

120 Iber Road, Unit 103 Stittsville, Ontario K2S 1E9 Tel (613) 836-0856 Fax (613) 836-7183 www.dsel.ca

TECHNICAL MEMORANDUM

DATE: 2020-07-15

ATTACHMENTS:

TO: Mohammad Abdul Mottalib, P.Eng

- SUBJECT: Zibi Ontario Block 206, Servicing Brief
- OUR FILE: DSEL Project No. 20-1178
 - MSS Water Demand Calculation Sheet, prepared by DSEL dated May 2018;
 - Block 206 Water Demand Calculation Sheet, prepared by DSEL dated July 2020;
 - Block 206 FUS Calculation Sheet, prepared by DSEL dated July 2020;
 - Block 206 EPANET Model Schematic, prepared by DSEL dated July 2020;
 - EPANET Model Output Files, prepared by DSEL Dated July 2020;
 - Extracted Pages from Temporary Pump Station Design Report prepared by Hatch dated November 23, 2018;
 - Block 206 Wastewater Discharge Calculation Sheet, prepared by DSEL – dated July 2020;
 - Ultimate Sanitary Design Sheet, prepared by DSEL dated June 2019;
 - Block 206 Storm Sewer Design Sheet, prepared by DSEL dated July 2020;
 - Zibi Ontario Master Plan, prepared by Fotenn Planning + Design dated December 2016;
 - Zibi Ontario Block 206 Site Plan and Site Statistics, prepared by Kohn Partnership Architects Inc.– dated July 6, 2020;

Windmill DREAM Developments has retained DSEL to prepare an amendment to the Functional Servicing and Stormwater Management Report in support of their Site Plan Control (SPC) application for Block 206 of the Zibi Ontario lands. The development of Block 206 was contemplated in the Master Servicing Plan, prepared by DSEL and dated June 2018 (*MSS*), refer to the Master Plan drawing in the *Drawings/Figures* folder of the attachments. The *MSS* contemplated approximately *612* m^2 of retail space, *198* residential units and *3,674* m^2 of office space for Block 206. The proposed Block 206 development results in an increase footprint to

<u>EMAIL</u>

Block 206 then contemplated in the MSS from a gross floor area of 18,275 m² to 20,554 m² including of **799** m² of retail space and **204** residential units composed of; 95 single bedroom units; 64 2-bedroom units; and 45 co-living suites consisting of a total of 180 beds.

Phase 1 buildings as well as Block 207 and Block 211 are planned to be constructed prior Block 206 and are submitted under separate applications. They have been included in the calculations for water and wastewater for this report for consistency in water modelling and pump station sizing.

Water Servicing

As contemplated in the **MSS**, water service for Block 206 will connect directly to the existing 200 mm diameter watermain within Chaudiere Private which was constructed during the first phase of the development.

The City of Ottawa was contacted to obtain boundary conditions for the full buildout of development and also boundary conditions for Phase 1 works which includes water demands for Blocks 205a, 208, 211, and 207.

The boundary conditions for proposed water demands are summarized in *Table 1* and *Table 2* below:

Water Demand – MSS					
Design Parameter	MSS Demand (L/min)	Boundary Condition ² (m H ₂ O / kPa) Connection @ Booth Street		Boundary Condition ² (m H ₂ O / kPa) Connection @ Wellington Street	
Average Daily Demand					
	685.1	61.2	600.4	59.7	585.9
Max Day + Fire Flow	1,427.2 + 22,000 =				
	23,427.2	46.5	456.2	52.6	516.2
Peak Hour	2,212.1	54.2	77.1	52.7	517.2

Table 1

Water Demand – Blocks 205a, 208, 211 and 207					
Design Parameter	Blocks 205a, 208, 211 and 207 Demand (L/min)	d 207 (m H ₂ O / kPa) and Connection @ Booth		Boundary Condition ² (m H ₂ O / kPa) Connection @ Wellington Street	
Average Daily Demand					
	117.2	61.3	601.4	59.8	586.8
Max Day + Fire Flow	255.6 + 19,000 =				
	19,255.6	49.1	481.7	51.6	506.4
Peak Hour	426.9	53.6	525.8	52.1	511.3

Table 2

As demonstrated, the development flow demands have little influence on the HGLs at the proposed connection locations.

The proposed water demands for the Block 206 development phase are summarized in *Table 3* below. Refer to *Appendix B,* in the attachments for water demand calculations.

Water Demand – Blocks 205a, 208, 211, 207 and 206		
Design Parameter	Blocks 205a, 208, 211, 207 and 206 Demand (L/min)	
Average Daily Demand	254.20	
Max Day + Fire Flow	547.76 + 21,000 = 21,547.76	
Peak Hour	1039.68	

 Table 3

 Water Demand – Blocks 205a, 208, 211, 207 and 206

Fire demand for Block 206 was calculated using the *City of Ottawa Technical Bulletin ISTB-2018-02*, and resulted in a fire flow of **21,000 L/min**. Please refer to correspondence in the **Appendix A** confirming the building is equipped with a fully supervised sprinkler system.

The hydraulic model, per the *Approved FSR*, was updated to confirm adequate pressure and fire flow is available to service Block 206. Pressures are summarized in *Table 4* below:

Node ID	Pressure (kPa)		
	Average Day Max Day + Fir Flow		Peak Hour
Block 206	605.4	175.3	520.1
Hydrant 4	600.1	240.7	515.7
Hydrant 5	590.6	142.6	506.2
Hydrant 6	605.4	178.0	520.2
Hydrant 7	592.7	219.1	508.4

Table 4 EPANET Results

Pressures during the fire flow scenario are above the minimum required per the *City of Ottawa Water Supply Guideline (2010)*. Pressure during the Average Day scenario pressures exceed the recommended pressures, thus, pressure reducing valves may be required, to be confirmed through the mechanical design of the proposed building. Hydrants have been located in accordance with the *MSS*.

Sanitary Servicing

Block 206 is proposed to be serviced by a connection to the 250 mm sanitary sewer within Chaudiere Private, constructed in Phase 1. The Phase 1 sanitary sewers were sized to convey the flow from Block 206, in accordance with the *Approved FSR*.

As indicated in the *Approved FSR*, a temporary pumping station was constructed within the footprint of the existing Building 535 to service the first phases of development The pump station design report, prepared by Hatch, and dated November 2018 (*Temp PS 2018*), indicates that the

temporary pumping station is designed to pump a peak wet weather flow of **13** *L*/s, refer to extracted pages from the **Temp PS 2018** report confirming the **13** *L*/s of design capacity.

The interim pump station is to service the development phases until the sanitary flow directed to the pump station exceeds 80% (**10.4 L/s**) of the interim pump station capacity, at which point the ultimate pump station is to be constructed in accordance with the site plan conditions.

Table 5, below, summarizes the anticipated wastewater discharge from the proposed Phase 1, 2 and 3 and Block 206 development.

Summary of Anticipated Wastewater Discharge				
Design Parameter	Approved Flow (L/s)	Phase 1, Block 211, 207 & 206 Flow (L/s)		
Average Dry Weather Flow Rate	3.0	4.4		
Peak Dry Weather Flow Rate	6.8	10.0		
Peak Wet Weather Flow Rate	7.2	10.7		

Table 5	
Summary of Anticipated Wastewater Discharge	

As shown in **Table 5**, above, it is anticipated that Block 206 will result in an increase in sanitary discharge, refer to **Appendix C** for sanitary calculation sheets. The overall sanitary flow to the pump station is 82% of the total capacity of the interim pump station. Since the overall sanitary flow being directed to the pump station exceeds 80% of the total capacity of the interim pump station, the ultimate pump station will need to be constructed in order to service the development of Block 206. The design and capacity for the ultimate pump station will be provided under a separate cover.

The anticipated increase in sanitary flow still results in less flow than what was contemplated in the **MSS**.

Stormwater Management

Storm water runoff from the proposed Block 206 development will discharge through a service connection to the 450mm diameter storm sewer within Chaudiere Private, which ultimately outlets to the north edge of Chaudière Island, east of Booth Street, consistent with the *Approved FSR*.

The proposed building footprint of Block 206 has been updated from the contemplated footprint in the **MSS**. Refer to the **SWM-1** drawing included in the attachments for updated catchment areas directed to the storm sewer. As shown in the revised storm design sheet, the sewers have sufficient capacity to convey the updated flows.

An Oil-Grit-Separator (**OGS**) was installed as part of Phase 1 development, which will provide **80% TSS Removal** prior to discharging to the Ottawa River. The overall imperviousness is consistent with previous approvals; therefor, the oil/grit separator (OGS) will continue to function as intended.

Quantity controls are not required per the approved **MSS**.

Required Permits / Approvals

The proposed development is subject to the site plan control approval process. The City of Ottawa must approve the engineering design drawings and reports prior to the issuance of site plan control.

An amendment to the previously issued Environmental Compliance Approval (ECA #1505-B96UCV) has been approved (ECA #6146-BQ8T7V) to reflect the new storm sewers; increase in service area to the interim pump station; and off-site sanitary infrastructure.

Yours truly, **David Schaeffer Engineering Ltd.**

David Schaeffer Engineering Ltd.

