

Transportation Impact Assessment – Step 4: Analysis

115 Lusk Street



TIA Plan Reports - Certification

On 14 June 2017, the Council of the City of Ottawa adopted new Transportation Impact Assessment (TIA) Guidelines. In adopting the guidelines, Council established a requirement for those preparing and delivering transportation impact assessments and reports to sign a letter of certification.

Individuals submitting TIA reports will be responsible for all aspects of development-related transportation assessment and reporting, and undertaking such work, in accordance and compliance with the City of Ottawa's Official Plan, the Transportation Master Plan and the Transportation Impact Assessment (2017) Guidelines.

By submitting the attached TIA report (and any associate documents) and signing this document, the individual acknowledges that s/he meets the four criteria listed below:

CERTIFICATION

- 1. I have reviewed and have a sound understanding of the objectives, needs and requirements of the City of Ottawa's Official Plan, Transportation Master Plan and the Transportation Impact Assessment (2017) Guidelines;
- 2. I have a sound knowledge of industry standard practice with respect to the preparation of transportation impact assessment reports, including multi modal level of service review;
- I have substantial experience (more than 5 years) in undertaking and delivering transportation impact studies (analysis, reporting and geometric design) with strong background knowledge in transportation planning, engineering or traffic operations; and
- 4. I am either a licensed¹ or registered¹ professional in good standing, whose field of expertise [check $\sqrt{\ }$ appropriate field(s)] is either transportation engineering \Box or transportation planning \Box .

License or registration body that oversees the profession is required to have a code of conduct and ethics guidelines that will ensure appropriate conduct and representation for transportation planning and/or transportation engineering works.

Dated at Ottawa this 9th day of April, 2020. (City)

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Signature of Individual certifier that she/he meets the above four criteria

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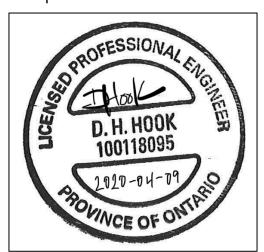
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Executive Summary

IBI Group (IBI) was retained by DCR Phoenix to undertake a Transportation Impact Assessment (TIA) in support of a Site Plan Control application for an approximate 280 square metre proposed restaurant and 567 square metre medical office development to be located at 115 Lusk Street, Ottawa. The development represents a parcel of land in the original 4401 Fallowfield Road Plan of Subdivision.

The site is expected to be fully built out in a single phase and occupied by 2023. The horizon year of the study was therefore taken as 2028, representing 5 years beyond the expected full build-out of the site. The site will be accessed via two full-movement private approaches with direct connections to Forager Street and Lusk Street. Both of these are local streets within the 4401 Fallowfield Road subdivision and provide access to O'Keefe Court and Fallowfield Road, respectively. A total of 55 vehicle parking spaces and 8 bicycle parking spaces will be provided.

Based on the traffic analysis results, the proposed development is expected to generate up to 13 and 32 two-way vehicular trips during the weekday morning and afternoon peak hours, respectively. These traffic volumes were distributed amongst two site access driveways, representing a marginal increase in traffic volumes with respect to the overall traffic projections expected within the 2028 study horizon year. The mode share targets were based on the South Nepean Traffic Assessment Zone (TAZ) and proportionally adjusted, in accordance with the Conditions of Approval for 4401 Fallowfield Road to yield an 85% auto/ 15% non-auto mode share split. It should also be noted that this study did not apply any pass-by reductions factors to the restaurant's trip generation, as it was determined that the overall impact on the adjacent road network would be minimal.

The intersection of Fallowfield & O'Keefe/ Cobble Hill is presently operating as a two-way stop controlled intersection. The results of the analysis indicate that, by 2023, traffic signals will be operationally required under background traffic conditions, however signals are not warranted within the timeframe of this study. With traffic signals in place, the intersection would be expected to operate at an acceptable level of service (LOS 'B') beyond the study horizon year. As site-generated traffic will not contribute significantly to any potential traffic operational issues at this intersection, it is recommended that the City continue monitoring this intersection on an annual basis to determine the appropriate timing for the introduction of traffic signals.

The results of the analysis indicate that the intersections of O'Keefe Court & Lusk Street and Fallowfield Road & Forager Street are expected to operate within acceptable standards (LOS 'D' or better) during the weekday morning and afternoon peak hours. Both are T-intersections that are configured with stop control on the minor road and do not warrant auxiliary lanes or future modifications to intersection control within the timeframe of this study.

A multi-modal analysis identifies deficiencies in the existing road network and potential remediation measures have been suggested in which the City could consider to meet these prescribed targets. It should be noted that, although these measures would improve for a range of transportation modes, they are not required to safely accommodate the transportation demands of the proposed development.

A Roadway Modification Application (RMA-2019-TPD-041B) was recently approved to satisfy a conditional requirement for the 4401 Fallowfield Road Subdivision. The RMA includes the right-in/right-out intersection at Fallowfield Road & Forager Street, a multi-use pathway along the west side of Fallowfield Road and a southbound bus stop on Fallowfield Road near the O'Keefe Court intersection. As there is already an approved RMA intended to address the implementation of the above noted design elements and no off-site geometric improvements are required as a direct result of the proposed development, an RMA will not be included with the submission of this Transportation Impact Assessment.

All study area intersections were shown to operate well within the capacity constraints of the adjacent transportation network, with the appropriate modifications in place (i.e. signalization of Fallowfield & O'Keefe/ Cobble Hill by 2023). Further, the proposed development will contribute a negligible volume of

IBI GROUP TRANSPORTATION IMPACT ASSESSMENT – STEP 4: ANALYSIS 115 LUSK STREET Submitted to DCR Phoenix

traffic to the adjacent road network. A post-development Monitoring Plan is, therefore, not a requirement of this study.

Based on the findings of this study, it is the overall opinion of IBI Group that the proposed development will integrate well with and can be safely accommodated by the adjacent transportation network with the recommended actions and modifications in place.

1 Introduction

IBI Group (IBI) was retained by DCR Phoenix to undertake a Transportation Impact Assessment (TIA) in support of a Site Plan Control application for a proposed restaurant and medical office development to be located at 115 Lusk Street, Ottawa. The development represents a parcel of land in the original 4401 Fallowfield Road Plan of Subdivision.

In accordance with the City of Ottawa's Transportation Impact Assessment Guidelines, published in June 2017, the following report is divided into four major components:

- Screening Prior to the commencement of a TIA, an initial assessment of the proposed development is undertaken to establish the need for a comprehensive review of the site based on three triggers: Trip Generation, Location and Safety.
- Scoping This component of the TIA report describes both the existing and planned conditions in the vicinity of the development and defines study parameters such as the study area, analysis periods and analysis years of the development. It also provides an opportunity to identify any scope exemptions that would eliminate elements of scope described in the TIA Guidelines but not relevant to the development proposal, based on consultation with City staff.
- **Forecasting** The Forecasting component of the TIA is intended to review both the development-generated travel demand and the background network travel demand. It also provides an opportunity to rationalize this demand to ensure projections are within the capacity constraints of the transportation network.
- Analysis This component documents the results of any analyses undertaken to ensure
 that the transportation related features of the proposed development are in conformance
 with prescribed technical standards and that its impacts on the transportation network are
 both sustainable and effectively managed. It also identifies a development strategy to
 ensure that what is being proposed is aligned with the City of Ottawa's policies and citybuilding objectives.

Throughout the development of a TIA report, each of the four study components above are submitted in draft form to the City of Ottawa and undergo a review by a designated Transportation Project Manager. Any comments received are addressed to the satisfaction of the City's Transportation Project Manager before proceeding with subsequent components of the study. All technical comments and responses throughout this process are included in **Appendix A**.

A Roadway Modification Application (RMA-2019-TPD-041B) was recently approved to satisfy a conditional requirement for the Subdivision. The RMA includes a right-in/right-out intersection at Fallowfield Road & Forager Street, a multi-use pathway along the west side of Fallowfield Road and a southbound bus stop on Fallowfield Road near the O'Keefe Court intersection. As such, an RMA will not be required as part of this TIA. The submission may require a post-development Monitoring Plan to track performance of the planned TIA Strategy, however the need for a Monitoring Plan will be confirmed through the analysis undertaken in this report.

2 TIA Screening

An initial screening was completed to confirm the need for a Transportation Impact Assessment by reviewing the following three triggers:

- Trip Generation: Preliminary trip generation estimates were developed based on the Institute of Transportation Engineers (ITE) Trip Generation Manual (10th Edition). A 1.28 person-trip conversion factor was applied to the base trip generation data to obtain person-trip generation. The 60 person-trip threshold prescribed by the TIA Guidelines is met during the weekday afternoon peak hour therefore the Trip Generation trigger is satisfied.
- Location: The proposed development will not be accessed from a boundary street that is
 designated as part of the City's Transit Priority, Rapid Transit network or Spine Bicycle
 Networks nor is the subject site within a Design Priority Area or Transit-Oriented
 Development zone, therefore, the Location trigger is not satisfied.
- Safety: Boundary street conditions were reviewed to determine if there is an elevated
 potential for safety concerns adjacent the site. Based on this review, there is no elevated
 potential for safety concerns adjacent to the site, therefore the Safety trigger is not
 satisfied.

As the proposed development meets the Trip Generation trigger, the need to undertake a Transportation Impact Assessment is confirmed.

A copy of the Screening Form is provided in **Appendix B**.

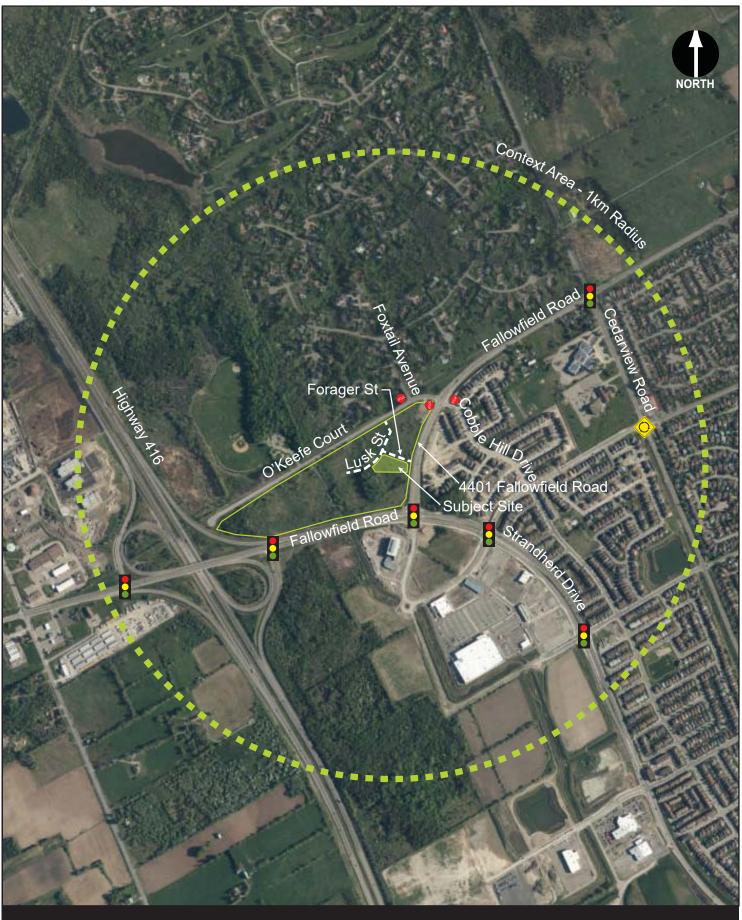
3 Project Scoping

3.1 Description of Proposed Development

3.1.1 Site Location

The proposed development is located within the 4401 Fallowfield Road business park adjacent to Lusk Street, Forager Street and Fallowfield Road. The municipal address of the subject site is 115 Lusk Street. The approximately 0.4 hectare site is currently undeveloped and, based on GeoOttawa, is zoned IP[2265] H(16) – Business Park Industrial Zone.

The site location and its surrounding context is illustrated in **Exhibit 1**.



3.1.2 Land Use Details

Table 1 summarizes the proposed land uses included in this development.

Table 1 - Land Use Statistics

| LAND USE | SIZE |
|--------------------|---|
| Quality Restaurant | 280 m ² (3,014 ft ²) |
| Medical Office | 567 m ² (6,103 ft ²) |

The proposed development is illustrated in Exhibit 2.

The site will be accessed via two full-movement private approaches with direct connections to Forager Street and Lusk Street. Both of these are local streets within the 4401 Fallowfield Road subdivision and provide access to O'Keefe Court and Fallowfield Road, respectively. A total of 55 vehicle parking spaces and 8 bicycle parking spaces will be provided.

3.1.3 Development Phasing & Date of Occupancy

The proposed development will be constructed in a single phase. It is anticipated that the development will be constructed and fully occupied by 2023.



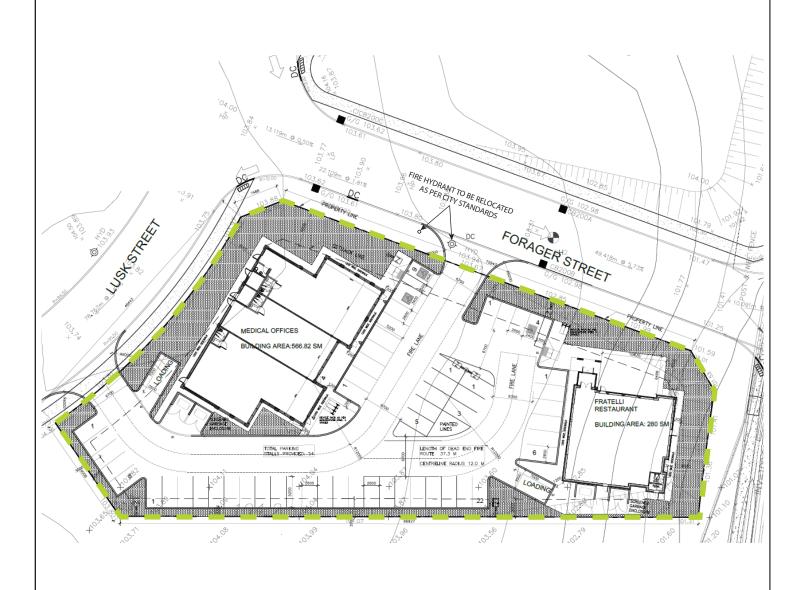


Exhibit 2: Proposed Development PROJECT No. 122508 DATE: April 2020 SCALE: 0m 10m

20m

3.2 Existing Conditions

3.2.1 Existing Road Network

3.2.1.1 Roadways

The proposed development is bound by the following street(s):

- Fallowfield Road is a two-lane undivided urban arterial roadway under the jurisdiction of the City of Ottawa with a right-of-way protection of 44.5m. From Highway 416 heading east, Fallowfield Road has a posted speed of 80km/h. At the intersection with Strandherd Drive, Fallowfield Road takes a 90-degree turn to the northeast and continues through to the study area with a reduced speed limit of 60 km/h.
- Lusk Street is a two-lane local road extending from O'Keefe Court and terminates in a cul-de-sac approximately 250m to the southwest and provides access to the 4401 Fallowfield Road business park. Lusk Street has a 20m right-of-way and an unposted speed limit of 50 km/h.
- Forager Street is a two-lane local road linking Lusk Street to Fallowfield Road and also provides access to the 4401 Fallowfield Road business park. Forager Street has a 20m right-of-way and an unposted speed limit of 50 km/h

Other streets within the vicinity of the proposed development are as follows:

- **Strandherd Drive** is a four-lane divided urban arterial road under the jurisdiction of the City of Ottawa with a posted speed limit of 80 km/h within the vicinity of the subject lands, and a right-of-way protection of 44.5m.
- O'Keefe Court is a two-lane road extending west from Fallowfield Road and terminating in a cul-de-sac approximately 800m west of the Fallowfield Road and O'Keefe Court intersection. The roadway has a rural cross-section with a posted speed limit of 50km/h. O'Keefe Court runs along the former Fallowfield Road alignment (prior to its realignment to Strandherd Drive). Its right-of-way (ROW) therefore varies and is generally 30m, however, additional ROW has been taken on a portion of the north side to accommodate a multi-use pathway (MUP).
- Cedarview Road is a City of Ottawa roadway that extends from Strandherd Drive in the south to Baseline Road in the north. Cedarview Road is a two-lane urban arterial road north of Fallowfield Road, with a 37.5m right-of-way protection. Between Fallowfield Road and Jockvale Road, it is a major collector with a 26m right-of-way. The posted speed limit on Cedarview Road is 60 km/h. South of Strandherd Drive and the VIA Rail corridor, Cedarview Road has been renamed Borrisokane Road and continues south to Barnsdale Road.
- **Foxtail Avenue** is a two-lane local road extending from O'Keefe Court that provides access for the Orchard Estates residential community. The posted speed limit is 40 km/h.

3.2.1.2 Intersections

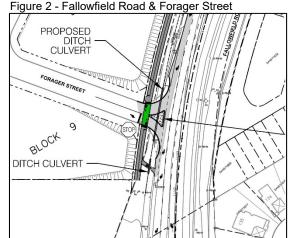
The following existing intersections have been identified as having the greatest potential to be impacted by the proposed development:

Fallowfield Road & O'Keefe Court / Cobble Hill Drive presently exists as a four-legged unsignalized intersection with stop-control on the O'Keefe Court and Cobble Hill Drive approaches. Each leg of the intersection is configured with a single through lane and auxiliary left-turn lane. Auxiliary right-turn lanes are provided along Fallowfield Road, while the sidestreets are configured with shared through-right lanes. The City of Ottawa is currently monitoring this intersection for implementation of traffic signals, once warranted.

Figure 1 - Fallowfield Road & O'Keefe Court / Cobble Hill Drive intersection



Fallowfield Road & Forager Street is a new three- legged intersection with an RMA which is intended to restrict access to right-in/right-out. A multi-use pathway (MUP) crossing is proposed on Forager Street to provide a connection for the future MUP to be located on the west side of Fallowfield Road. Each leg of the intersection is configured with a single through lane, with an auxiliary right-turn lane on the southbound approach only.



3.2.1.3 Traffic Management Measures

There are currently no traffic management or traffic calming measures on the boundary streets within the vicinity of the proposed development.

3.2.1.4 Nearby Driveways

There are currently no driveways within 200m of either proposed site access location. The adjacent Hampton Inn and Suites Hotel currently under construction and located immediately to the southwest of the 115 Lusk Street site will include private approaches, with the nearest being approximately 3 metres from the property line shared with the subject development.

3.2.1.5 Existing Traffic Volumes

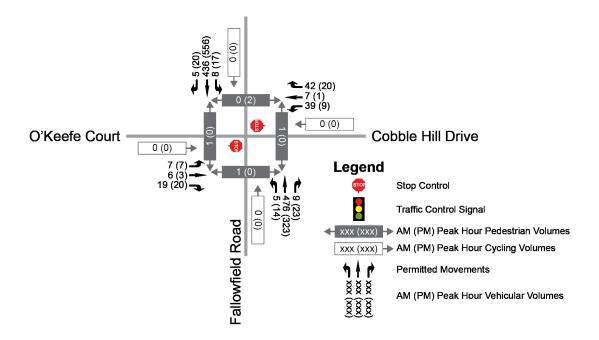
Weekday morning and afternoon peak hour turning movement counts were obtained by IBI staff at the following intersection(s):

Fallowfield Road and O'Keefe Court/ Cobble Hill Drive (IBI Group – January 30, 2018)

A growth rate was applied to the through volumes along Fallowfield Road to approximate existing (2019) traffic volumes. Justification of background traffic volumes is discussed further in the Forecasting section of this report.

Peak hour vehicular, pedestrian and cyclist traffic volumes representative of existing (2019) conditions are shown in **Figure 3**. Traffic count data is provided in **Appendix C**.

Figure 3 - Existing (2019) Traffic



3.2.2 Existing Bicycle and Pedestrian Facilities

The section of Fallowfield Road within the context area is designated as a Spine cycling route, and presently provides paved shoulders on both sides of the road. A bike pocket exists along Fallowfield Road on the southbound approach to the Fallowfield Road & O'Keefe Court / Cobble Hill Drive intersection. A multi-use pathway (MUP) presently exists along the north side of O'Keefe Court from Lytle Park in the west to Cedarview Road in the east. Uni-directional cycle tracks are provided on both sides of Strandherd Drive from Fallowfield Road to Maravista Drive with cross-rides, two-stage left-turn bike boxes and bicycle signals at key signalized intersections within the context area. There are no exclusive bicycle facilities crossing Strandherd Drive, however pedestrian crosswalks are provided at each signalized intersection.

No formal pedestrian facilities are provided within the vicinity of the proposed development with the exception of concrete sidewalks (corner refuge) at the intersection of Fallowfield Road and O'Keefe Court/ Cobble Hill Drive, as well as within the reconstructed section of Strandherd Drive through the context area.

3.2.3 Existing Transit Facilities and Service

OC Transpo operates the following transit routes within close proximity to the proposed development:

 Route #179 provides weekday peak period service between the Citi-Gate development off of Strandherd Drive and the Fallowfield VIA Rail Station and operates on a 15-minute headway.

 Route #272 provides weekday peak period service between the Cobble Hill residential development in Barrhaven South and Tunney's Pasture Station and operates on a 10minute headway.

The nearest bus stops to the proposed development are located at the corner of Fallowfield Road & O'Keefe Court / Cobble Hill Drive, located approximately 270m walking distance from the proposed development.

Transit service maps for the above noted transit routes are provided in **Appendix D**.

3.2.4 Collision History

A review of historical collision data has been conducted for the road network surrounding the proposed development. The TIA Guidelines require a safety review if at least six collisions for any one movement or of a discernible pattern, over a five-year period have occurred. **Table 2** summarizes all reported collisions between January 1, 2014 and December 31, 2018.

Table 2 - Reported Collisions within Vicinity of Proposed Development

| LOCATION | # OF REPORTED COLLISIONS |
|--|--------------------------|
| INTERSECTIONS | |
| Fallowfield Road & Strandherd Drive | 35 |
| Fallowfield Road & O'Keefe Court / Cobble Hill Drive | 1 |
| SEGMENTS | |
| Fallowfield Road – Strandherd Drive to O'Keefe Court / Cobber Hill Drive | 1 |
| O'Keefe Court – Fallowfield Road to cul-de-sac | 1 |

Based on the collision history summarized above, the Fallowfield Road & Strandherd Drive intersection may require further review in the Analysis section of the report.

Detailed collision records are provided in **Appendix E**.

3.3 Planned Conditions

3.3.1 Transportation Network

3.3.1.1 Future Road Network Projects

The 2013 Transportation Master Plan (TMP) outlines future road network modifications in the 2031 'Affordable Network'. The following projects were noted that may have an impact on traffic patterns within the vicinity of the site:

• Strandherd Drive – Planned widening of Strandherd Drive from two to four lanes. The first phase included widening between Fallowfield Road and Maravista Drive (Phase 1: 2014-2019) and was completed in 2015. The second phase includes widening between Maravista Drive and Jockvale Road (Phase 2: 2020-2025).

The 2019 City-Wide Development Charges Background Study (March 15, 2019) identifies the following revisions for the timing of the TMP road network modifications described above:

• Strandherd Drive Phase 2 – The timing for the second phase of the planned widening has been revised to 2020-2024.

Figure 4 illustrates the planned changes to the arterial road network projects in the broader area, as per the TMP Affordable Plan.

PROPOSED DEVELOPMENT

Phase 1 (2014 - 2019) Widening Phase 1 (2014 - 2019) New Road

Phase 2 (2020 - 2025) Widening Phase 2 (2020 - 2025) New Road

Figure 4 - Future Road Network Projects

Source: 2013 Transportation Master Plan – Map 11 '2031 Affordable Network'

Although not part of the '2031 Affordable Network' the TMP indicates that Fallowfield Road may be widened between Strandherd Drive and Greenbank Road some time beyond the TMP's 2031 horizon.

3.3.1.2 Future Transit Facilities and Services

The 2013 TMP outlines the future rapid transit and transit priority (RTTP) network. The TMP does not identify any planned RTTP projects within the vicinity of the proposed development as part of the '2031 Affordable Network' or '2031 Network Concept'. The Roadway Modification Application (RMA) completed for the Fallowfield/ Forager intersection includes a new southbound bus stop on Fallowfield Road south of O'Keefe Court.

3.3.1.3 Future Cycling and Pedestrian Facilities

Although Fallowfield Road is identified as a Spine cycling route, the Ottawa Cycling Plan (2013) does not describe any planned improvements to bicycle infrastructure along this section of roadway within the study area.

A proposed north-south Major Pathway, identified as part of the Ultimate Cycling Network, will connect to the existing multi-use pathway north of O'Keefe Court, continue south through 4401 Fallowfield Road prior to following Highway 416 towards the Jock River. **Figure 5** shows the future cycling network in the vicinity of the proposed development. The RMA includes a portion of the multi-use pathway on the west side of Fallowfield Road along the 4401 Fallowfield subdivision frontage.

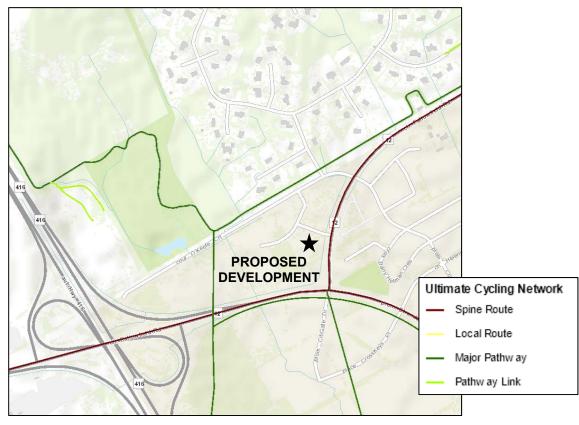


Figure 5 - Ultimate Cycling Network

No additional pedestrian network modifications are planned within the vicinity of the proposed development.

3.3.2 Future Adjacent Developments

The City of Ottawa Transportation Impact Assessment (TIA) Guidelines specify that all significant developments proposed within the surrounding area which are likely to occur within the study's horizon year must be identified and taken into consideration in the development of future background traffic projections.

The subject site forms part of the 4401 Fallowfield Road Plan of Subdivision (previously referred to as the Highway 416 Lands development). It is located in the northwest quadrant of the Fallowfield Road and Strandherd Drive intersection that will eventually consist of two hotels and an office park.

All current development applications within the context area of the proposed development have been summarized below in **Table 3**.

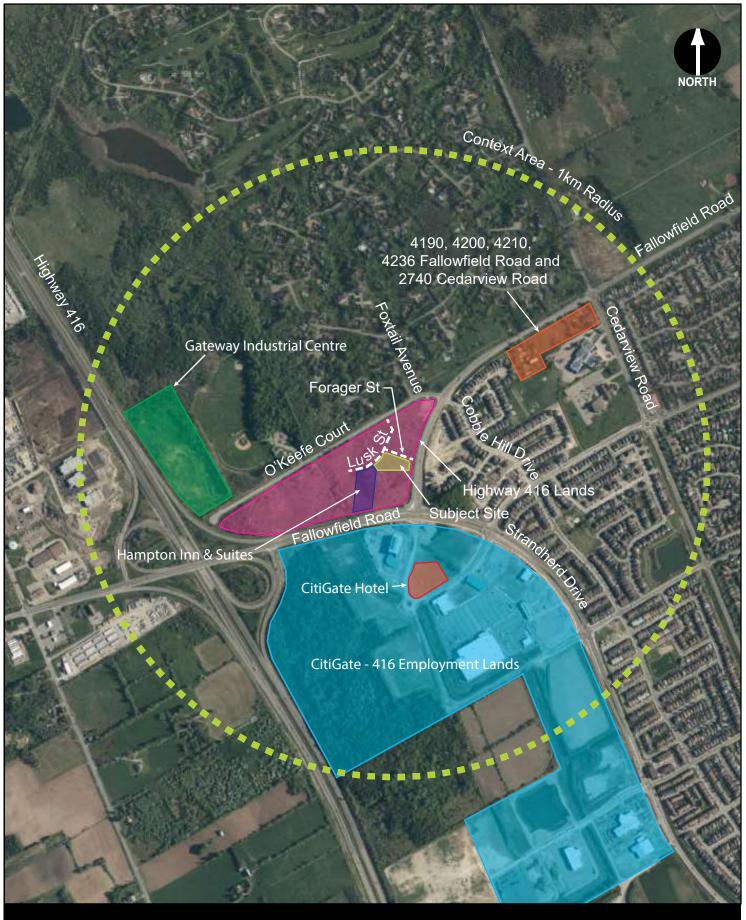
Table 3 - Future Adjacent Developments

| DEVELOPMENT | TIA | LAND USE AND SIZE | TARGETED BUILD-OUT ¹ |
|---|--|---|------------------------------------|
| Highway 416 Lands (4401 Fallowfield Road) | IBI Group (2015) | 2 Hotels 496,168 ft² Business Park | 2017 |
| Hampton Inn & Suites ² | IBI Group (2018) | • 102 Hotel Rooms | 2019 |
| Gateway Industrial Centre (4497 O'Keefe Court) | Delcan (2008) | 279,653 ft ² General Light Industrial | Unknown |
| 4190, 4200, 4210, 4236 Fallowfield Road and 2740 Cedarview Road | Id Road and (2018) • 194 Residential Units | | 2023 |
| CitiGate – 416 Novatech Employment Lands (2012) | | 350,000 ft² Shopping Centre 200 Hotel Rooms Gas Station (8 fuel positions) 16.56 ha Business Park 67.65 ha Office Park 10.5 ha New Car Sales | 2029 |
| CitiGate Hotel (4433 Strandherd Drive) ³ | Novatech (2019) | • 99 Hotel Rooms | 2020 |

Notes:

- 1. Target build-out date may be outdated for some developments
- 2. Located within the Highway 416 Lands development.
- 3. Located within the City Gate 416 Employment Lands development.

