT BE INSTALLED UNTIL THE MANUFACTURER'S REPRESENTATIVE HAS COMPLETED A PRE-CONSTRUCTION MEETING WITH THE INSTALLERS.
- 2. STORMTECH SC-310 & SC-740 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH SC-310/SC-740/SC-780 CONSTRUCTION GUIDE".
- 4. THE FOUNDATION STONE SHALL BE LEVELED AND COMPACTED PRIOR TO PLACING CHAMBERS.
- 5. JOINTS BETWEEN CHAMBERS SHALL BE PROPERLY SEATED PRIOR TO PLACING STONE.
- 6. MAINTAIN MINIMUM 150 mm (6") SPACING BETWEEN THE CHAMBER ROWS. EMBEDMENT STONE SURROUNDING CHAMBERS MUST BE A CLEAN, CRUSHED, ANGULAR STONE 20-50 mm (3/4-2").

CHAMBERS ARE NOT TO BE BACKFILLED WITH A DOZER OR AN EXCAVATOR SITUATED OVER THE CHAMBERS.

- 8. THE CONTRACTOR MUST REPORT ANY KNOWN DISCREPANCIES WITH CHAMBER FOUNDATION MATERIALS BEARING CAPACITIES TO THE SITE DESIGN ENGINEER.
- ADS RECOMMENDS THE USE OF "FLEXSTORM CATCH IT" INSERTS DURING CONSTRUCTION FOR ALL INLETS TO PROTECT THE SUBSURFACE STORMWATER MANAGEMENT SYSTEM FROM CONSTRUCTION SITE RUNOFF.
- NOTES FOR CONSTRUCTION EQUIPMENT STORMTECH SC-310 & SC-740 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE".
- 2. THE USE OF CONSTRUCTION EQUIPMENT OVER SC-310 & SC-740 CHAMBERS IS LIMITED:

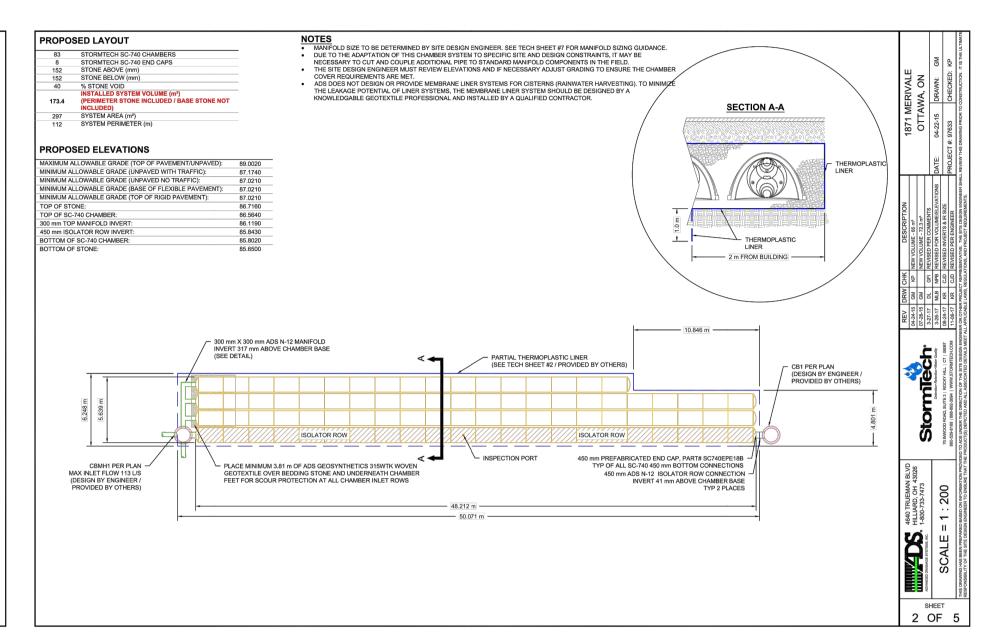
 NO EQUIPMENT IS ALLOWED ON BARE CHAMBERS.