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Per: Genavieve Greenberg

Per: Brandon Chow

Reviewed by, **David Schaeffer Engineering Ltd.**

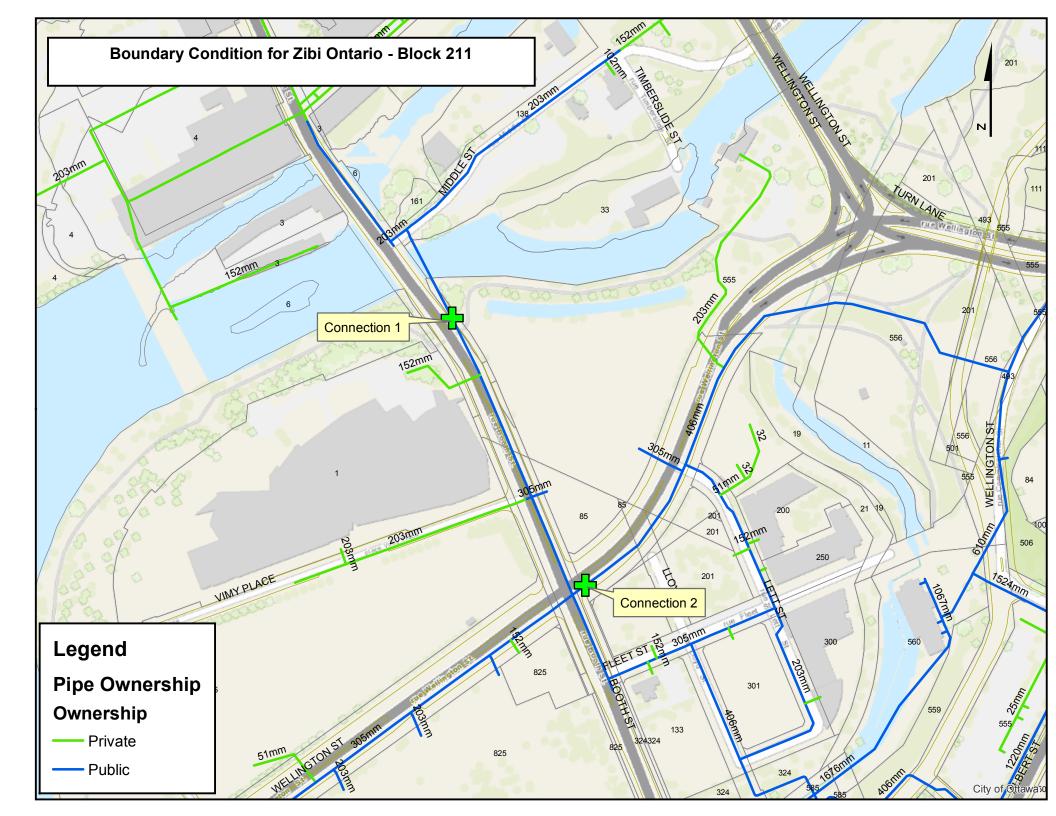


Per: Adam Fobert, P. Eng

Z:\Projects\20-1178_Windmill_Zibi-Block-206-207\B_Design\B3_Reports\B3-2_Servicing (DSEL)\2020-06-01_Block 206_subm1\2020-07-13_1178_memo-ggg.docx

APPENDIX A

Pre-Consultation



To: Subject: Robert Freel RE: Chaudiere/Albert Island Development - Water Boundary Condition Request

From: Mottalib, Abdul [mailto:Abdul.Mottalib@ottawa.ca]
Sent: April-08-15 10:30 AM
To: 'Robert Freel'
Cc: Mottalib, Abdul; 'Adam Fobert'
Subject: FW: Chaudiere/Albert Island Development - Water Boundary Condition Request

Hi Bobby,

Please see below as requested.

Thanks,

Abdul Mottalib, P. Eng.

From: Sent: April 08, 2015 10:20 AM To: Mottalib, Abdul Subject: RE: Chaudiere/Albert Island Development - Water Boundary Condition Request

The following are boundary conditions, HGL, for hydraulic analysis at the Chaudière/Albert Islands (Pressure Zone 1W), assumed to be connected to (see attached PDF for location):

- 1) 406mm on Wellington
- 2) 305mm on Booth

Minimum HGL = 108.1m (same at both locations)

Maximum HGL = 115.1m (same at both locations), the maximum pressure is estimated to be greater than 80 psi. A pressure check at completion of construction is recommended to determine if pressure control is required.

Fire Flow*	Connection 1 (Wellington)
150 L/s	110.6m
217 L/s	110.0m
250 L/s	109.6m
300 L/s	109.0m

367 L/s	108.0m
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*Includes Max Day demands of 23.79 L/s distributed evenly between both connection points (i.e. 11.9 L/s at each connection point)

Fire Flow*	Connection 2 (Booth)
150 L/s	109.0m
217 L/s	107.0m
250 L/s	105.8m
300 L/s	103.7m
367 L/s	100.4m

*Includes Max Day demands of 23.79 L/s distributed evenly between both connection points (i.e. 11.9 L/s at each connection point)

These are for current conditions and are based on computer model simulation.

Disclaimer: The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation.

From: Robert Freel [mailto:rfreel@dsel.ca]
Sent: April 01, 2015 5:21 PM
To: Mottalib, Abdul
Subject: RE: Chaudiere/Albert Island Development - Water Boundary Condition Request

Good afternoon Abdul,

We would like to request updated watermain boundary conditions for the above referenced site. Please see the anticipated demands below.

- 1. Location of Service / Street Number: Connection 1 and 2 as shown on the previous request attached
- 2. Type of development and the amount of fire flow required for the proposed development:
 - Proposed development is a mixed use community.
 - It is anticipated that the development will be services via a connections 1 and 2 as shown by the attached map.
 - Can you provide the available fire flow for the following demands as determined by the FUS:
 - o 9,000L/min
 - o **13,000L/min**
 - o 15,000L/min
 - o 18,000L/min

o 22,000L/min

3. The estimated demand for the proposed conditions is summarized below:

	L/min	L/s
Avg. Daily	685.1	11.42
Max Day	1427.2	23.79
Peak Hour	2212.1	36.87

Thanks,

Bobby Freel, P.Eng.

DSEL

david schaeffer engineering ltd.

120 Iber Road, Unit 203 Stittsville, ON K2S 1E9

phone: (613) 836-0856 ext.258 **cell**: (613) 314-7675 **email**: rfreel@DSEL.ca

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Steve Merrick

From:	Buchanan, Richard <richard.buchanan@ottawa.ca></richard.buchanan@ottawa.ca>
Sent:	Thursday, June 6, 2019 12:18 PM
То:	Steve Merrick
Subject:	Zibi Ontario - Block 211 - Boundary Condition Request
Attachments:	image006.emz; image011.emz; Zibi Ontario - Block 211 June 2019.pdf

Hi Steve

The following are boundary conditions, HGL, for hydraulic analysis at Zibi Ontario (zone 1W) assumed to be connected to the 406mm on Booth (connection 1) and 406mm on Wellington (connection 2). See attached PDF for locations.

The water demands provided include demands for Phase 1, Phase 2 and Block 211 (205A, 207, 208, 211)

Minimum HGL = 107.5m, same at both connections

Maximum HGL = 115.2m, same at both connections. The maximum pressure is estimated to be greater than 80 psi. A pressure check at completion of construction is recommended to determine if pressure control is required.

MaxDay + Fireflow (317 L/s) = 103.0m, Booth St connection

MaxDay + Fireflow (317 L/s) = 107.0m, Wellington connection

These are for current conditions and are based on computer model simulation.

Disclaimer: The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation.

Richard Buchanan, CET

Coordinator, Front Ending Agreements and Brownfields Programs Planning Services, Development Review Branch Planning, Infrastructure and Economic Development Department City of Ottawa | Ville d'Ottawa 613.580.2424 ext./poste 27801 ottawa.ca/planning / ottawa.ca/urbanisme

From: Steve Merrick <<u>SMerrick@dsel.ca</u>> Sent: June 05, 2019 9:34 AM To: Buchanan, Richard <<u>Richard.Buchanan@ottawa.ca</u>> Subject: Zibi Ontario - Block 211 - Boundary Condition Request CAUTION: This email originated from an External Sender. Please do not click links or open attachments unless you recognize the source.

ATTENTION : Ce courriel provient d'un expéditeur externe. Ne cliquez sur aucun lien et n'ouvrez pas de pièce jointe, excepté si vous connaissez l'expéditeur.

Hi Richard,

Hope all is well, I wanted to reach out to obtain boundary conditions for the above noted site.

1. Location of Service / Street Number: **3 Booth Street**

2. Type of development: **The proposed next phase of development on Chaudiere Island** east of Booth Street, known as Block 211. The proposed development is a 9 storey building consisting of 1140m² of retail space and 15164m² of office space and 2 levels of underground parking

- 3. Proposed Connection points:
 - Connection 1 to existing 406mm watermain with Booth Street North of War Museum
 - **Connection 2 to existin 406mm watermain within Wellington Street** *@* **Booth Street** *Please see the diagram below for reference.*

4. Please provide pressures for the following water demand scenarios required for the proposed development. The water demands below include demands for Phase 1, Phase 2 and Block 211 (205A, 207, 208, 211)

	L/min
Avg. Daily	117.4
Max Day + FUS 1	255.6 + 19,000 = 19255.6
Peak Hour	426.9



Steve Merrick, P.Eng. Project Manager / Intermediate Designer

DSEL

david schaeffer engineering ltd.