The locations of the adjacent developments described above are shown in **Exhibit 3**.



3.3.3 Network Concept Screenline

Network screenline analysis is not expected to be necessary for this development, as it does not trigger the threshold prescribed in the TIA Guidelines of 200 person-trips or more during the peak hour. Detailed trip generation calculations will be provided in the Forecasting section of the report.

3.4 Study Area

The information presented thus far provides a base level of information for the development's context. Based on preliminary estimates of trip generation completed for the TIA Screening, the proposed development is expected to be a low traffic generator with roughly 60 person-trips expected during the weekday afternoon peak hour. Travel demand will be subsequently stratified by mode shares, divided amongst the two proposed site access intersections and further diluted by the variation in travel routes within the broader study area. As such, the proposed development is expected to contribute minimal downstream impacts to intersections on the periphery of the context area such as Cedarview Road and Fallowfield Road.

Strandherd Drive from Fallowfield Road to Maravista Drive was also exempt from the study area, as this segment of road was reconstructed in 2015 following the City's Complete Streets design philosophy to accommodate multi-modal travel demands beyond the TMP's ultimate planning horizon of 2031. Consideration was given to the proposed development travel demands as part of the Highway 416 Lands CTS.

With respect to the exemptions discussed above, this TIA will focus on site-specific impacts, integration with its boundary streets, including a functional review of the site access geometry and intersection control, on-site drive aisle requirements to accommodate proposed design vehicles and a review of the site's parking and loading requirements.

A condensed study area is proposed for this TIA, which will consist of the following intersections:

- Fallowfield Road & O'Keefe Court / Cobble Hill Drive
- O'Keefe Court & Lusk Street
- Fallowfield Road & Forager Street

The study area is consistent with the recent TIA for the adjacent Hampton Inn and Suites.

Multi-modal level of service (MMLOS) analysis will be limited to Fallowfield Road between Forager Street and O'Keefe Court. Intersection MMLOS is only required for signalized intersections, and based on the low traffic generation projected for this development, it is unlikely that it will trigger the need for traffic signals at any of the three study area intersections. This will be verified through intersection capacity analysis in the Analysis component of the report.

3.5 Time Periods

Based on a preliminary review of trip generation rates associated with the proposed land uses, the peak weekly traffic generation is expected to occur on Saturdays. For the purposes of comparison, the weekday morning and afternoon peak periods represent 37% and 87% of this peak demand, respectively. It is important to note however that the Saturday peak likely does not coincide with the peak hour of adjacent street traffic, therefore the weekday morning and afternoon peak hour will constitute the critical analysis periods for this study.

3.6 Study Horizon Year

Traffic analyses associated with TIA's typically involve a review of existing conditions, as well as the anticipated future conditions, both with- and without the proposed development, at the year of

full-occupancy as well as five years beyond. Phased developments will often require interim analyses to provide a timeline for any necessary transportation infrastructure improvements.

It is expected that the proposed development will be constructed and fully occupied in a single phase in 2023. The horizon year for this study is therefore 2028.

3.7 Exemptions Review

The TIA Guidelines provide exemption considerations for elements of the Design Review and Network Impact components. **Table 4** summarizes the TIA modules that are not applicable to this study.

Table 4 - Exemptions Review

| TIA MODULE | ELEMENT | EXEMPTION CONISDERATIONS | REQUIRED |
|---|----------------------------------|--|----------|
| DESIGN REVIEW | COMPONENT | | |
| 4.1 Development Design | 4.1.2 Circulation and Access | Only required for site plans | ✓ |
| | 4.1.3 New Street Networks | Only required for plans of subdivision | × |
| 4.2 Parking | 4.2.1 Parking Supply | Only required for site plans | ✓ |
| | 4.2.2 Spillover Parking | Only required for site plans where parking supply is 15% below unconstrained demand | × |
| NETWORK IMPAC | T COMPONENT | | |
| 4.5 Transportation Demand Management | All Elements | Not required for site plans expected to have fewer than 60 employees and/or students on location at any given time | × |
| 4.6 Neighbourhood Traffic Management | 4.6.1 Adjacent Neighbourhoods | Only required when the development relies on local or collector streets for access and total volumes exceed ATM capacity thresholds | ✓ |
| 4.8 Network Concept | n/a | Only required when proposed development generates more than 200 person-trips during the peak hour in excess of the equivalent volume permitted by established zoning | × |

4 Forecasting

4.1 Development Generated Traffic

4.1.1 Trip Generation Methodology

Peak hour site-generated traffic volumes were developed using the Institute of Transportation Engineers (ITE) Trip Generation Manual (10th Edition). The TIA Guidelines indicate that vehicle-trip generation rates from the ITE Trip Generation Manual should be converted to person-trips through the application of a 1.28 vehicle-to-person-trip conversion factor.

Following the application of the vehicle-to-person-trip conversion factor, the person-trips were then subdivided based on representative mode share percentages applicable to the study area to determine the number of vehicle, transit, pedestrian, cycling and other trip types.

Target mode shares were developed based on the local mode shares from the OD Survey and adjusted to account for Condition 6b of the Conditions of Approval of the Draft Plan of Subdivision of 4401 Fallowfield Road. Condition 6b indicates that all TIAs prepared for Site Plan Applications within the 4401 Fallowfield Road subdivision must assume a maximum non-auto mode share (transit, walking, cycling and other) of 15%. Furthermore, Condition 6a indicates that the cumulative vehicle-trip generation of all sites within the 4401 Fallowfield Road subdivision shall not exceed 739 vehicles per hour during the weekday morning and afternoon peak periods.

4.1.2 Trip Generation Results

4.1.2.1 Base Vehicle Trip Generation

Peak hour vehicular traffic volumes associated with the 115 Lusk Street development were determined using appropriate peak hour trip generation rates from the ITE Trip Generation Manual.

The vehicular trip generation results for the proposed development have been summarized in **Table 5**.

Table 5 - Base Vehicular Trip Generation Results

| LANDLICE | SIZE | PERIOD | GENERATED TRIPS (VPH) | | |
|--------------------------|--------------------|--------|-----------------------|-----|-------|
| LAND USE | | | IN | OUT | TOTAL |
| 720 – Medical Offices | 567 m ² | AM | 11 | 6 | 17 |
| 720 Medical Offices | | PM | 8 | 13 | 21 |
| 931 – Quality Restaurant | 280 m ² | AM | 1 | 1 | 2 |
| 331 – Quality Nestaurant | | PM | 16 | 8 | 24 |

Notes: vph = Vehicles per Hour

4.1.2.2 Person Trip Generation

The TIA Guidelines indicate that a 1.28 vehicle-to-person-trip conversion rate should be utilized to convert the base vehicular trip generation results into person trips.

The resulting number of person-trips the proposed development is expected to generate is summarized in **Table 6** below.

Table 6 - Person-Trip Generation

| LANDUCE | DEDIOD | PERSON TRIPS (PPH) | | | |
|--------------------|--------|--------------------|-----|-------|--|
| LAND USE | PERIOD | IN | OUT | TOTAL | |
| Medical Offices | AM | 13 | 8 | 21 | |
| iviedical Offices | PM | 11 | 16 | 27 | |
| Ovality Destayment | AM | 1 | 1 | 2 | |
| Quality Restaurant | PM | 20 | 10 | 30 | |

Notes: pph = persons per hour

4.1.2.3 Mode Share Proportions

The 2011 TRANS Origin-Destination (O-D) Survey provides approximations of the existing modal share within the South Nepean Traffic Assessment Zone (TAZ). Relevant extracts from the 2011 O-D Survey are provided in **Appendix F**.

Of the available data, the average of the weekday AM and PM peak 'Within District' mode shares was determined to be the most appropriate existing mode share references, as the subject development is expected to primarily draw traffic from the local area.

Given the context of the proposed development, the mode shares specific to this development may deviate from the average mode share experienced in the South Nepean TAZ. As discussed below, adjustments were made to all the mode shares to better represent the mode shares for the proposed development.

The subject development is located on the opposite side of Fallowfield Road from the majority of the local residential developments, with only one signalized intersection in its vicinity providing a controlled crossing of Fallowfield Road. At present, limited active transportation facilities are provided in the study area, and although isolated measures are planned in the near term, there is a decreased likelihood of significant pedestrian or cycling demand being generated by the site. It is expected, however, that the intersection of Fallowfield Road & O'Keefe Court / Cobble Hill Drive will eventually become signalized which will improve the accessibility of the site for pedestrians. This is expected to result in an increase in pedestrian demand which is reflected in the 2028 mode share targets.

Despite the planned inclusion of a southbound bus stop on Fallowfield Road south of O'Keefe Court as part of the approved RMA for the Fallowfield Road & Forager Street intersection, the transit mode share is expected to remain low, as transit service existing on the east side of Fallowfield Road will be partially inaccessible due to the lack of controlled pedestrian crossings on Fallowfield Road adjacent to the site.

Given the low probability of site-generated trips occurring by non-auto travel modes (transit, cycling, walking and other) within the horizon year of this study, the mode shares of all non-auto travel modes were proportionally adjusted to yield a total non-auto mode share of 15% in accordance with the Conditions of Approval for 4401 Fallowfield Road. The difference in mode share was reallocated to the auto driver and auto passenger mode shares.

Table 7 below summarizes the 2011 OD Survey mode shares as well as the target mode shares.

Table 7 - 2011 OD Survey Mode Shares and Proposed Mode Share Targets

| TRAVEL MODE | 2011 OD SURVEY MODE SHARES | 2023 MODE SHARE TARGETS | 2028 MODE SHARE TARGETS | |
|------------------------------|-------------------------------|----------------------------|----------------------------|--|
| Auto Driver | 40% | 57% | 57% | |
| Auto Passenger | 20% | 28% | 28% | |
| Total Auto Mode Share | 60% | 85% | 85% | |
| Transit | 4% | 2% | 2% | |
| Cycling | 2% | 0% | 0% | |
| Walking | 19% | 7% | 13% | |
| Other | 16% | 6% | 0% | |
| Total Non-Auto Mode Share | 40% | 15% | 15% | |

4.1.2.4 Trip Reduction Factors

Deduction of Existing Development Trips

Not Applicable: The proposed development lands are currently undeveloped, and do not generate any traffic volumes.

Pass-by Traffic

Based on survey data collected for the *ITE Trip Generation Handbook (3rd edition)*, the Quality Restaurant land use was shown to generate an average of 44% pass-by trips. This study conservatively did not apply any pass-by reduction factors, as the overall impact on the adjacent road network is expected to be minimal.

Synergy/ Internalization

Not Applicable: The proposed development will not generate internal person-trips between the proposed land uses. Non-auto trips are likely to occur to/from other sites within the 4401 Fallowfield Road subdivision, such as the adjacent Hampton Inn and Suites.

4.1.2.5 Trip Generation by Mode

The mode share targets from **Table 7** were applied to the number of development-generated person-trips to establish the expected number of trips per travel mode, as summarized in **Table 8** below.

Table 8 - Peak Hour Person Trips by Mode

| | 2023 | | | 2028 | | | | |
|----------------|------|-----|----|------|----|-----|----|-----|
| MODE | AM | | РМ | | АМ | | PM | |
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| Auto Driver | 8 | 5 | 17 | 15 | 8 | 5 | 17 | 15 |
| Auto Passenger | 4 | 3 | 9 | 7 | 4 | 3 | 9 | 7 |
| Transit | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 |
| Cycling | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Walking | 1 | 1 | 2 | 2 | 2 | 2 | 4 | 4 |
| Other | 1 | 1 | 2 | 2 | 0 | 0 | 0 | 0 |
| Total | 2 | 4 | 5 | 7 | 2 | 4 | 5 | 7 |

4.1.2.6 Cumulative 4401 Fallowfield Road Trip Generation

Condition 6A of the Conditions of Approval of the Draft Plan of Subdivision of 4401 Fallowfield Road indicates that the total vehicle-trip generation of the subdivision shall not exceed 739 vehicle-trips per hour during the weekday morning and afternoon peak hours. **Table 9** summarizes the total and cumulative number of vehicle-trips generated during the weekday morning and afternoon peak hours by all sub-developments within 4401 Fallowfield Road subdivision which have been approved or are currently undergoing a Site Plan Control Application.

Table 9 - Cumulative 4401 Fallowfield Road Trip Generation

| SUB-DEVELOPMENT | TOTAL AM (PM) VEHICLE TRIPS | CUMULATIVE AM (PM) VEHICLE TRIPS | |
|----------------------|--------------------------------|-------------------------------------|--|
| Hampton Inn & Suites | 56 (64) | 56 (64) | |
| 115 Lusk Street | 13 (32) | 69 (96) | |
| Total from Curren | 69 (96) | | |
| Total Allowa | 739 (739) | | |
| Percentage of | 9% (13%) | | |

As indicated above, the proposed development will not exceed the maximum permissible vehicular generation of the 4401 Fallowfield Road subdivision.

4.1.3 Trip Distribution and Assignment

As the proposed development is expected to primarily draw traffic from local residential areas, site-generated traffic has been distributed to the road network based on the concentrations of housing in the vicinity of the subject development:

- 40% to/from the southwest via Fallowfield Road
- 60% to/from the east via Fallowfield Road

Utilizing the estimated number of new auto trips and applying the above distribution, future sitegenerated traffic volumes are illustrated for each of the study area intersections in **Exhibit 4**.

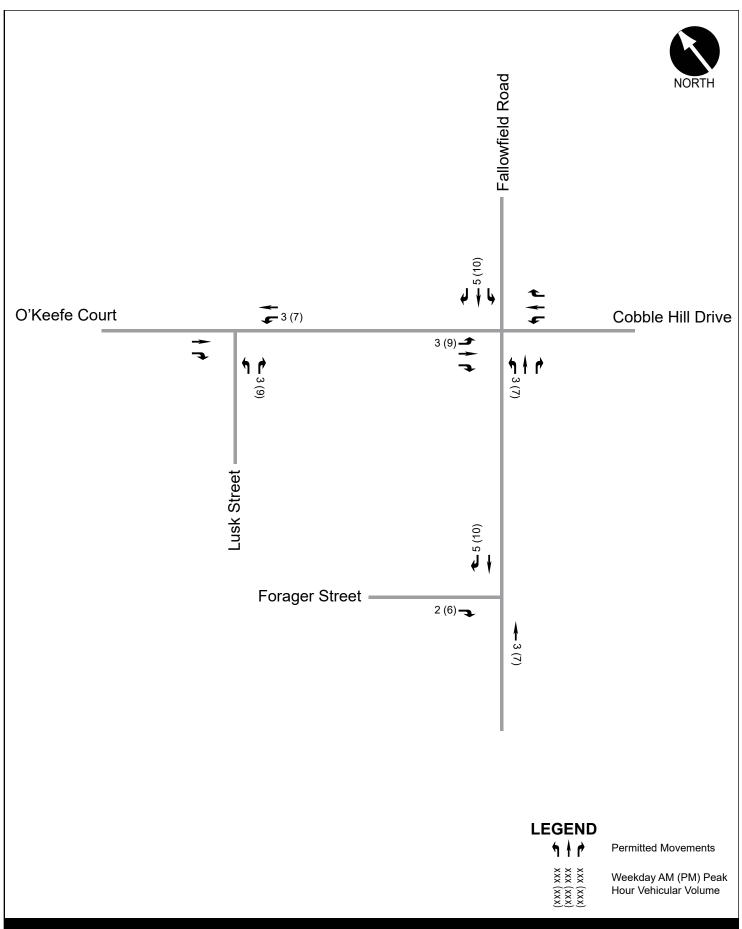




Exhibit 4: Site-Generated AM & PM Peak Hour Traffic

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4.2 Background Network Traffic

4.2.1 Changes to the Background Transportation Network

To properly assess future traffic conditions, planned modifications to the transportation network that may impact travel patterns or demand within the study area must be considered. The Scoping section of this TIA reviewed the anticipated changes to the study area transportation network based on the Transportation Master Plan (TMP), the Ottawa Cycling Plan, the Ottawa Pedestrian Plan and the 2019 City-Wide Development Charges Background Study and determined that there are no major road, pedestrian or cycling network modifications planned within the study area prior to the 2028 horizon.

The intersection of Fallowfield Road/ O'Keefe/ Cobble Hill is being monitored by City staff for traffic signal warrants. As discussed previously, an RMA was recently approved for the right-in/right-out intersection of Fallowfield Road & Forager Street which includes an isolated section of multi-use path (MUP) on the west side of Fallowfield Road and a southbound bus stop on Fallowfield Road along the 4401 Fallowfield Road, south of O'Keefe Court.

4.2.2 General Background Growth Rates

The background growth rate is intended to represent regional growth from outside the study area that will travel along the adjacent road network. Consistent with the adjacent Hampton Inn & Suites TIA, a 2% rate of linear growth per annum is proposed within the study area for the calculation of future background traffic.

The background growth rate was only been applied to the through movements on Fallowfield Road as traffic generation relating to all known future adjacent developments has been explicitly accounted for in the analysis.

4.2.3 Other Area Development

All current adjacent development applications within the study area were previously identified in **Table 3**. All of the developments identified have been accounted for in the future background volume projections. The developments represent specific areas of growth within the study area and are therefore considered in addition to the general background growth rate discussed previously. **Table 10** summarizes the vehicle trip generation of all current adjacent background development applications.

Table 10 - Adjacent Development Vehicle Trip Generation

| | TIA | VEHICLE TRIP GENERATION | | | | |
|---|---------------------|-------------------------|-----|------|------|--|
| DEVELOPMENT | | A | M | PM | | |
| | | IN | OUT | IN | OUT | |
| Highway 416 Lands (4401 Fallowfield Road) | IBI Group (2015) | 630 | 109 | 137 | 533 | |
| Hampton Inn & Suites | IBI Group (2018) | 33 | 23 | 33 | 31 | |
| Gateway Industrial Centre (4497 O'Keefe Court) | Delcan (2008) | 20 | 97 | 94 | 46 | |
| 4190, 4200, 4210, 4236 Fallowfield Road and 2740 Cedarview Road | Novatech (2018) | 108 | 33 | 131 | 76 | |
| | Novatech (2012) | Interim (2019) | | | | |
| CitiGate – 416 | | 741 | 216 | 664 | 1015 | |
| Employment Lands | | Ultimate (2029) | | | | |
| | | 3494 | 635 | 1128 | 3316 | |
| CitiGate Hotel (4433 Strandherd Drive) | Novatech (2019) | 29 | 20 | 27 | 26 | |

It should be noted that some of the developments shown in **Table 10** above are not expected to be fully built out by the horizon year of the study or are sub-developments within a larger development. Background development traffic volumes have been adjusted appropriately to account for this.

The CitiGate – 416 Employment Lands is a large multi-phase development that has been partially been built out and is expected to be fully built out by 2029. The projected traffic volumes generated by this development at the 2023 and 2028 analysis years were linearly interpolated and considered the development status at the time of the recorded traffic counts utilized in this study.

It was assumed that the Gateway Industrial Centre (4497 O'Keefe Court) development would be fully built out by the 2023 analysis year.

4.3 Demand Rationalization

The purpose of this section is to rationalize future travel demands within the study area to account for potential capacity limitations in the transportation network and its ability to effectively accommodate the additional demand generated by a new development.

4.3.1 Description of Capacity Issues

The TIA recently completed for the adjacent Hampton Inn and Suites indicated study area intersections including Fallowfield Road & O'Keefe Court/ Cobble Hill Drive as well as Lusk Street/ O'Keefe Court would operate below their theoretical capacities (i.e. LOS 'D' or better) beyond the build-out year of the proposed development.

4.3.2 Adjustment to Development Generated Demands

The proposed development is only expected to generate 32 two-way vehicle-trips during the weekday morning and afternoon peak hours of adjacent street traffic and therefore unlikely to trigger any capacity issues.

4.3.3 Adjustment to Background Network Demands

As no further capacity issues have been identified, no adjustments to background network demands are necessary.

The TIA recently completed for Hampton Inn and Suites did not assign any traffic to the Fallowfield/ Forager intersection. Now that the current study has assumed a reassignment of trips to this intersection.

4.4 Traffic Volume Summary

4.4.1 Future Background Traffic Volumes

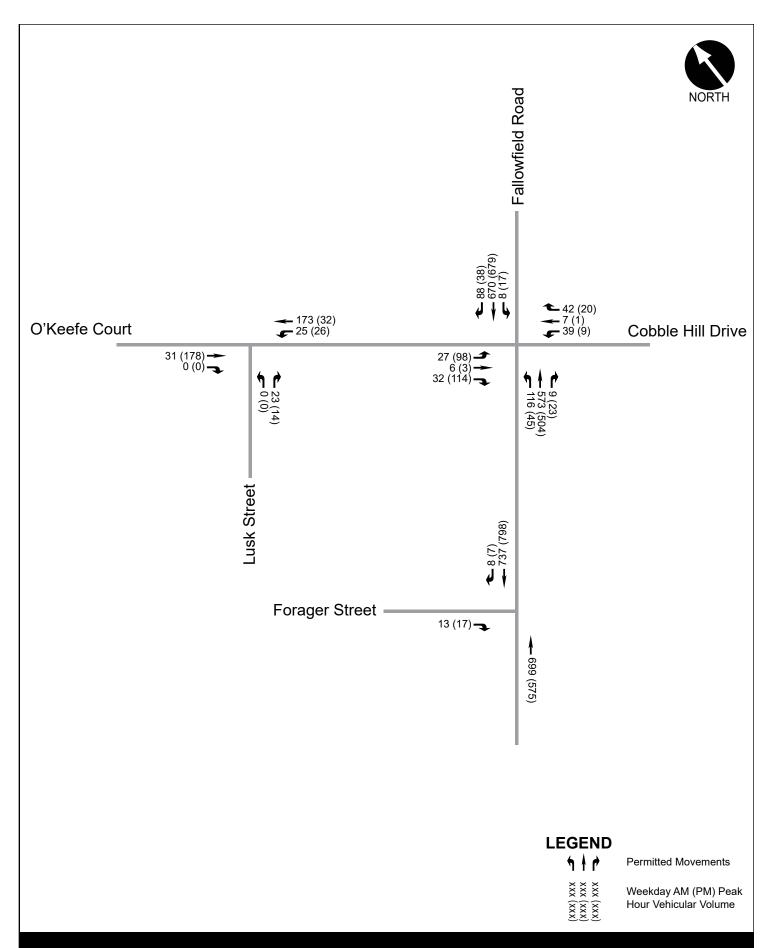
Future background traffic volumes projections have been established by combining the adjacent development traffic and background traffic derived through the application of a growth rate as discussed previously.

Exhibit 5 and **Exhibit 6** present the future background traffic volumes anticipated for the 2023 build-out year, as well as the 2028 study horizon, respectively.

4.4.2 Future Total Traffic Volumes

Future total volumes have been derived by combining the site-generated traffic from **Exhibit 4** with the future background volumes from **Exhibit 5** and **Exhibit 6**.

Exhibit 7 and **Exhibit 8** present the future total traffic volumes anticipated for 2023 and 2028 analysis years, respectively.





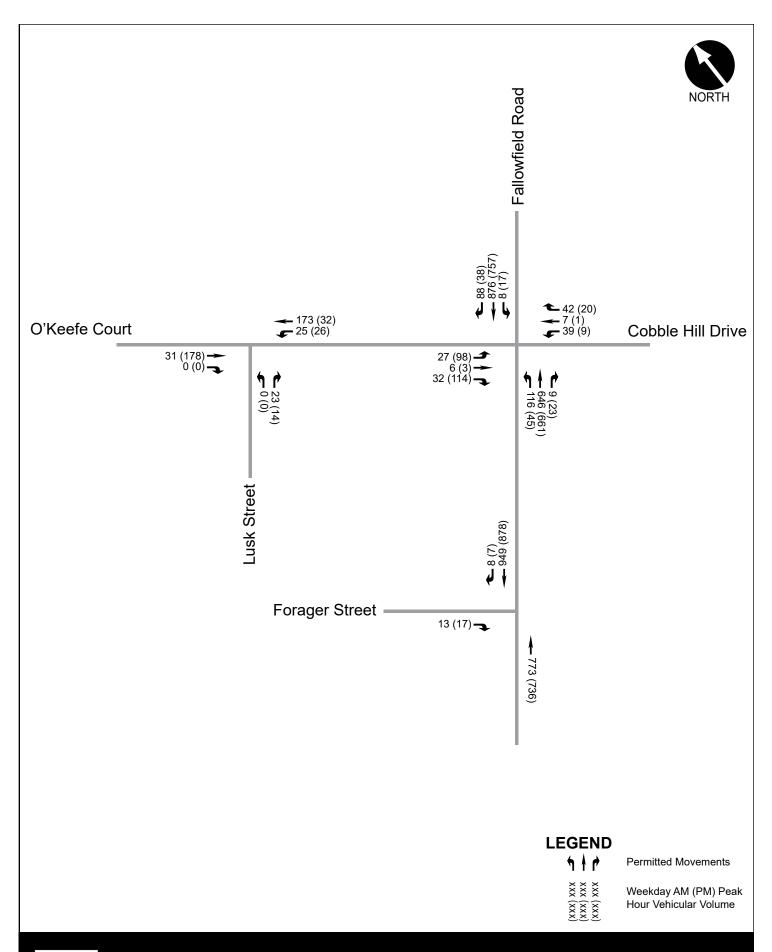




Exhibit 6: Exhibit 6: PROJECT No. Future (2028) Background DATE:
Traffic SCALE: Traffic

122508 April 2020 N.T.S.

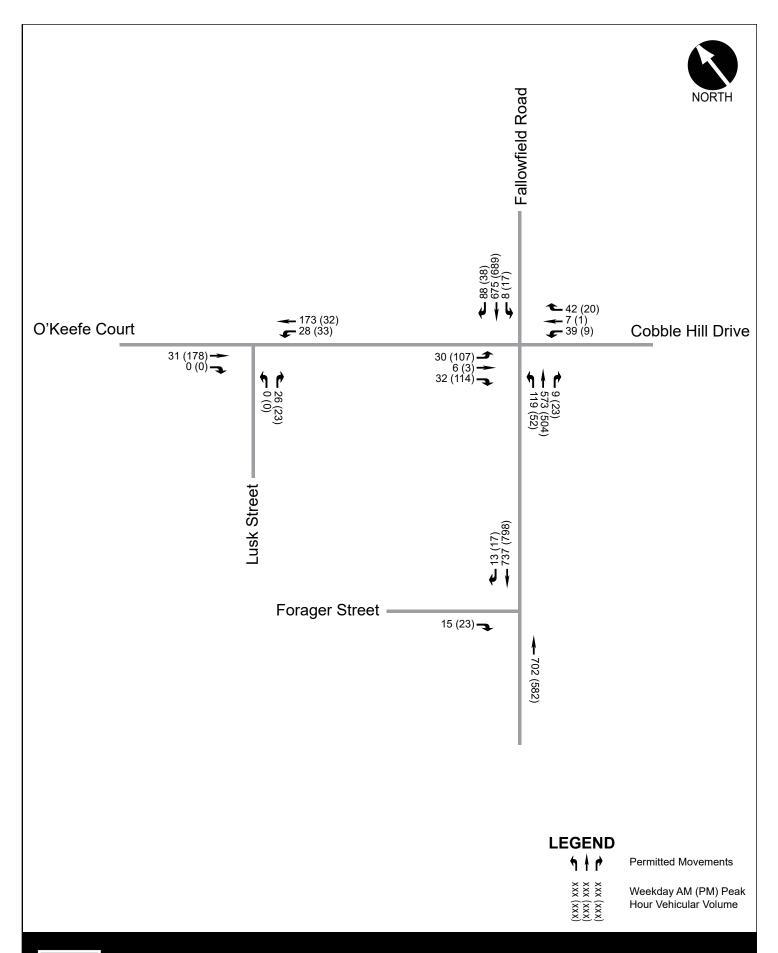
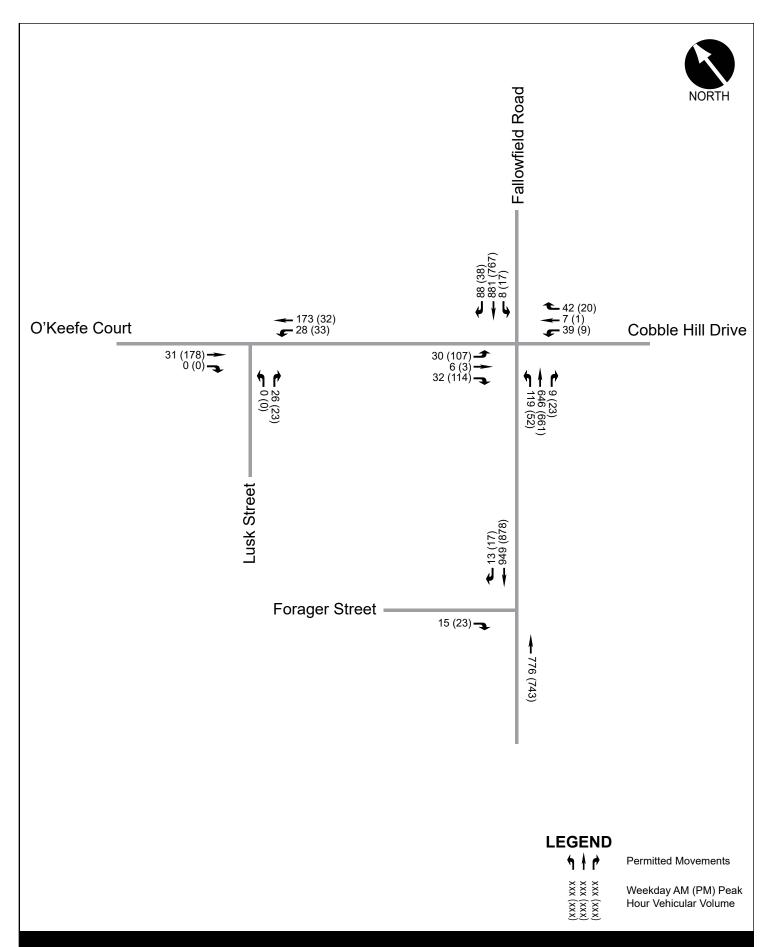




Exhibit 7: Future (2023) Total Traffic

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5 Analysis

5.1 Development Design

5.1.1 Design for Sustainable Modes

The proposed development is located an approximate 600m walking distance from an existing bus stop at the corner of Fallowfield Road & O'Keefe Court / Cobble Hill Drive, assuming that transit users cross Fallowfield Road at Strandherd Drive. The RMA for the Fallowfield Road & Forager Street intersection indicates that a new southbound bus stop will be constructed on Fallowfield Road south of O'Keefe Court, thereby reducing the walking distance to transit to approximately 200m.