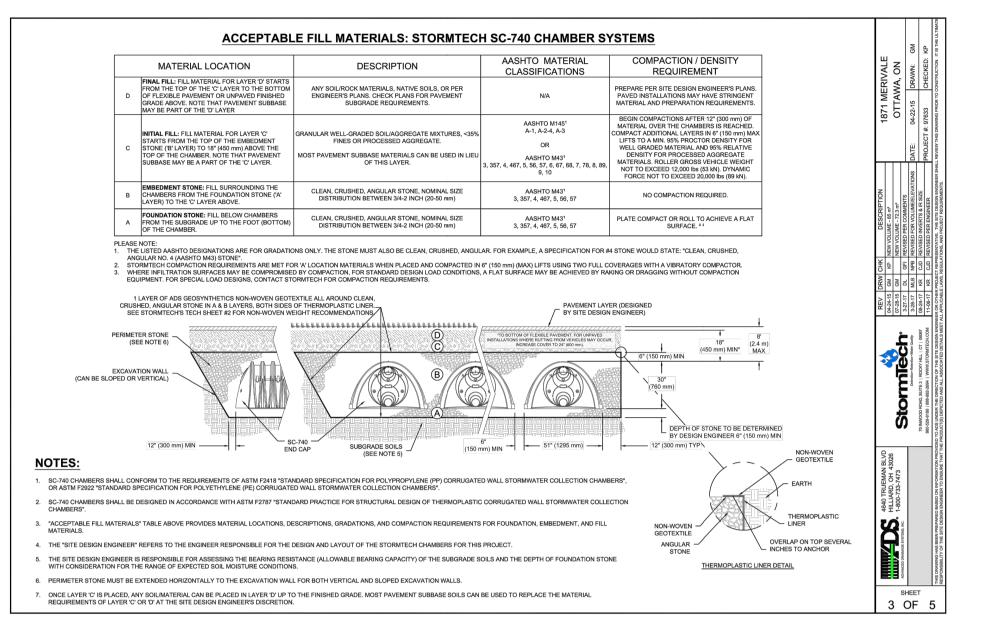
 NO RUBBER TIRED LOADERS, DIMP TRUCKS, OR EXCAVATORS ARE ALLOWED UNTIL PROPER FILL DEPTHS ARE REACHED IN ACCORDANCE WITH THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE".

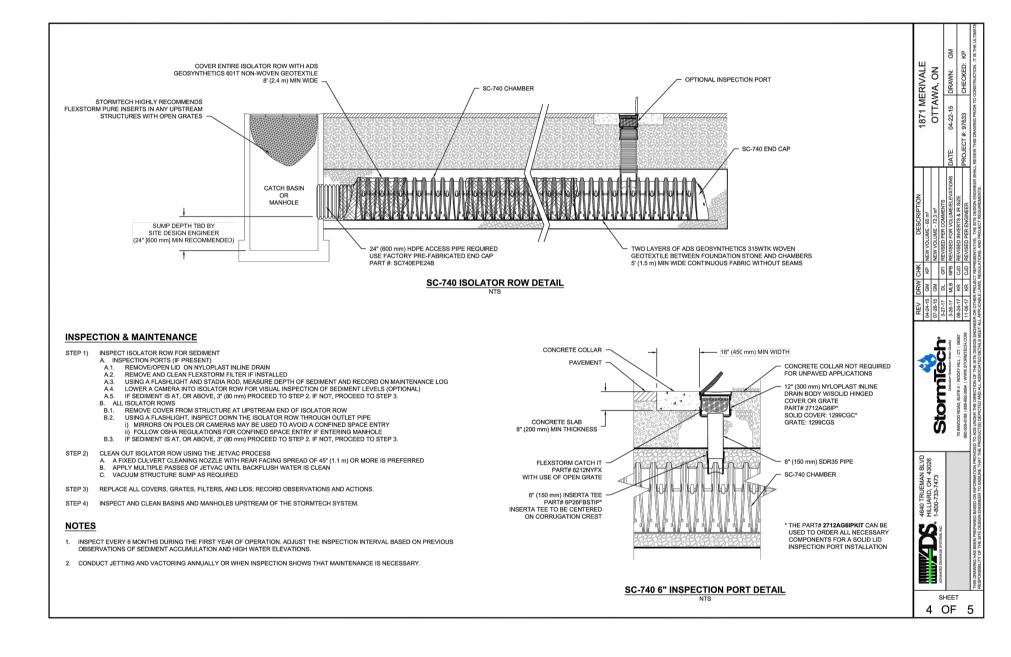
 WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT CAN BE FOUND IN THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE".
- 3. FULL 900 mm (36") OF STABILIZED COVER MATERIALS OVER THE CHAMBERS IS REQUIRED FOR DUMP TRUCK TRAVEL OR DUMPING.

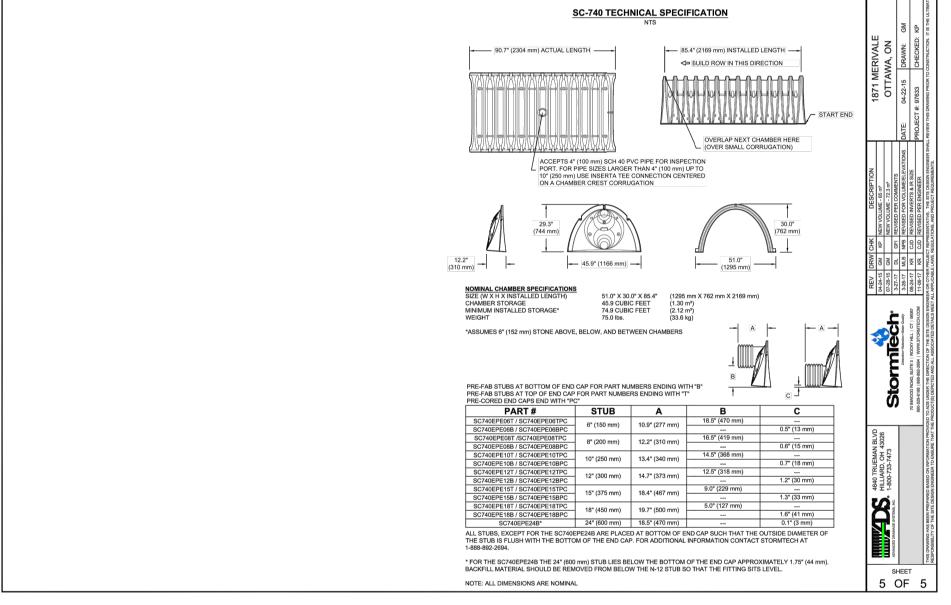
USE OF A DOZER TO PUSH EMBEDMENT STONE BETWEEN THE ROWS OF CHAMBERS MAY CAUSE DAMAGE TO THE CHAMBERS AND IS NOT AN ACCEPTABLE BACKFILL METHOD. ANY CHAMBERS DAMAGED BY THE "DUMP AND PUSH" METHOD ARE NOT COVERED UNDER THE STORMTECH STANDARD WARRANTY.