120 Iber Road, Unit 103 Stittsville, ON K2S 1E9

phone: (613) 836-0856 ext. 561 **cell**: (613) 222-7816 **email**: smerrick@DSEL.ca

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Genavieve Greenberg

From:	Genavieve Greenberg
Sent:	Thursday, July 9, 2020 12:46 PM
То:	Genavieve Greenberg
Subject:	FW: Block 206 - Ground Floor Coord

From: Ivana Masnikosa <<u>imasnikosa@kohnarchitects.com</u>>
Sent: June 17, 2020 2:07 PM
To: Brandon Chow <<u>BChow@dsel.ca</u>>
Cc: Cormac Murray <<u>cmurray@teeplearch.com</u>>; Sean Lawrence <<u>slawrence@kohnarchitects.com</u>>; tdiamant
<<u>tdiamant@teeplearch.com</u>>; Shannon Card <<u>card@csw.ca</u>>
Subject: RE: Block 206 - Ground Floor Coord

Brandon, sorry, Restaurant number of seats: around 150, not around 200. Regards,

Ivana Masnikosa BArch, OAA Architect

Kohn Partnership Architects Inc. 116 Spadina Avenue, Suite 501, Toronto, ON, Canada, M5V 2K6 Telephone +1 416-703-6700 Ext. 2031 imasnikosa@kohnarchitects.com

From: Ivana Masnikosa
Sent: June 17, 2020 2:06 PM
To: Brandon Chow <<u>BChow@dsel.ca</u>>
Cc: Cormac Murray <<u>cmurray@teeplearch.com</u>>; Sean Lawrence <<u>slawrence@kohnarchitects.com</u>>; tdiamant
<<u>tdiamant@teeplearch.com</u>>; Shannon Card <<u>card@csw.ca</u>>
Subject: RE: Block 206 - Ground Floor Coord

Hi Brandon,

Here are my answers:

Block 206 GFA: 20,567m2/221,382sf Retail: 8,603sf Residents' Amenity Areas: 11,790sf No. of Residential units: 204

Block 207 GFA:7,238m2/77,914sf Retail: 6,290 sf Restaurant: 6,270 sf (if P1 level is included) / 4,230sf (only Ground Floor, without Restaurant space on P1 level) Restaurant number of seats: around 200 Offices: 60,950sf

Both 206&207 are Construction Class 3 (Non-Combustible) and C-1 (Noncumbustible).

Regards,

Ivana Masnikosa BArch, OAA Architect

Kohn Partnership Architects Inc. 116 Spadina Avenue, Suite 501, Toronto, ON, Canada, M5V 2K6 Telephone +1 416-703-6700 Ext. 2031 imasnikosa@kohnarchitects.com

From: Brandon Chow <<u>BChow@dsel.ca</u>>
Sent: June 17, 2020 12:23 PM
To: Ivana Masnikosa <<u>imasnikosa@kohnarchitects.com</u>>
Cc: Cormac Murray <<u>cmurray@teeplearch.com</u>>; Sean Lawrence <<u>slawrence@kohnarchitects.com</u>>; tdiamant
<<u>ttdiamant@teeplearch.com</u>>; Shannon Card <<u>card@csw.ca</u>>
Subject: RE: Block 206 - Ground Floor Coord

Can you provide the following:

- Building gross floor areas
- Office area
- Retail area
- Restaurant # of seats
- Residential unit counts
- Building construction class & occupancy type per ISO guide (attached)
- 1) Confirm the ISO construction class. Sections 1, 2 and 3 on pages 3 to 8 provides definitions to clarify. Note that ISO refers only to fire-resistive for fire ratings not less than 1-hour.
- Construction Class 1 (Frame)
- Construction Class 2 (Joisted Masonry)
- Construction Class 3 (Non-Combustible)
- Construction Class 4 (Masonry Non-Combustible)
- Construction Class 5 (Modified Fire Resistive)
- Construction Class 6 (Fire Resistive)
- 2) Confirm the ISO occupancy type. See Chapter 3 (pages 11-13) in the ISO guide.
- C-1 (Noncombustible)
- C-2 (Limited Combustibility)
- C-3 (Combustible)
- C-4 (Free Burning)
- C-5 (Rapid Burning or Flash Burning)

Let me know if you have any questions.

Thanks,

Brandon Chow Project Coordinator / Intermediate Designer

DSEL

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120 Iber Road, Unit 103

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phone: (613) 836-0856 ext.532 fax: (613) 836-7183 email: <u>bchow@DSEL.ca</u>

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From: Ivana Masnikosa <<u>imasnikosa@kohnarchitects.com</u>>
Sent: June 17, 2020 11:36 AM
To: Brandon Chow <<u>BChow@dsel.ca</u>>
Cc: Cormac Murray <<u>cmurray@teeplearch.com</u>>; Sean Lawrence <<u>slawrence@kohnarchitects.com</u>>; tdiamant
<<u>tdiamant@teeplearch.com</u>>; Shannon Card <<u>card@csw.ca</u>>
Subject: RE: Block 206 - Ground Floor Coord

Hi Brandon,

USF for 206 is the same as for 207, and sprinkler system is fully supervised as well.

What site stats do you need, only selected ones - best if you send me the list so that I calculate only those we need.

Regards,

Ivana Masnikosa BArch, OAA Architect

Kohn Partnership Architects Inc. 116 Spadina Avenue, Suite 501, Toronto, ON, Canada, M5V 2K6 Telephone +1 416-703-6700 Ext. 2031 imasnikosa@kohnarchitects.com

From: Brandon Chow <<u>BChow@dsel.ca</u>>
Sent: June 17, 2020 10:57 AM
To: Ivana Masnikosa <<u>imasnikosa@kohnarchitects.com</u>>
Cc: Cormac Murray <<u>cmurray@teeplearch.com</u>>; Sean Lawrence <<u>slawrence@kohnarchitects.com</u>>; tdiamant
<<u>tdiamant@teeplearch.com</u>>; Shannon Card <<u>card@csw.ca</u>>
Subject: RE: Block 206 - Ground Floor Coord

Hi Ivana,

Thanks for the Block 207 info. Can we get the site stats for Block 206 and for Block 207?

Can you also provide the following for Block 206.

- Building USF elevation
- Confirm the sprinkler system will be fully supervised (supervised system including water flow and control valve alarm service)

Brandon Chow Project Coordinator / Intermediate Designer

APPENDIX B

Water Supply

Windmill Zibi - Ontario Proposed Conditions (MSS)

Water Demand Design Flows per Unit Count City of Ottawa - Water Distribution Guidelines, July 2010



Phase	Block	Туре	Unit	Rate	No. of Units	Avg Day L/min	Max Day L/min	Peak Hour L/min
1	208	Office	75	L/p/d	287	15.0	22.4	40.4
1	208	Retail		L/m²/d	445	1.5	2.3	4.2
1	205.5A	Res	474.6	L/unit/d	71	23.4	58.5	128.7
1	205.5A	Retail		L/m²/d	1825	6.3	9.5	17.1
1	207	Office	75	L/p/d	385	20.1	30.1	54.2
1	207	Retail		L/m²/d	597	2.1	3.1	5.6
1	206	Res	474.6	L/unit/d	198	65.3	163.1	358.9
1	206	Office		L/p/d	395	20.6	30.8	55.5
1	206	Retail		L/m²/d	612	2.1	3.2	5.7
1	204A	Office	75	L/p/d	1049	54.6	136.6	300.5
1	204A	Retail	5	L/m ² /d	1626	5.6	8.5	15.2
2	211	Office	75	L/p/d	839	43.7	109.3	240.4
2	211	Retail		L/m²/d	1301	4.5	6.8	12.2
L	2	rtotai		L/III / G	1001	1.0	0.0	12.2
3	209	Office	75	L/p/d	965	50.3	75.4	135.7
3	209	Retail		L/m²/d	1496	5.2	13.0	28.6
3	210A&B	Office		L/p/d	495	25.8	38.7	69.6
3	210A&B	Retail		L/m²/d	767	2.7	4.0	7.2
	210/102	rtotai		<u>_</u> /u		2.1	1.0	7.2
4	205B	Res	474.6	L/unit/d	67	22.1	55.2	121.5
4	205B	Office		L/p/d	163	8.5	12.8	23.0
4	205B	Retail	5	L/m²/d	253	0.9	1.3	2.4
4	204B	Res	474.6	L/unit/d	115	37.9	94.8	208.5
4	204B	Retail		L/p/d	264	13.8	20.7	37.2
4	204B	Office	5	L/m²/d	410	1.4	2.1	3.8
5	201	Res	474.6	L/unit/d	170	56.0	140.1	308.2
5	201	Office		L/p/d	182	9.5	14.2	25.5
5	201	Retail	5	L/m²/d	281	1.0	1.5	2.6
5	202	Res		L/unit/d	90	29.7	74.2	163.1
5	202	Office		L/p/d	107	5.6	8.4	15.1
5	202	Retail	5	L/m²/d	166	0.6	0.9	1.6
5	203	Res		L/unit/d	180	59.3	148.3	326.3
5	203	Retail		L/p/d	306	16.0	23.9	43.1
5	203	Retail		L/m²/d	475	1.6	2.5	4.5
6	212	Office	75	l /p/d	1804	94.0	140.9	253.7
				L/p/d L/m²/d				
6	212	Retail	5	L/m /a	2796	9.7	14.6	26.2
7	213	Res	474.6	L/unit/d	200	65.9	164.8	362.5
7	213	Office		L/p/d	150	7.8	11.7	21.1
7	213	Retail	5	L/m²/d	233	0.8	1.2	2.2
8	214	Office	75	L/p/d	587	30.6	45.9	82.6
8	214	Retail	5	L/m ² /d	910	3.2	4.7	8.5
8	214	Office		L/p/d	587	30.6	4.7	82.6
8	215	Retail		L/m ² /d	910	3.2	7.9	17.4
		0.00	_				-	
EO	1	Office	75	L/p/d	12	0.6	0.9	1.7
					Total	858.9	1754.6	3624.5

Notes:

* Development stats per Windmill schedule dated 2016-02-01 and additional information received via email 2016-02-08.

* Office unit rate per Ontario Building Code 8.2.1.3.B.

* Residential Unit rate assuming 65% one bedroom (1.4p/unit), 30% two bedroom (2.1 p/unit), 5% three bedroom (3.0p/unit)

* Special Event area washrooms only per Windmill email 2016-02-08.