The TDM-Supportive Development Design and Infrastructure Checklist as well as the TDM Measures Checklist were completed and are provided in **Appendix G**. These checklists identify anticipated measures that are being considered in association with the proposed development to offset the vehicular impact on the adjacent road network.

5.1.2 Circulation and Access

A separate loading bay has been provided for each building on the site, as shown in **Exhibit 2**, which have been designed to accommodate a standard delivery vehicle.

Separate waste collection locations have also been provided for each building on the site, as shown in **Exhibit 2**. A loading bay near each garbage location will provide space for a standard waste collection vehicle to park while workers collect the waste.

5.1.3 New Street Networks

Not Applicable: The New Street Networks element is exempt from this TIA, as defined in the study scope. This element is not required for Site Plan Control applications.

5.2 Parking

5.2.1 Parking Supply

Based on the size of the proposed restaurant and medical office, a minimum of 45 vehicle parking spaces are required to meet the Zoning Bylaw requirements. The site plan indicates that 54 vehicle parking spaces will be provided, therefore the proposed parking supply is within the permissible range.

The Zoning Bylaw also requires a minimum number of bicycle parking spaces for each land use within the subject development. A total of five bicycle parking spaces will be provided, exceeding the three spaces required.

5.2.2 Spillover Parking

The minimum parking supply requirement specified in the Zoning Bylaw has been met, therefore, no further review of parking is necessary for the purposes of this study.

5.3 Boundary Streets

There are three existing boundary streets adjacent to the proposed development: Lusk Street, Forager Street and Fallowfield Road. As discussed in Section 3.4, segment-based MMLOS analysis will be limited to Fallowfield Road between Forager and O'Keefe/ Cobble Hill.

Both Lusk Street and Forager Street are classified as local roads, and were recently constructed in accordance with the latest City road design standards, therefore no Multi-Modal Level of Service (MMLOS) analysis is provided for either road segment. Given their classification as 'local' roads, both are in essence Complete Streets, as they provide sufficient facilities for active and motorized modes of travel. Concrete sidewalks 2.0 metres in width are proposed along one side of each local road. A sidewalk is provided along the proposed development's frontage on Lusk Street, which will continue across the site access driveway, while the sidewalk on Forager Street will be constructed on the north side of the road, opposite the development. As such, the inclusion of site access driveways along Lusk Street and Forager Street are not anticipated to negatively impact the design of either local road.

5.3.1 Mobility

Segment-based Multi-Modal Level of Service (MMLOS) results for Fallowfield Road between Forager Street and O'Keefe Court / Cobble Hill Drive are provided in **Table 11** below.

Details of the MMLOS analysis are provided in **Appendix H**.

Table 11 - Segment MMLOS Results

| | | LEVEL OF SERVICE BY MODE | | | | | |
|---|-------------------------|--------------------------|-------------------|------------------|--|--|--|
| LOCATION | PEDESTRIAN (PLOS) | BICYCLE (BLOS) | TRANSIT (TLOS) | TRUCK (TkLOS) | | | |
| SEGMENTS | | | | | | | |
| Fallowfield Road – Forager Street to O'Keefe Court / Cobble Hill Drive | F (Target: C) | F (Target: C) | D (Target: D) | C (Target: E) | | | |

Based on the above, this segment of Fallowfield Road is not currently meeting its pedestrian and bicycle level of service targets. The following measures have been identified which could help achieve these targets:

- A reduction in operating speeds to 60 km/h or less;
- A 2.0m wide sidewalk separated from the road with a minimum 2.0m wide boulevard on either side of Fallowfield Road or the implementation of a multi-use path; and
- Bike lanes on both sides of Fallowfield Road or physically separated cycling facilities such as multi-use pathways.

As discussed previously, the approved RMA includes the planned implementation of a multi-use pathway along the west side of Fallowfield Road and a southbound bus stop on Fallowfield Road near the O'Keefe Court intersection, which should help to significantly improve both the PLOS and BLOS.

5.3.2 Road Safety

A summary of all reported collisions within the study period over the past 5 years was presented in the Scoping section of this TIA. The City requires a safety review if at least six collisions for any one movement or of a discernible pattern, over a five-year period have occurred. Based on the review of re-occurring events identified in the Scoping section of this report, none of the study area roadway segments or intersections require further analysis.

5.4 Access Intersections

5.4.1 Location and Design of Access

The proposed development will provide two new full-movement access intersections: one on Lusk Street and the other on Forager Street. The proposed site access driveways are in conformance with the City of Ottawa Private Approach By-law 2003-447, with particular confirmation of the following items:

- <u>Width</u>: A private approach should have a minimum width of 2.4m and a maximum width of 9.0m.
 - ➤ Both site access driveways will be 6.7m wide.
- <u>Distance from Intersecting Road</u>: For a commercial development on or within 46m of an arterial or major collector with between 50 and 99 parking spaces, the proposed private approach must be at least 30 metres from the nearest intersecting street line.
 - The proposed access on Forager Street is approximately 45m from the nearest intersecting street line at Fallowfield Road and is therefore in compliance with the by-law.
- Quantity and Spacing of Private Approaches: For sites with frontage between 46 and 150 metres, one (1) two-way and two (2) one-way, or two (2) two-way private approaches are permitted. Any two private approaches must be separated by at least 9.0m and can be reduced to 2.0m in the case of two one-way driveways. On lots that abut more than one roadway, these provisions apply to each frontage separately.
 - ➤ The frontage on Lusk Street is 46m and therefore the single proposed two-way private approach is compliant with the by-law. ✓
 - ➤ The frontage on Forager Street is 73m and therefore the single proposed twoway private approach is compliant with the by-law. ✓
- <u>Distance from Property Line</u>: Private approaches must be at least 3.0m from the abutting
 property line, however this requirement can be reduced to 0.3m provided that the access
 is a safe distance from the access serving the adjacent property, sight lines are adequate
 and that it does not create a traffic hazard.
 - Both proposed private approaches exceed the minimum distance required.
- Grade of Private Approach: The grade of a private approach serving a parking area of more than 50 spaces must not exceed 2% within the private property for a distance of 9m from the highway/curb line.
 - ➤ The grade of both private approaches will not exceed 2% within 9m of the curb line.

The Transportation Association of Canada's (TAC) Geometric Design Guide for Canadian Roads (June 2017) does not suggest a minimum clear throat length for site access driveways proposed on local roads. The clear throat length is provided to ensure that any queues that form due to onsite circulation blockages do not spillback onto collector and arterial roads. Given the low traffic volumes typically expected on local roads such as Lusk and Forager, occasional queue spillback is not likely to result in traffic operational issues.

5.4.2 Access Intersection Control

The proposed site access driveways on Lusk Street and Forager Street will both be stop-controlled, which is expected to be sufficient given the low site-generated traffic volumes presented in the Forecasting section of this report.

5.4.3 Intersection Design (MMLOS)

Not Applicable – Both proposed site access driveways will be unsignalized, therefore Multi-Modal Level of Service (MMLOS) analysis is not required.

5.5 Transportation Demand Management (TDM)

Not Applicable – The Transportation Demand Management (TDM) element is exempt from this TIA, as defined in the study scope. This element is not required for non-residential site plans that are projected to have fewer than 60 employees and/or students on location at any given time.

Based on the employee densities indicated in the *ITE Parking Generation Manual (4th Edition)* for the restaurant and medical office land uses, it is anticipated that there will only be up to 36 employees on site at any given time. As such, the TDM element is not required.

5.5.1 Context for TDM

Not Applicable.

5.5.2 Need and Opportunity

Not Applicable.

5.5.3 TDM Program

Not Applicable.

5.6 Neighbourhood Traffic Management

5.6.1 Adjacent Neighbourhoods

The proposed development relies on the following collector or lower-classification roads for access to the arterial road network: O'Keefe Court, Lusk Street and Forager Street. With the development of the 4401 Fallowfield Road Subdivision lands, O'Keefe Court is expected to function as a collector road, while Lusk Street and Forager Street will operate as local roads. To determine if neighbourhood traffic management measures are required, traffic volumes projected in the study horizon year are compared against the appropriate liveability thresholds, as prescribed in the TIA Guidelines.

The livability threshold for a local road is 120 vehicles per hour. Based on Future (2028) Total Traffic volumes, Lusk Street and Forager Street will be required to accommodate up to 56 and 40 vehicles per hour, respectively, during the weekday afternoon peak hour. As such, both local roads are anticipated to operate well below the 120 vehicle per hour threshold within the timeframe of this study.

Total traffic volume projections along O'Keefe Court indicate that it may slightly exceed its threshold of 300 vehicles per hour during the weekday afternoon peak hour, with up to 315 vehicles approaching Fallowfield Road. It should be noted, however, that it is not uncommon for a collector road to exceed this threshold approaching an arterial road, and that two-way volumes on O'Keefe Court through the remainder of the study area are expected operate within this threshold. As such, a neighbourhood traffic management plan will not be required for this TIA.

5.7 Transit

5.7.1 Route Capacity

The estimated future site-generated transit passenger demand was provided in the Forecasting component of this study. The results have been summarized in **Table 12** below.

Table 12 - Development Generated Transit Demand

| DEDICE | PEAK PERIOD DEMAND | | | |
|--------|--------------------|-----|--|--|
| PERIOD | IN | OUT | | |
| AM | 0 | 0 | | |
| PM | 1 | 0 | | |

As indicated in **Table 12** above, the subject development is expected to contribute a negligible increase in transit ridership to the existing transit network, therefore no additional transit capacity will be required to accommodate the proposed development.

5.7.1 Transit Priority Measures

Transit priority measures are not required at any of the signalized study area intersections to support the projected travel demands within the timeframe of this study.

5.8 Review of Network Concept

Not Applicable – The Network Concept element is exempt from this TIA, as defined in the study scope. This element is not required for proposed developments expected to generate less than 200 person-trips during the weekday morning and afternoon peak hours.

5.9 Intersection Design

The following sections summarize the methodology and results of the multi-modal intersection capacity analysis conducted within the study area.

5.9.1 Intersection Control

5.9.1.1 Traffic Signal Warrants

Traffic signal warrants were completed for the intersection of Fallowfield Road & O'Keefe Court / Cobble Hill Drive. Based on the results of the analysis, traffic signals are not warranted at this intersection under Future (2028) Total Traffic conditions.

The results of the traffic signal warrant analysis are provided in **Appendix I**.

5.9.1.2 Roundabout Analysis

The feasibility of implementing a roundabout was evaluated at the intersection of Fallowfield & O'Keefe/ Cobble Hill. It was determined that this form of traffic control would not be feasible, given that only one of the suitability factors had been met.

The results of the Roundabout Feasibility Screening Tool are provided in Appendix I.

5.9.2 Intersection Analysis Criteria (Automobile)

The following section outlines the City of Ottawa's methodology for determining motor vehicle Level of Service (LOS) at signalized and unsignalized intersections.

5.9.2.1 Signalized Intersections

In qualitative terms, the Level of Service (LOS) defines operational conditions within a traffic stream and their perception by motorists. A LOS definition generally describes these conditions in terms of such factors as delay, speed and travel time, freedom to manoeuvre, traffic interruptions, safety, comfort and convenience. LOS can also be related to the ratio of the volume to capacity (v/c) which is simply the relationship of the traffic volume (either measured or forecast) to the capability of the intersection or road section to accommodate a given traffic volume. This capability varies depending on the factors described above. LOS are given letter designations from 'A' to 'F'. LOS 'A' represents the best operating conditions and LOS 'E' represents the level at which the intersection or an approach to the intersection is carrying the maximum traffic volume that can, practicably, be accommodated. LOS 'F' indicates that the intersection is operating beyond its theoretical capacity.

The City of Ottawa has developed criteria as part of the Transportation Impact Assessment Guidelines, which directly relate the volume to capacity (v/c) ratio of a signalized intersection to a LOS designation. These criteria are as follows:

| LOS | VOLUME TO CAPACITY RATIO (v/c) |
|-----|-----------------------------------|
| А | 0 to 0.60 |
| В | 0.61 to 0.70 |
| С | 0.71 to 0.80 |
| D | 0.81 to 0.90 |
| E | 0.91 to 1.00 |
| F | > 1.00 |

Table 13 - LOS Criteria for Signalized Intersections

The intersection capacity analysis technique provides an indication of the LOS for each movement at the intersection under consideration and for the intersection as a whole. The overall v/c ratio for an intersection is defined as the sum of equivalent volumes for all critical movements at the intersection divided by the sum of capacities for all critical movements.

The Level of Service calculation is based on locally-specific parameters as described in the TIA Guidelines and incorporates existing signal timing plans obtained from the City of Ottawa. The analysis existing conditions utilized a Peak Hour Factor (PHF) of 0.90, while future conditions considers optimized signal timing plans and use of a Peak Hour Factor (PHF) of 1.0 to recognize peak spreading beyond a 15-minute period in congested conditions.

5.9.2.2 Unsignalized Intersections

The capacity of an unsignalized intersection can also be expressed in terms of the LOS it provides. For an unsignalized intersection, the Level of Service is defined in terms of the average movement delays at the intersection. This is defined as the total elapsed time from when a vehicle stops at the end of the queue until the vehicle departs from the stop line; this includes the time required for

a vehicle to travel from the last-in-queue position to the first-in-queue position. The average delay for any particular minor movement at the un-signalized intersection is a function of the capacity of the approach and the degree of saturation.

The Highway Capacity Manual 2010 (HCM), prepared by the Transportation Research Board, includes the following Levels of Service criteria for un-signalized intersections, related to average movement delays at the intersection, as indicated in **Table 14**.

Table 14 - LOS Criteria for Unsignalized Intersections

| LOS | DELAY (seconds) |
|-----|-----------------|
| А | <10 |
| В | >10 and <15 |
| С | >15 and <25 |
| D | >25 and <35 |
| E | >35 and <50 |
| F | >50 |

The unsignalized intersection capacity analysis technique included in the HCM and used in the current study provides an indication of the Level of Service for each movement of the intersection under consideration. By this technique, the performance of the unsignalized intersection can be compared under varying traffic scenarios, using the Level of Service concept in a qualitative sense. One unsignalized intersection can be compared with another unsignalized intersection using this concept. Level of Service 'E' represents the capacity of the movement under consideration and generally, in large urban areas, Level of Service 'D' is considered to represent an acceptable operating condition. Level of Service 'E' is considered an acceptable operating condition for planning purposes for intersections located within Ottawa's Urban Core the downtown and its vicinity). Level of Service 'F' indicates that the movement is operating beyond its design capacity.

5.9.3 Intersection Capacity Analysis

Following the established intersection capacity analysis criteria described above, the existing and future conditions are analyzed during the weekday peak hour traffic volumes derived in this study.

The following section presents the results of the intersection capacity analysis. All tables summarize study area intersection LOS results during the weekday morning and afternoon peak hour periods.

The Synchro output files have been provided in **Appendix J**.

5.9.3.1 Existing (2019) Traffic

An intersection capacity analysis has been undertaken using the Existing (2019) Traffic volumes presented in **Figure 3**, yielding the following results:

Table 15 - Intersection Capacity Analysis: Existing (2019) Traffic

| | | AM PEA | K HOUR | PM PEAK HOUR | |
|--|------------------------------|-----------|-----------------------------------|----------------------------------|-----------------------------------|
| INTERSECTION | INTERSECTION TRAFFIC CONTROL | | CRITICAL MOVEMENTS (V/C OR DELAY) | OVERALL LOS (V/C OR DELAY) | CRITICAL MOVEMENTS (V/C OR DELAY) |
| Fallowfield Road & O'Keefe Court / Cobble Hill Drive | Unsignalized | D (28.2s) | EBL (28.2s) | D (26.5s) | EBL (26.5s) |

Based on the above, the intersection of Fallowfield & O'Keefe/ Cobble Hill is operating at an acceptable level of service (LOS 'D' or better) under Existing Traffic conditions.

5.9.3.2 Future (2023) Background Traffic

An intersection capacity analysis has been undertaken using the Future (2023) Background Traffic volumes presented in **Exhibit 5**, yielding the following results:

Table 16 - Intersection Capacity Analysis: 2023 Background Traffic

| | | AM PEA | K HOUR | PM PEAK HOUR | |
|---------------------------------------|--------------------|----------------|-----------------------|----------------|-----------------------|
| INTERSECTION | TRAFFIC CONTROL | OVERALL LOS | CRITICAL MOVEMENTS | OVERALL LOS | CRITICAL MOVEMENTS |
| | | (V/C OR DELAY) | (V/C OR DELAY) | (V/C OR DELAY) | (V/C OR DELAY) |
| Fallowfield Road & O'Keefe Court / | Unsignalized | F (83.6s) | WBTRL (83.6s) | F (104.6s) | EBL (104.6s) |
| Cobble Hill Drive | Signalized | A (0.51) | WBTRL (0.56) | A (0.54) | EBL (0.60) |
| Lusk Street & O'Keefe Court | Unsignalized | A (8.5s) | NBRL (8.5s) | A (9.2s) | NBRL (9.2s) |
| Fallowfield Road & Forager Street | Unsignalized | B (13.8s) | EBR (13.8s) | B (14.7s) | EBR (14.7s) |

By 2023, it is expected that the Fallowfield & O'Keefe/ Cobble Hill intersection will operate over its theoretical capacity as a stop-controlled intersection under background traffic conditions. Analysis indicates that signalization of the intersection will be required to achieve an acceptable level of service (LOS 'D' or better) during the weekday morning and afternoon peak hours.

The intersections of Lusk Street & O'Keefe Court and Fallowfield Road & Forager Street were shown to operate at Level of Service 'C' or better as two-way stop-controlled intersections, which is well within acceptable standards.

5.9.3.3 Future (2028) Background Traffic

An intersection capacity analysis has been undertaken using the Future (2028) Background Traffic volumes presented in **Exhibit 6**, yielding the following results:

Table 17 - Intersection Capacity Analysis: 2028 Background Traffic

| | | AM PEA | K HOUR | PM PEA | PM PEAK HOUR | |
|--|--------------------|----------------|--------------------|----------------|-----------------------|--|
| INTERSECTION | TRAFFIC CONTROL | OVERALL LOS | CRITICAL MOVEMENTS | OVERALL LOS | CRITICAL MOVEMENTS | |
| | | (V/C OR DELAY) | (V/C OR DELAY) | (V/C OR DELAY) | (V/C OR DELAY) | |
| Fallowfield Road & O'Keefe Court / Cobble Hill Drive | Signalized | A (0.59) | SBT (0.60) | A (0.59) | EBL (0.60) | |
| Lusk Street & O'Keefe Court | Unsignalized | A (8.5s) | NBRL (8.5s) | A (9.2s) | NBRL (9.2s) | |
| Fallowfield Road & Forager Street | Unsignalized | C (16.8s) | EBR (16.8s) | C (15.8s) | EBR (15.8s) | |

All study area intersections are expected to operate acceptably (LOS 'D' or better) under Future (2028) Background Traffic conditions, with the Fallowfield Road & O'Keefe Court / Cobble Hill Drive intersection signalized.

5.9.3.4 Future (2023) Total Traffic

An intersection capacity analysis has been undertaken using the Future (2023) Total Traffic volumes presented in **Exhibit 7**, yielding the following results:

Table 18 - Intersection Capacity Analysis: 2023 Total Traffic

| | | AM PEA | K HOUR | PM PEAK HOUR | | |
|--|--------------------|----------------|-----------------------|----------------|-----------------------|--|
| INTERSECTION | TRAFFIC CONTROL | OVERALL LOS | CRITICAL MOVEMENTS | OVERALL LOS | CRITICAL MOVEMENTS | |
| | | (V/C OR DELAY) | (V/C OR DELAY) | (V/C OR DELAY) | (V/C OR DELAY) | |
| Fallowfield Road & O'Keefe Court / Cobble Hill Drive | Signalized | A (0.51) | WBTRL (0.56) | A (0.56) | EBL (0.62) | |
| Lusk Street & O'Keefe Court | Unsignalized | A (8.5s) | NBRL (8.5s) | A (9.3s) | NBRL (9.3s) | |
| Fallowfield Road & Forager Street | Unsignalized | B (13.8s) | EBR (13.8s) | B (14.8s) | EBR (14.8s) | |

Based on the above results, all study area intersections are expected to operate at Level of Service 'B' or better with the addition of site-generated traffic, provided that the intersection of Fallowfield Road & O'Keefe Court / Cobble Hill Drive is signalized.

5.9.3.5 Future (2028) Total Traffic

An intersection capacity analysis has been undertaken using the Future (2028) Total Traffic volumes presented in **Exhibit 8**, yielding the following results:

Table 19 - Intersection Capacity Analysis: 2028 Total Traffic

| | | AM PEA | K HOUR | PM PEAK HOUR | | |
|--|--------------------|----------------|-----------------------|----------------|-----------------------|--|
| INTERSECTION | TRAFFIC CONTROL | OVERALL LOS | CRITICAL MOVEMENTS | OVERALL LOS | CRITICAL MOVEMENTS | |
| | | (V/C OR DELAY) | (V/C OR DELAY) | (V/C OR DELAY) | (V/C OR DELAY) | |
| Fallowfield Road & O'Keefe Court / Cobble Hill Drive | Signalized | A (0.59) | SBT (0.60) | B (0.62) | SBT (0.65) | |
| Lusk Street & O'Keefe Court | Unsignalized | A (8.5s) | NBRL (8.5s) | A (9.3s) | NBRL (9.3s) | |
| Fallowfield Road & Forager Street | Unsignalized | C (16.8s) | EBR (16.8s) | C (16.0s) | EBR (16.0s) | |

All study area intersections are expected to operate at a Level of Service of 'C' or better under Future (2028) Total Traffic conditions without any additional intersection modifications beyond what was required to accommodate background traffic volumes.

5.9.4 Intersection Design (MMLOS)

Analysis of conditions for each mode has been conducted based on the methodology prescribed in the City of Ottawa Multi-Modal Level of Service Guidelines. The Level of Service for each mode has been calculated for each intersection where signals exist or are anticipated.

The Future (2028) Total Traffic intersection MMLOS results have been summarized in **Table 20**. Detailed analysis results for existing and future conditions are provided **Appendix H**.

Table 20 - Intersection MMLOS - Future Conditions

| | LEVEL OF SERVICE BY MODE | | | | | |
|--|--------------------------|-------------------------|-------------------|-------------------------|--|--|
| LOCATION | PEDESTRIAN (PLOS) | BICYCLE (BLOS) | TRANSIT (TLOS) | TRUCK (TkLOS) | | |
| INTERSECTIONS | | | | | | |
| Fallowfield Road & O'Keefe Court / Cobble Hill Drive | E (Target: C) | F (Target: C) | B (Target: D) | F (Target: E) | | |

5.9.4.1 Summary of Potential Improvements

Based on the MMLOS results outlined in **Table 20** above, the following measures have been identified that could improve conditions for each travel mode:

Pedestrians

The PLOS at intersections is based on several factors including the number of traffic lanes that pedestrians must cross, corner radii, and whether the crossing allows for permissive or protective right or left turns, among others. The City of Ottawa minimum target for PLOS is 'C'.

The results of the analysis indicate that the intersection of Fallowfield Road & O'Keefe Court / Cobble Hill Drive is expected to experience a PLOS of 'E' primarily due to the level of traffic exposure pedestrians crossing the north/south approaches will experience in combination with the

pedestrian delays. Providing enhanced pedestrian features such as a median, pedestrian leading interval, zebra stripe high-visibility crosswalk markings on the north and south approaches would reduce the level of pedestrian exposure on those crossings. The above features in combination with a reduced cycle length from the standard length of 120s to 70s would achieve a PLOS of 'C'. It should be noted, however, that a reduction in the cycle length may result in negative impacts to the vehicle level of service. Alternatively, design of the intersection as a 'protected intersection' will help attain the PLOS target.

Cyclists

The BLOS at intersections is dependent on several factors: the number of lanes that the cyclist is required to cross to make a left-turn; the presence of a dedicated right-turn lane on the approach; and the operating speed of each approach. The City target for BLOS is 'C'.

The results of the analysis indicate that cycling facilities at the Fallowfield Road & O'Keefe Court / Cobble Hill Drive intersection are not sufficient to achieve the BLOS target. Given the high operating speeds at this location, only the provision of physically separated cycling facilities with two-stage, left-turn bike boxes on all approaches will be sufficient to achieve the BLOS target. Alternatively, design of the intersection as a 'protected intersection' will help attain the BLOS target.

Transit

Intersection TLOS is based on the average signal delay experienced by transit vehicles at each intersection. The City Target TLOS is 'D'.

The results of the analysis indicate that the eastbound and westbound approaches are expected to experience average delays between 20 and 45 seconds during the weekday peak hours, however as there are no transit routes that utilize either approach, neither is factored into the TLOS calculation. Both the northbound and southbound approaches do currently serve as transit routes and are expected to experience minimal average delays of 10s or less, therefore the overall intersection TLOS is 'B' and well within the City's target.