CONTACT STORMTECH AT 1-888-892-2694 WITH ANY QUESTIONS ON INSTALLATION REQUIREMENTS OR WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT









USE AND INTERPRETATION OF DRAWINGS

GENERAL CONDITIONS OF THE CONTRACT FOR CONSTRUCTION ARE PART OF THE CONTRACT DOCUMENTS AND DESCRIBE USE AND INTENT OF THE DRAWING. THE CONTRACT DOCUMENTS INCLUDE NOT ONLY THE DRAWINGS. BUT ALSO THE OWNER-CONTRACTOR REQUIRED BY ALL. WORK NOT COMPLETELY DELINEATED HEREON SHALL BE CONSTRUCTED OF THE SAME MATERIALS AND DETAILED SIMILARLY AS WORK SHOWN MORE COMPLETELY ELSEWHERE IN THE CONTRACT DOCUMENTS.

BY USE OF THE DRAWINGS FOR CONSTRUCTION OF THE PROJECT, THE OWNER CONFIRMS THAT HE HAS REVIEWED AND APPROVED THE DRAWINGS. THE CONTRACTOR CONFIRMS THAT HE HAS VISITED THE SITE, FAMILIARIZED HIMSELF WITH THE LOCAL CONDITIONS, VERIFIED FIELD DIMENSIONS AND CORRELATED HIS OBSERVATIONS WITH THE REQUIREMENTS OF THE CONTRACT DOCUMENTS.

AS INSTRUMENTS OF SERVICE, ALL DRAWINGS, SPECIFICATIONS, CADD FILES OR OTHER ELECTRONIC MEDIA AND COPIED THERE OF FURNISHED BY THE ENGINEER ARE HIS PROPERTY. THEY ARE TO BE USED ONLY FOR THIS PROJECT AND ARE NOT TO BE USED ON ANY OTHER PROJECT, INCLUDING REPEATS OF THE PROJECT. CHANGES TO THE DRAWINGS MAY ONLY BE MADE BY THE ENGINEER.

UNLESS THE REVISION TITLE IS "ISSUED FOR CONSTRUCTION", THESE DRAWINGS SHALL BE CONSIDERED PRELIMINARY AND SHALL NOT BE USED AS A CONSTRUCTION DOCUMENT. THESE DRAWINGS ILLUSTRATES THE WORK TO BE DONE. THE ENGINEER IS NOT RESPONSIBLE FOR THE MEANS, METHODS, TECHNIQUES, SEQUENCES, AND PROCEDURES USED TO DO THE WORK, OR THE SAFETY ASPECTS OF CONSTRUCTION, AND NOTHING ON THESE

DRAWINGS EXPRESSED OR IMPLIED CHANGES THIS CONDITION. CONTRACTOR SHALL DETERMINE ALL CONDITIONS AT THE SITE AND SHALL BE RESPONSIBLE FOR KNOWING HOW THEY AFFECT THE WORK. SUBMITTAL OF A BID TO PERFORM THIS WORK IS ACKNOWLEDGEMENT OF THE RESPONSIBILITIES, AND THAT THEY HAVE BEEN FULLY CONSIDERED IN PLANNING OF THE WORK, AND THE BID PRICE. NO CLAIMS FOR EXTRA CHARGES DUE TO THESE CONDITIONS WILL BE FORTHCOMING.

IN THE EVENT THE CLIENT, THE CLIENT, THE CLIENT, PLANS, SPECIFICATIONS OR SUBCONTRACTORS, OR ANYONE FOR WHOM THE CLIENT IS LEGALLY LIABLE MAKES OR PERMITS TO BE MADE ANY CHANGES TO ANY REPORTS, PLANS, SPECIFICATIONS OR OTHER CONSTRUCTION DOCUMENTS PREPARED BY LRL ASSOCIATES LTD. (LRL) WITHOUT OBTAINING LRL'S PRIOR WRITTEN CONSENT, THE CLIENT SHALL ASSUME FULL RESPONSIBILITY FOR THE RESULTS OF SUCH CHANGES. THEREFORE THE CLIENT AGREES TO WAIVE ANY CLAIM AGAINST LRL AND TO RELEASE LRL FROM ANY LIABILITY ARISING DIRECTLY OR INDIRECTLY FROM SUCH UNAUTHORIZED CHANGES.