* Energy Ottawa maximum employees to work at Chaudiere Office provided by EO via letter dated March 1, 2016

Estimated Total Residential Population

Max Day PF Peak Hour PF 1844 2.5 5.5

Windmill Zibi - Ontario Block 206

Water Demand Design Flows per Unit Count City of Ottawa - Water Distribution Guidelines, July 2010



Phase	Block	Туре	Unit	Rate	No. of Units	Avg Day L/min	Max Day L/min	Peak Hour L/min
1	208	Office	75	L/9.3m ² /d	975	5.46	8.19	14.75
1	208	Retail	2.5	L/m²/d	736	1.28	1.92	3.45
1	208	Restaurant	125	L/seat/d	8	0.69	1.04	1.88
1	205A	Res	474.6	L/unit/d	71	23.40	114.66	173.16
1	205A	Retail		L/m²/d	754	1.31	1.96	3.53
3	207	Office	75	L/9.3m ² /d	6451	36.13	54.19	97.55
3	207	Retail	2.5	L/m²/d	575	1.00	1.50	2.70
3	207	Restaurant	125	L/seat/d	150	13.02	19.53	35.16
4	206	Res	280.0	L/unit/d	447	86.92	217.29	478.04
4	206	Retail	2.5	L/m²/d	799	1.39	2.08	3.75
2	211	Office	75	L/9.3m ² /d	14480	81.09	121.64	218.95
2	211	Retail	2.5	L/m²/d	1082	1.88	2.82	5.07
1	EO	Office	75	L/p/d	12	0.63	0.94	1.69
					Total	254.20	547.76	1039.68

Notes:

* Development stats per Windmill schedule dated 2016-02-01 and additional information received via email 2016-02-08.

* Office unit rate per Ontario Building Code 8.2.1.3.B. Assuming 1 employee per 9.3m² of floor space.

* Residential Unit rate assuming 65% one bedroom (1.4p/unit), 30% two bedroom (2.1 p/unit), 5% three bedroom (3.0p/unit)

* Residential Unit rate for Block 206 as per Water Supply Guidelines, unit count per email correspondence dated 2020-06-22.

* Number of Residential units estimated as 850gfa / unit per Windmill development stats dated 2016-02-01.

* Windmill estimated maximum number of employees occupying Albert Island

* Energy Ottawa maximum employees to work at Chaudiere Office provided by EO via letter dated March 1, 2016

	Max	<pre>CODE CODE CODE CODE CODE CODE CODE CODE</pre>
Estimated Total Residential Population	128	4.9
Estimated Total Residential Population Block 206	447	4.9

25000.0 L/min rounded to the nearest 1,000 L/min

Fire Flow Estimation per Fire Un Water Supply For Public Fire Protection - 199		, DSEL
Fire Flow Required		
1. Base Requirement		
$F = 220C\sqrt{A}$	L/min	Where F is the fire flow, C is the Type of construction and A is the Total floor area
Type of Construction:	Non-Combusti	ble Construction
	C 0.8A 20554.0	Type of Construction Coefficient per FUS Part II, Section 1 m ² Total floor area based on FUS Part II section 1
Fire Flow	25232.5	L/min

Adjustments

2. Reduction for Occupancy Type

	Non-Combustible	-25%	%				
	Fire Flow	18750.	0 L/min	-			
3. Re	eduction for Sprinkler Protection	n					
	Sprinklered - Supervised	-50%	%				
* Residential l	Unit rate for Block 206 as per Wat			t per e	email corres	pondence	dated 2020-06-22.
	Reduction	-937	5 L/min				
4. Inc	crease for Separation Distance						
	Cons. of Exposed Wall	S.D	Lw	На	LH	EC	
N	Non-Combustible	20.1m-30m	46		2	92	10%
S	Non-Combustible	10.1m-20m	35		6	210	15%
E	Non-Combustible	3.1m-10m	43		6	258	20%
w	Non-Combustible	10.1m-20m	48		16	768	15%
		% Increase					60% value not to exceed 75%
	Increase	11250.	0 L/min	-			
	Lw = Length of the Exposed Wa	11					
	$H_0 = pumber of storoup of the or$						

Ha = number of storeys of the adjacent structure

LH = Length-height factor of exposed wall. Value rounded up.

EC = Exposure Charge

Total Fire Flow

Fire Flow 20625.0 L/min fire flow not to exceed 45,000 L/min nor be less than 2,000 L/min per FUS Section **21000.0 L/min** rounded to the nearest 1,000 L/min

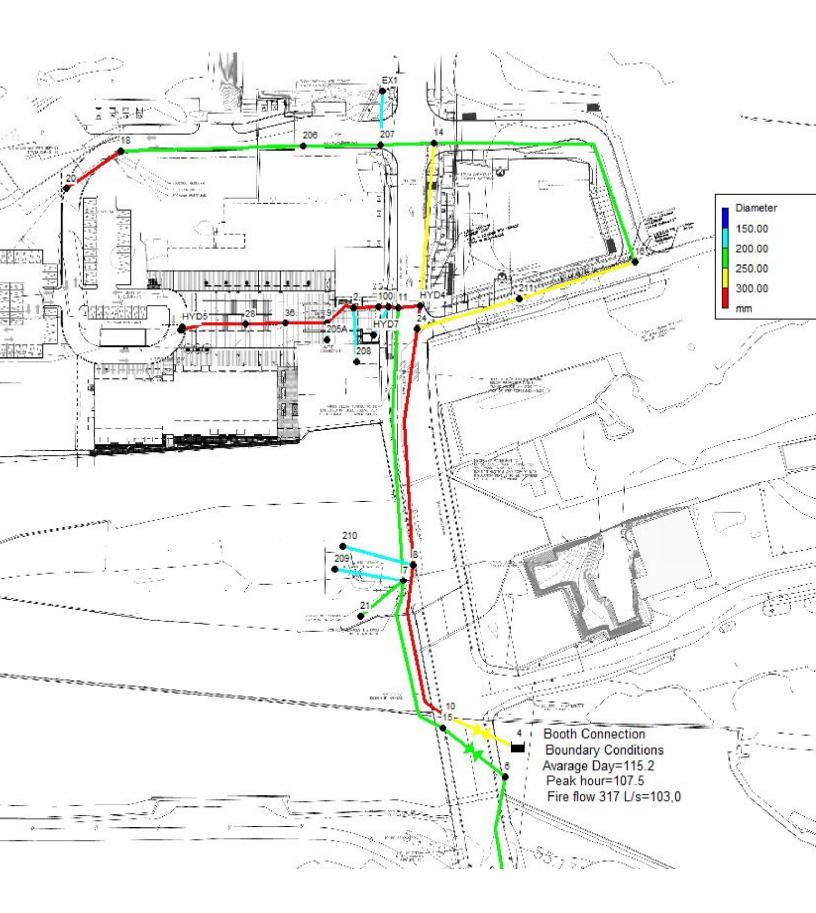
Notes:

-Type of construction, Occupancy Type and Sprinkler Protection information provided by KPMB Architects

-Calculations based on Fire Underwriters Survey - Part II

- Number of stories for Block 213 estimated based on Master Plan





	AVERAGE	DAY
Page 1	2020-07-1	5 6:59:45 AM
*********	***************************************	******
*	EPANET	*
*	Hydraulic and Water Quality	*
*	Analysis for Pipe Networks	*
*	Version 2.0	*
******	***************************************	*****

Input File: 2020-07-14_1178_ggg_AVG.net

Link - Node Table:

Link	Start	End	-	Diameter
ID	Node	Node	m	mm
1	5	6	270	200
2	15	7	130	200
3	10	8	130	300
4	7	209	15	150
5	7	11	190	200
6	8	24	98	300
7	HYD4	11	17	300
8	11	3	17	300
9	HYD7	3	3	150
10	100	3	39	300
11	HYD4	14	76	250
13	14	207	48.45	200
14	207	EX1	8.57	150
18	20	18	24.2	300
19	21	7	1.5	200
20	8	210	1.5	150
21	207	HYD6	21.15	200
22	211	24	8.9	250
23	24	HYD4	4.2	300
26	205B	30	1.9	300
27	30	HYD5	0.65	150
28	30	28	27.55	300
29	28	36	16.4	300
31	36	9	17.8	300
32	9	2	42.7	300
33	2	100	9.5	300
39	9	205A	15	150
40	2	208	15	150
17	211	16	75	250
24	14	16	108	200
12	206	18	40.27	200
25	HYD6	206	2	200
15	4	10	#N/A	250 Valve
16	6	15	#N/A	200 Valve

Noue	RESULLS	

Node Results	:			
Node ID	Demand LPM	Head m	Pressure m	Quality
 HYD7	0.00	114.57	60.42	0.00
3	0.00	114.57	60.47	0.00
6	0.00	115.19	61.29	0.00
7	0.00	114.57	60.57	0.00
8	0.00	114.57	60.57	0.00
209	0.00	114.57	60.27	0.00
11	0.00	114.57	61.17	0.00
HYD4	0.00	114.57	61.17	0.00

				AVERAGE DAY
100	0.00	114.57	60.22	0.00
14	0.00	114.56	63.25	0.00
207	50.15	114.56	61.17	0.00
EX1	0.60	114.56	63.16	0.00
18	0.00	114.56	60.41	0.00
20	0.00	114.56	60.19	0.00
21	0.00	114.57	60.57	0.00
210	0.00	114.57	60.27	0.00
211	82.97	114.57	61.38	0.00
24	0.00	114.57	61.17	0.00
28	0.00	114.57	59.81	0.00
205B	0.00	114.57	60.53	0.00
30	0.00	114.57	60.53	0.00
HYD5	0.00	114.57	60.20	0.00
9	0.00	114.57	60.42	0.00
2	0.00	114.57	60.22	0.00
36	0.00	114.57	59.99	0.00
205A	24.70	114.57	60.23	0.00
208	7.40	114.57	60.73	0.00
10	0.00	114.57	60.57	0.00
15	0.00	114.57	60.30	0.00
16	0.00	114.57	63.57	0.00
206	88.31	114.56	61.71	0.00
HYD6	0.00	114.56	61.71	0.00
4	-170.53	115.20	0.00	0.00 Reservoir
5	-83.60	115.20	0.00	0.00 Reservoir

Link Results:

Link	Flow	VelocityUnit	Hoodlocc	Status
ID	LPM	m/s	m/km	Status
1	83.60	0.04	0.03	Open
2	83.60	0.04	0.03	Open
3	170.53	0.04	0.01	Open
4	0.00	0.00	0.00	Open
5	83.60	0.04	0.02	Open
6	170.53	0.04	0.01	Open
7	-51.50	0.01	0.00	Open