Trucks

The Truck LOS (TkLOS) is based on the right-turn radii, as well as the number of receiving lanes for vehicles making a right-turn from the traffic lane being analyzed. The City of Ottawa target for TKLOS is 'E'.

Overall, the intersection TkLOS target is not attainable as a result of the tight right-turn radii to/from Cobble Hill Drive. Turning movement count data indicates that trucks infrequently utilize Cobble Hill, which is consistent with its classification as a local road and non-truck route. Given that its primary function is to provide access to adjacent residential subdivisions, the substandard right-turn radii is considered acceptable in this context. It should be noted that the right-turn radii to/from O'Keefe Court meets the TkLOS target, which is appropriate given that the Highway 416 Lands development is classified is expected to generate regular truck traffic.

The recommended measures listed above are intended only as suggestions to the City on how the MMLOS within the study area could be improved and do not identify measures to be implemented as a direct consequence of this development. The remediation measures described above would improve mobility and comfort for cyclists but are not required to accommodate the proposed development.

5.10 Geometric Review

The following section provides a review of all geometric requirements for the study area intersections.

5.10.1 Sight Distance and Corner Clearances

The Lusk Street site access driveway is located on the outside of a horizontal curve which should afford this access favorable sightlines upstream and downstream of the intersection, while the Forager Street site access driveway is located on a short, straight segment with no significant horizontal or vertical curves. Despite its curvilinear alignment, the Lusk Street access allows for visibility in excess of the 85-metre distance required by TAC for road with a 60km/h design speed. Given that Forager Street is approximately 80m in length, vehicular are not expected to reach high operating speeds (i.e. 60 km/h) within such a short distance. Provided that vegetation is kept clear of the intersection sightlines, sight distances and corner clearances are not expected to be a concern for either of the proposed development's site access driveways.

5.10.2 Auxiliary Lane Analyses

Auxiliary turning lane requirements for all study area intersections are described as follows:

5.10.2.1 Auxiliary Left-Turn Lane Requirements (Unsignalized)

The intersection of O'Keefe Court & Lusk Street does not warrant a left-turn lane based on the advancing and opposing volumes projected at this intersection under Future (2028) Total Traffic conditions.

The future intersection configuration per the approved RMA will restrict the Fallowfield & Forager intersection to right-in/ right-out movements, therefore it was not necessary to assess left-turn lane requirements at this intersection.

The results of the left-turn lane warrant analysis are provided in **Appendix K**.

5.10.2.2 Auxiliary Left-Turn Lane Requirements (Signalized)

A review of auxiliary left-turn lane storage requirements was completed at all signalized intersections within the study area under Future (2028) Total Traffic conditions. The review compared the projected 95th percentile queue lengths from Synchro operational results, and the standard queue length calculation based on the following equation:

$$Storage\ Length = \frac{NL}{C} \times 1.5$$

Where:

N = number of vehicles per hour

L = Length occupied by a vehicle in the queue = 7 m

C = number of traffic signal cycles per hour

The results of the auxiliary left-turn lane analysis are summarized below in **Table 21** below.

Table 21 - Auxiliary Left-Turn Storage Analysis at Signalized Intersections

| INTERSECTION | APPROACH | 95TH %ILE QUEUE LENGTH (M) | CALCULATED QUEUE LENGTH (M) | EXISTING PARALLEL LENGTH (M) | STORAGE DEFICIENCY (M) |
|--------------------------------------|----------|-------------------------------------|-----------------------------------|------------------------------------|---|
| | NB | 5 | 10 | 140 | Existing Storage Adequate |
| Fallowfield Road & | SB | 5 | 0 | 60 | Existing Storage Adequate |
| O'Keefe Court / Cobble Hill Drive | EB | 25 | 10 | 50 | Existing Storage Adequate |
| | WB | 30¹ | 5 | - | Existing Storage Adequate ² |

Notes: ¹ Synchro queues were determined based on existing shared lane configuration ² Through volumes are nominal during weekday peak hours (i.e. less than 10 veh/h)

As per the results of the queue length analyses presented

April 9, 2020 41 **Table** 21 above, the existing parallel lanes have sufficient storage to accommodate the projected Future (2028) Total Traffic demand. No modifications to the existing auxiliary lanes are required within the timeframe of this study.

Synchro results indicate that with the existing shared through-left configuration, queue lengths during the weekday peak hours would be at most 16 and 27 metres on the eastbound and westbound approaches, respectively, under Future (2028) Total Traffic conditions. Queue lengths of this magnitude can be considered within an acceptable range for spillback on a through lane given the nominal through volumes of less than 10 vehicles per hour expected on these movements during the weekday peak hours.

5.10.2.3 Auxiliary Right-Turn Lane Requirements (Unsignalized)

The Transportation Association of Canada (TAC) suggests that auxiliary right-turn lanes be considered "when the volume of decelerating or accelerating vehicles compared with through vehicles causes undue hazard." Consideration for auxiliary right-turn lanes is typically given when the right-turning traffic exceeds 10% of the through volume and is at least 60 vehicles per hour.

The RMA for the Fallowfield/ Forager intersection has been designed with a parallel lane that includes sufficient deceleration length. No storage is required on this lane.

5.10.2.4 Auxiliary Right-Turn Lane Requirements (Signalized)

Similarly for signalized intersections, Section 9.14 of TAC suggests that auxiliary right-turn lanes shall be considered when more than 10% of vehicles on an approach are turning right and when the peak hour demand exceeds 60 vehicles. The purpose of this guideline is to mitigate operational impacts to through-traffic, particularly on high-speed arterial roadways such as Fallowfield Road, and may not be applicable in all circumstances.

The results of the auxiliary right-turn lane analysis are summarized in Table 22 below:

Table 22 – Auxiliary Right-Turn Lane Storage Analysis at Signalized Intersections

| INTERSECTION | APPROACH | RIGHT TURN VOLUME | APPROACH VEHICLES TURNING RIGHT (%) | 95TH %ILE QUEUE LENGTH (M) | EXISTING PARALLEL LENGTH (M) | STORAGE DEFICIENCY (M) |
|---|----------|-------------------------|-------------------------------------|-------------------------------------|------------------------------------|--|
| Fallowfield Road & O'Keefe Court/ Cobble Hill Drive | NB | 23 | 3% | <10 | 115 | Existing Storage Adequate |
| | SB | 88 | 9% | <10 | 25 | Existing Storage Adequate |
| | EB | 114 | 51% | 201 | - | Existing Storage Adequate ² |
| | WB | 42 | 48% | 30¹ | - | Existing Storage Adequate ² |

Notes: 1 Synchro queues were determined based on existing shared lane configuration

Although the eastbound and westbound approaches technically meet the criteria for a right-turn lane, the through volumes on these approaches were observed to be nominal (i.e. 10 vehicles or less) during the weekday peak hours. Synchro results indicate that with the existing shared through-right configuration, queue lengths during the weekday peak hours would be at most 16 and 27 metres on the eastbound and westbound approaches, respectively, under Future (2028) Total Traffic conditions. Queue lengths of this magnitude can be considered within an acceptable range for spillback on a through lane given the nominal through volumes expected. Further, the right-turn criteria is typically more applicable along high-speed arterial roads and is not considered appropriate in this context.

Based on the traffic volumes projections developed for this TIA, no additional right-turn facilities are required as a result of projected background or site-generated volumes at signalized study area intersections.

5.11 Summary of Improvements Indicated and Modification Options

As per the intersection capacity, Multi-Modal Level of Service and auxiliary lane analyses results presented above, off-site improvements to the adjacent road network have been recommended in order to accommodate the transportation demands of both background and site-generated traffic. The MMLOS results indicate existing deficiencies with respect user comfort and safety that could be considered for implementation by the City but are not required to safely accommodate the proposed development.

5.11.1 Fallowfield Road & O'Keefe Court/ Cobble Hill Drive

The intersection of Fallowfield & O'Keefe/ Cobble Hill is presently operating as a two-way stop-controlled intersection. The results of the analysis indicates that, by 2023, traffic signals will be operationally required under background traffic conditions, however traffic signals are not warranted within the timeframe of this study. As indicated in **Exhibit 4**, the proposed development

² Through volumes are nominal during weekday peak hours (i.e. less than 10 veh/h)

is only expected to contribute nominal volumes at this intersection. With traffic signals in place, the intersection would be expected to operate at an acceptable level of service (i.e. LOS 'B') under Future (2028) Total Traffic conditions. It is recommended that the City monitor this intersection on an annual basis to determine the appropriate timing for its signalization.

An analysis of auxiliary lane requirements found that auxiliary lane storage at this intersection is sufficient and can accommodate future travel demands within the context of this study.

Based on the MMLOS analysis, in order to meet the Pedestrian Level of Service and Bicycle Level of Service targets, various measures would need to be implemented. To attain the PLOS target, zebra stripe high-visibility crosswalk markings, a pedestrian leading interval and a median on the northbound/ southbound approaches are required in conjunction with a reduce cycle length to satisfy the Pedestrian Delay Evaluation. The implementation of bike lanes or higher-order cycling facilities on all approaches, along with two-stage, left-turn bike boxes are required to meet the BLOS targets. Alternatively, design of the intersection as a 'protected intersection' with fully-integrated pedestrian and cycling facilities will help attain the PLOS and BLOS targets. These features should be considered by the City upon signalization of this intersection but are not required to accommodate the proposed development.

5.11.2 O'Keefe Court & Lusk Street

O'Keefe Court & Lusk Street is a new three-legged intersection that is expected to operate at a high level of service (i.e. LOS 'A') beyond the horizon year of this study with stop control on Lusk Street and free-flow along O'Keefe Court.

Analysis indicated that left- or right-turn auxiliary lanes are not required on any of the intersection approaches within the timeframe of this study.

5.11.3 Fallowfield Road & Forager Street

Fallowfield Road & Forager Street is a new three-legged intersection with an approved RMA intended to restrict movements to right-in/right-out. With these turning restrictions in place, the intersection is anticipated to operate at LOS 'C' or better within the timeframe of this study.

6 Conclusion

The proposed restaurant and medical office development at 115 Lusk Street is expected to generate up to 13 and 32 two-way vehicular trips during the weekday morning and afternoon peak hours, respectively. These traffic volumes were distributed amongst two site access driveways, representing a marginal increase in traffic volumes with respect to the overall traffic projections expected within the 2028 study horizon year. The mode share targets were based on the South Nepean Traffic Assessment Zone (TAZ) and proportionally adjusted, in accordance with the Conditions of Approval for 4401 Fallowfield Road to yield an 85% auto/ 15% non-auto mode share split. It should also be noted that this study did not apply any pass-by reductions factors to the restaurant's trip generation, as it was determined that the overall impact on the adjacent road network would be minimal.

The intersection of Fallowfield & O'Keefe/ Cobble Hill is presently operating as a two-way stop controlled intersection. The results of the analysis indicate that, by 2023, traffic signals will be operationally required under background traffic conditions, however signals are not warranted within the timeframe of this study. With traffic signals in place, the intersection would be expected to operate at LOS 'B' beyond the study horizon year. As site-generated traffic will not contribute significantly to any potential traffic operational issues at this intersection, it is recommended that the City continue monitoring this intersection on an annual basis to determine the appropriate timing for the introduction of traffic signals.

The results of the analysis indicate that the intersections of O'Keefe Court & Lusk Street and Fallowfield Road & Forager Street are expected to operate within acceptable standards (LOS 'D' or better) during the weekday morning and afternoon peak hours. Both are T-intersections that are configured with stop control on the minor road and do not warrant auxiliary lanes or future modifications to intersection control within the timeframe of this study.

A multi-modal analysis identifies deficiencies in the existing road network and potential remediation measures have been suggested in which the City could consider to meet these prescribed targets. It should be noted that, although these measures would improve for a range of transportation modes, they are not required to safely accommodate the transportation demands of the proposed development.

A Roadway Modification Application (RMA-2019-TPD-041B) was recently approved to satisfy a conditional requirement for the 4401 Fallowfield Road Subdivision. The RMA includes the right-in/right-out intersection at Fallowfield Road & Forager Street, a multi-use pathway along the west side of Fallowfield Road and a southbound bus stop on Fallowfield Road near the O'Keefe Court intersection. As there is already an approved RMA intended to address the implementation of the above noted design elements and no off-site geometric improvements are required as a direct result of the proposed development, an RMA will not be included with the submission of this Transportation Impact Assessment.

All study area intersections were shown to operate well within the capacity constraints of the adjacent transportation network, with the appropriate modifications in place (i.e. signalization of Fallowfield & O'Keefe/ Cobble Hill by 2023). Further, the proposed development will contribute a negligible volume of traffic to the adjacent road network. A post-development Monitoring Plan is, therefore, <u>not</u> a requirement of this study.

Based on the findings of this study, it is the overall opinion of IBI Group that the proposed development will integrate well with and can be safely accommodated by the adjacent transportation network with the recommended actions and modifications in place.

Appendix A – City Circulation Comments

April 9, 2020

Step 1 & 2 Submission (Screening & Scoping) – Circulation Comments & Response

Report Submitted: October 29, 2019 Comments Received: November 1, 2019

Transportation Project Manager: Josiane Gervais

Module 2.3 - Exceptions Review

Table 4: Possible Exemptions

| Module | Element | Exe | mption Considerations |
|--------------------------------------|--------------|---------------|--|
| 4.5 Transportation Demand Management | All elements | fewer than 60 | for non-residential site plans expected to have employees and/or students on location at e — Please confirm how many employees are r the site. |

- > The exact number of employees envisioned for the site is not available yet. However, the ITE Parking Generation Manual (4th Edition) provides average employee densities for a variety of land uses. The average employee densities relevant to this site are as follows:
 - o Office (ITE Land Use 701): 3.4 employees / 1000 ft²
 - O Quality Restaurant (ITE Land Use 931): 4.2 employees / 1000 ft²
 The medical office and restaurant will be 600 m² (6458 ft²) and 300 m² (3229 ft²), respectively, which, when multiplied by their respective employee densities, results in a total of 36 employees for both land uses combined. The Transportation Demand Management module is therefore exempt from the study.

Step 3 Submission (Forecasting) - Circulation Comments & Response

Report Submitted: December 31, 2019 Comments Received: January 17, 2020

Transportation Project Manager: Josiane Gervais

Transportation Engineering Services

- Consider increasing the walking mode share at ultimate build-out (while staying below the 15% non-auto mode outlined within the subdivision conditions). Once O'Keefe/Fallowfield is signalized, there may be a few more walking trips to the development.
 - ➢ IBI Response: The mode share targets for 2023 and 2028 have been separated, with the 2028 analysis year adjusted to reflect a higher pedestrian mode share anticipated by this time. The 15% non-auto mode share target in 2028 will be stratified as follows: 2% transit, 0% cycling, 13% walking and 0% other mode share target. The mode share targets for 2023 have not been modified.
- Provide the number of trips from the other developments in a table.
 - ➤ IBI Response: A table has been added in Section 4.2.3 summarizing the number of trips generated by each adjacent development.

Traffic Signal Operations

No comments.

Development Review Transportation

• No comments.

Appendix B – Screening Form



City of Ottawa 2017 TIA Guidelines Screening Form

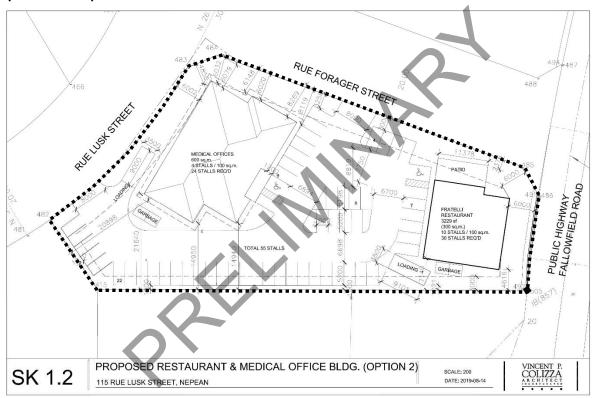
1. Description of Proposed Development

| Municipal Address | 115 Lusk Street |
|--------------------------|---|
| Description of Location | South Nepean – North of Strandherd Drive, West of Fallowfield Road and east of Highway 416 |
| | O. Keels Count. Strandherd Drive |
| Land Use Classification | Quality Restaurant and Medical Office |
| Development Size (units) | N/A |
| Development Size (m²) | Quality Restaurant – 300 m ² |
| | Medical Office – 600 m ² |
| Number of Accesses and | One (1) access off of Lusk Street |
| Locations | One (1) access off of Forager Street |
| Phase of Development | Single Phase |
| Buildout Year | 2023 (Assumed) |

If available, please attach a sketch of the development or site plan to this form.



Proposed Development:





2. Trip Generation Trigger

Considering the Development's Land Use type and Size (as filled out in the previous section), please refer to the Trip Generation Trigger checks below.

| Land Use Type | Minimum Development Size |
|-------------------------------------|--------------------------|
| Single-family homes | 40 units |
| Townhomes or apartments | 90 units |
| Office | 3,500 m ² |
| Industrial | 5,000 m ² |
| Fast-food restaurant or coffee shop | 100 m ² |
| Destination retail | 1,000 m² |
| Gas station or convenience market | 75 m ² |

^{*} If the development has a land use type other than what is presented in the table above, estimates of person-trip generation may be made based on average trip generation characteristics represented in the current edition of the Institute of Transportation Engineers (ITE) Trip Generation Manual.

Preliminary trip generation estimates were calculated based on average trip generation characteristics derived from the applicable land indicated in the Institute of Transportation Engineers (ITE) Trip Generation (10th Edition), the Quality Restaurant land use (931) and Medical-Dental Office Building land use (720). The 1.28 person-trip conversion factor recommended in the TIA Guidelines was applied to the base trip generation results to obtain the equivalent person-trip generation.

As indicated below, trip generation may slightly exceed the 60 person-trip threshold during the weekday afternoon peak hour, therefore the trip generation trigger is satisfied.

| Baseline Vehicle Trips | | | | | | | | | | | |
|--|-------|-------------|---------------|-----|-----------|-------|-----|-----------|-------|--|--|
| | | | | 1 | AM Peak H | our | | PM Peak H | lour | | |
| ITE Land Use | Units | Size | | In | Out | Total | ln | Out | Total | | |
| 720: Medical-Dental Office Bldg | ft2 | 6458.35 | Equation: | | T=2.78*X | | | T=3.46*X | | | |
| | | % C | Distribution: | 62% | 38% | 100% | 39% | 61% | 100% | | |
| | | Baseline Ve | hicle Trips: | 11 | 7 | 18 | 9 | 14 | 22 | | |
| 931: Quality Restaurant | ft2 | 3229.17 | Equation: | | T=0.73*X | | | T=7.80* | X | | |
| | | % E | Distribution: | 50% | 50% | 100% | 67% | 33% | 100% | | |
| | | Baseline Ve | hicle Trips: | 1 | 1 | 2 | 17 | 8 | 25 | | |
| | | | Subtotal: | 12 | 8 | 20 | 26 | 22 | 48 | | |
| Note: Directional distribution is not p Person Trips | | | | | | | | | | | |
| | | | | ı | AM Peak H | our | | PM Peak H | lour | | |
| ITE Land Use | | | | In | Out | Total | In | Out | Total | | |
| 720: Medical-Dental Office Bldg | | Convers | sion Factor | 1.2 | 28 | | 1. | 28 | | | |
| | | | | 14 | 9 | 23 | 11 | 17 | 29 | | |
| | | 0 | | 1.2 | 20 | | 1 | 28 | | | |
| 931: Quality Restaurant | | Convers | sion Factor | 1.2 | 20 | | | | | | |
| 931: Quality Restaurant | | Convers | sion Factor | 2 | 2 | 3 | 22 | 11 | 32 | | |



Transportation Impact Assessment Screening Form

3. Location Triggers

| | Yes | No |
|--|-----|----------|
| Does the development propose a new driveway to a boundary street that is designated as part of the City's Transit Priority, Rapid Transit or Spine Bicycle Networks? | | ✓ |
| Is the development in a Design Priority Area (DPA) or Transit-oriented Development (TOD) zone?* | | ✓ |

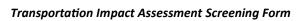
^{*}DPA and TOD are identified in the City of Ottawa Official Plan (DPA in Section 2.5.1 and Schedules A and B; TOD in Annex 6). See Chapter 4 for a list of City of Ottawa Planning and Engineering documents that support the completion of TIA).

Based on the results above, the Location Trigger is <u>NOT</u> satisfied.

4. Safety Triggers

| | Yes | No |
|---|-----|--------------|
| Are posted speed limits on a boundary street are 80 km/hr or greater? | | \checkmark |
| Are there any horizontal/vertical curvatures on a boundary street limits sight lines at a proposed driveway? | | ✓ |
| Is the proposed driveway within the area of influence of an adjacent traffic signal or roundabout (i.e. within 300 m of intersection in rural conditions, or within 150 m of intersection in urban/ suburban conditions)? | | ✓ |
| Is the proposed driveway within auxiliary lanes of an intersection? | | \checkmark |
| Does the proposed driveway make use of an existing median break that serves an existing site? | | ✓ |
| Is there is a documented history of traffic operations or safety concerns on the boundary streets within 500 m of the development? | | ✓ |
| Does the development include a drive-thru facility? | | ✓ |

Based on the results above, the Safety Trigger is NOT satisfied.





5. Summary

| | Yes | No |
|---|----------|----------|
| Does the development satisfy the Trip Generation Trigger? | √ | |
| Does the development satisfy the Location Trigger? | | ✓ |
| Does the development satisfy the Safety Trigger? | | ✓ |

CONCLUSION: The Trip Generation Trigger is satisfied, therefore a TIA is required.

Appendix C – Traffic Data

Survey Date: Tuesday January 30 2018
Weather: Sunny

TURNING MOVEMENT COUNT SUMMARY - ALL MODES

IBI

 AM Peak Hour:
 8:00 AM
 to
 9:00 AM

 MD Peak Hour:
 12:15 PM
 to
 1:15 PM

 PM Peak Hour:
 4:30 PM
 to
 5:30 PM

AADT FACTOR: 1.1

| | | | | | | | Turnir | ng Mov | /emer | nt Coun | t - Ful | ll Study | y Sumi | mary F | Report | (Vehic | les) | | | | | | | |
|-----------------|----------|--------------------|------------------------|--|----------------------|----------------------|---------------------|-----------------------|---------------------------------|--------------------|-------------|---------------|-------------|--------|------------|---------|-------------|-----|-----|--------------------------------|---------|-------------|---------------|--------|
| Time I | Dovind | | | <mark>lowfield Ro</mark> Iorthbound | | | | | llowfield R Southbour | | | N/S STREET | | (| O'Keefe Co | | | | (| O'Keefe Cou Westboun | | | E/W STREET | Grand |
| Time i | renoa | LT | ST | RT | U-Turns | NB TOTAL | LT | ST | RT | U-Turns | SB TOTAL | TOTAL | LT | ST | RT | U-Turns | EB TOTAL | LT | ST | RT | U-Turns | WB TOTAL | TOTAL | TOTAL |
| 7:00 | 8:00 | 3 | 488 | 12 | 0 | 503 | 9 | 288 | 3 | 1 | 301 | 804 | 4 | 5 | 8 | 0 | 17 | 33 | 7 | 38 | 0 | 78 | 95 | 899 |
| 8:00 | 9:00 | 9 | 923 | 12 | 0 | 944 | 14 | 896 | 11 | 0 | 921 | 1865 | 6 | 12 | 22 | 0 | 40 | 78 | 12 | 82 | 0 | 172 | 212 | 2077 |
| 9:00 | 10:00 | 7 | 196 | 9 | 0 | 212 | 7 | 243 | 4 | 0 | 254 | 466 | 3 | 3 | 11 | 0 | 17 | 16 | 8 | 20 | 0 | 44 | 61 | 527 |
| AVG AN | VI Pk HR | 6 | 536 | 11 | 0 | 553 | 10 | 476 | 6 | 0 | 492 | 1045 | 4 | 7 | 14 | 0 | 25 | 42 | 9 | 47 | 0 | 98 | 123 | 1168 |
| 11:30 | 12:30 | 4 | 486 | 9 | 0 | 499 | 5 | 205 | 2 | 0 | 212 | 711 | 2 | 4 | 12 | 0 | 18 | 17 | 4 | 17 | 0 | 38 | 56 | 767 |
| 12:30 | 13:30 | 3 | 923 | 14 | 0 | 940 | 10 | 388 | 14 | 0 | 412 | 1352 | 8 | 5 | 12 | 0 | 25 | 15 | 14 | 29 | 0 | 58 | 83 | 1435 |
| AVG MI | D Pk HR | 4 | 705 | 12 | 0 | 720 | 8 | 297 | 8 | 0 | 312 | 1032 | 5 | 5 | 12 | 0 | 22 | 16 | 9 | 23 | 0 | 48 | 70 | 1101 |
| 15:00 | 16:00 | 8 | 869 | 14 | 0 | 891 | 87 | 461 | 9 | 0 | 557 | 1448 | 3 | 3 | 9 | 0 | 15 | 13 | 2 | 23 | 0 | 38 | 53 | 1501 |
| 16:00 | 17:00 | 8 | 814 | 16 | 0 | 838 | 16 | 564 | 6 | 0 | 586 | 1424 | 6 | 2 | 12 | 1 | 21 | 10 | 2 | 21 | 0 | 33 | 54 | 1478 |
| 17:00 | 18:00 | 25 | 239 | 7 | 0 | 271 | 48 | 1073 | 11 | 0 | 1132 | 1403 | 11 | 5 | 26 | 1 | 43 | 19 | 1 | 40 | 0 | 60 | 103 | 1506 |
| AVG PN | M Pk HR | 14 | 641 | 12 | 0 | 667 | 50 | 699 | 9 | 0 | 758 | 1425 | 7 | 3 | 16 | 1 | 26 | 14 | 2 | 28 | 0 | 44 | 70 | 1495 |
| TO ⁻ | TAL | 77 | 6,178 | 116 | 0 | 6,371 | 214 | 4,890 | 74 | 1 | 5,179 | 11,550 | 52 | 50 | 138 | 2 | 242 | 259 | 68 | 340 | 0 | 667 | 909 | 12,459 |
| EQ 1 | 12Hr | 107 | 8588 | 161 | 0 | 8855 | 297 | 6797 | 103 | 2 | 7199 | 16054 | 73 | 70 | 191 | 3 | 337 | 360 | 95 | 472 | 0 | 927 | 1264 | 17318 |
| | Note: | These volum | es are calcul | ated by mu | ltiplying the t | otals by the | appropriat | e expansion | factor. | | 1.39 | • | | | | | | | | | | | | |
| AVG | 12Hr | 117 | 9446 | 177 | 0 | 9740 | 326 | 7477 | 113 | 2 | 7919 | 17659 | 80 | 77 | 210 | 3 | 370 | 397 | 104 | 519 | 0 | 1020 | 1390 | 19049 |
| | Note: | These volum | es are calcul | ated by mu | ltiplying the E | quivalent 1 | 2 hr. totals | by the AAD | T factor. | | 1.1 | 1 | | | | | | | | | | | | |
| AVG | | 154 These volum | 12375 es are calcul | 231 ated by mu | 0 Itiplying the A | 12760 werage Dail | 428 y 12hr. tota | 9795 als by the 12 | 148 2 to 24 exp | 3 ansion factor | 10373 | 23134 | 105 1.31 | 100 | 276 | 4 | 485 | 519 | 136 | 680 | 0 | 1336 | 1821 | 24955 |

| | | T | urning Movement Count - Full | Study S | fummary Report (Pedestrians) | | | |
|--------------|--------|-------------------------------------|-------------------------------------|-----------------|---------------------------------------|---------------------------------------|-------|-------|
| T : a | Daviad | Fallowfield Road | Fallowfield Road | N/S | O'Keefe Court | O'Keefe Court | E/W | Grand |
| Time | Period | NB Approach (East or West Crossing) | SB Approach (East or West Crossing) | STREET TOTAL | EB Approach (North or South Crossing) | WB Approach (North or South Crossing) | TOTAL | TOTAL |
| 7:00 | 8:00 | 0 | 0 | 0 | 0 | 1 | 1 | 1 |
| 8:00 | 9:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:00 | 10:00 | 1 | 0 | 1 | 1 | 16 | 17 | 18 |
| 11:30 | 12:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:30 | 13:30 | 0 | 1 | 1 | 0 | 0 | 0 | 1 |
| 15:00 | 16:00 | 0 | 2 | 2 | 0 | 0 | 0 | 2 |
| 16:00 | 17:00 | 0 | 15 | 15 | 0 | 0 | 0 | 15 |
| 17:00 | 18:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TO | TAL: | 1 | 18 | 19 | 1 | 17 | 18 | 37 |

| | | Turning Movement Count - Fu | II Stud | y Summary Report (Cyclists) | | | |
|-------------|------------------|-----------------------------|---------|-----------------------------|---------------|-----|-------|
| Time Devied | Fallowfield Road | Fallowfield Road | N/S | O'Keefe Court | O'Keefe Court | E/W | Grand |

| Time | renou | Northbound | Southbound | TOTAL | Eastbound | Westbound | TOTAL | TOTAL |
|-------|-------|------------|------------|-------|-----------|-----------|-------|-------|
| 7:00 | 8:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 | 9:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:00 | 10:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:30 | 12:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:30 | 13:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15:00 | 16:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:00 | 17:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:00 | 18:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| тот | ΓAL: | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

| | | | | | | Tui | rning I | Moven | nent C | Count - | Full St | udy Su | mmar | y Repo | ort (He | eavy Ve | hicles) | | | | | | | |
|-------------|-------|----|--------------------------------|----|---------|-----------------------------|---------|-------|--------|---------|---------------|-----------|------|--------|---------|---------|-------------|----|---------------|-------|---------|-------------|-------|-------|
| Time Period | | | owfield Ro orthbound | | | Fallowfield Road Southbound | | | | | N/S STREET | Fasthound | | | | | | (| E/W STREET | Grand | | | | |
| Time | renou | LT | ST | RT | U-Turns | NB TOTAL | LT | ST | RT | U-Turns | SB TOTAL | TOTAL | LT | ST | RT | U-Turns | EB TOTAL | LT | ST | RT | U-Turns | WB TOTAL | TOTAL | TOTAL |
| 7:00 | 8:00 | 1 | 18 | 0 | 0 | 19 | 0 | 20 | 0 | 0 | 20 | 39 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 2 | 41 |
| 8:00 | 9:00 | 0 | 23 | 5 | 0 | 28 | 1 | 18 | 0 | 0 | 19 | 47 | 0 | 0 | 1 | 0 | 1 | 1 | 1 | 0 | 0 | 2 | 3 | 50 |
| 9:00 | 10:00 | 0 | 12 | 1 | 0 | 13 | 0 | 36 | 0 | 0 | 36 | 49 | 0 | 0 | 1 | 0 | 1 | 1 | 1 | 1 | 0 | 3 | 4 | 53 |
| 11:30 | 12:30 | 0 | 7 | 2 | 0 | 9 | 0 | 21 | 0 | 0 | 21 | 30 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 1 | 0 | 2 | 3 | 33 |
| 12:30 | 13:30 | 0 | 10 | 0 | 0 | 10 | 0 | 8 | 0 | 0 | 8 | 18 | 1 | 1 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 1 | 3 | 21 |
| 15:00 | 16:00 | 0 | 22 | 1 | 0 | 23 | 0 | 19 | 0 | 0 | 19 | 42 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 0 | 6 | 6 | 48 |
| 16:00 | 17:00 | 0 | 10 | 1 | 0 | 11 | 1 | 22 | 0 | 0 | 23 | 34 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 34 |
| 17:00 | 18:00 | 0 | 6 | 0 | 0 | 6 | 0 | 13 | 0 | 0 | 13 | 19 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 2 | 2 | 21 |
| TOT | TAL: | 1 | 108 | 10 | 0 | 119 | 2 | 157 | 0 | 0 | 159 | 278 | 1 | 2 | 3 | 0 | 6 | 4 | 4 | 9 | 0 | 17 | 23 | 301 |