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NOT AUTHENTIC UNLESS SIGNED AND DATED



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07 AS PER CITY COMMENTS G.C. 03 OCT 2018 06 AS PER CITY COMMENTS G.C. 30 AUG 2018 05 AS PER CITY COMMENTS G.C. 20 JUL 2018 04 ISSUED FOR SPA G.C. 05 JUN 2018 03 AS PER CITY COMMENTS G.C. 26 OCT 2017 02 AS PER CITY COMMENTS G.C. 25 AUG 2017 01 ISSUED FOR SPA G.C. 24 MAR 2017 REVISIONS BY DATE

BENSON AUTO PARTS MR. GERRY BENSON 700 EDUCATION ROAD, CONRWALL, ONTARIO K6H 6B8, TEL. 613-936-7850 G.C.

PROPOSED BENSON AUTO PARTS COMMERCIAL DEVELOPMENT 1871 MERIVALE ROAD, NEPEAN, ON

PROJEC

CONSTRUCTION DETAILS PLAN

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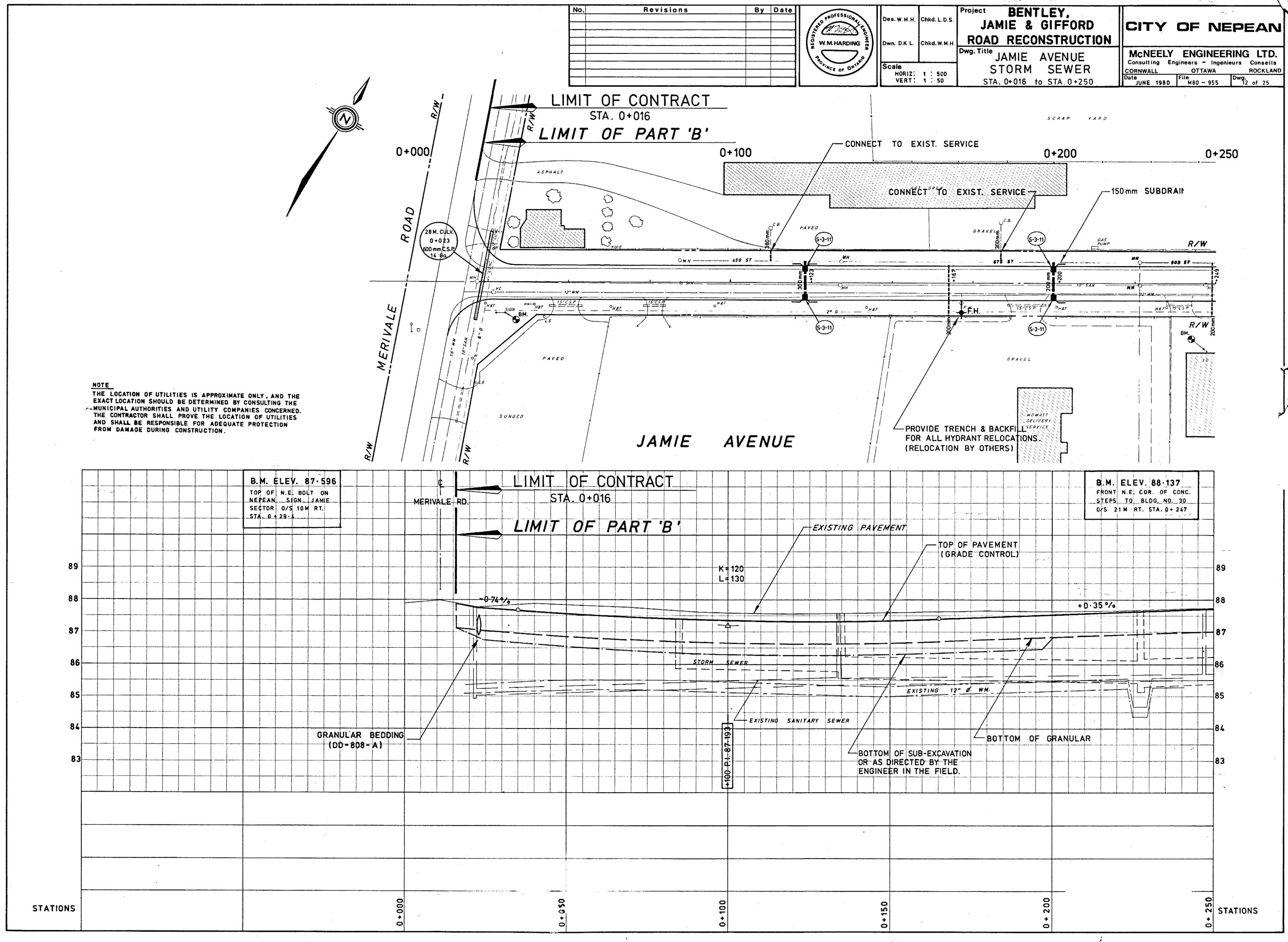
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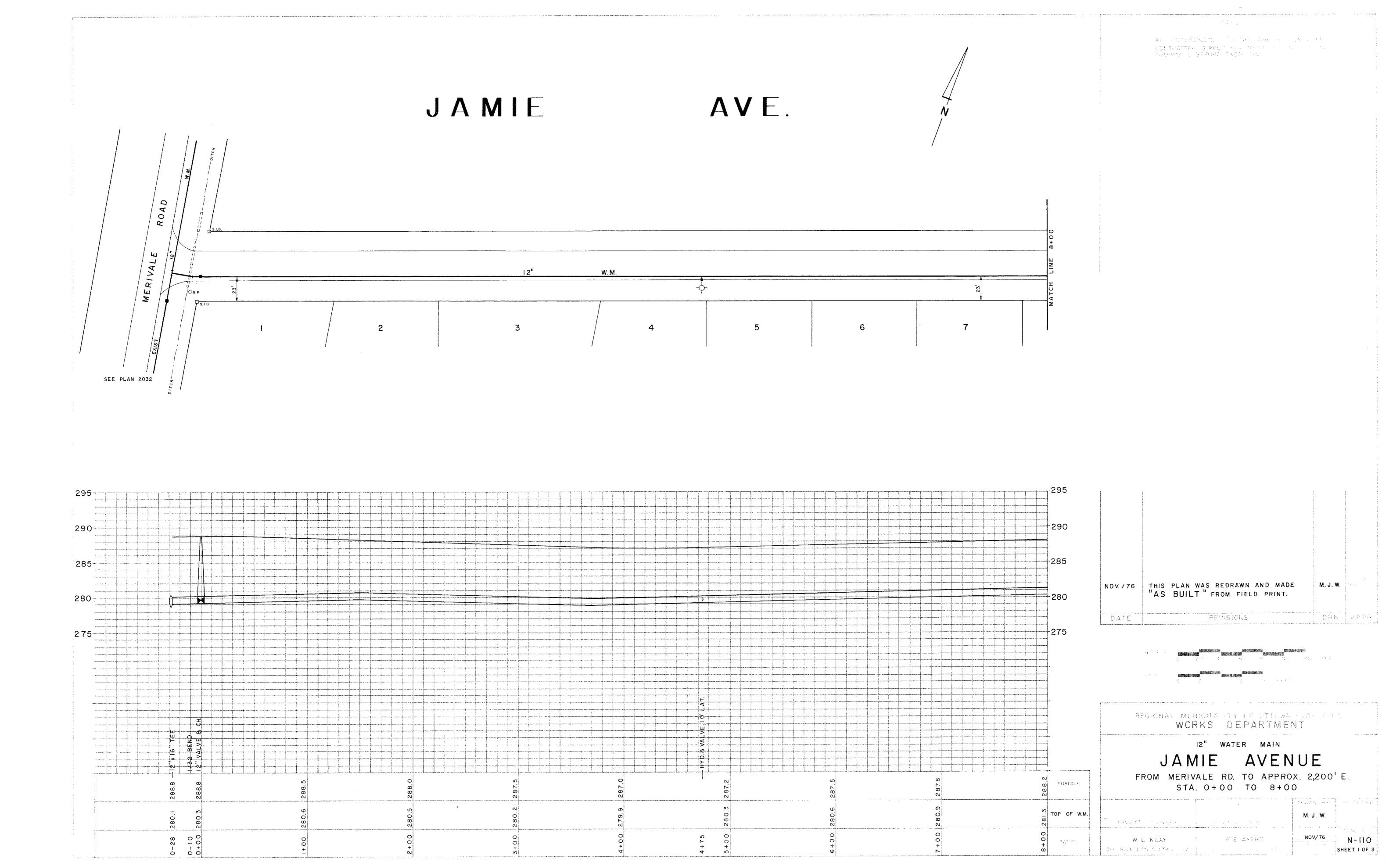
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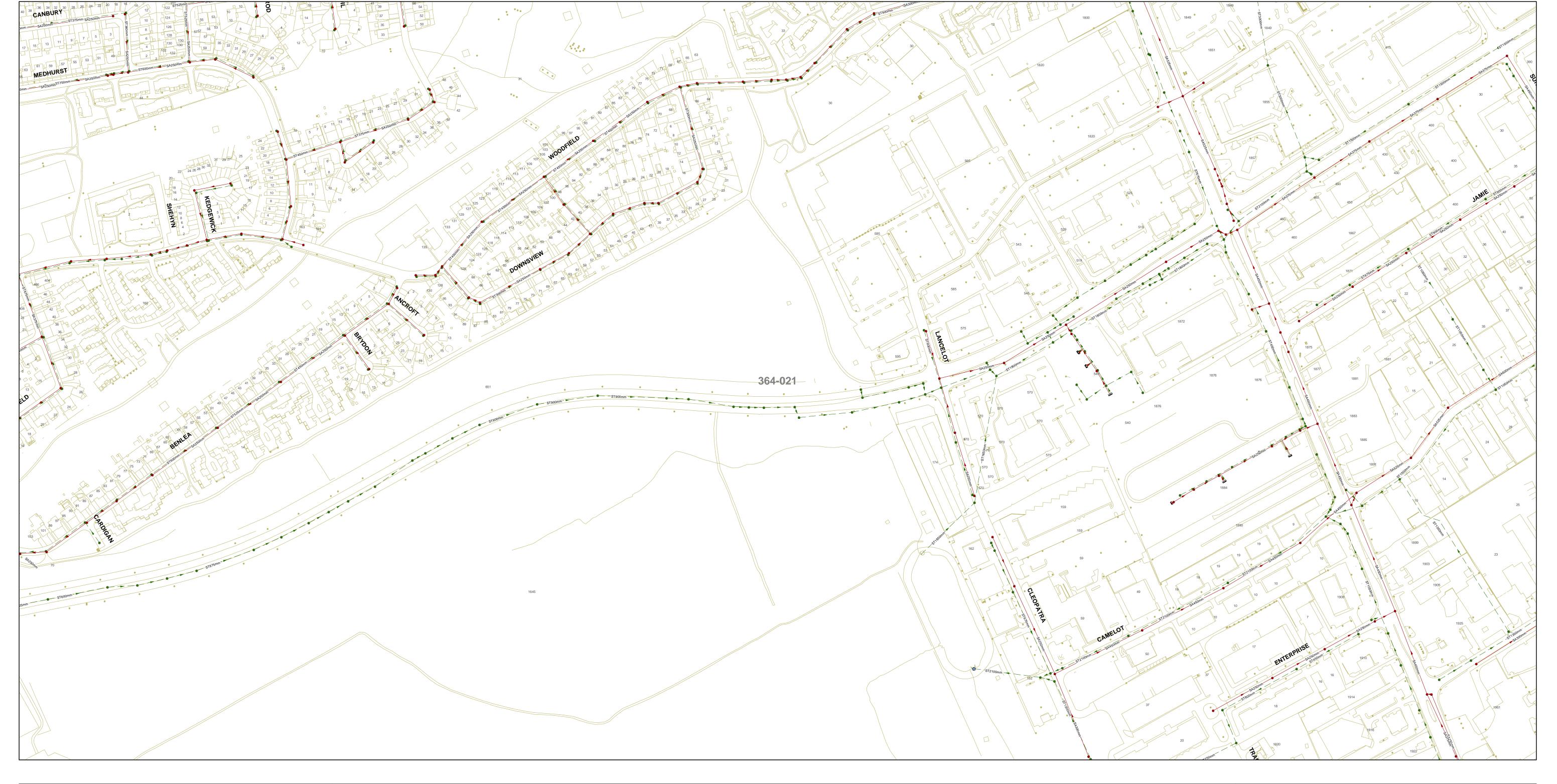
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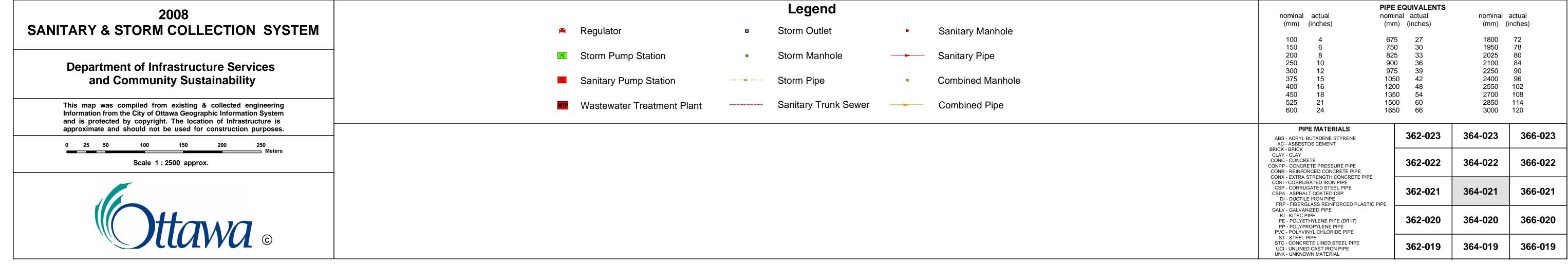
APPENDIX H