Link	Flow	VelocityUnit	Hoodloss	Status
ID	LPM	m/s	m/km	Status
 3	32.10	0.01	0.00	Open
Ð	0.00	0.00	0.00	Open
10	-32.10	0.01	0.00	Open
11	104.40	0.04	0.01	0pen
13	139.06	0.07	0.07	0pen
14	0.60	0.00	0.00	0pen
18	0.00	0.00	0.00	0pen
19	0.00	0.00	0.00	0pen
20	0.00	0.00	0.00	0pen
21	88.31	0.05	0.04	0pen
22	-117.63	0.04	0.03	0pen
23	52.91	0.01	0.00	0pen
26	0.00	0.00	0.00	0pen
27	0.00	0.00	0.00	0pen
28	0.00	0.00	0.00	Open
29	-0.01	0.00	0.00	Open
31	-0.01	0.00	0.00	Open
32	-24.70	0.01	0.00	Open
33	-32.10	0.01	0.00	Open
39	24.70	0.02	0.02	Open
40	7.40	0.01	0.00	Open

				AVERAGE DAY
17	34.66	0.01	0.00	Open
24	-34.66	0.02	0.01	Open
12	0.00	0.00	0.00	Open
25	88.31	0.05	0.07	0pen
15	170.53	0.06	0.63	Open Valve
16	83.60	0.04	0.62	Open Valve

	MAX DAY + FIRE FLOW	
Page 1	2020-07-15 7:03:37	7 AM
******	*******	****
*	EPANET	*
*	Hydraulic and Water Quality	*
*	Analysis for Pipe Networks	*
*	Version 2.0	*
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Input File: 2020-07-09_1178_ggg_ff.net

Link - Node Table:

Link	Start	End		Diameter
ID	Node	Node	m	mm
1	5	6	270	200
2	15	7	130	200
3	10	8	130	300
4	7	209	15	150
5	7	11	190	200
6	8	24	98	300
7	HYD4	11	17	300
8	11	HYD7	17	300
9	hyd	HYD7	3	150
10	100	HYD7	39	300
11	HYD4	14	76	250
13	14	207	48.45	200
14	207	EX1	8.57	150
18	20	18	24.2	300
19	21	7	1.5	200
20	8	210	1.5	150
21	207	HYD6	21.15	200
22	211	24	8.9	250
23	24	HYD4	4.2	300
26	205B	30	1.9	300
27	30	HYD5	0.65	150
28	30	28	27.55	300
29	28	36	16.4	300
31	36	9	17.8	300
32	9	2	42.7	300
33	2	100	9.5	300
39	9	205A	15	150
40	2	208	15	150
17	211	16	75	250
24	14	16	108	200
12	206	18	40.27	200
25	HYD6	206	2	200
15	4	10	#N/A	250 Valve
16	6	15	#N/A	200 Valve

Node	Results	•

Page 2 Node Results:				
 Node	Demand	 Head	Pressure	Quality
ID	LPM	m	m	
 hyd	0.00	 76.43	22.28	0.00
HYD7	5678.00	76.43	22.33	0.00
6	0.00	94.14	40.24	0.00
7	0.00	84.99	30.99	0.00
8	0.00	84.00	30.00	0.00
209	0.00	84.99	30.69	0.00
11	0.00	77.52	24.12	0.00
HYD4	3966.00	77,94	24.54	0.00

			MAX	DAY + FIRE FLOW
100	0.00	76.10	21.75	0.00
14	0.00	77.07	25.76	0.00
207	75.22	73.11	19.72	0.00
EX1	0.90	73.11	21.71	0.00
18	0.00	70.72	16.57	0.00
20	0.00	70.72	16.35	0.00
21	0.00	84.99	30.99	0.00
210	0.00	84.00	29.70	0.00
211	124.46	78.41	25.22	0.00
24	0.00	78.48	25.08	0.00
28	0.00	75.20	20.44	0.00
205B	0.00	74.94	20.90	0.00
30	0.00	74.94	20.90	0.00
HYD5	5678.00	68.91	14.54	0.00
9	0.00	75.53	21.38	0.00
2	0.00	75.95	21.60	0.00
36	0.00	75.37	20.79	0.00
205A	116.60	75.52	21.18	0.00
208	11.20	75.95	22.11	0.00
10	0.00	95.09	41.09	0.00
15	0.00	91.50	37.23	0.00
16	0.00	78.19	27.19	0.00
206	219.37	70.72	17.87	0.00
HYD6	5678.00	70.72	18.14	0.00
4	-17001.89	103.00	0.00	0.00 Reservoir
5	-4545.87	107.00	0.00	0.00 Reservoir

Link Results:

Link	Flow	VelocityUnit	Headloss	Status
ID	LPM	m/s	m/km	
1	4545.87	2.41	47.62	Open
2	4545.87	2.41	50.05	Open
3	17001.89	4.01	85.30	Open
4	0.00	0.00	0.00	Open
5	4545.87	2.41	39.30	Open
6	17001.88	4.01	56.31	Open
7	6937.93	1.64	24.19	Open

Link			nit Headloss	Status	
ID	LPM	m/s	m/km		
 3	11483.80	2.71	64.35	Open	
Ð	0.00	0.00	0.00	0pen	
10	-5805.80	1.37	8.48	0pen	
11	4027.60	1.37	11.43	0pen	
13	5973.49	3.17	81.60	0pen	
14	0.90	0.00	0.00	0pen	
18	0.00	0.00	0.00	0pen	
19	0.00	0.00	0.00	0pen	
20	0.00	0.00	0.00	0pen	
21	5897.37	3.13	112.99	Open	
22	-2070.35	0.70	8.06	Open	
23	14931.54	3.52	130.53	Open	
26	0.00	0.00	0.00	Open	
27	5678.00	5.36	9265.69	Open	
28	-5678.00	1.34	9.71	Open	
29	-5678.00	1.34	10.07	Open	
31	-5678.00	1.34	8.78	Open	
32	-5794.60	1.37	9.88	Open	
33	-5805.80	1.37	16.06	Open	
39	116.60	0.11	0.29	Open	
40	11.20	0.01	0.00	Open	

AY + FIRE FLOW
0pen
0pen
0pen
Open
Open Valve
Open Valve

	PEAK HC	UR
Page 1	2020-07-1	5 7:04:51 AM
**********	***************	******
*	EPANET	*
*	Hydraulic and Water Quality	*
*	Analysis for Pipe Networks	*
*	Version 2.0	*
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Input File: 2020-07-14_1178_ggg_PEAK.net

Link - Node Table:

ID Node 1 5 2 15 3 10 4 7	Node 6 7 8 209 11	m 270 130 130 15	mm 200 200 300
2 15 3 10	7 8 209 11	130 130	200
3 10	8 209 11	130	
	209 11		300
4 7	11	15	
		15	150
5 7		190	200
6 8	24	98	300
7 HYD4	11	17	300
8 11	3	17	300
9 HYD7	3	3	150
10 100	3	39	300
11 HYD4	14	76	250
13 14	207	48.45	200
14 207	EX1	8.57	150
18 20	18	24.2	300
19 21	7	1.5	200
20 8	210	1.5	150
21 207	HYD6	21.15	200
22 211	24	8.9	250
23 24	HYD4	4.2	300
26 205B	30	1.9	300
27 30	HYD5	0.65	150
28 30	28	27.55	300
29 28	36	16.4	300
31 36	9	17.8	300
32 9	2	42.7	300
33 2	100	9.5	300
39 9	205A	15	150
40 2	208	15	150
17 211	16	75	250
24 14	16	108	200
12 206	18	40.27	200
25 HYD6	206	2	200
15 4	10	#N/A	250 Valve
16 6	15	#N/A	200 Valve

Noue	Results

Node Results	:			
Node ID	Demand LPM	Head m	Pressure m	Quality
 HYD7	0.00	105.97	51.82	0.00
3	0.00	105.97	51.87	0.00
6	0.00	107.45	53.55	0.00
7	0.00	106.00	52.00	0.00
8	0.00	105.99	51.99	0.00
209	0.00	106.00	51.70	0.00
11	0.00	105.97	52.57	0.00
HYD4	0.00	105.97	52.57	0.00

				PEAK HOUR
100	0.00	105.97	51.62	0.00
14	0.00	105.95	54.64	0.00
207	135.41	105.90	52.51	0.00
EX1	1.70	105.90	54.50	0.00
18	0.00	105.87	51.72	0.00
20	0.00	105.87	51.50	0.00
21	0.00	106.00	52.00	0.00
210	0.00	105.99	51.69	0.00
211	224.02	105.97	52.78	0.00
24	0.00	105.97	52.57	0.00
28	0.00	105.97	51.21	0.00
205B	0.00	105.97	51.93	0.00
30	0.00	105.97	51.93	0.00
HYD5	0.00	105.97	51.60	0.00
9	0.00	105.97	51.82	0.00
2	0.00	105.97	51.62	0.00
36	0.00	105.97	51.39	0.00
205A	176.70	105.96	51.62	0.00
208	20.10	105.97	52.13	0.00
10	0.00	106.02	52.02	0.00
15	0.00	106.03	51.76	0.00
16	0.00	105.96	54.96	0.00
206	481.79	105.87	53.02	0.00
HYD6	0.00	105.88	53.03	0.00
4	-792.69	107.50	0.00	0.00 Reservoir
5	-247.04	107.50	0.00	0.00 Reservoir

Link Results:

Link ID	Flow LPM	VelocityUnit m/s	t Headloss m/km	Status
1	247.04	0.13	0.20	Open
2	247.04	0.13	0.21	Open
3	792.69	0.19	0.25	Open
4	0.00	0.00	0.00	Open
5	247.03	0.13	0.18	Open
6	792.69	0.19	0.19	Open
7	-50.23	0.01	0.00	Open