Appendix D – OC Transpo Routes

April 9, 2020



179

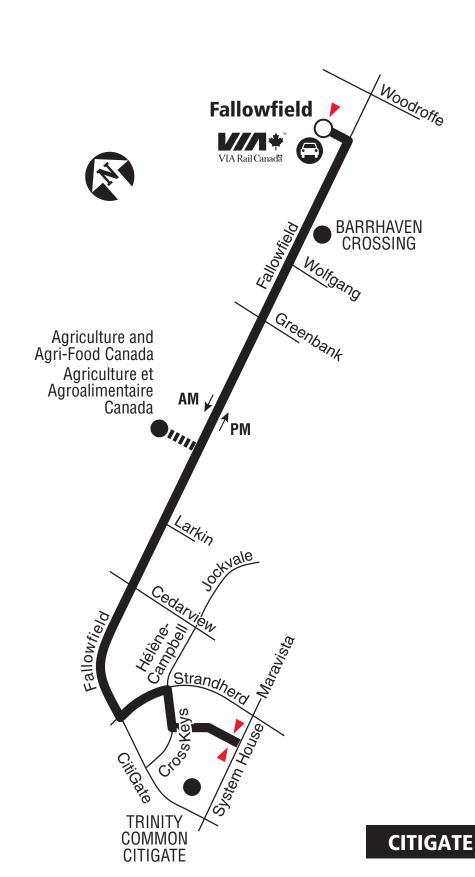
FALLOWFIELD CITIGATE

Local

Monday to Friday / Lundi au vendredi

Peak periods only Périodes de pointe seulement

FALLOWFIELD



0

Transitway & Station

Some trips / Quelques trajets
Park & Ride / Parc-o-bus



Timepoint / Heures de passage

2019.06



Security / Sécurité 613-741-2478

Effective June 25, 2017 En vigueur 25 juin 2017

C Transpo

INFO 613-741-4390 octranspo.com



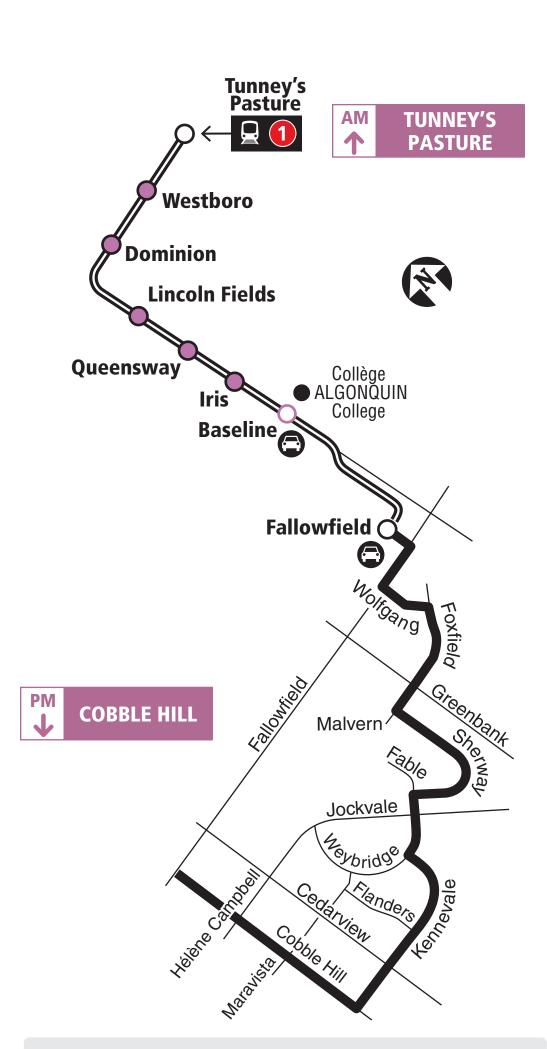


COBBLE HILL TUNNEY'S PASTURE

Connexion

Monday to Friday / Lundi au vendredi

Peak periods only Périodes de pointe seulement



Transitway & Station

Limited stops: Off only in AM / No stop in PM Arrêts limités : Débarquement en AM seul. /

Aucun arrêt en PM

AM: Off only - PM: Full Service

AM: Débarquement seul. - PM: Service complet

Park & Ride / Parc-o-bus

2019.07



Future route after O-Train Line 1 is open **Trajet du circuit après l'ouverture** de la Ligne 1 de l'O-Train

Lost and Found / Objets perdus...... **613-563-4011** Security / Sécurité 613-741-2478



INFO 613-741-4390 octranspo.com

Appendix E – Collision Data



City Operations - Transportation Services

Collision Details Report - Public Version

From: January 1, 2014 **To:** December 31, 2018

Location: CEDARVIEW RD @ FALLOWFIELD RD

Traffic Control: Traffic signal Total Collisions: 29

| Date/Day/Time | Environment | Impact Type | Classification | Surface Cond'n | Veh. Dir | Vehicle Manoeuver | Vehicle type | First Event | No. Ped |
|------------------------|-------------|------------------|----------------|-------------------|----------|---------------------|------------------------------|---------------------|---------|
| 2018-Aug-16, Thu,08:29 | Clear | Rear end | P.D. only | Dry | West | Going ahead | Automobile, station wagon | Other motor vehicle | |
| | | | | | West | Slowing or stopping | Automobile, station wagon | Other motor vehicle | |
| 2018-Jul-30, Mon,13:56 | Clear | Turning movement | P.D. only | Dry | South | Turning left | Automobile, station wagon | Other motor vehicle | |
| | | | | | North | Going ahead | Passenger van | Other motor vehicle | |
| 2018-Jul-09, Mon,11:21 | Clear | Rear end | P.D. only | Dry | South | Going ahead | Automobile, station wagon | Other motor vehicle | |
| | | | | | South | Stopped | Automobile, station wagon | Other motor vehicle | |
| 2018-Jun-22, Fri,08:35 | Clear | Turning movement | P.D. only | Dry | West | Slowing or stopping | Automobile, station wagon | Other motor vehicle | |
| | | | | | East | Turning left | Automobile, station wagon | Other motor vehicle | |
| 2018-Jun-14, Thu,08:35 | Rain | Rear end | P.D. only | Wet | East | Going ahead | Automobile, station wagon | Other motor vehicle | |
| | | | | | East | Slowing or stopping | Automobile, station wagon | Other motor vehicle | |
| 2018-May-22, Tue,08:18 | Clear | Turning movement | P.D. only | Dry | South | Turning left | Automobile, station wagon | Other motor vehicle | |

October 10, 2019 Page 1 of 11

| | | | | | North | Going ahead | Automobile, station wagon | Other motor vehicle |
|------------------------|-------|------------------|------------------|------------|-------|---------------------|------------------------------|---------------------|
| 2018-Jan-22, Mon,18:13 | Snow | Turning movement | P.D. only | Loose snow | East | | Automobile, station wagon | Other motor vehicle |
| | | | | | West | Turning left | Automobile, station wagon | Other motor vehicle |
| | | | | | East | Slowing or stopping | Automobile, station wagon | Other motor vehicle |
| 2017-Dec-18, Mon,22:05 | Snow | Sideswipe | Non-fatal injury | Loose snow | South | Changing lanes | Unknown | Other motor vehicle |
| | | | | | South | Going ahead | Passenger van | Other motor vehicle |
| 2017-Nov-04, Sat,11:29 | Clear | Turning movement | P.D. only | Dry | North | Turning left | Pick-up truck | Other motor vehicle |
| | | | | | South | Turning right | Automobile, station wagon | Other motor vehicle |
| 2017-Nov-02, Thu,16:27 | Rain | Rear end | P.D. only | Wet | West | Slowing or stopping | Automobile, station wagon | Skidding/sliding |
| | | | | | West | Stopped | Automobile, station wagon | Other motor vehicle |
| 2017-Mar-21, Tue,17:18 | Clear | Rear end | P.D. only | Wet | South | Slowing or stopping | Automobile, station wagon | Other motor vehicle |
| | | | | | South | Stopped | Pick-up truck | Other motor vehicle |
| 2017-Feb-15, Wed,18:11 | Snow | Angle | P.D. only | Loose snow | South | Turning left | Automobile, station wagon | Other motor vehicle |
| | | | | | West | Going ahead | Snow plow | Other motor vehicle |

October 10, 2019 Page 2 of 11

| 2017-Jan-27, Fri,16:46 | Snow | Turning movement | Non-fatal injury | Wet | East | Turning left | Automobile, station wagon | Other motor vehicle |
|------------------------|-------|------------------|------------------|-------|-------|---------------------|---------------------------|---------------------|
| | | | | | West | Going ahead | Automobile, station wagon | Other motor vehicle |
| 2016-Jun-27, Mon,14:50 | Clear | Angle | P.D. only | Dry | East | Turning right | Automobile, station wagon | Other motor vehicle |
| | | | | | South | Unknown | Unknown | Other motor vehicle |
| 2016-Feb-25, Thu,18:49 | Snow | Rear end | Non-fatal injury | Slush | North | Slowing or stopping | Automobile, station wagon | Other motor vehicle |
| | | | | | North | Stopped | Automobile, station wagon | Other motor vehicle |
| 2016-Feb-22, Mon,13:47 | Clear | Sideswipe | Non-fatal injury | Dry | North | Changing lanes | Passenger van | Other motor vehicle |
| | | | | | North | Turning left | Automobile, station wagon | Other motor vehicle |
| 2016-Jan-11, Mon,17:30 | Clear | Other | P.D. only | Wet | North | Reversing | Automobile, station wagon | Other motor vehicle |
| | | | | | South | Stopped | Automobile, station wagon | Other motor vehicle |
| 2016-Jan-06, Wed,07:26 | Clear | Turning movement | P.D. only | Dry | South | Turning left | Passenger van | Other motor vehicle |
| | | | | | North | Going ahead | Pick-up truck | Other motor vehicle |
| 2015-Oct-31, Sat,01:40 | Clear | Turning movement | P.D. only | Dry | South | Turning left | Passenger van | Other motor vehicle |
| | | | | | North | Going ahead | Automobile, station wagon | Other motor vehicle |

October 10, 2019 Page 3 of 11

| 2015-Jul-01, Wed,07:35 | Rain | Angle | P.D. only | Wet | North | Turning left | Truck and trailer | Other motor vehicle |
|------------------------|-------|------------------|------------------|-----|-------|---------------|------------------------------|---------------------|
| | | | | | East | Going ahead | Automobile, station wagon | Other motor vehicle |
| 2015-Jun-23, Tue,08:00 | Clear | Rear end | P.D. only | Dry | West | Turning right | Automobile, station wagon | Other motor vehicle |
| | | | | | West | Turning right | Pick-up truck | Other motor vehicle |
| 2015-Apr-12, Sun,13:48 | Clear | Sideswipe | Non-fatal injury | Dry | South | Turning left | Automobile, station wagon | Cyclist |
| | | | | | South | Turning left | Bicycle | Other motor vehicle |
| 2014-Oct-22, Wed,14:00 | Clear | Angle | P.D. only | Dry | East | Going ahead | Automobile, station wagon | Other motor vehicle |
| | | | | | South | Going ahead | Automobile, station wagon | Other motor vehicle |
| 2014-Oct-11, Sat,22:48 | Clear | Turning movement | P.D. only | Wet | North | Turning left | Automobile, station wagon | Other motor vehicle |
| | | | | | South | Going ahead | Automobile, station wagon | Other motor vehicle |
| 2014-Oct-05, Sun,17:28 | Clear | Angle | P.D. only | Dry | South | Going ahead | Passenger van | Other motor vehicle |
| | | | | | East | Going ahead | Automobile, station wagon | Other motor vehicle |
| 2014-Aug-04, Mon,11:48 | Clear | Angle | Non-fatal injury | Dry | West | Going ahead | Pick-up truck | Other motor vehicle |
| | | | | | North | Going ahead | Pick-up truck | Other motor vehicle |

October 10, 2019 Page 4 of 11

| 2014-Aug-02, Sat,13:04 | Clear | Rear end | P.D. only | Dry | West | Slowing or stopping | g Automobile, station wagon | Other motor vehicle |
|------------------------|-------|-----------|------------------|-----|-------|---------------------|--------------------------------|---------------------|
| | | | | | West | Stopped | Automobile, station wagon | Other motor vehicle |
| 2014-Apr-04, Fri,07:39 | Clear | Angle | Non-fatal injury | Dry | West | Going ahead | Automobile, station wagon | Other motor vehicle |
| | | | | | South | Going ahead | Passenger van | Other motor vehicle |
| 2014-Feb-11, Tue,17:00 | Clear | Sideswipe | P.D. only | Dry | West | Overtaking | Automobile, station wagon | Other motor vehicle |
| | | | | | West | Stopped | Automobile, station wagon | Other motor vehicle |

Location: FALLOWFIELD RD @ O'KEEFE CRT

Traffic Control: Stop sign Total Collisions: 1

| Date/Day/Time | Environment | Impact Type | Classification | Surface Cond'n | Veh. Dir | Vehicle Manoeuve | r Vehicle type | First Event | No. Ped |
|------------------------|-------------|-------------|----------------|-------------------|----------|------------------|---------------------------|---------------------|---------|
| 2015-Sep-28, Mon,07:47 | Clear | Angle | P.D. only | Dry | South | Going ahead | Automobile, station wagon | Other motor vehicle | |
| | | | | | East | Going ahead | Pick-up truck | Other motor vehicle | |

Location: FALLOWFIELD RD @ STRANDHERD DR

Traffic Control: Traffic signal Total Collisions: 35

| Date/Day/Time | Environment | Impact Type | Classification | Surface Cond'n | Veh. Dir | Vehicle Manoeuve | r Vehicle type | First Event | No. Ped |
|------------------------|-------------|------------------|------------------|-------------------|----------|------------------|---------------------------|---------------------|---------|
| 2018-Dec-22, Sat,08:04 | Snow | Turning movement | P.D. only | Loose snow | West | Going ahead | Automobile, station wagon | Other motor vehicle | |
| | | | | | East | Turning left | Automobile, station wagon | Other motor vehicle | |
| 2018-Oct-24, Wed,08:45 | Clear | Rear end | Non-fatal injury | Dry | West | Changing lanes | Automobile, station wagon | Other motor vehicle | |

October 10, 2019 Page 5 of 11

| | | | | | West | Stopped | Automobile, station wagon | Other motor vehicle |
|------------------------|-------|-----------|------------------|-----|-------|---------------|---------------------------|---------------------|
| 2018-Sep-17, Mon,14:10 | Clear | Rear end | P.D. only | Dry | South | Turning right | Pick-up truck | Other motor vehicle |
| | | | | | South | Turning right | Automobile, station wagon | Other motor vehicle |
| 2018-Sep-10, Mon,07:45 | Clear | Sideswipe | P.D. only | Dry | West | Unknown | Unknown | Other motor vehicle |
| | | | | | West | Going ahead | Automobile, station wagon | Other motor vehicle |
| 2018-Aug-16, Thu,12:28 | Clear | Rear end | P.D. only | Dry | West | Going ahead | Automobile, station wagon | Other motor vehicle |
| | | | | | West | Stopped | Automobile, station wagon | Other motor vehicle |
| 2018-Jun-24, Sun,14:01 | Clear | Rear end | P.D. only | Dry | South | Turning right | Automobile, station wagon | Other motor vehicle |
| | | | | | South | Turning right | Automobile, station wagon | Other motor vehicle |
| 2018-Jun-19, Tue,21:05 | Clear | Angle | Non-fatal injury | Dry | South | Going ahead | Motorcycle | Other motor vehicle |
| | | | | | East | Going ahead | Automobile, station wagon | Other motor vehicle |
| 2018-Apr-26, Thu,16:11 | Clear | Rear end | P.D. only | Dry | South | Turning right | Automobile, station wagon | Other motor vehicle |
| | | | | | South | Turning right | Passenger van | Other motor vehicle |
| 2018-Mar-09, Fri,10:55 | Snow | Angle | Non-fatal injury | Wet | West | Going ahead | Automobile, station wagon | Other motor vehicle |

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| | | | | | South | Turning left | Pick-up truck | Other motor vehicle |
|------------------------|-------|----------|------------------|-------|-------|---------------------|------------------------------|---------------------|
| 2018-Feb-16, Fri,15:35 | Clear | Rear end | P.D. only | Dry | East | | Automobile, station wagon | Other motor vehicle |
| | | | | | East | | Automobile, station wagon | Other motor vehicle |
| 2018-Feb-09, Fri,17:45 | Clear | Rear end | Non-fatal injury | Wet | West | Slowing or stopping | Automobile, station wagon | Skidding/sliding |
| | | | | | West | Slowing or stopping | Automobile, station wagon | Other motor vehicle |
| 2018-Feb-08, Thu,15:46 | Clear | Angle | P.D. only | Dry | East | | Automobile, station wagon | Other motor vehicle |
| | | | | | South | Going ahead | Pick-up truck | Other motor vehicle |
| 2018-Jan-08, Mon,12:55 | Snow | Rear end | Non-fatal injury | Slush | East | Slowing or stopping | Pick-up truck | Skidding/sliding |
| | | | | | East | | Automobile, station wagon | Other motor vehicle |
| 2017-Nov-17, Fri,12:02 | Clear | Rear end | P.D. only | Dry | West | Going ahead | Pick-up truck | Other motor vehicle |
| | | | | | West | Stopped | Passenger van | Other motor vehicle |
| 2017-Oct-17, Tue,17:28 | Clear | Rear end | P.D. only | Dry | West | | Automobile, station wagon | Other motor vehicle |
| | | | | | West | | Automobile, station wagon | Other motor vehicle |
| 2017-Sep-20, Wed,20:10 | Clear | Rear end | P.D. only | Dry | West | | Automobile, station wagon | Other motor vehicle |

October 10, 2019 Page 7 of 11

| | | | | | West | Turning right | Automobile, station wagon | Other motor vehicle |
|------------------------|-------|-----------|------------------|-----|-------|----------------|---------------------------|---------------------|
| 2017-Aug-15, Tue,14:45 | Clear | Angle | Non-fatal injury | Dry | East | Going ahead | Passenger van | Other motor vehicle |
| | | | | | North | Turning left | Pick-up truck | Other motor vehicle |
| 2017-Aug-12, Sat,18:56 | Rain | Rear end | Non-fatal injury | Wet | West | Going ahead | Automobile, station wagon | Other motor vehicle |
| | | | | | West | Stopped | Automobile, station wagon | Other motor vehicle |
| 2017-Jul-26, Wed,07:34 | Clear | Sideswipe | P.D. only | Dry | West | Changing lanes | Automobile, station wagon | Other motor vehicle |
| | | | | | West | Going ahead | Automobile, station wagon | Other motor vehicle |
| 2017-Jul-14, Fri,18:11 | Clear | Rear end | P.D. only | Dry | South | Turning right | Pick-up truck | Other motor vehicle |
| | | | | | South | Stopped | Automobile, station wagon | Other motor vehicle |
| | | | | | South | Merging | Automobile, station wagon | Other motor vehicle |
| 2017-Jun-05, Mon,14:45 | Clear | Rear end | P.D. only | Dry | South | Turning right | Automobile, station wagon | Other motor vehicle |
| | | | | | South | Turning right | Automobile, station wagon | Other motor vehicle |
| | | | | | South | Turning right | Automobile, station wagon | Other motor vehicle |
| 2017-Apr-20, Thu,08:40 | Clear | Rear end | P.D. only | Dry | East | Turning left | Automobile, station wagon | Other motor vehicle |
| | | | | | East | Turning left | Pick-up truck | Other motor vehicle |

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| 2017-Feb-26, Sun,14:09 | Clear | Sideswipe | P.D. only | Dry | West | Changing lanes | Automobile, station wagon | Other motor vehicle |
|------------------------|-------|-------------|-----------|-------|------|---------------------|------------------------------|---------------------|
| | | | | | West | Changing lanes | · · | Other motor vehicle |
| 2017-Jan-12, Thu,06:25 | Rain | Approaching | P.D. only | Wet | West | Unknown | Unknown | Other motor vehicle |
| | | | | | East | Going ahead | Pick-up truck | Other motor vehicle |
| 2016-Jun-18, Sat,13:50 | Clear | Rear end | P.D. only | Dry | West | Going ahead | Automobile, station wagon | Other motor vehicle |
| | | | | | West | Stopped | Automobile, station wagon | Other motor vehicle |
| 2016-Feb-20, Sat,03:57 | Rain | Rear end | P.D. only | Slush | West | Going ahead | Automobile, station wagon | Other motor vehicle |
| | | | | | West | Stopped | Automobile, station wagon | Other motor vehicle |
| 2016-Jan-19, Tue,06:27 | Clear | Rear end | P.D. only | Ice | West | Slowing or stopping | Automobile, station wagon | Other motor vehicle |
| | | | | | West | Stopped | Automobile, station wagon | Other motor vehicle |
| 2016-Jan-13, Wed,15:11 | Clear | Sideswipe | P.D. only | Wet | West | Changing lanes | Pick-up truck | Other motor vehicle |
| | | | | | West | Going ahead | Pick-up truck | Other motor vehicle |
| 2015-Aug-14, Fri,16:39 | Clear | Sideswipe | P.D. only | Dry | East | Changing lanes | Automobile, station wagon | Other motor vehicle |
| | | | | | East | Going ahead | Automobile, station wagon | Other motor vehicle |

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| 2015-Jul-22, Wed,20:20 | Clear | Rear end | P.D. only | Dry | East | Turning left | Pick-up truck | Other motor vehicle | |
|------------------------|-------|-------------|------------------|-----|-------|------------------|---------------------------|------------------------|---|
| | | | | | East | Turning left | Automobile, station wagon | Other motor vehicle | |
| | | _ | | _ | | | | | |
| 2015-Feb-24, Tue,12:48 | Clear | Rear end | P.D. only | Dry | West | Going ahead | Automobile, station wagon | Other motor vehicle | |
| | | | | | West | Going ahead | Automobile, station wagon | Other motor vehicle | |
| 2014-Oct-20, Mon,08:45 | Clear | SMV other | Non-fatal injury | Dry | East | Going ahead | Automobile, station wagon | Pedestrian | 1 |
| 2044 Aug 20 Ed 00:50 | Class | Deerand | D.D. colu | D | Cauth | Transis a vialet | A ta a la ila | Othermoter | |
| 2014-Aug-29, Fri,08:56 | Clear | Rear end | P.D. only | Dry | South | Turning right | Automobile, station wagon | Other motor vehicle | |
| | | | | | South | Turning right | Pick-up truck | Other motor vehicle | |
| 2014 Jun 09 Sun 04:47 | Cloar | SMV other | D.D. only | Dny | West | Coing shood | Automobile, | Curb | |
| 2014-Jun-08, Sun,04:47 | Clear | Siviv other | P.D. only | Dry | west | Going ahead | station wagon | Curb | |
| | | | | | | | | | |
| 2014-Mar-26, Wed,17:53 | Clear | Rear end | Non-fatal injury | Dry | East | Going ahead | Pick-up truck | Other motor vehicle | |
| | | | | | East | Stopped | Pick-up truck | Other motor vehicle | |
| | | | | | East | Stopped | Pick-up truck | Other motor vehicle | |

Location: FALLOWFIELD RD btwn O'KEEFE CRT & CEDARVIEW RD

Traffic Control: No control

Total Collisions: 4

| Date/Day/Time | Environment | Impact Type | Classification | Surface Cond'n | Veh. Dir | Vehicle Manoeuve | er Vehicle type | First Event | No. Ped |
|------------------------|-------------|-------------|----------------|-------------------|----------|------------------|---------------------------|---------------------|---------|
| 2016-Sep-01, Thu,11:31 | Clear | Sideswipe | P.D. only | Dry | East | Overtaking | Pick-up truck | Other motor vehicle | |
| | | | | | East | Going ahead | Automobile, station wagon | Other motor vehicle | |

October 10, 2019 Page 10 of 11

| 2016-Jul-24, Sun,00:39 | Clear | Approaching | P.D. only | Dry | East | Going ahead | Pick-up truck | Other motor vehicle |
|------------------------|-------|-------------|-----------|------------|------|----------------|---------------------------|---------------------|
| | | | | | West | Going ahead | Automobile, station wagon | Other motor vehicle |
| 2015-Jan-29, Thu,17:52 | Snow | SMV other | P.D. only | Loose snow | East | Going ahead | Automobile, station wagon | Ditch |
| 2014-Nov-05, Wed,07:20 | Clear | Sideswipe | P.D. only | Dry | East | Changing lanes | Pick-up truck | Other motor vehicle |
| | | | | | East | Going ahead | Truck - dump | Other motor vehicle |

Location: FALLOWFIELD RD btwn STRANDHERD DR & O'KEEFE CRT

Traffic Control: No control

Total Collisions: 1

| Date/Day/Time | Environment | Impact Type | Classification | Surface Cond'n | Veh. Dir | Vehicle Manoeuver Vehicle type | First Event | No. Ped |
|------------------------|-------------|-------------|----------------|-------------------|----------|---|---------------------|---------|
| 2016-Apr-22, Fri,15:13 | Rain | Rear end | P.D. only | Wet | South | Slowing or stopping Automobile, station wagon | Other motor vehicle | |
| | | | | | South | Slowing or stopping Automobile, station wagon | Other motor vehicle | |

Location: O'KEEFE CRT btwn FOXTAIL AVE & FALLOWFIELD RD

Traffic Control: No control

Total Collisions: 1

| Date/Day/Time | Environment | Impact Type | Classification | Surface Cond'n | Veh. Dir | Vehicle Manoeuve | er Vehicle type | First Event | No. Ped |
|------------------------|-------------|-------------|----------------|-------------------|----------|------------------|-----------------|---------------------|---------|
| 2015-Aug-26, Wed,16:49 | Clear | Rear end | P.D. only | Dry | West | Unknown | Unknown | Other motor vehicle | |
| | | | | | West | Stopped | Pick-up truck | Other motor vehicle | |

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Appendix F – Trip Generation Data

April 9, 2020 6

Medical-Dental Office Building

(720)

Vehicle Trip Ends vs: 1000 Sq. Ft. GFA

On a: Weekday,

Peak Hour of Adjacent Street Traffic,

One Hour Between 7 and 9 a.m. Setting/Location: General Urban/Suburban

Number of Studies: 4

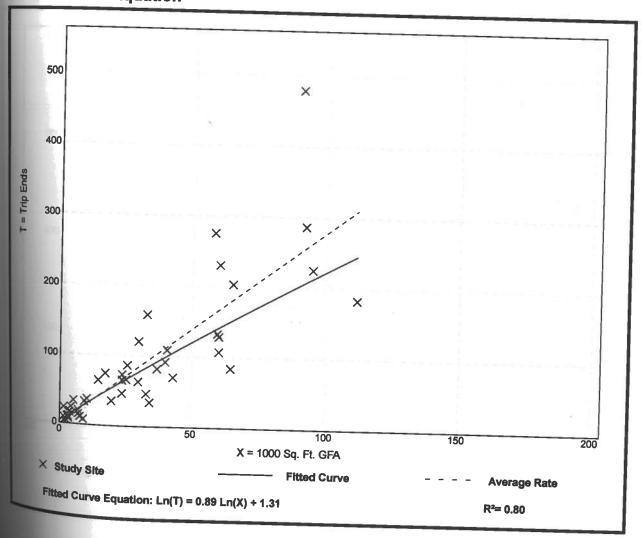
1000 Sq. Ft. GFA: 32

Directional Distribution: 78% entering, 22% exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

| | Par 1999 od: I t. Ol A | |
|--------------|------------------------|--------------------|
| Average Rate | Range of Rates | Standard Deviation |
| 2.78 | 0.85 - 14.30 | 1.28 |
| | | |

Data Plot and Equation



Medical-Dental Office Building

(720)

Vehicle Trip Ends vs: 1000 Sq. Ft. GFA

On a: Weekday,

Peak Hour of Adjacent Street Traffic,

One Hour Between 4 and 6 p.m.