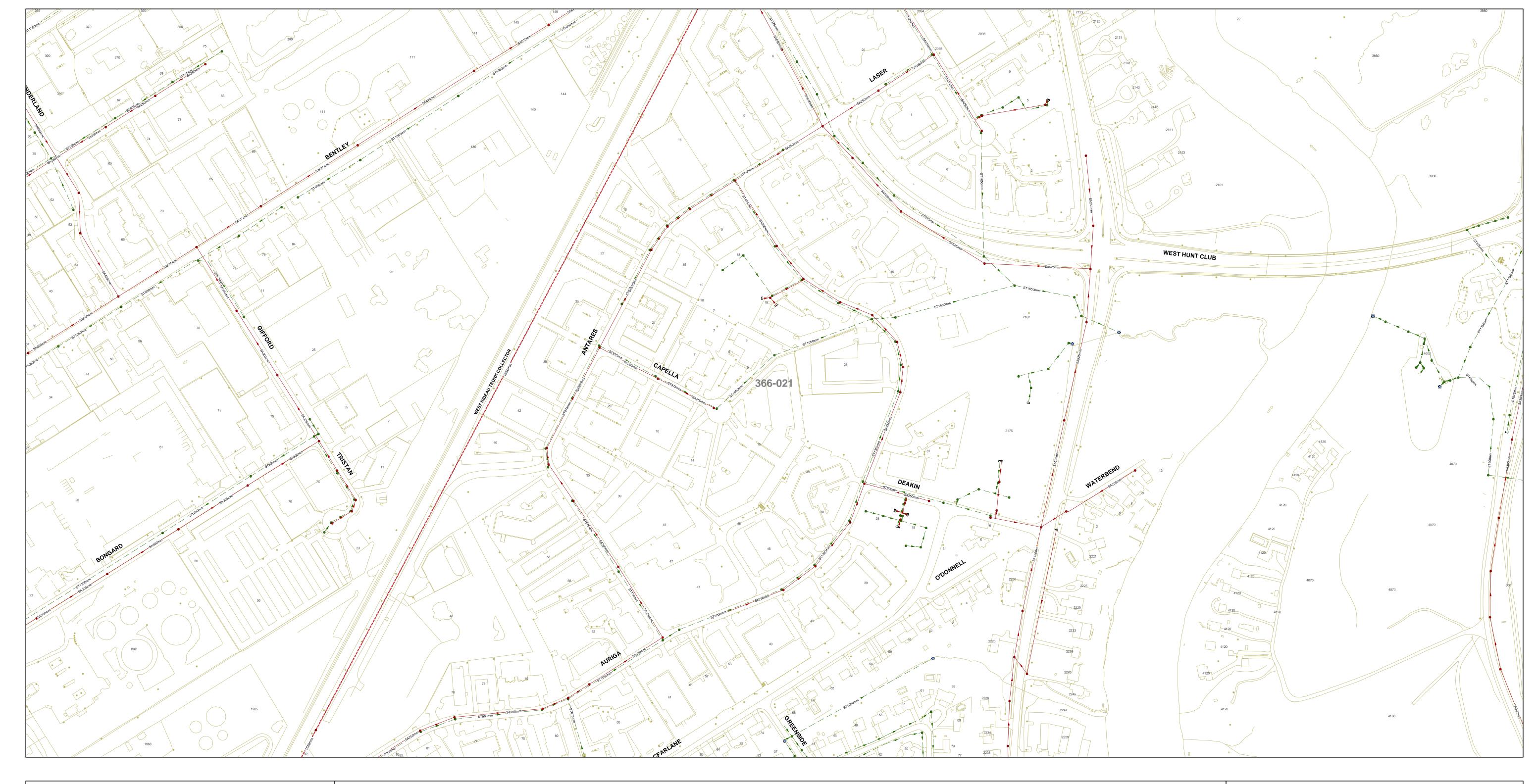
Jamie Avenue As-Built Drawings













APPENDIX IBoundary Conditions

From: Fraser, Mark < Mark.Fraser@ottawa.ca>

Sent: July-05-17 4:01 PM **To:** Michel Gagnon

Cc: Marty Benson; Guillaume Courtois

Subject: RE: 1871 Merivale Road **Attachments:** 1871 Merivale July 2017.pdf

Hi Michel,

Please find below boundary conditions for hydraulic analysis as requested based on the provided anticipated water demands:

Proposed Development Location: 1871 Merivale Road

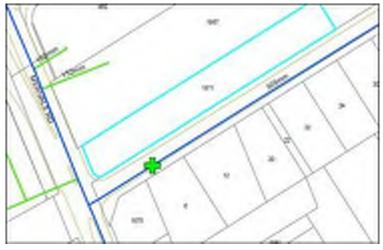
Average Day = 2.78 L/s **Max Day** = 4.16 L/s **Peak Hour** = 5.0L/s **Fire Flow** = 135 L/s

City of Ottawa Boundary Conditions:

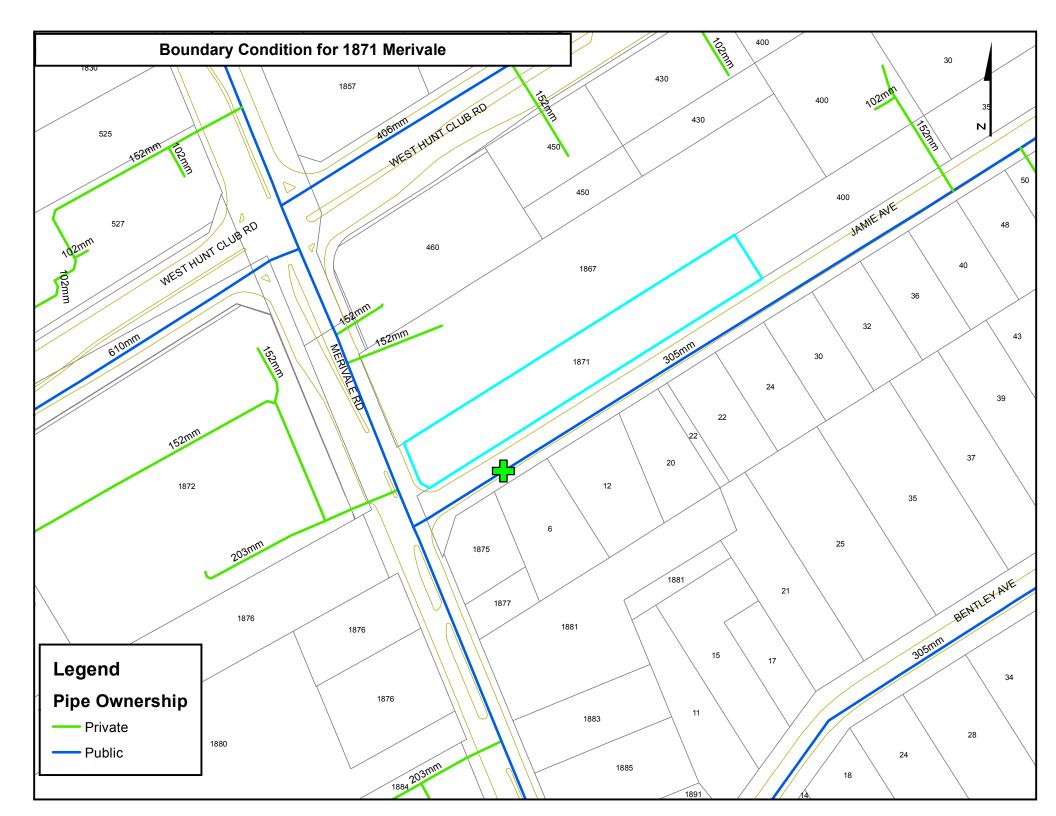
The following are boundary conditions, HGL, for hydraulic analysis at 1871 Merivale (Pressure Zone 2W) assumed to be connected to the 305mm on Jamie Ave.:

Minimum HGL = **126.7m** Maximum HGL = **134.5m** MaxDay + FireFlow (135 L/s) = **127.4m**

These are for current conditions and are based on computer model simulation.



Please refer to City of Ottawa, *Ottawa Design Guidelines – Water Distribution*, First Edition, July 2010, WDG001 Clause 4.2.2 for watermain pressure and demand objectives.



APPENDIX J
RVCA Correspondence

Guillaume Courtois

From: Eric Lalande <eric.lalande@rvca.ca>

Sent: July-16-18 10:58 AM **To:** Guillaume Courtois

Subject: RE: 130828 - Benson, 1871 Merivale Road, Nepean, ON --- RVCA Requirements

Follow Up Flag: Follow up Flag Status: Flagged

Hi Guillaume,

The RVCA requires an enhanced level of protection (80% TSS removal) for development, prior to outletting to a watercourse. It would appear that the site at 1871 Merivale, outlets to a stormwater facility which provides quality control. As such, no on-site quality controls are required from the RVCA. I would note that the pond was cleaned out in 1998, I am curious when the most recent maintenance was performed. (If you could get that from the City to include in your report, that would be helpful.)

Thank you,

Eric Lalande, MCIP, RPP

Planner, Rideau Valley Conservation Authority 613-692-3571 x1137

From: Jamie Batchelor

Sent: Monday, July 16, 2018 10:41 AM

To: 'Guillaume Courtois' <gcourtois@lrl.ca>
Cc: Eric Lalande <eric.lalande@rvca.ca>

Subject: RE: 130828 - Benson, 1871 Merivale Road, Nepean, ON --- RVCA Requirements

Good Morning Guillaume,

I have forded your request to Eric Lalande who would be the RVCA Planner for this area.

From: Guillaume Courtois [mailto:gcourtois@lrl.ca]

Sent: Monday, July 16, 2018 10:13 AM

To: Jamie Batchelor < jamie.batchelor@rvca.ca>

Subject: 130828 - Benson, 1871 Merivale Road, Nepean, ON --- RVCA Requirements

Hi Jamie,

My name is Guillaume Courtois. I'm the Civil Designer for the proposed Benson project located at 1871 Merivale Road, Nepean, ON. We have received correspondence from the City of Ottawa stating we are to contact the RVCA regarding water quality treatment for the subject site. Would you be able to inform me of the RVCA requirements for this project? Please use the following link for access to our latest project documents for your use:

https://lrl.sharefile.com/d-s6b45783e7874f63a

If you require anything further, or if I should be contacting someone else, please let me know.

Best regards,

Guillaume Courtois, C.E.T.

Civil Engineering Technologist

LRL Associates Ltd.

5430 Canotek Road

Ottawa, Ontario K1J 9G2

(613) 842-3434 or (877) 632-5664 ext. 221

Fax: (613) 842-4338 Email: gcourtois@lrl.ca Website: www.LRL.ca