Link	Flow	VelocityUni	+ Hoodloss	Status	
ID	LPM	m/s		Status	
 8	196.80	0.05	0.02	Open	
9	0.00	0.00	0.00	Open	
10	-196.80	0.05	0.02	Open	
11	455.79	0.15	0.20	Open	
13	618.90	0.33	1.14	Open	
14	1.70	0.00	0.00	Open	
18	0.00	0.00	0.00	Open	
19	0.00	0.00	0.00	Open	
20	0.00	0.00	0.00	Open	
21	481.79	0.26	0.94	Open	
22	-387.14	0.13	0.31	Open	
23	405.56	0.10	0.12	Open	
26	0.00	0.00	0.00	Open	
27	0.00	0.00	0.00	Open	
28	0.00	0.00	0.00	Open	
29	0.00	0.00	0.00	Open	
31	0.00	0.00	0.00	Open	
32	-176.70	0.04	0.01	Open	
33	-196.80	0.05	0.02	Open	
39	176.70	0.17	0.63	Open	
40	20.10	0.02	0.01	Open	

				PEAK HOUR
17	163.12	0.06	0.03	Open
24	-163.12	0.09	0.10	Open
12	0.00	0.00	0.00	Open
25	481.79	0.26	1.93	Open
15	792.69	0.27	1.48	Open Valve
16	247.04	0.13	1.42	Open Valve

APPENDIX C

Wastewater Collection

ΗΔΤCΗ

3 Design of the Pumping Station

3.1 Sizing of the Wet Well

The existing wet well is proposed to be used for temporary pumping. The flow of the pumping station (13 L/s) will be accommodated by 1 duty and 1 standby pump, each of which will be able to handle the nominal inflow individually. For conceptual design purposes, a flow rate of 13 L/s was taken. The wet well capacity required to achieve a given pump cycle time can be calculated as follows:

$$V = \frac{T_c \cdot Q}{4}$$

Where:

V = Wet well volume in L;

 T_c = Pump Cycle Time in seconds;

Q = Pump discharge rate in L/s.

For a pump cycle time of 5 minutes (i.e. a combined 12 starts per hour) the wet well volume can be calculated as:

$$V = \frac{T_c \cdot Q}{4} = \frac{300s \cdot 13 \, L/s}{4} = 975L$$

Based on a 2.4 m diameter round wet well, and an allowance for equipment in the wet well, a live volume depth of 0.23 m is required. Hatch has, in the design allowed for a live wet well depth of 0.5 m, this will provide for less start stop cycles, and provide for somewhat better running times.

It is noted that Hatch has used a reduced cycle time from what Hatch usually uses since this is a temporary pumping station and pump rotation for longevity is not as much of an issue as in permanent pumping stations. For these small flow rates, pumps often have up to 30 allowable starts and stops per hour per pump. As such, the live wet well volume required could be considered conservative. As such the existing wet well is sufficient to have adequate pump cycle times to avoid overloading the pump motors.

3.2 Emergency Storage

DSEL has confirmed the overflow elevation / lowest level at which an overflow occurs at 50.5 m, refer to an email exchange between Hatch and the building consultant for the project, attached in Appendix 4.

The MOECP requires a minimum of 30 minutes of emergency storage for similar pumping stations. Hatch has provided for 30 minutes of storage, based on an overflow invert elevation of 50.0 m in the design of the system. The storage is a combination of the volumes available in MH's 100, 101 as well as 102, along with the pumping station itself. It requires one MH (100) to be upsized to 1800 mm to ensure adequate storage. The storage volume attainable is ~ 24,080 L, or approximately 31 minutes. Full calculations are attached to this report.

3.3 Sizing and Pressure Class of the Forcemain, and System Curve

The PPS is to pump an updated peak sanitary flow = 32.7 L/s. This flow is to be conveyed through twin forcemains. The TPS is to pump a peak WWF of 13 L/s, using the same forcemains. At present, the timeframe for which the temporary PS is to be used, is uncertain.

ΗΔΤCΗ

The MOECP Design Guidelines generally call for a design velocity of > 0.6 m/s for forcemains, with a range of 0.6 m/s to 1.1 m/s as minimum for self-cleansing. The velocity of sewage in the forcemain during normal operation should be in the range of 0.9 m/s to 1.5 m/s, as recommended in section 7.2.5.2 of the "Ottawa Sewer Design Guidelines". The forcemain should have a minimum nominal diameter of 100 mm, as specified in section 7.2.5.1 of the "Ottawa Sewer Design Guidelines".

In principle Hatch prefers to have velocities at the higher end of this spectrum and we often aim to achieve velocities at around 1.25 m/s and, in case of large forcemain diameters, even higher (at \sim 1.5 m/s). In part, this is as a result of larger forcemains being more susceptible to sedimentation issues (and more difficult re-suspending of sediment). However, especially on smaller forcemains (up to \sim 400 mm), maintaining higher velocities can become limiting from a friction perspective. As such, we prefer to have the overall forcemain velocity (in this case) at around 1.25 m/s, more so since there will be a not insignificant number of low points along the main, with an acceptable velocity range of \sim 1.0 m/s to 1.5 m/s at nominal flow.

For a flow of 32.7 L/s this would require a theoretical forcemain diameter range of \sim 166 mm to 204 mm (all ID) with an ideal diameter of 182 mm (ID). The forcemain design was based on PVC 200 mm SDR 26 – ID 201.2 mm.

For the interim PS, this would mean a nominal velocity of 0.41 m/s, which is below the requirements of the MOECP design guidelines, based on a firm flow rate of 13 L/s. While forcemains can operate at that velocity for quite some time, there should be some pre-cautions in the design of these to minimize the potential long term issues, which include:

- Minimizing low / high points along the forcemain route;
- Allowance for swabbing at the PS, and temporary swab catcher at the discharge manhole;

• There may be issues with residence times in the forcemain, at the given length. This could (depending on the discharge location and other flows in the downstream sewer) result in H₂S corrosion downstream of the discharge location.

The static head of this pumping station will range between 13.8 m and 14.3 m during normal operation, based on wet well volume as defined in Section 3.1 above and the forcemain discharge elevation of 60.83 m (pipe obvert). The following friction losses have been calculated for the forcemain, in accordance with City of Ottawa and MOE requirements, for a nominal flow of 13.0 L/s:

- Hazen Williams C (HW-C) = 110: 1.4 m;
- HW-C = 120: 1.2 m;
- HW-C = 130: 1.0 m.

A system curve has been calculated from 0 L/s to 30.0 L/s using the HW-C factors above for the 200 mm forcemain. Minor losses were estimated by allowing for a 'k' value of 15 for fittings and pipework inside the pumping station. This 'k' value results in an additional dynamic head of 0.13 m at a flow rate of 13.0L/s. A graph of the system curve is attached. (Appendix 1: Figure 1). The following lines have been plotted:

- Maximum static head, and friction losses based on a HW-C of 110, along with minor losses;
- Intermediate static head, and friction losses based on a HW-C of 120, along with minor losses;
- Minimum static head, and friction losses based on a HW-C of 130, along with minor losses.

Wastewater Design Flows per Unit Count City of Ottawa Sewer Design Guidelines, 2012



Peak Flow 0.4

Extraneous Flow Allowances

Site Area 1.234 ha

Phase	Block	Туре	Unit	Rate	No. of Units	Average Flow (L/s)	Peaking Factor (-)	Peak Flow (L/s)
1	208	Office	75	L/p/d	105	0.1	1.5	0.1
1	208	Retail	5	L/m²/d	736	0.1	1.5	0.1
1	205A	Res	474.6	L/unit/d	71	0.4	3.6	1.4
1	205A	Retail	5	L/m²/d	754	0.1	1.5	0.1
2	207	Office	75	L/p/d	544	0.5	1.5	0.7
2	207	Retail	5	L/m²/d	644	0.1	1.5	0.1
2	207	Restaurant	125	L/seat/d	300	0.4	1.5	0.7
3	211	Office	75	L/9.3m ² /d	14480	1.4	2.5	3.4
3	211	Retail	2.5	L/m²/d	1082	0.0	3.5	0.1
1	EX1	Office	75	L/p/d	12	0.01	1.50	0.02
	1				Total	3.0	1	6.8
			Total W	letweather	Flow Estimate			7.2

Notes:

* Development stats per Windmill schedule dated 2016-02-01 and additional information received via email 2016-02-08.

P.F.

* Office unit rate per Ontario Building Code 8.2.1.3.B. assuming 9.3m²/p

* Residential Unit rate assuming 70% one bedroom (1.4p/unit), 30% two bedroom (2.1 p/unit)

* Retail unit rate per City of Ottawa sewer design guidelines and assumes a 12 hour commercial operation

Estimated Total Residential Population 128 3.6

Wastewater Design Flows per Unit Count City of Ottawa Sewer Design Guidelines, 2012



Peak Flow

Extraneous Flow Allowances 0.7

Site Area

2 **ha**

Phase	Block	Туре	Unit	Rate	No. of Units	Average Flow	Peaking Factor	Peak Flow
						(L/s)	(-)	(L/s)
1	208	Office	75	L/9.3m ² /d	2,527	0.2	1.5	0.4
1	205A	Res	280	L/p/d	127	0.4	3.4	1.4
1	205A	Retail	2.8	L/m²/d	750	0.0	1.5	0.0
2	211	Office	75	L/9.3m ² /d	14,480	1.4	1.5	2.0
2	211	Retail	2.8	L/m²/d	1,082	0.0	1.5	0.1
3	207	Office	75	L/9.3m ² /d	6,451	0.6	1.5	0.9
3	207	Retail	2.8	L/m²/d	575	0.0	1.5	0.0
3	207	Restaurant	125	L/seat/d	150	0.2	1.5	0.3
4	206	Res	280	L/p/d	447	1.4	3.4	4.9
4	206	Retail	2.8	L/m²/d	799	0.0	1.5	0.0
1	EO	Office	75	L/p/d	10	0.01	1.50	0.01
1	ZIBI	Office	75	L/p/d	20	0.02	1.50	0.03
					Total	4.4		10.0
			Total W	letweather	Flow Estimate			10.7

* Energy Ottawa office - 10 p per Energy Ottawa email dated July 21, 2017.