Setting/Location:

General Urban/Suburban

Number of Studies:

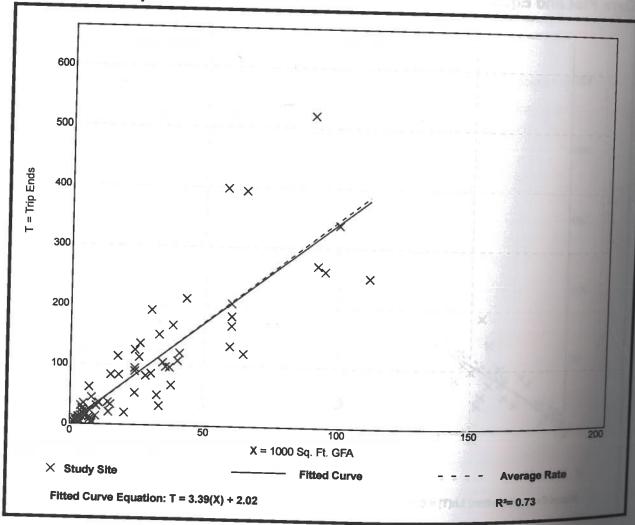
65 28

1000 Sq. Ft. GFA: Directional Distribution: 28% entering, 72% exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
|--------------|----------------|--------------------|
| 3.46 | 0.25 - 8.86 | |
| | 0.23 - 0.86 | 1.58 |

Data Plot and Equation



Quality Restaurant (931)

Vehicle Trip Ends vs: Seats

On a: Weekday,

Peak Hour of Adjacent Street Traffic,

One Hour Between 7 and 9 a.m.

Setting/Location:

General Urban/Suburban

Number of Studies: Avg. Num. of Seats: 355

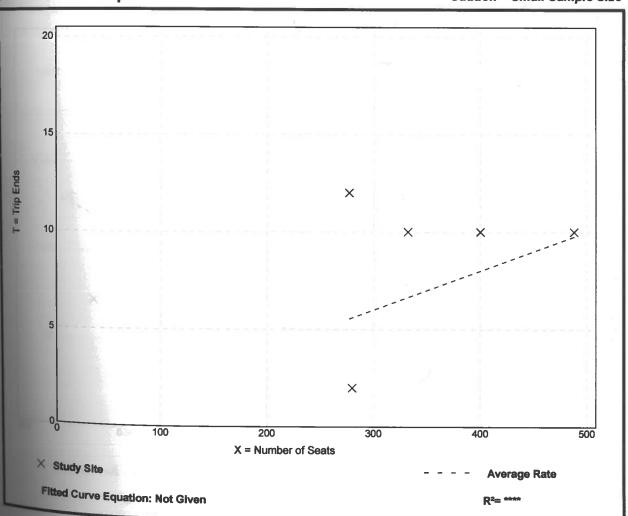
Directional Distribution: Not Available

Vehicle Trip Generation per Seat

| Average Rate | Range of Rates | Standard Deviation |
|--------------|----------------|--------------------|
| 0.02 | 0.01 - 0.04 | 0.01 |

Data Plot and Equation

Caution - Small Sample Size





Quality Restaurant (931)

Vehicle Trip Ends vs: Seats

On a: Weekday,

Peak Hour of Adjacent Street Traffic,

One Hour Between 4 and 6 p.m.

Setting/Location:

General Urban/Suburban

Number of Studies: 11

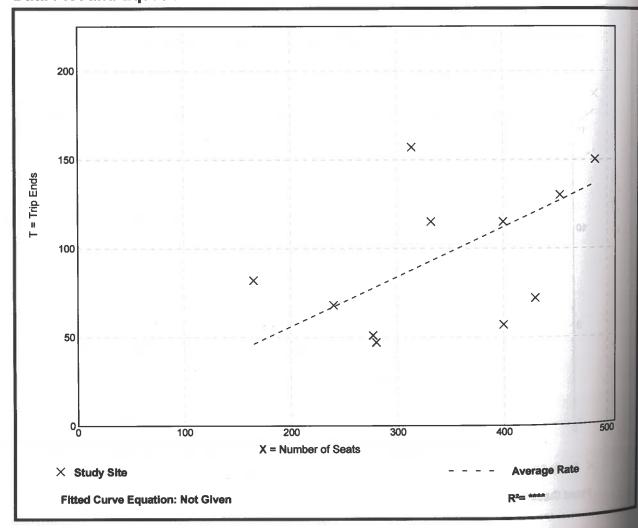
Avg. Num. of Seats: 344

Directional Distribution: 67% entering, 33% exiting

Vehicle Trip Generation per Seat

| Average Rate | Range of Rates | Standard Deviation |
|--------------|----------------|--------------------|
| 0.28 | 0.14 - 0.50 | 0.11 |

Data Plot and Equation





South Nepean

Demographic Characteristics

| Population | 72,750 | Actively Trav | /elled | 57,830 |
|---------------------------|--------|---------------|----------|---------|
| Employed Population | 35,540 | Number of \ | ehicles/ | 44,130 |
| Households | 26,260 | Area (km²) | | 54.8 |
| | | | | |
| Occupation | | | | |
| Status (age 5+) | | Male | Female | Total |
| Full Time Employed | | 17,630 | 14,730 | 32,350 |
| Part Time Employed | | 620 | 2,570 | 3,190 |
| Student | | 9,910 | 9,420 | 19,340 |
| Retiree | | 3,420 | 4,200 | 7,620 |
| Unemployed | | 720 | 500 | 1,220 |
| Homemaker | | 180 | 2,390 | 2,570 |
| Other | | 270 | 540 | 810 |
| Total: | | 32,750 | 34,350 | 67,100 |
| | | | | |
| Traveller Characteristics | | Male | Female | Total |
| Transit Pass Holders | | 5,590 | 6,100 | 11,700 |
| Licensed Drivers | | 24,480 | 25,260 | 49,740 |
| Telecommuters | | 60 | 310 | 370 |
| Trips made by residents | | 88,180 | 97,380 | 185,550 |

| tal: | 32,750 | 34,350 | 67,100 | 0 975 15 3 | A End Feb |
|-------------------------|--------|--------|----------|----------------|-----------|
| eveller Characteristics | Male | Female | Total | 7 | K |
| ansit Pass Holders | 5,590 | 6,100 | 11,700 | | |
| ensed Drivers | 24,480 | 25,260 | 49,740 | Household Size | |
| lecommuters | 60 | 310 | 370 | 1 person | 3, |
| | | | | 2 persons | 7, |
| ps made by residents | 88,180 | 97,380 | 185,550 | 3 persons | 5, |
| | | | <u> </u> | 4 persons | 6, |
| | | | | 5+ persons | 3. |

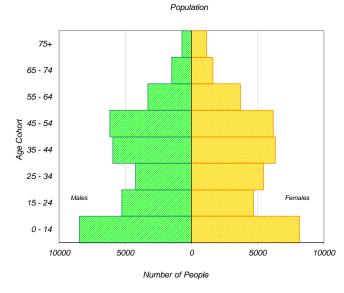
| Bayshore / Cedarview Merivale Hunt Club & South Gloup | ester N.eitrim |
|--|--|
| Hunt Club | |
| | NA G |
| | |
| 150 PM 15 | MORE ST |
| The state of the s | H5 ad |
| South Nepean | |
| | The state of the s |
| Rural Southwest and Paul Range Rural Southwest | 12 13 |
| Rural Southeast | la mo |
| 0 935 15 3 49 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | STATE |
| 0 805 1.5 3 45 0 60 | N N N N N N N N N N N N N N N N N N N |

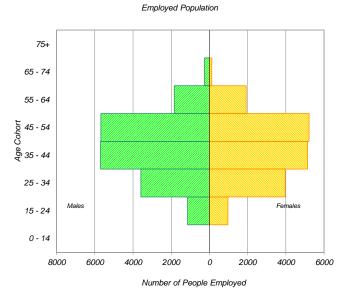
| Household Size | | |
|----------------|--------|------|
| 1 person | 3,560 | 14% |
| 2 persons | 7,300 | 28% |
| 3 persons | 5,500 | 21% |
| 4 persons | 6,320 | 24% |
| 5+ persons | 3,590 | 14% |
| Total: | 26,260 | 100% |

| Households by Vehicle Availability | | | | | |
|------------------------------------|--------|------|--|--|--|
| 0 vehicles 810 35 | | | | | |
| 1 vehicle | 9,500 | 36% | | | |
| 2 vehicles | 13,800 | 53% | | | |
| 3 vehicles | 1,730 | 7% | | | |
| 4+ vehicles | 410 | 2% | | | |
| Total: | 26,260 | 100% | | | |

| Households by Dwelling Typ | e | |
|----------------------------|--------|------|
| Single-detached | 14,530 | 55% |
| Semi-detached | 3,090 | 12% |
| Townhouse | 7,770 | 30% |
| Apartment/Condo | 870 | 3% |
| Total: | 26.260 | 100% |

| Selected Indicators | |
|---------------------------------|------|
| Daily Trips per Person (age 5+) | 2.77 |
| Vehicles per Person | 0.61 |
| Number of Persons per Household | 2.77 |
| Daily Trips per Household | 7.07 |
| Vehicles per Household | 1.68 |
| Workers per Household | 1.35 |
| Population Density (Pop/km2) | 1330 |
| | |



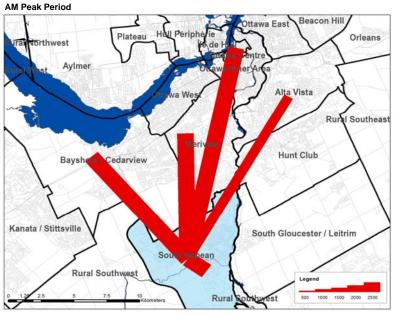


^{*} In 2005 data was only collected for household members aged $11^{^{\star}}$ therefore these results cannot be compared to the 2011 data.



Travel Patterns

Top Five Destinations of Trips from South Nepean



| ; | Summary of Trips to and from South Nepean | | | | | | |
|---|---|-----------------|------------------|----------|---------|--|--|
| | AM Peak Period (6:30 - 8:59) | Destinations of | ns of Origins of | | | | |
| | | Trips From | | Trips To | | | |
| 1 | Districts | District | % Total | District | % Total | | |
| (| Ottawa Centre | 3,820 | 9% | 30 | 0% | | |
| | Ottawa Inner Area | 2,270 | 5% | 340 | 1% | | |
| (| Ottawa East | 630 | 2% | 50 | 0% | | |
| | Beacon Hill | 370 | 1% | 50 | 0% | | |
| / | Alta Vista | 2,360 | 6% | 460 | 2% | | |
| ı | Hunt Club | 920 | 2% | 440 | 2% | | |
| ı | Merivale | 4,310 | 10% | 790 | 3% | | |
| (| Ottawa West | 1,830 | 4% | 160 | 1% | | |
| E | Bayshore / Cedarview | 3,230 | 8% | 700 | 3% | | |
| (| Orléans | 330 | 1% | 200 | 1% | | |
| F | Rural East | 20 | 0% | 60 | 0% | | |
| F | Rural Southeast | 250 | 1% | 580 | 2% | | |
| 9 | South Gloucester / Leitrim | 100 | 0% | 310 | 1% | | |
| 9 | South Nepean | 17,260 | 42% | 17,260 | 74% | | |
| F | Rural Southwest | 580 | 1% | 970 | 4% | | |
| ı | Kanata / Stittsvile | 1,800 | 4% | 690 | 3% | | |
| F | Rural West | 80 | 0% | 30 | 0% | | |
| î | le de Hull | 840 | 2% | 50 | 0% | | |
| H | Hull Périphérie | 260 | 1% | 40 | 0% | | |
| 1 | Plateau | 0 | 0% | 40 | 0% | | |
| 1 | Aylmer | 60 | 0% | 40 | 0% | | |
| F | Rural Northwest | 40 | 0% | 40 | 0% | | |
| 1 | Pointe Gatineau | 0 | 0% | 0 | 0% | | |
| (| Gatineau Est | 0 | 0% | 20 | 0% | | |
| ı | Rural Northeast | 10 | 0% | 20 | 0% | | |
| _ | Buckingham / Masson-Angers | 20 | 0% | 0 | 0% | | |
| (| Ontario Sub-Total: | 40,160 | 97% | 23,120 | 99% | | |
| (| Québec Sub-Total: | 1,230 | 3% | 250 | 1% | | |
| 1 | Total: | 41,390 | 100% | 23,370 | 100% | | |

Trips by Trip Purpose

| 24 Hours | From District | 1 | o District | Wi | thin District | |
|---------------------------|---------------|--------|---------------|------|---------------|--------|
| Work or related | 25,640 | 41% | 5,290 | 8% | 4,680 | 6% |
| School | 5,310 | 8% | 1,430 | 2% | 10,610 | 13% |
| Shopping | 4,940 | 8% | 4,220 | 7% | 12,840 | 16% |
| Leisure | 6,960 | 11% | 4,020 | 6% | 5,760 | 7% |
| Medical | 1,720 | 3% | 900 | 1% | 840 | 1% |
| Pick-up / drive passenger | 4,040 | 6% | 3,920 | 6% | 7,530 | 9% |
| Return Home | 11,460 | 18% | 40,960 | 65% | 34,630 | 43% |
| Other | 2,640 | 4% | 2,090 | 3% | 3,020 | 4% |
| Total: | 62,710 | 100% | 62,830 | 100% | 79,910 | 100% |
| AM Peak (06:30 - 08:59) | From District | 1 | o District | Wi | thin District | |
| Work or related | 18,160 | 75% | 2,890 | 47% | 2,120 | 12% |
| School | 3,280 | 14% | 1,170 | 19% | 9,180 | 53% |
| Shopping | 180 | 1% | 70 | 1% | 720 | 4% |
| Leisure | 350 | 1% | 230 | 4% | 220 | 1% |
| Medical | 400 | 2% | 60 | 1% | 100 | 1% |
| Pick-up / drive passenger | 1,060 | 4% | 770 | 13% | 2,860 | 17% |
| Return Home | 210 | 1% | 640 | 10% | 1,070 | 6% |
| Other | 520 | 2% 290 | | 5% | 990 | 6% |
| Total: | 24,160 | 100% | 6,120 | 100% | 17,260 | 100% |
| PM Peak (15:30 - 17:59) | From District | 1 | o District | Wi | thin District | |
| Work or related | 410 | 5% | 290 | 1% | 410 | 2% |
| School | 250 | 3% | 0 | 0% | 50 | 0% |
| Shopping | 900 | 11% | 1,090 | 5% | 2,090 | 11% |
| Leisure | 1,420 | 17% | 790 | 3% | 1,840 | 10% |
| Medical | 190 | 2% | 230 | 1% | 90 | 0% |
| Pick-up / drive passenger | 820 | 10% | 1,700 | 7% | 1,610 | 9% |
| Return Home | 3,800 | 47% | 18,990 | 81% | 11,810 | 64% |
| Other | 360 | 4% | 490 | 2% | 540 | 3% |
| Total: | 8,150 | 100% | 23,580 | 100% | 18,440 | 100% |
| Peak Period (%) | Total: | 9 | % of 24 Hours | W | ithin Distric | ct (%) |
| 24 Hours | 205,450 | | | | 39% | |

47,540

50,170

23%

24%

36%

37%

Trips by Primary Travel Mode

| 24 Hours | From District | | To District | Wit | thin District | : |
|-------------------------|---------------|------|-------------|-------|---------------|------|
| Auto Driver | 41,340 | 66% | 41,280 | 66% | 39,110 | 49% |
| Auto Passenger | 9,400 | 15% | 10,030 | 16% | 15,320 | 19% |
| Transit | 9,990 | 16% | 9,520 | 15% | 2,260 | 3% |
| Bicycle | 310 | 0% | 320 | 1% | 960 | 1% |
| Walk | 80 | 0% | 170 | 0% | 13,060 | 16% |
| Other | 1,600 | 3% | 1,520 | 2% | 9,210 | 12% |
| Total: | 62,720 | 100% | 62,840 | 100% | 79,920 | 100% |
| AM Peak (06:30 - 08:59) | From District | | To District | Wit | thin District | : |
| Auto Driver | 14,570 | 60% | 4,360 | 71% | 5,800 | 34% |
| Auto Passenger | 1,930 | 8% | 780 | 13% | 3,210 | 19% |
| Transit | 6,610 | 27% | 330 | 5% | 730 | 4% |
| Bicycle | 80 | 0% | 50 | 1% | 320 | 2% |
| Walk | 20 | 0% | 10 | 0% | 3,000 | 17% |
| Other | 930 | 4% | 590 | 10% | 4,200 | 24% |
| Total: | 24,140 | 100% | 6,120 | 100% | 17,260 | 100% |
| PM Peak (15:30 - 17:59) | From District | | To District | Wit | thin District | : |
| Auto Driver | 5,840 | 72% | 14,640 | 62% | 8,420 | 46% |
| Auto Passenger | 1,730 | 21% | 2,680 | 11% | 3,930 | 21% |
| Transit | 350 | 4% | 5,770 | 24% | 650 | 4% |
| Bicycle | 80 | 1% | 110 | 0% | 150 | 1% |
| Walk | 30 | 0% | 0 | 0% | 3,680 | 20% |
| Other | 100 | 1% | 380 | 2% | 1,590 | 9% |
| Total: | 8,130 | 100% | 23,580 | 100% | 18,420 | 100% |
| Avg Vehicle Occupancy | From District | | To District | Wi | thin District | : |
| 24 Hours | 1.23 | | 1.24 | | 1.39 | |
| AM Peak Period | 1.13 | | 1.18 | | 1.55 | |
| PM Peak Period | 1.30 | | 1.18 | | 1.47 | |
| Transit Modal Split | From District | | To District | \A/i+ | thin District | |
| 24 Hours | 16% | | 16% | 771 | 4% | |
| AM Peak Period | 29% | | 6% | | 4% 7% | |
| PM Peak Period | 4% | | 25% | | 5% | |
| rivi reak ref100 | 470 | | 23% | | 370 | |

AM Peak Period

PM Peak Period

Appendix G – TDM Checklist

April 9, 2020 7

TDM-Supportive Development Design and Infrastructure Checklist:

Non-Residential Developments (office, institutional, retail or industrial)

| Legend | | | | |
|----------|--|--|--|--|
| REQUIRED | The Official Plan or Zoning By-law provides related guidance that must be followed | | | |
| BASIC | The measure is generally feasible and effective, and in most cases would benefit the development and its users | | | |
| BETTER | The measure could maximize support for users of sustainable modes, and optimize development performance | | | |

| TDM-supportive design & infrastructure measures: Non-residential developments | | | Check if completed & add descriptions, explanations or plan/drawing references |
|--|-------|--|---|
| | 1. | WALKING & CYCLING: ROUTES | |
| | 1.1 | Building location & access points | |
| BASIC | 1.1.1 | Locate building close to the street, and do not locate parking areas between the street and building entrances | ☑ |
| BASIC | 1.1.2 | Locate building entrances in order to minimize walking distances to sidewalks and transit stops/stations | $oxed{oxed}$ |
| BASIC | 1.1.3 | Locate building doors and windows to ensure visibility of pedestrians from the building, for their security and comfort | |
| | 1.2 | Facilities for walking & cycling | |
| REQUIRED | 1.2.1 | Provide convenient, direct access to stations or major stops along rapid transit routes within 600 metres; minimize walking distances from buildings to rapid transit; provide pedestrian-friendly, weather-protected (where possible) environment between rapid transit accesses and building entrances; ensure quality linkages from sidewalks through building entrances to integrated stops/stations (see Official Plan policy 4.3.3) | N/A - no rapid transit service exists within the vicinity of the proposed development |
| REQUIRED | 1.2.2 | Provide safe, direct and attractive pedestrian access from public sidewalks to building entrances through such measures as: reducing distances between public sidewalks and major building entrances; providing walkways from public streets to major building entrances; within a site, providing walkways along the front of adjoining buildings, between adjacent buildings, and connecting areas where people may congregate, such as courtyards and transit stops; and providing weather protection through canopies, colonnades, and other design elements wherever possible (see Official Plan policy 4.3.12) | A network of sidewalks is proposed within the development |

| | TDM-s | supportive design & infrastructure measures: Non-residential developments | Check if completed & add descriptions, explanations or plan/drawing references |
|----------|-------|--|--|
| REQUIRED | 1.2.3 | Provide sidewalks of smooth, well-drained walking surfaces of contrasting materials or treatments to differentiate pedestrian areas from vehicle areas, and provide marked pedestrian crosswalks at intersection sidewalks (see Official Plan policy 4.3.10) | All sidewalks will be constructed per City standards |
| REQUIRED | 1.2.4 | Make sidewalks and open space areas easily accessible through features such as gradual grade transition, depressed curbs at street corners and convenient access to extra-wide parking spaces and ramps (see Official Plan policy 4.3.10) | Proposed pedestrian facilities will conform to AODA standards |
| REQUIRED | 1.2.5 | Include adequately spaced inter-block/street cycling and pedestrian connections to facilitate travel by active transportation. Provide links to the existing or planned network of public sidewalks, multi-use pathways and onroad cycle routes. Where public sidewalks and multi-use pathways intersect with roads, consider providing traffic control devices to give priority to cyclists and pedestrians (see Official Plan policy 4.3.11) | |
| BASIC | 1.2.6 | Provide safe, direct and attractive walking routes from building entrances to nearby transit stops | |
| BASIC | 1.2.7 | Ensure that walking routes to transit stops are secure, visible, lighted, shaded and wind-protected wherever possible | |
| BASIC | 1.2.8 | Design roads used for access or circulation by cyclists using a target operating speed of no more than 30 km/h, or provide a separated cycling facility | |
| | 1.3 | Amenities for walking & cycling | |
| BASIC | 1.3.1 | Provide lighting, landscaping and benches along walking and cycling routes between building entrances and streets, sidewalks and trails | |
| BASIC | 1.3.2 | Provide wayfinding signage for site access (where required, e.g. when multiple buildings or entrances exist) and egress (where warranted, such as when directions to reach transit stops/stations, trails or other common destinations are not obvious) | |

| | TDM-s | upportive design & infrastructure measures: Non-residential developments | Check if completed & add descriptions, explanations or plan/drawing references |
|----------|-------|---|---|
| | 2. | WALKING & CYCLING: END-OF-TRIP FACILITY | TIES |
| | 2.1 | Bicycle parking | |
| REQUIRED | 2.1.1 | Provide bicycle parking in highly visible and lighted areas, sheltered from the weather wherever possible (see Official Plan policy 4.3.6) | |
| REQUIRED | 2.1.2 | Provide the number of bicycle parking spaces specified for various land uses in different parts of Ottawa; provide convenient access to main entrances or well-used areas (see Zoning By-law Section 111) | Number of bicycle parking spaces exceeds Zoning Bylaw requirements and are located within close proximity to building entrances |
| REQUIRED | 2.1.3 | Ensure that bicycle parking spaces and access aisles meet minimum dimensions; that no more than 50% of spaces are vertical spaces; and that parking racks are securely anchored (see Zoning By-law Section 111) | All 5 bicycyle parking spaces are horizontal |
| BASIC | 2.1.4 | Provide bicycle parking spaces equivalent to the expected number of commuter cyclists (assuming the cycling mode share target is met), plus the expected peak number of customer/visitor cyclists | |
| BETTER | 2.1.5 | Provide bicycle parking spaces equivalent to the expected number of commuter and customer/visitor cyclists, plus an additional buffer (e.g. 25 percent extra) to encourage other cyclists and ensure adequate capacity in peak cycling season | |
| | 2.2 | Secure bicycle parking | |
| REQUIRED | 2.2.1 | Where more than 50 bicycle parking spaces are provided for a single office building, locate at least 25% of spaces within a building/structure, a secure area (e.g. supervised parking lot or enclosure) or bicycle lockers (see Zoning By-law Section 111) | N/A |
| BETTER | 2.2.2 | Provide secure bicycle parking spaces equivalent to the expected number of commuter cyclists (assuming the cycling mode share target is met) | |
| | 2.3 | Shower & change facilities | |
| BASIC | 2.3.1 | Provide shower and change facilities for the use of active commuters | |
| BETTER | 2.3.2 | In addition to shower and change facilities, provide dedicated lockers, grooming stations, drying racks and laundry facilities for the use of active commuters | |
| | 2.4 | Bicycle repair station | |
| BETTER | 2.4.1 | Provide a permanent bike repair station, with commonly used tools and an air pump, adjacent to the main bicycle parking area (or secure bicycle parking area, if provided) | |

| | TDM-s | supportive design & infrastructure measures: Non-residential developments | Check if completed & add descriptions, explanations or plan/drawing references |
|--------|-------|---|--|
| | 3. | TRANSIT | |
| | 3.1 | Customer amenities | |
| BASIC | 3.1.1 | Provide shelters, lighting and benches at any on-site transit stops | |
| BASIC | 3.1.2 | Where the site abuts an off-site transit stop and insufficient space exists for a transit shelter in the public right-of-way, protect land for a shelter and/or install a shelter | |
| BETTER | 3.1.3 | Provide a secure and comfortable interior waiting area by integrating any on-site transit stops into the building | |
| | 4. | RIDESHARING | |
| | 4.1 | Pick-up & drop-off facilities | |
| BASIC | 4.1.1 | Provide a designated area for carpool drivers (plus taxis and ride-hailing services) to drop off or pick up passengers without using fire lanes or other no-stopping zones | |
| | 4.2 | Carpool parking | |
| BASIC | 4.2.1 | Provide signed parking spaces for carpools in a priority location close to a major building entrance, sufficient in number to accommodate the mode share target for carpools | |
| BETTER | 4.2.2 | At large developments, provide spaces for carpools in a separate, access-controlled parking area to simplify enforcement | |
| | 5. | CARSHARING & BIKESHARING | |
| | 5.1 | Carshare parking spaces | |
| BETTER | 5.1.1 | Provide carshare parking spaces in permitted non-residential zones, occupying either required or provided parking spaces (see Zoning By-law Section 94) | |
| | 5.2 | Bikeshare station location | |
| BETTER | 5.2.1 | Provide a designated bikeshare station area near a major building entrance, preferably lighted and sheltered with a direct walkway connection | |

| | TDM-s | supportive design & infrastructure measures: Non-residential developments | Check if completed & add descriptions, explanations or plan/drawing references |
|----------|-------|--|--|
| | 6. | PARKING | |
| | 6.1 | Number of parking spaces | |
| REQUIRED | 6.1.1 | Do not provide more parking than permitted by zoning, nor less than required by zoning, unless a variance is being applied for | Parking supply is within the permissible range specified in the Zoning Bylaw |
| BASIC | 6.1.2 | Provide parking for long-term and short-term users that is consistent with mode share targets, considering the potential for visitors to use off-site public parking | |
| BASIC | 6.1.3 | Where a site features more than one use, provide shared parking and reduce the cumulative number of parking spaces accordingly (see Zoning By-law Section 104) | |
| BETTER | 6.1.4 | Reduce the minimum number of parking spaces required by zoning by one space for each 13 square metres of gross floor area provided as shower rooms, change rooms, locker rooms and other facilities for cyclists in conjunction with bicycle parking (see Zoning By-law Section 111) | |
| | 6.2 | Separate long-term & short-term parking areas | |
| BETTER | 6.2.1 | Separate short-term and long-term parking areas using signage or physical barriers, to permit access controls and simplify enforcement (i.e. to discourage employees from parking in visitor spaces, and vice versa) | |
| | 7. | OTHER | |
| | 7.1 | On-site amenities to minimize off-site trips | |
| BETTER | 7.1.1 | Provide on-site amenities to minimize mid-day or mid-commute errands | |