Development Statistic Summary: Block 208

	Office	2527				
Block 205A						
	Retail	750				
	Residential		p/unit	р		
	1 Bedroom	33 units		1.4		46
	2 Bedroom	37 units		2.1		78
	3 Bedroom	1 units		3.1		3
Block 211: 2	2020-02-05 REV 4, K		rchitect			
	Retail	1082 m ²				
	Office	14480 m ²				
Block 207						
	Office	6451 m ²				
	Retail	575 m ²				
	Restaurant	582 m ²				
Block 206						
	Standard Units		p/unit	р		
	1 Bedroom	95 units		1.4		133
	2 Bedroom	64 units		2.1		134
	Cohabitation Units					
		180 beds		1		180
					P.F.	
	Estimated Total Re	esidential Populatio	n	574	3.4	
	Retail	799 m ²				

SANITARY SEWER CALCULATION SHEET

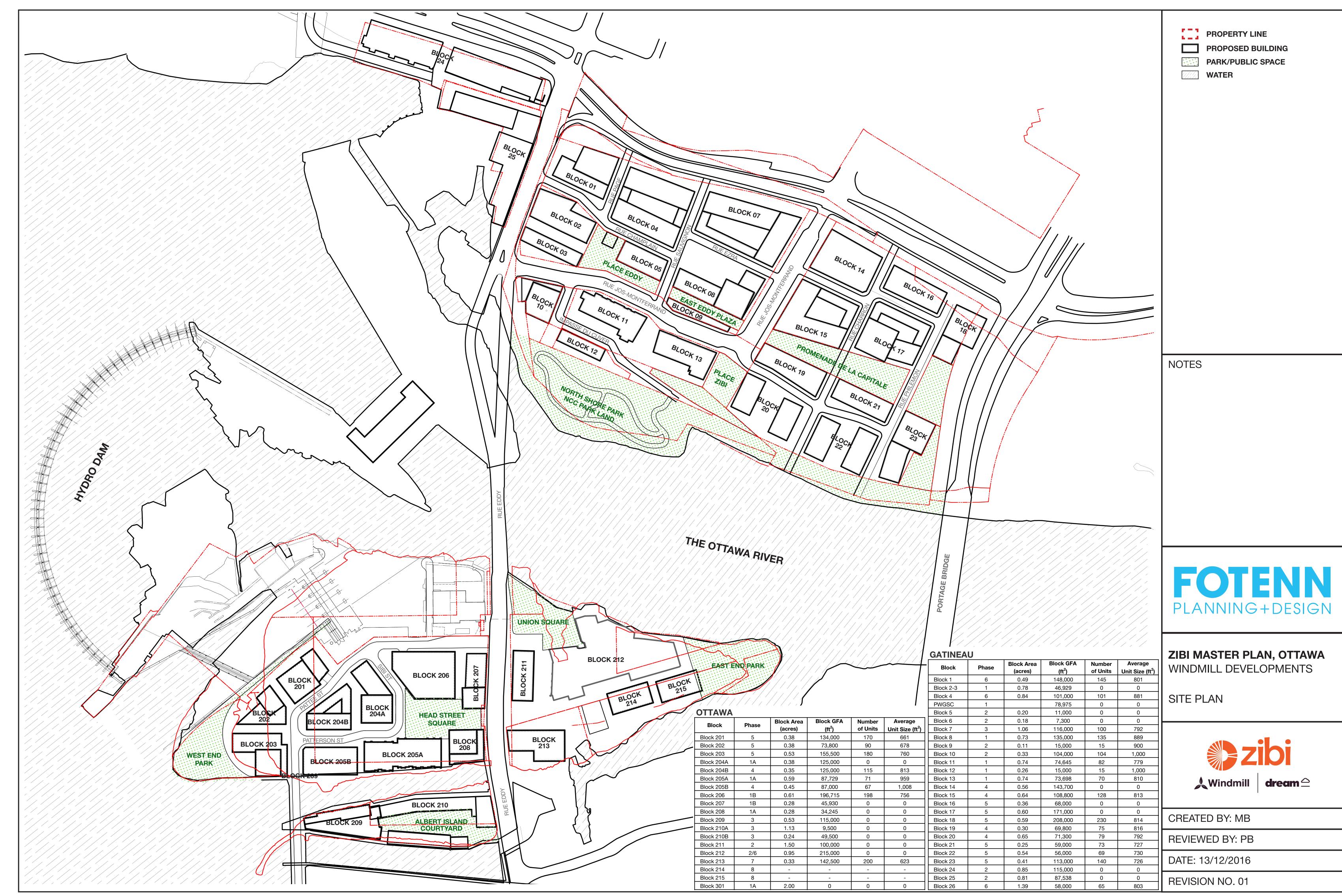
SANITARY SEWER	CALCULA	TION SH	IEET																	6	Ha	M	
Manning's n=0.013	7.01			AREA AND PO			1		сомм	INSTIT	PARK	C+I+I		INFILTRATIO		1	-			PIPE	<i>un</i>	VM	
STREET	FROM M.H.	TO M.H.	AREA (ha)	UNITS POP.		POP.	PEAK FACT.	FLOW	REA ACCU AREA ha) (ha)	AREA ACC ARE (ha) (ha	U. AREA ACCI	J. PEAK A FLOW*	TOTAL AREA (ha)		INFILT. FLOW (I/s)	TOTAL FLOW (I/s)	DIST (m)	DIA (mm)	SLOPE (%)	CAP. (FULL) (I/s)	RATIO Q act/Q cap	-	(ACT.) (m/s)
Chaudiere West																							
Block 208			3.00		3.00				0.00	0.0	0.0	0.8	3.00	3.00	0.99	1.79							
Block 205a				121		121	3.6	1.40	0.00				0.00			1.70							
Block 207								1.00	0.00				0.00			1.10							
Block 206 Block 204a				447		447	3.4	4.92	0.00				0.00			6.02 3.00							
Block 205b				114		114	3.6	1.32	0.00	0.0			0.00			1.72							
Block 204b				196		196	3.5	2.24	0.00				0.00			3.04							
Block 201				289		289	3.5	3.25	0.00				0.00			3.75							
Block 202				153		153	3.6	1.76	0.00				0.00			2.06							-
Block 203 Block 209			-	306		306	3.5	3.43	0.00				0.00			4.33 2.80			-	+		-	-
Block 209			-				1		0.00				0.00			1.40	+	1	1	-		-	1
Total to Zaida Eddy Private					3.00	1626			0.00	0.0	0.0	13.4	3.00										
Zaida Eddy Private																							
	102	101			3.00	1626	3.1		0.00				0.00		0.99	30.85	18.3	250	0.38	36.66	0.84	0.75	0.84
Block 213		100	0.28	340	3.28	1966	3.1	19.58	0.00			0.4	0.28	3.28				050	0.00	10.00			4.05
Block 211	101	100 401A	0.47		3.75 3.75	1966 1966	3.1 3.1	19.58 19.58	0.00				0.47		1.24	38.32 38.32	14.8 75.9	250 300	0.60	46.06	0.83	0.94	1.05
Block 212	100	401A	0.55		4.30	1966	3.1	19.56	0.00				0.00		1.24	30.32	75.9	300	0.23	40.30	0.63	0.00	0.73
Block 214			0.00		4.30	1966			0.00				0.00			0.00							
Block 215					4.30	1966			0.00	0.0	0.0) 1.7	0.00	4.30		0.00							
	401A	402A			4.30	1966	3.1	19.58	0.00				0.00		1.42	47.10	61.5	300	0.44	64.14	0.73	0.91	0.99
	402A	SAN PS			4.30	1966	3.1	19.58	0.00	0.0	0.0	26.1	0.00	4.30	1.42	47.10	5.8	300	0.35	57.21	0.82	0.81	0.90
* Constant Inflow used for Office/Reta	ail/Restaurant Space	, refer to Sanita	ary Design Sh	neet prepared for th	he Master Se	rvicing Stud	y (DSEL	Project# 14-71	7) dated Jun	2018													
					+					+ $-$													
					+		-													-		-	+
														_									
				PARAMETERS	1 1		1	II	I	Desi	gned:	1		PROJEC	T:	1	1	1	1	1	1	1	1
Park Flow = Average Daily Flow = Comm/Inst Flow = Industrial Flow =	9300 280 28000 35000	L/ha/da l/p/day L/ha/da L/ha/da	0.10764 0.3241 0.40509	l/s/Ha	Extraneous Minimum V	elocity =		0.330 L/s 0.600 m/s	5	Chec	ked:			LOCATIO	DN:				City of	Ottawa			
Max Res. Peak Factor = Commercial/Inst./Park Peak Factor = Institutional =	4.00 1.50 0.32	l/s/Ha			Manning's Townhouse Single hou	e coeff=	(Conc)	0.013 (Pv 2.7 3.4	c) 0.01	Dwg	. Reference: ary Drainage Plan, Dwg	s. No.		File Ref:				Date:	7/13/2020			Sheet No). <u>1</u> f 1