Appendix H – MMLOS Analysis

April 9, 2020 8

Multi-Modal Level of Service

115 Lusk Street TIA

Scenario: Future Conditions

| INTER | SECTIONS | | d & O'Keefe (| | | | | | |
|-----------------|--|------------------------|--|--|------------------------|---|------|---|--|
| | | NORTH leg | SOUTH leg | EAST leg | WEST leg | | | | |
| | Lanes (do NOT include lanes protected by bulb-outs) | | 4 | 2 | 3 | | | | |
| | Median Island Refuge | No Median | No Median | No Median | No Median | | | | |
| | Conflicting Left Turns (from street to right) | Permissive | Permissive | Permissive | Permissive | | | | |
| | Conflicting Right Turns (from street to left) | Permissive or | Permissive or | Permissive or | Permissive or | | | | |
| | | yield control | yield control | yield control | yield control | | | | |
| | RTOR? (from street to left) Ped Leading Interval? (on cross street) | RTOR allowed No | RTOR allowed No | RTOR allowed No | RTOR allowed No | | | | |
| | Corner Radius | > 10m to 15m | > 5m to 10m | > 5m to 10m | > 10m to 15m | | | | |
| Pedestrian | | No right turn | No right turn | No right turn | No right turn | | | | |
| str | Right Turn Channel | channel | channel | channel | channel | | | | |
| ge | O | Standard | Standard | Standard | Standard | | | | |
| a | Crosswalk Type | transverse markings | transverse markings | transverse markings | transverse markings | | | | |
| | LOC (DETCI) | 53 | 54 | 86 | 70 | | | | |
| | LOS (PETSI) | D | D | В | С | | | | |
| | Cycle Length (sec) | 120 | 120 | 120 | 120 | | | | |
| | Pedestrian Walk Time (solid white symbol) (sec) | 7 54.3 | 7 | 7 54.3 | 7 | | | | |
| | LOS (Delay,seconds) | 54.3 E | 54.3 E | 54.3 E | 54.3 E | | | | |
| | Overall Level of Service | _ | | | | | | | |
| | Overall Level of Service | Bike Pocket at | | <u> </u> | | | | | |
| | Type of Bikeway | Intersection | Mixed Traffic | Mixed Traffic | Mixed Traffic | | | | |
| | Turning Speed (based on corner radius & angle) | Slow | Slow | | | | | | |
| | Right Turn Storage Length | ≤ 50m | > 50m | | | | | | |
| | Dual Right Turn? | No | No | ., | ., | | | | |
| <u>is</u> : | Shared Through-Right? Bike Box? | No No | No No | Yes No | Yes No | | | | |
| Cyclist | | | | No Lanes | | | | | |
| O | Number of Lanes Crossed for Left Turns | 1 Lane Crossed | 1 Lane Crossed | Crossed | 1 Lane Crossed | | | | |
| | Operating Speed on Approach | ≥ 60km/h | ≥ 60km/h | ≥ 60km/h | ≥ 60km/h | | | | |
| | Dual Left Turn Lanes? | No | No | No | No | | | | |
| | Level of Service | E | F | - D | F | | | | |
| | | | | | | | | | |
| Sit | Average Signal Delay | ≤10 sec | ≤10 sec | | | | | | |
| Transit | Level of Service | | | <u>.</u> В | | | | | |
| | Turning Radius (Right Turn) | 10 to 15m | < 10m | < 10m | 10 to 15m | | | | |
| × | Number of Receiving Lanes | 10 10 15111 | 1 | 1 | 10 10 15111 | | | | |
| Truck | Training Laries | E | F | F | E | | | | |
| - | | | | = | | | | | |
| 0 | | | | | | | | | |
| Auto | Level of Service | | B (AM) | / B (PM) | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| SEGMI | ENTS | | Fallowfield – | Forager Street to 2 | O'Keete Court 3 | _ | | - | |
| | Sidewalk Width | | No Sidewalk | | ა | | | | |
| _ | Boulevard Width | | N/A | | | | | | |
| riar | AADT | | N/A | | | | | | |
| sti | | | | | | | | | |
| | On-Street Parking | | N/A | | | | | | |
| ed | On-Street Parking Operating Speed | | | | | | | | |
| Pedestrian | Operating Speed | | N/A | | | | | | |
| Ped | Operating Speed Level of Service | | N/A 61 km/h or more | F | | | | - | |
| Ped | Operating Speed Level of Service Type of Bikeway | | N/A 61 km/h or more | F Mixed Traffic | | | | | |
| Ped | Operating Speed Level of Service Type of Bikeway Number of Travel Lanes (per direction) | | N/A 61 km/h or more | F Mixed Traffic avel Lane Per Dire | ection | | | | |
| Ped | Operating Speed Level of Service Type of Bikeway Number of Travel Lanes (per direction) Raised Median? | | N/A 61 km/h or more | | ection | | | | |
| | Operating Speed Level of Service Type of Bikeway Number of Travel Lanes (per direction) Raised Median? Bike Lane Width | | N/A 61 km/h or more | | ection | | | | |
| | Operating Speed Level of Service Type of Bikeway Number of Travel Lanes (per direction) Raised Median? Bike Lane Width Operating Speed Bike Lane Blockages (Commercial Areas) | | N/A 61 km/h or more | avel Lane Per Dire | ection | | | | |
| Cyclist | Operating Speed Level of Service Type of Bikeway Number of Travel Lanes (per direction) Raised Median? Bike Lane Width Operating Speed Bike Lane Blockages (Commercial Areas) Median Refuge | | N/A 61 km/h or more | avel Lane Per Dire | ection | | | | |
| | Operating Speed Level of Service Type of Bikeway Number of Travel Lanes (per direction) Raised Median? Bike Lane Width Operating Speed Bike Lane Blockages (Commercial Areas) Median Refuge Number of Travel Lanes on Sidestreet | | N/A 61 km/h or more | avel Lane Per Dire | ection | | | | |
| | Operating Speed Level of Service Type of Bikeway Number of Travel Lanes (per direction) Raised Median? Bike Lane Width Operating Speed Bike Lane Blockages (Commercial Areas) Median Refuge Number of Travel Lanes on Sidestreet Sidestreet Operating Speed | | N/A 61 km/h or more | avel Lane Per Dire | ection | | | | |
| | Operating Speed Level of Service Type of Bikeway Number of Travel Lanes (per direction) Raised Median? Bike Lane Width Operating Speed Bike Lane Blockages (Commercial Areas) Median Refuge Number of Travel Lanes on Sidestreet | | N/A 61 km/h or more | avel Lane Per Dire | ection | | | | |
| Cyclist | Operating Speed Level of Service Type of Bikeway Number of Travel Lanes (per direction) Raised Median? Bike Lane Width Operating Speed Bike Lane Blockages (Commercial Areas) Median Refuge Number of Travel Lanes on Sidestreet Sidestreet Operating Speed | | N/A 61 km/h or more F | avel Lane Per Dire ≥ 70 km/h Mixed Traffic | | | | | |
| Cyclist | Operating Speed Level of Service Type of Bikeway Number of Travel Lanes (per direction) Raised Median? Bike Lane Width Operating Speed Bike Lane Blockages (Commercial Areas) Median Refuge Number of Travel Lanes on Sidestreet Sidestreet Operating Speed | | N/A 61 km/h or more F | avel Lane Per Dire ≥ 70 km/h | | | | | |
| Cyclist | Operating Speed Level of Service Type of Bikeway Number of Travel Lanes (per direction) Raised Median? Bike Lane Width Operating Speed Bike Lane Blockages (Commercial Areas) Median Refuge Number of Travel Lanes on Sidestreet Sidestreet Operating Speed Level of Service Facility Type Friction | | N/A 61 km/h or more F | avel Lane Per Dire ≥ 70 km/h Mixed Traffic | | | | | |
| | Operating Speed Level of Service Type of Bikeway Number of Travel Lanes (per direction) Raised Median? Bike Lane Width Operating Speed Bike Lane Blockages (Commercial Areas) Median Refuge Number of Travel Lanes on Sidestreet Sidestreet Operating Speed Level of Service Facility Type Friction Level of Service | | N/A 61 km/h or more F 1 Tra | avel Lane Per Dire ≥ 70 km/h Mixed Traffic I parking/driveway | | | | | |
| Transit Cyclist | Operating Speed Level of Service Type of Bikeway Number of Travel Lanes (per direction) Raised Median? Bike Lane Width Operating Speed Bike Lane Blockages (Commercial Areas) Median Refuge Number of Travel Lanes on Sidestreet Sidestreet Operating Speed Level of Service Facility Type Friction Level of Service Curb Lane Width | | N/A 61 km/h or more F 1 Tra Limited | avel Lane Per Dire ≥ 70 km/h Mixed Traffic I parking/driveway | | | | | |
| Transit Cyclist | Operating Speed Level of Service Type of Bikeway Number of Travel Lanes (per direction) Raised Median? Bike Lane Width Operating Speed Bike Lane Blockages (Commercial Areas) Median Refuge Number of Travel Lanes on Sidestreet Sidestreet Operating Speed Level of Service Facility Type Friction Level of Service | | N/A 61 km/h or more F 1 Tra | avel Lane Per Dire ≥ 70 km/h Mixed Traffic I parking/driveway | | | | | |
| Cyclist | Operating Speed Level of Service Type of Bikeway Number of Travel Lanes (per direction) Raised Median? Bike Lane Width Operating Speed Bike Lane Blockages (Commercial Areas) Median Refuge Number of Travel Lanes on Sidestreet Sidestreet Operating Speed Level of Service Facility Type Friction Level of Service Curb Lane Width | | N/A 61 km/h or more F 1 Tra Limited | avel Lane Per Dire ≥ 70 km/h Mixed Traffic I parking/driveway | | | | | |

Appendix I – Intersection Control Warrants

April 9, 2020 9

| Input Dat | a She | et | | Analysis | Sheet | Results | Sheet | Proposed | d Collision | |) Justificati | on: | |
|--|---|------------------------------------|------------------------------------|-----------------------------------|--------------------|--|----------------------|--|--|-------------------------------------|--------------------|--|------------------------------|
| What are the int | tersecting r | oadways? | Fa | allowfield Roa | ad & O'Kee | efe Court / 0 | Cobble Hill D | rive | | | | | ▼ |
| What is the dire | ction of the | Main Road | street? | Nor | th-South | • | When was t | he data colle | ected? | Future (202 | 8) Total Tra | iffic | |
| | | | | | | | | | | | | | |
| Justification | 1 - 4: Vo | olume Wa | rrants | | | | | | | | | | |
| a Number of I | anes on the | e Main Roa | d? | 1 | • | | | | | | | | |
| b Number of I | anes on the | e Minor Roa | ıd? | 1 | • | | | | | | | | |
| c How many a | approaches | ? 4 | • | | | | | | | | | | |
| d What is the | operating e | environmen | 1? | Urban | • | Popula | ition >= 10,000 | AND | Speed < 70 I | cm/hr | | | |
| e What is the | | | | intersection? | (Please fi | · | | | | | | | |
| C. What is the | | | | | | | , | | | l | | | |
| | | | | ☐ Minor F: | astbound A | pproach | ∣ Main So | | proach | Minor W | estbound A | | Dadastriana |
| Hour Ending | | rthbound A | | | , | | | ş <u>.</u> | | | | <u>.</u> | Pedestrians Crossing Main |
| | LT | TH | RT | LT | TH | RT | LT | TH | RT | LT | TH | RT | |
| 7:00 | LT 119 | TH 646 | RT 9 | LT 30 | TH 6 | RT 32 | LT 8 | TH 881 | 88 | 39 | | RT 42 | Crossing Main |
| 7:00 8:00 | LT 119 60 | TH 646 323 | RT 9 5 | LT 30 15 | TH 6 3 | RT 32 16 | LT 8 4 | TH 881 441 | 88 44 | 39 20 | | RT 42 21 | Crossing Main |
| 7:00 8:00 9:00 | LT 119 60 60 | TH 646 323 323 | RT 9 5 | LT 30 15 15 | TH 6 3 3 | RT 32 16 16 | LT 8 4 | TH 881 441 441 | 88 44 44 | 39 20 20 | | RT 42 21 21 | Crossing Main |
| 7:00 8:00 9:00 10:00 | LT 119 60 60 60 | TH 646 323 323 323 | RT 9 5 5 5 5 | LT 30 15 15 | TH 6 3 3 3 3 | RT 32 16 16 | 8 4 4 4 | TH 881 441 441 441 | 88 44 44 44 | 39 20 20 20 | | RT 42 21 21 21 | Crossing Main |
| 7:00 8:00 9:00 | LT 119 60 60 60 | TH 646 323 323 | RT 9 5 | LT 30 15 15 | TH 6 3 3 | RT 32 16 16 | 8 4 4 | TH 881 441 441 | 88 44 44 44 38 | 39 20 20 | | RT 42 21 21 | Crossing Main |
| 7:00 8:00 9:00 10:00 | LT 119 60 60 60 60 52 | TH 646 323 323 323 661 331 | 8T 9 5 5 5 23 | LT 30 15 15 15 17 107 | TH 6 3 3 3 3 3 3 | 8T 32 16 16 16 16 114 | LT 8 4 4 4 17 9 | TH 881 441 441 441 | 88 44 44 44 44 38 | 39 20 20 20 20 9 | | RT 42 21 21 21 21 20 | Crossing Main |
| 7:00 8:00 9:00 10:00 15:00 | LT 119 60 60 60 52 26 26 | TH 646 323 323 323 661 | RT 9 5 5 5 23 12 12 | LT 30 15 15 15 17 107 54 | TH 6 3 3 3 2 2 | RT 32 16 16 16 17 17 18 18 19 19 19 19 19 19 19 19 | LT 8 4 4 4 17 9 9 | TH 881 441 441 441 767 | 88 44 44 44 38 19 | 39 20 20 20 20 9 | | RT 42 21 21 21 20 | Crossing Main |
| 7:00 8:00 9:00 10:00 15:00 | LT 119 60 60 60 52 26 | TH 646 323 323 323 661 331 | 8T 9 5 5 5 23 12 | LT 30 15 15 15 17 15 15 15 15 107 | TH 6 3 3 3 3 2 | RT 32 16 16 16 114 57 | LT 8 4 4 4 17 9 | TH 881 441 441 441 767 384 | 88 44 44 44 38 19 | 39 20 20 20 20 9 | | RT 42 21 21 21 21 20 10 | Crossing Main |
| 7:00 8:00 9:00 10:00 15:00 16:00 17:00 | LT 119 60 60 50 52 26 26 | TH 646 323 323 323 323 661 331 331 | RT 9 5 5 5 23 12 12 | LT 30 15 15 15 107 54 54 | TH 6 3 3 3 3 2 2 | RT 32 16 16 16 16 17 114 57 57 | LT 8 4 4 4 17 9 9 | TH 881 441 441 441 767 384 384 | 88 44 44 44 38 19 | 39 20 20 20 9 5 5 | | RT 42 21 21 21 20 10 10 | Crossing Main |
| 7:00 8:00 9:00 10:00 15:00 16:00 17:00 | LT 119 60 60 60 52 26 26 | TH 646 323 323 323 661 331 331 331 | 8T 9 5 5 5 23 12 12 12 | LT 30 15 15 15 15 54 54 54 | TH 6 3 3 3 3 2 2 2 | RT 32 16 16 16 17 17 18 19 19 10 10 10 10 10 10 10 10 | LT 8 4 4 4 17 9 9 9 | TH 881 441 441 441 767 384 384 384 | 88 44 44 44 38 19 19 | 39 20 20 20 9 5 5 | TH 7 4 4 4 1 1 1 1 | RT 42 21 21 21 21 20 10 10 | Crossing Main Road |
| 7:00 8:00 9:00 10:00 15:00 16:00 17:00 | LT 119 60 60 60 52 26 26 | TH 646 323 323 323 661 331 331 331 | 8T 9 5 5 5 23 12 12 12 | LT 30 15 15 15 15 54 54 54 | TH 6 3 3 3 3 2 2 2 | RT 32 16 16 16 17 17 18 19 19 10 10 10 10 10 10 10 10 | LT 8 4 4 4 17 9 9 9 | TH 881 441 441 441 767 384 384 384 | 88 44 44 44 38 19 19 | 39 20 20 20 9 5 5 | TH 7 4 4 4 1 1 1 1 | RT 42 21 21 21 21 20 10 10 | Crossing Main Road |

Justification 5: Collision Experience

| Preceding Months | Number of Collisions* |
|---------------------|-----------------------|
| 1-12 | |
| 13-24 | |
| 25-36 | |

* Include only collisions that are susceptable to correction through the installation of traffic signal control

Justification 6: Pedestrian Volume

a.- Please fill in table below summarizing total pedestrians crossing major roadway at the intersection or in proximity to the intersection (zones). Please reference Section 4.8 of the Manual for further explanation and graphical representation.

| | Zon | e 1 | Zor | 1е 2 | Zone 3 (i | f needed) | Zone 4 (| (if needed) | Total |
|---------------------------------------|-------------|------------|----------|------------|-----------|------------|----------|-------------|-------|
| | Assisted | Unassisted | Assisted | Unassisted | Assisted | Unassisted | Assisted | Unassisted | Total |
| Total 8 hour pedestrian volume | | | | | | | | | |
| Factored 8 hour pedestrian volume | С |) | (| 0 | (|) | | 0 | |
| % Assigned to crossing rate | | | | | | | | | |
| Net 8 Hour Pedestrian Volume at Cross | sing | | | | | | | | 0 |
| Net 8 Hour Vehicular Volume on Street | Being Cross | ed | | | | | | | 6,411 |

b.- Please fill in table below summarizing delay to pedestrians crossing major roadway at the intersection or in proximity to the intersection (zones). Please reference Section 4.8 of the Manual for further explanation and graphical representation.

| | Zor | ne 1 | Zoi | ne 2 | Zone 3 (if | needed) | Zone 4 (| if needed) | Total |
|--|----------|------------|----------|------------|------------|------------|----------|------------|-------|
| | Assisted | Unassisted | Assisted | Unassisted | Assisted | Unassisted | Assisted | Unassisted | Total |
| Total 8 hour pedestrian volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Total 8 hour pedestrians delayed greater than 10 seconds | | | | | | | | | |
| Factored volume of total pedestrians | (|) | | 0 | C |) | | 0 | |
| Factored volume of delayed pedestrians | (|) | | 0 | C |) | | 0 | |
| % Assigned to Crossing Rate | 0' | % | 0 | % | 09 | % | (| 0% | |
| Net 8 Hour Volume of Total Pedestrian | 5 | | | | | | | | 0 |
| Net 8 Hour Volume of Delayed Pedestr | ians | | | | | | | | 0 |

| Results | Sheet | | <u>I</u> nput Sheet | Analy | sis Sheet | Propo | sed Collision | | GO TO Jus |
|-------------------------|-------------|-------------|--------------------------|------------|------------------|-------------|---------------|--|-----------|
| | | | Court / Cobble Hill Driv | ve Count D | Date: Future (20 | 28) Total T | raffic | | |
| Summary I | Results | | | | · | · | | | |
| | Justificati | ion | Complian | ce | Signal Ju | |] | | |
| 1. Minimum Vehicular | A Total | l Volume | 100 | % | YES | NO V | - | | |
| Volume | B Cros | sing Volume | 69 | % | | | | | |
| 2. Delay to Cross | A Main | Road | 100 | % | | ~ | | | |
| Traffic | B Cros | sing Road | 74 | % | | | | | |
| 3. Combination | A Justi | ficaton 1 | 69 | % | | V | | | |
| | B Justi | fication 2 | 74 | % | | | | | |
| 4. 4-Hr Volume | | | 67 | % | | ~ | | | |
| | | | | | | | 7 | | |
| 5. Collision Exp | erience | | 0 | % | | ~ | | | |
| | | | | | | | 1 | | |
| 6. Pedestrians | A Volur | me | Justification no | ot met | | | | | |

~

Justification not met

B Delay



City of Ottawa Roundabout Initial Feasability Screening Tool

The intent of this screening tool is to provide a relatively quick assessment of the feasibility of a roundabout at a particular intersection in comparison to other appropriate forms of traffic control or road modifications including all-way stop control, traffic signals, auxiliary lanes, etc. The intended outcome of this tool is to provide enough information to assist staff in deciding whether or not to proceed with an Intersection Control Study to investigate the feasibility of a roundabout in more detail.

| 1 | Project Name: | 115 Lusk Street - Transportation Impact Assessment |
|---|---|--|
| 2 | Intersection: | Fallowfield Road & O'Keefe Court / Cobble Hill Drive |
| | | |
| 3 | Location and Description of Intersection: Lane Configuration, total or approach AADT, distance to nearby intersection(s), etc. Attach or sketch a diagram and include existing and/or horizon-year turning movements. If an existing intersection then indicate type of control | The intersection is currently configured as a two-way stop-controlled intersection with free-flow on Fallowfield Road. |
| 4 | What traditional modifications are proposed? All-way stop control, traffic signals, auxiliary lanes, etc. Attach or sketch a diagram if necessary. | Traffic signals. |
| 5 | What size of roundabout is being considered? Describe, and attach a Roundabout Traffic Flow Worksheet | Multi-lane roundabout. |
| 6 | Why is a roundabout being considered? | As an alternative to traffic signals. |



7 a roundabout?

Are there contra-indications for If "Yes" is indicated for one or more of the contra-indications then a roundabout may be problematic at the subject intersection. That is not to say that a

| No. | Contra-Indication | Outcome |
|-----|--|----------|
| 1 | Is there insufficient property at the intersection (i.e. less than 44 metres diameter if considering a single-lane roundabout, and less than 60 metres if considering a two-lane roundabout) or property constraints that would require demolition of adjacent structures? | Yes No X |
| 2 | Are there any instances where stopping sight distance (SSD) of a roundabout yield line may not be attainable (i.e. the intersection is on a crest vertical curve)? | Yes No X |
| 3 | Is there an existing uncontrolled approach with a grade in excess of 4 percent? | Yes No X |
| 4 | Is the intersection located within a coordinated signal system? | Yes No X |
| 5 | Is there a closely-spaced traffic signal or railway crossing that could not be controlled with a nearby roundabout? | Yes No X |
| 6 | Are significant differences in directional flows or any situations of sudden high demand expected? | Yes No x |
| 7 | Are there known visually-impaired pedestrians that cross this intersection? | Yes No X |

8 Are there suitability factors for a roundabout?

If "Yes" is indicated for two or more of the suitability factors then a roundabout should be technically feasible at the subject intersection..

| No. | Suitability Factor | Outcome |
|-----|--|----------|
| 1 | Does the intersection currently experience an average collision frequency of more than 1.5 injury crashes per year, or a collision rate in excess of 1 injury crash per 1 million vehicles entering (MVE)? | Yes No X |
| 2 | Has there been a fatal crash at the intersection in the last 10 years? | Yes No X |
| 3 | Are capacity problems currently being experienced, or expected in the future? | Yes X No |
| 4 | Are traffic signals warranted, or expected to be warranted in the future? | Yes No X |
| 5 | Does the intersection have more than 4 legs, or unusual geometry? | Yes No X |
| 6 | Will Planned modifications to the intersection require that nearby structures be widened (i.e. to accommodate left-turn lanes)? | Yes No X |
| 7 | Is the intersection located at a transition between rural and urban environments (i.e. an urban boundary) such that a roundabout could act as a means of speed transition? | Yes No X |



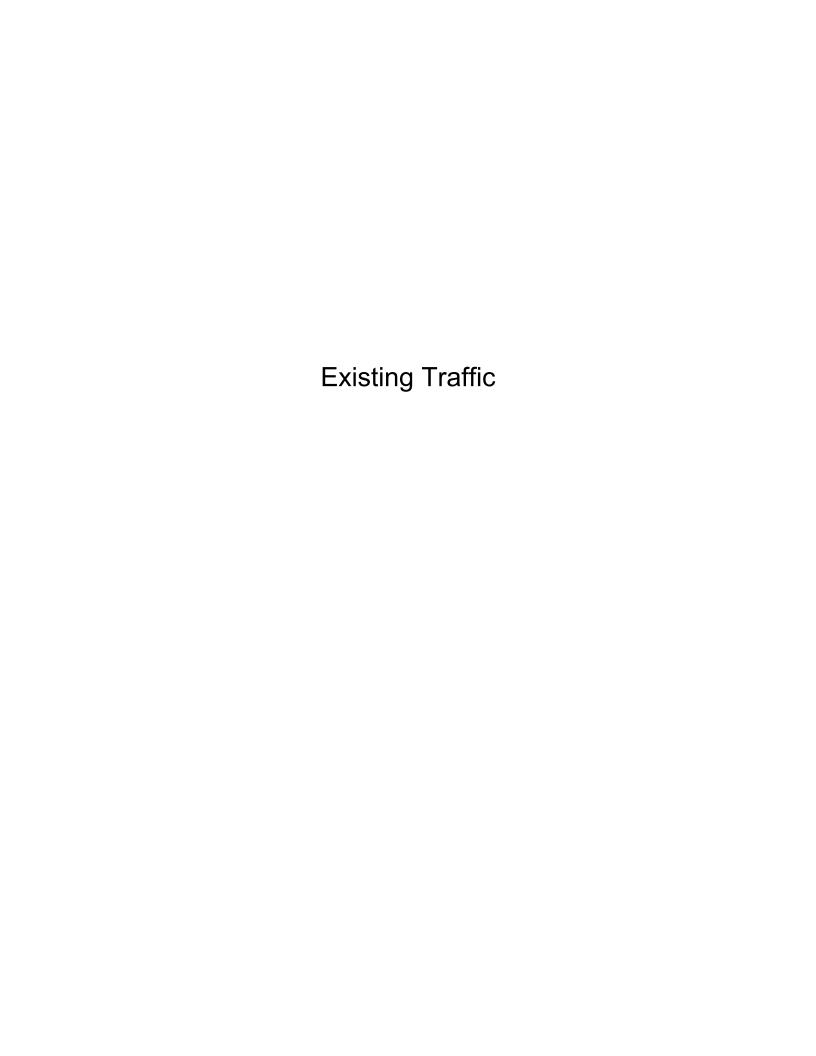
9 Conclusions/recommendation whether to proceed with an Intersection Control Study:

The results of the Roundabout Screening Tool indicate that the a roundabout is not feasible or recommended at the intersection of Fallowfield & O'Keefe/ Cobble Hill, given that only one of the suitability factors is met.