APPENDIX D

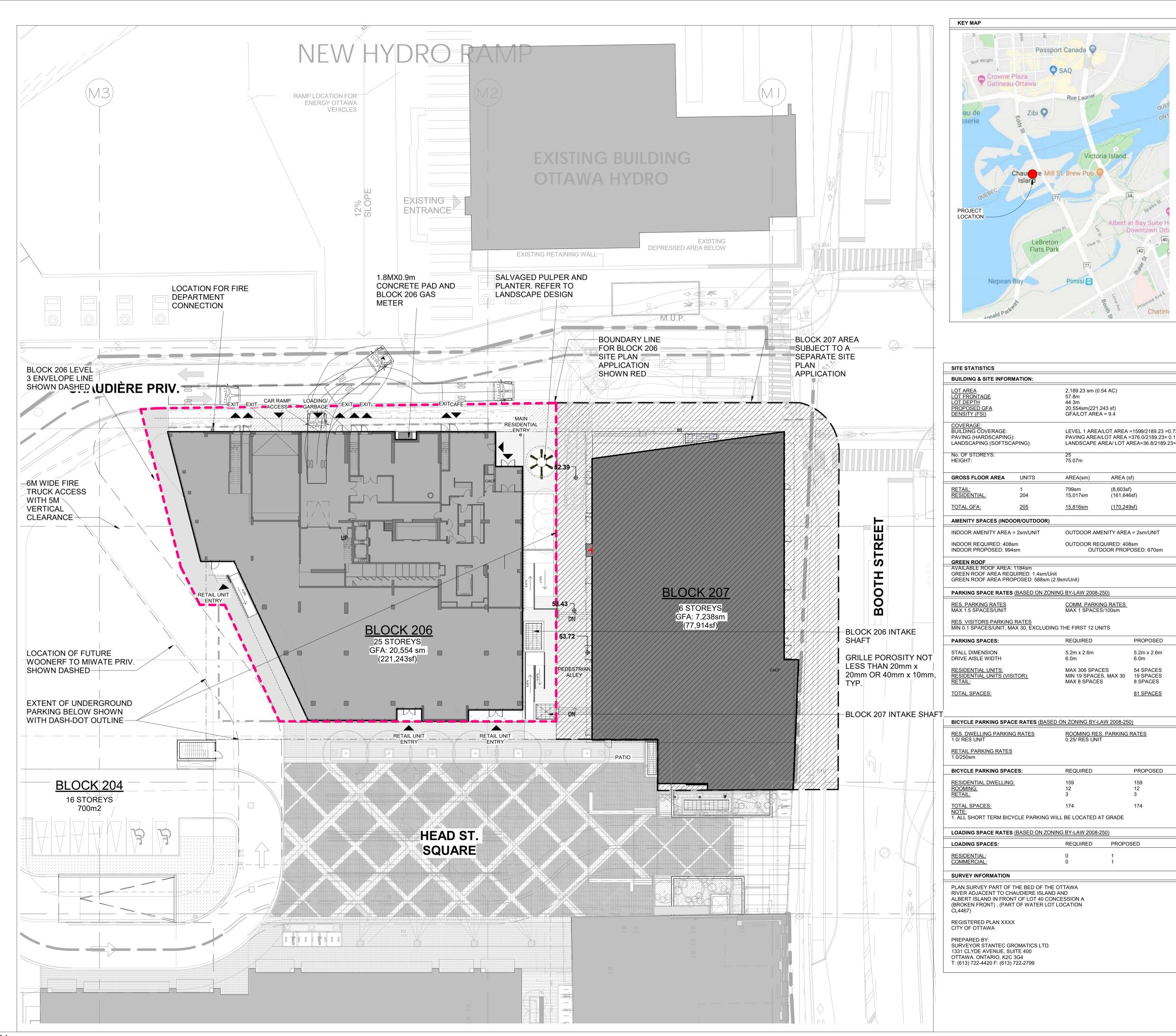
Stormwater Management

													S	ewer Data				
Area ID	Up	Down	Area	С	Indiv AxC	Acc AxC	Тc	Ι	Q	DIA	Slope	Length	A _{hydraulic}	R	Velocity	Qcap	Time Flow 0	Q / Q full
			(ha)	(-)			(min)	(mm/hr)	(L/s)	(mm)	(%)	(m)	(m ²)	(m)	(m/s)	(L/s)	(min)	(-)
FUT	STM106	STM105	0.153	0.90	0.14	0.14	10.0	104.2	39.9	450	1.00	21.6	0.159	0.113	1.79	285.1	0.2	0.14
	STM105	STM104	0.000	0.85	0.00	0.14	10.2	103.1	39.5	450	1.10	10.7	0.159	0.113	1.88	299.0	0.1	0.13
104B			0.795	0.85	0.68													
206			0.159	0.90	0.14													
207	STM104	STM103	0.123	0.90	0.11	1.07	10.3	102.7	304.3	450	1.50	99.6	0.159	0.113	2.20	349.2	0.8	0.87
	STM103	STM102	0.000	0.00	0.00	1.07	11.1	98.9	293.3	525	0.60	29.1	0.216	0.131	1.54	333.1	0.3	0.88
	STM102	STM101	0.000	0.00	0.00	1.07	11.4	97.5	289.0	600	0.50	13.6	0.283	0.150	1.54	434.2	0.1	0.67
	STM101	HW100	0.000	0.00	0.00	1.07	11.5	96.8	287.0	600	0.50	21.3	0.283	0.150	1.54	434.2	0.2	0.66

DRAWINGS / FIGURES



Block	Phase	Block Area	Block GFA	Number	Average
BIOOR	1 11400	(acres)	(ft²)	of Units	Unit Size (ft ²)
ck 1	6	0.49	148,000	145	801
ck 2-3	1	0.78	46,929	0	0
ck 4	6	0.84	101,000	101	881
/GSC	1		78,975	0	0
ck 5	2	0.20	11,000	0	0
ck 6	2	0.18	7,300	0	0
ck 7	3	1.06	116,000	100	792
ck 8	1	0.73	135,000	135	889
ck 9	2	0.11	15,000	15	900
ck 10	2	0.33	104,000	104	1,000
ck 11	1	0.74	74,645	82	779
ck 12	1	0.26	15,000	15	1,000
ck 13	1	0.74	73,698	70	810
ck 14	4	0.56	143,700	0	0
ck 15	4	0.64	108,800	128	813
ck 16	5	0.36	68,000	0	0
ck 17	5	0.60	171,000	0	0
ck 18	5	0.59	208,000	230	814
ck 19	4	0.30	69,800	75	816
ck 20	4	0.65	71,300	79	792
ck 21	5	0.25	59,000	73	727
ck 22	5	0.54	56,000	69	730
ck 23	5	0.41	113,000	140	726
ck 24	2	0.85	115,000	0	0
ck 25	2	0.81	87,538	0	0
ck 26	6	1.39	58,000	65	803



2,189,23 sm (0.54 AC) 57 8m 44 3m 44 3m 45 3m 20,354sm (221,243 sf) GFALOT AREA = 9.4 LEVEL 1 AREALOT AREA = 1599/2189,23 = 0.17 LANDSCAPE AREALOT AREA = 376.0/2189,23 = 0.17 LANDSCAPE AREA/LOT AREA = 36.8/2189,23 = 0.17 AREA(sm) AREA (sf) 75.07m (8.603sf) 75.07m (9.603sf) 75.07m (9.603sf) 75.07m (9.603sf) 75.07m (9.603sf) 0UTDOOR AMENITY AREA = 2sm/UNIT OUTDOOR REQUIRED: 406sm OUTDOOR REQUIRED: 406sm OUTDOOR PROPOSED: 670sm 0UTDOOR REQUIRED: 400sm OUTDOOR PROPOSED: 670sm Init (2.9sm/Unit) Starting and a start spaces/100sm NING BY-LAW 2008-250) Start spaces/100sm REQUIRED PROPOSED 6.0m 6.0m 6.0m 5.2m x 2.6m 6.0m 5.2m x 2.6m 6.0m 5.4 SPACES MAX 8 SPACES 54 SPACES 8 SPACES 8 SPACES 8 SPACES 8 SPACES 8 SPACES 8 SPACES 9.25/ RES UNIT SS SPACES 8 SPACES 159 12 12 3 15					
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PAVING AREA/LOT AREA = 376.0/2189.23= 0.17 LANDSCAPE AREA/ LOT AREA = 36.8/2189.23=0.017 25 75.07m AREA(sm) AREA (sf) 799sm (8,603sf) 15,017sm 15,017sm (161,646sf) 15,816sm (170,249sf) OUTDOOR AMENITY AREA = 2sm/UNIT OUTDOOR REQUIRED: 408sm OUTDOOR PROPOSED: 670sm Jnit (2.9sm/Unit) NING BY-LAW 2008-250) COMM. PARKING RATES MAX 1 SPACES/100sm NOPOSED S2m x 2.6m 6.0m 6.2m x 2.6m 6.0m A SPACES MAX 306 SPACES MAX 306 SPACES MAX 8 SPACES MAX 306 SPACES MAX 8 SPACES BI SPACES MAX 8 SPACES REQUIRED PROPOSED PROPOSED A SPACES MAX 8 SPACES BI SPACES BI SPACES PROPOSED ED ON ZONING BY-LAW 2008-250) REQUIRED PROPOSED 159 159 159 159 12 10		57.8m 44.3m 20,554sm(221,243	sf)		
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799sm (8,603sf) 15,017sm (161,646sf) 15,816sm (170,249sf) OUTDOOR AMENITY AREA = 2sm/UNIT OUTDOOR REQUIRED: 408sm OUTDOOR PROPOSED: 670sm Jnit (209sm/Unit) INING BY-LAW 2008-250) COMM. PARKING RATES MAX 1 SPACES/100sm ING THE FIRST 12 UNITS REQUIRED 5.2m x 2.6m 5.2m x 2.6m 6.0m 6.0m MAX 306 SPACES 54 SPACES MAX 306 SPACES 54 SPACES MAX 306 SPACES 54 SPACES MAX 8 SPACES 8 SPACES 8 SPACES 19 SPACES 8 SPACES 19 SPACES 8 SPACES 3 3 174 174 159 12 152 12 3 3 174 174 VINING BY-LAW 2008-250) <td colspan<="" td=""><td></td><td></td><td></td><td></td></td>	<td></td> <td></td> <td></td> <td></td>				
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Project ZIBI ONTARIO BLOCK 206

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