Appendix J – Intersection Capacity Analyses

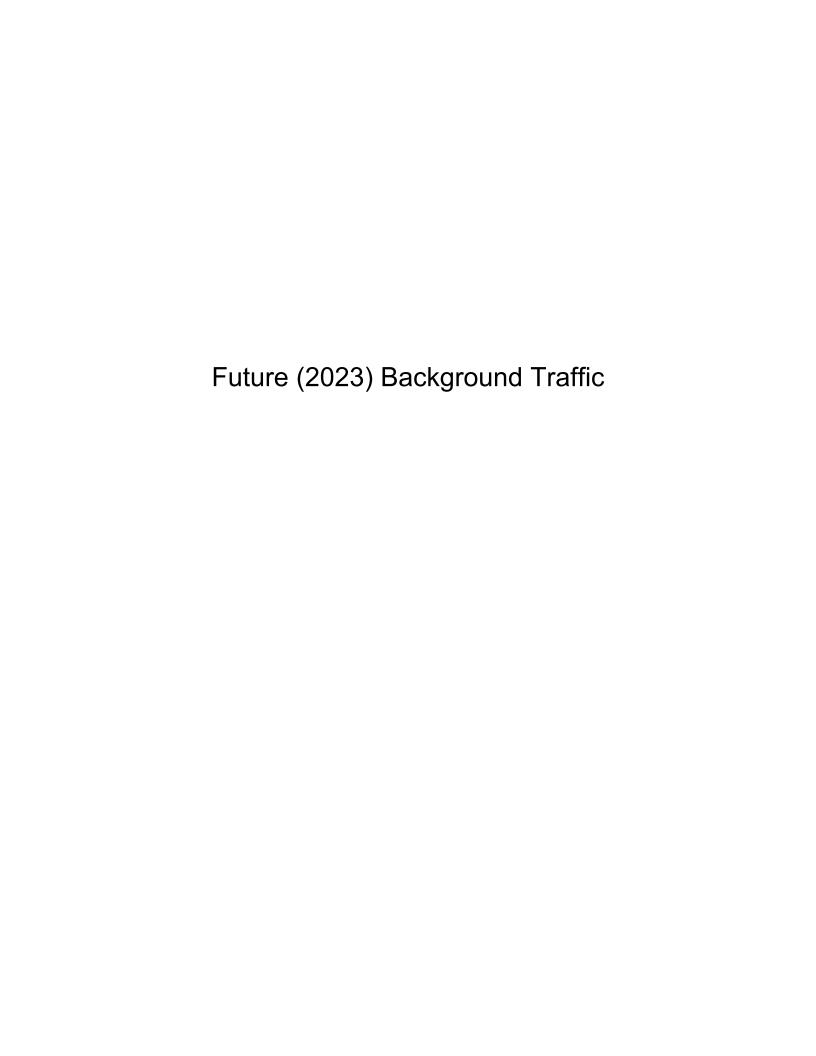
April 9, 2020 10



| Intersection | | | | | | | | | | | | |
|------------------------|---------|----------|-------|--------|-------|--------|--------|-------|------|--------|------|------|
| Int Delay, s/veh | 2.8 | | | | | | | | | | | |
| | | | | | | | | | | 0.51 | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ₽ | | | 4 | | | | 7 | | | 7 |
| Traffic Vol, veh/h | 7 | 6 | 19 | 39 | 7 | 42 | 5 | 496 | 9 | 8 | 454 | 5 |
| Future Vol, veh/h | 7 | 6 | 19 | 39 | 7 | 42 | 5 | 496 | 9 | 8 | 454 | 5 |
| Conflicting Peds, #/hr | 0 | 0 | 1 | 1 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 1 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 500 | - | - | - | - | - | 1400 | - | 0 | 600 | - | 250 |
| Veh in Median Storage, | , # - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, % | 0 | 0 | 5 | 3 | 14 | 0 | 0 | 5 | 56 | 12 | 4 | 0 |
| Mvmt Flow | 8 | 7 | 21 | 43 | 8 | 47 | 6 | 551 | 10 | 9 | 504 | 6 |
| | | | | | | | | | | | | |
| Major/Minor N | /linor2 | | | Minor1 | | | Major1 | | N | Major2 | | |
| Conflicting Flow All | 1119 | 1097 | 506 | 1104 | 1093 | 552 | 511 | 0 | 0 | 562 | 0 | 0 |
| Stage 1 | 523 | 523 | - | 564 | 564 | - | - | - | - | - | - | - |
| Stage 2 | 596 | 574 | _ | 540 | 529 | _ | _ | _ | _ | _ | _ | _ |
| Critical Hdwy | 7.1 | 6.5 | 6.25 | 7.13 | 6.64 | 6.2 | 4.1 | _ | _ | 4.22 | _ | _ |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | 0.25 | 6.13 | 5.64 | - 0.2 | | _ | _ | - 1.22 | _ | _ |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | _ | 6.13 | 5.64 | _ | _ | _ | _ | _ | _ | _ |
| Follow-up Hdwy | 3.5 | 4 | 3.345 | 3.527 | 4.126 | 3.3 | 2.2 | _ | _ | 2.308 | _ | _ |
| Pot Cap-1 Maneuver | 186 | 215 | 560 | 188 | 204 | 537 | 1065 | _ | _ | 961 | _ | _ |
| Stage 1 | 541 | 534 | - | 509 | 490 | | - | _ | _ | - 701 | _ | _ |
| Stage 2 | 494 | 506 | | 524 | 508 | | | _ | _ | | - | _ |
| Platoon blocked, % | 177 | 000 | | UZ-T | 000 | | | _ | _ | | _ | _ |
| Mov Cap-1 Maneuver | 163 | 211 | 559 | 174 | 201 | 536 | 1064 | _ | _ | 960 | _ | _ |
| Mov Cap-2 Maneuver | 163 | 211 | - | 174 | 201 | - 500 | - 1007 | _ | _ | | _ | _ |
| Stage 1 | 537 | 529 | _ | 505 | 487 | _ | _ | _ | _ | _ | _ | _ |
| Stage 2 | 441 | 502 | _ | 493 | 503 | _ | _ | _ | _ | _ | _ | _ |
| Jiugo Z | 771 | 302 | | 773 | 303 | | | | | | | |
| | | | | , | | | | | | 65 | | |
| Approach | EB | | | WB | | | NB | | | SB | | |
| HCM Control Delay, s | 17.7 | | | 26.8 | | | 0.1 | | | 0.2 | | |
| HCM LOS | С | | | D | | | | | | | | |
| | | | | | | | | | | | | |
| Minor Lane/Major Mvmt | t | NBL | NBT | NBR | EBLn1 | EBLn2V | VBLn1 | SBL | SBT | SBR | | |
| Capacity (veh/h) | | 1064 | - | - | 4.0 | 400 | 261 | 960 | - | - | | |
| HCM Lane V/C Ratio | | 0.005 | _ | | 0.048 | 0.069 | 0.375 | 0.009 | _ | _ | | |
| HCM Control Delay (s) | | 8.4 | - | - | 28.2 | 14.7 | 26.8 | 8.8 | - | - | | |
| HCM Lane LOS | | A | _ | - | D | В | D | A | - | - | | |
| HCM 95th %tile Q(veh) | | 0 | - | - | 0.1 | 0.2 | 1.7 | 0 | - | - | | |
| | | | | | 0.1 | 0.2 | 1.7 | | | | | |

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| Intersection | | | | | | | | | | | | |
|------------------------|---------|----------|------|--------|-----------|-----------|--------|----------|------|--------|---------|------|
| Int Delay, s/veh | 1.2 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ች | f) | | | 4 | | ች | | 7 | | | 7 |
| Traffic Vol, veh/h | 7 | 3 | 20 | 9 | 1 | 20 | 14 | 337 | 23 | 17 | 578 | 20 |
| Future Vol, veh/h | 7 | 3 | 20 | 9 | 1 | 20 | 14 | 337 | 23 | 17 | 578 | 20 |
| Conflicting Peds, #/hr | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 500 | - | - | - | - | - | 1400 | - | 0 | 600 | - | 250 |
| Veh in Median Storage, | , # - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, % | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 6 | 4 | 0 |
| Mvmt Flow | 8 | 3 | 22 | 10 | 1 | 22 | 16 | 374 | 26 | 19 | 642 | 22 |
| | | | | | | | | | | | | |
| Major/Minor N | /linor2 | | ľ | Minor1 | | ľ | Major1 | | ſ | Major2 | | |
| Conflicting Flow All | 1113 | 1112 | 642 | 1110 | 1108 | 376 | 664 | 0 | 0 | 400 | 0 | 0 |
| Stage 1 | 680 | 680 | - | 406 | 406 | - | - | - | - | - | - | - |
| Stage 2 | 433 | 432 | - | 704 | 702 | - | - | - | - | - | - | - |
| Critical Hdwy | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 | 4.1 | - | - | 4.16 | - | - |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | - | 6.1 | 5.5 | - | - | _ | _ | - | _ | _ |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | - | 6.1 | 5.5 | - | - | _ | - | _ | - | _ |
| Follow-up Hdwy | 3.5 | 4 | 3.3 | 3.5 | 4 | 3.3 | 2.2 | - | - | 2.254 | - | - |
| Pot Cap-1 Maneuver | 187 | 211 | 478 | 188 | 212 | 675 | 935 | - | - | 1137 | - | - |
| Stage 1 | 444 | 454 | - | 626 | 601 | - | - | - | - | - | - | - |
| Stage 2 | 605 | 586 | - | 431 | 443 | - | - | - | - | - | - | - |
| Platoon blocked, % | | | | | | | | - | - | | - | - |
| Mov Cap-1 Maneuver | 175 | 204 | 478 | 173 | 205 | 674 | 935 | - | - | 1137 | - | - |
| Mov Cap-2 Maneuver | 175 | 204 | - | 173 | 205 | - | - | - | - | - | - | - |
| Stage 1 | 436 | 446 | - | 615 | 591 | - | - | - | - | - | - | - |
| Stage 2 | 573 | 576 | - | 401 | 435 | - | - | - | - | - | - | - |
| | | | | | | | | | | | | |
| Approach | EB | | | WB | | | NB | | | SB | | |
| HCM Control Delay, s | 17.2 | | | 16.5 | | | 0.3 | | | 0.2 | | |
| HCM LOS | C | | | С | | | | | | | | |
| | | | | | | | | | | | | |
| Minor Lane/Major Mvmt | | NBL | NBT | NBR I | FBI n1 | EBLn2V | VBI n1 | SBL | SBT | SBR | | |
| Capacity (veh/h) | | 935 | 1101 | | 175 | 407 | 347 | 1137 | | ODIT | | |
| HCM Lane V/C Ratio | | 0.017 | - | _ | | | 0.096 | | - | | | |
| HCM Control Delay (s) | | 8.9 | - | - | 26.5 | 14.4 | 16.5 | 8.2 | - | - | | |
| HCM Lane LOS | | 0.9 A | - | - | 20.5 D | 14.4 B | 10.5 | 0.2 A | - | - | | |
| HCM 95th %tile Q(veh) | | 0.1 | - | - | 0.1 | 0.2 | 0.3 | 0.1 | - | - | | |
| HOW FOUT FOUTE Q(VEH) | | 0.1 | | | U. I | 0.2 | 0.5 | 0.1 | _ | | | |



| Intersection | | | | | | | | | | | | |
|-------------------------------------|-----------|-------|--------|--------|--------|--------------|--------|----------|----------|----------|----------|------------|
| Int Delay, s/veh | 7 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | T T | 1> | LDI | VVDL | 4 | אטיי | NDL | <u> </u> | NDK 7 | JDL 1 | <u> </u> | 30K |
| Traffic Vol, veh/h | 27 | 6 | 32 | 39 | 7 | 42 | 116 | 573 | 9 | 8 | 670 | 88 |
| Future Vol, veh/h | 27 | 6 | 32 | 39 | 7 | 42 | 116 | 573 | 9 | 8 | 670 | 88 |
| Conflicting Peds, #/hr | 0 | 0 | 1 | 1 | 0 | 0 | 1 | 0 | 1 | 1 | 0/0 | 1 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | Stop - | 310p | None | 310p | 310p | None | - | - | None | - | - | None |
| Storage Length | 500 | - | INOLIC | - | - | - | 1400 | - | 0 | 600 | - | 250 |
| Veh in Median Storage, | | 0 | - | _ | 0 | _ | 1400 | 0 | - | - | 0 | 250 |
| Grade, % | .# - | 0 | _ | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, % | 0 | 0 | 5 | 3 | 14 | 0 | 0 | 5 | 56 | 12 | 4 | 0 |
| Mymt Flow | 27 | 6 | 32 | 39 | 7 | 42 | 116 | 573 | 9 | 8 | 670 | 88 |
| IVIVIIIL F IUW | 21 | U | 32 | 37 | 1 | 42 | 110 | 5/3 | 9 | 0 | 070 | 00 |
| | | | | | | | | | | | | |
| | /linor2 | | | Minor1 | | | Major1 | | N | Major2 | | |
| Conflicting Flow All | 1521 | 1502 | 672 | 1556 | 1581 | 574 | 759 | 0 | 0 | 583 | 0 | 0 |
| Stage 1 | 687 | 687 | - | 806 | 806 | - | - | - | - | - | - | - |
| Stage 2 | 834 | 815 | - | 750 | 775 | - | - | - | - | - | - | - |
| Critical Hdwy | 7.1 | 6.5 | 6.25 | 7.13 | 6.64 | 6.2 | 4.1 | - | - | 4.22 | - | - |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | - | 6.13 | 5.64 | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | - | 6.13 | 5.64 | - | - | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 4 | 3.345 | 3.527 | 4.126 | 3.3 | 2.2 | - | - | 2.308 | - | - |
| Pot Cap-1 Maneuver | 98 | 123 | 451 | 91 | 102 | 522 | 862 | - | - | 944 | - | - |
| Stage 1 | 440 | 450 | - | 374 | 378 | - | - | - | - | - | - | - |
| Stage 2 | 365 | 394 | - | 402 | 391 | - | - | - | - | - | - | - |
| Platoon blocked, % | | | | | | | | - | - | | - | - |
| Mov Cap-1 Maneuver | 75 | 105 | 450 | 72 | 87 | 521 | 861 | - | - | 943 | - | - |
| Mov Cap-2 Maneuver | 75 | 105 | - | 72 | 87 | - | - | - | - | - | - | - |
| Stage 1 | 380 | 446 | - | 323 | 327 | - | - | - | - | - | - | - |
| Stage 2 | 284 | 340 | - | 365 | 387 | - | - | - | - | - | - | - |
| | | | | | | | | | | | | |
| Approach | EB | | | WB | | | NB | | | SB | | |
| HCM Control Delay, s | 43.4 | | | 83.6 | | | 1.6 | | | 0.1 | | |
| HCM LOS | F | | | F | | | 1.0 | | | J. 1 | | |
| | _ | | | • | | | | | | | | |
| Minor Lane/Major Mvm | | NBL | NBT | NIPD | ERI n1 | EBLn2V | VRI n1 | SBL | SBT | SBR | | |
| | | | NDI | NDK | | | | | 301 | אטכ | | |
| Capacity (veh/h) HCM Lane V/C Ratio | | 861 | - | - | 75 | 296 0.128 | 125 | 943 | - | - | | |
| | | 0.135 | - | - | | | | | - | - | | |
| HCM Lang LOS | | 9.8 | - | - | 77.9 | 18.9 | 83.6 | 8.8 | - | - | | |
| HCM CEth O(tillo O(toh) | | A | - | - | F | C | F | A | - | - | | |
| HCM 95th %tile Q(veh) | | 0.5 | - | - | 1.4 | 0.4 | 3.9 | 0 | - | - | | |

| | ۶ | → | • | € | + | • | • | † | <i>></i> | / | ţ | ✓ |
|-------------------------|---------|----------|-------|---------|-------|-------|---------|----------|-------------|----------|---------|---------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | f) | | | 4 | | ሻ | 1 | 7 | ሻ | | 7 |
| Traffic Volume (vph) | 27 | 6 | 32 | 39 | 7 | 42 | 116 | 573 | 9 | 8 | 670 | 88 |
| Future Volume (vph) | 27 | 6 | 32 | 39 | 7 | 42 | 116 | 573 | 9 | 8 | 670 | 88 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Storage Length (m) | 50.0 | | 0.0 | 0.0 | | 0.0 | 140.0 | | 0.0 | 60.0 | | 25.0 |
| Storage Lanes | 1 | | 0 | 0 | | 0 | 1 | | 1 | 1 | | 1 |
| Taper Length (m) | 7.5 | | | 7.5 | | | 7.5 | | | 7.5 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | | 0.98 | ,,,,, | | 1.00 | ,,,,, | 1.00 | ,,,,, | 0.98 | 1.00 | | 0.98 |
| Frt | | 0.874 | | | 0.936 | | | | 0.850 | | | 0.850 |
| Flt Protected | 0.950 | | | | 0.978 | | 0.950 | | | 0.950 | | 0.000 |
| Satd. Flow (prot) | 1729 | 1498 | 0 | 0 | 1626 | 0 | 1729 | 1733 | 992 | 1544 | 1750 | 1547 |
| Flt Permitted | 0.680 | | | | 0.839 | Ū | 0.382 | .,,,, | ,,_ | 0.430 | | |
| Satd. Flow (perm) | 1238 | 1498 | 0 | 0 | 1394 | 0 | 695 | 1733 | 969 | 698 | 1750 | 1512 |
| Right Turn on Red | 1200 | 1170 | Yes | U | 1071 | Yes | 070 | 1700 | Yes | 070 | 1700 | Yes |
| Satd. Flow (RTOR) | | 32 | 103 | | 36 | 103 | | | 23 | | | 51 |
| Link Speed (k/h) | | 50 | | | 50 | | | 60 | 20 | | 60 | 31 |
| Link Distance (m) | | 201.1 | | | 305.1 | | | 207.2 | | | 300.4 | |
| Travel Time (s) | | 14.5 | | | 22.0 | | | 12.4 | | | 18.0 | |
| Confl. Peds. (#/hr) | | 14.5 | 1 | 1 | 22.0 | | 1 | 12.7 | 1 | 1 | 10.0 | 1 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Heavy Vehicles (%) | 0% | 0% | 5% | 3% | 14% | 0% | 0% | 5% | 56% | 12% | 4% | 0% |
| Adj. Flow (vph) | 27 | 6 | 32 | 39 | 7 | 42 | 116 | 573 | 9 | 8 | 670 | 88 |
| Shared Lane Traffic (%) | 21 | U | 32 | 37 | , | 72 | 110 | 373 | , | U | 070 | 00 |
| Lane Group Flow (vph) | 27 | 38 | 0 | 0 | 88 | 0 | 116 | 573 | 9 | 8 | 670 | 88 |
| Turn Type | Perm | NA | U | Perm | NA | U | Perm | NA | Perm | Perm | NA | Perm |
| Protected Phases | 1 Cilli | 4 | | 1 Cilli | 8 | | 1 Citii | 2 | 1 Cilli | 1 Cilli | 6 | 1 Cilli |
| Permitted Phases | 4 | Т. | | 8 | U | | 2 | | 2 | 6 | 0 | 6 |
| Detector Phase | 4 | 4 | | 8 | 8 | | 2 | 2 | 2 | 6 | 6 | 6 |
| Switch Phase | ' | ' | | | U | | | | | J | | J |
| Minimum Initial (s) | 5.0 | 5.0 | | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 33.5 | 33.5 | | 33.5 | 33.5 | | 27.4 | 27.4 | 27.4 | 27.4 | 27.4 | 27.4 |
| Total Split (s) | 34.0 | 34.0 | | 34.0 | 34.0 | | 86.0 | 86.0 | 86.0 | 86.0 | 86.0 | 86.0 |
| Total Split (%) | 28.3% | 28.3% | | 28.3% | 28.3% | | 71.7% | 71.7% | 71.7% | 71.7% | 71.7% | 71.7% |
| Maximum Green (s) | 28.5 | 28.5 | | 28.5 | 28.5 | | 80.6 | 80.6 | 80.6 | 80.6 | 80.6 | 80.6 |
| Yellow Time (s) | 3.6 | 3.6 | | 3.6 | 3.6 | | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 |
| All-Red Time (s) | 1.9 | 1.9 | | 1.9 | 1.9 | | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 1.7 | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.5 | 5.5 | | | 5.5 | | 5.4 | 5.4 | 5.4 | 5.4 | 5.4 | 5.4 |
| Lead/Lag | 0.0 | 0.0 | | | 0.0 | | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| Lead-Lag Optimize? | | | | | | | | | | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None | | None | None | | Max | Max | Max | Max | Max | Max |
| Walk Time (s) | 7.0 | 7.0 | | 7.0 | 7.0 | | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Flash Dont Walk (s) | 21.0 | 21.0 | | 21.0 | 21.0 | | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 |
| Pedestrian Calls (#/hr) | 0 | 0 | | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Act Effct Green (s) | 9.4 | 9.4 | | U | 9.4 | | 87.5 | 87.5 | 87.5 | 87.5 | 87.5 | 87.5 |
| Actuated g/C Ratio | 0.09 | 0.09 | | | 0.09 | | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 |
| v/c Ratio | 0.09 | 0.09 | | | 0.09 | | 0.04 | 0.39 | 0.04 | 0.04 | 0.46 | 0.04 |
| VIC IXAIIO | 0.24 | U.ZJ | | | 0.50 | | 0.20 | 0.37 | 0.01 | 0.01 | 0.40 | 0.07 |

| | • | - | • | • | • | • | 4 | † | ~ | \ | ļ | 4 |
|------------------------|------|-------|-----|-----|-------|-----|-------|----------|------|----------|-------|------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 47.9 | 20.5 | | | 41.5 | | 3.7 | 4.0 | 0.4 | 2.8 | 4.5 | 1.5 |
| Queue Delay | 0.0 | 0.0 | | | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 47.9 | 20.5 | | | 41.5 | | 3.7 | 4.0 | 0.4 | 2.8 | 4.5 | 1.5 |
| LOS | D | С | | | D | | Α | Α | Α | Α | Α | Α |
| Approach Delay | | 31.9 | | | 41.5 | | | 3.9 | | | 4.1 | |
| Approach LOS | | С | | | D | | | Α | | | Α | |
| Queue Length 50th (m) | 5.1 | 1.1 | | | 10.0 | | 4.1 | 25.3 | 0.0 | 0.3 | 32.2 | 1.1 |
| Queue Length 95th (m) | 13.2 | 10.3 | | | 24.7 | | 11.1 | 49.7 | 0.5 | 1.4 | 62.9 | 4.7 |
| Internal Link Dist (m) | | 177.1 | | | 281.1 | | | 183.2 | | | 276.4 | |
| Turn Bay Length (m) | 50.0 | | | | | | 140.0 | | | 60.0 | | 25.0 |
| Base Capacity (vph) | 337 | 432 | | | 406 | | 582 | 1451 | 815 | 584 | 1466 | 1275 |
| Starvation Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.08 | 0.09 | | | 0.22 | | 0.20 | 0.39 | 0.01 | 0.01 | 0.46 | 0.07 |
| Intersection Summary | | | | | | | | | | | | |

Area Type: Other

Cycle Length: 120

Actuated Cycle Length: 104.5

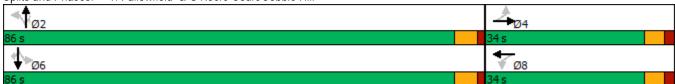
Natural Cycle: 70

Control Type: Semi Act-Uncoord Maximum v/c Ratio: 0.56

Intersection Signal Delay: 7.2 Intersection LOS: A Intersection Capacity Utilization 69.6% ICU Level of Service C

Analysis Period (min) 15

Splits and Phases: 1: Fallowfield & O'Keefe Court/Cobble Hill



Synchro 10 Report Lanes, Volumes, Timings ΕM March 2020

| Intersection | | | | | | |
|--------------------------|-------|-------|---------|------|--------|------|
| Int Delay, s/veh | 1.5 | | | | | |
| | | | | | | |
| | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | Þ | | | 4 | ¥ | |
| Traffic Vol, veh/h | 31 | 0 | 25 | 173 | 0 | 23 |
| Future Vol, veh/h | 31 | 0 | 25 | 173 | 0 | 23 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, # | # 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, % | 3 | 0 | 0 | 6 | 0 | 0 |
| Mvmt Flow | 31 | 0 | 25 | 173 | 0 | 23 |
| | 0. | | | .,, | | |
| | | | | | | |
| | ajor1 | | /lajor2 | Λ | Minor1 | |
| Conflicting Flow All | 0 | 0 | 31 | 0 | 254 | 31 |
| Stage 1 | - | - | - | - | 31 | - |
| Stage 2 | - | - | - | - | 223 | - |
| Critical Hdwy | - | - | 4.1 | - | 6.4 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.4 | - |
| Follow-up Hdwy | - | - | 2.2 | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | - | - | 1595 | - | 739 | 1049 |
| Stage 1 | - | - | - | - | 997 | - |
| Stage 2 | - | - | - | - | 819 | - |
| Platoon blocked, % | _ | - | | _ | | |
| Mov Cap-1 Maneuver | _ | _ | 1595 | _ | 726 | 1049 |
| Mov Cap-2 Maneuver | _ | _ | - | _ | 726 | - |
| Stage 1 | _ | | | | 997 | |
| Stage 2 | _ | | | | 805 | _ |
| Staye 2 | - | - | - | - | 000 | - |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 0.9 | | 8.5 | |
| HCM LOS | | | | | Α | |
| | | | | | | |
| Minor Long/Maior M | | JDI1 | EDT | EDD | WDI | MDT |
| Minor Lane/Major Mvmt | ľ | VBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | 1049 | - | | 1595 | - |
| HCM Lane V/C Ratio | | 0.022 | - | - | 0.016 | - |
| HCM Control Delay (s) | | 8.5 | - | - | 7.3 | 0 |
| HCM Lane LOS | | Α | - | - | Α | Α |
| HCM 95th %tile Q(veh) | | 0.1 | - | - | 0 | - |

| Intersection | | | | | | |
|------------------------|--------|-------|---------|----------|---------|------|
| Int Delay, s/veh | 0.1 | | | | | |
| | | EDE | ND | NDT | CDT | CDD |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | | 7 | | ^ | | 7 |
| Traffic Vol, veh/h | 0 | 13 | 0 | 699 | 737 | 8 |
| Future Vol, veh/h | 0 | 13 | 0 | 699 | 737 | 8 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 0 | - | - | - | 250 |
| Veh in Median Storage | | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, % | 0 | 0 | 0 | 6 | 4 | 0 |
| Mvmt Flow | 0 | 13 | 0 | 699 | 737 | 8 |
| | | | | | | |
| N 4 - 1 - 11/N 41 - 11 | A' O | | 1-!1 | | 4-! | |
| | Minor2 | | /lajor1 | | /lajor2 | |
| Conflicting Flow All | - | 737 | - | 0 | - | 0 |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | 6.2 | - | - | - | - |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | 3.3 | - | - | - | - |
| Pot Cap-1 Maneuver | 0 | 422 | 0 | - | - | - |
| Stage 1 | 0 | - | 0 | - | - | - |
| Stage 2 | 0 | - | 0 | - | - | - |
| Platoon blocked, % | | | | - | - | - |
| Mov Cap-1 Maneuver | - | 422 | - | - | - | - |
| Mov Cap-2 Maneuver | _ | - | - | - | - | - |
| Stage 1 | - | - | _ | - | - | - |
| Stage 2 | _ | _ | _ | _ | _ | _ |
| Jugo Z | | | | | | |
| | | | | | | |
| Approach | EB | | NB | | SB | |
| HCM Control Delay, s | 13.8 | | 0 | | 0 | |
| HCM LOS | В | | | | | |
| | | | | | | |
| Minor Lane/Major Mvm | ıt | NBT E | DI n1 | SBT | SBR | |
| | it . | | | SBI | SBK | |
| Capacity (veh/h) | | - | | - | - | |
| HCM Lane V/C Ratio | | | 0.031 | - | - | |
| HCM Control Delay (s) | | - | | - | - | |
| HCM Lane LOS | | - | В | - | - | |
| HCM 95th %tile Q(veh) | | - | 0.1 | - | - | |

| Interception | | | | | | | | | | | | |
|---------------------------------------|------------|-------------|----------|------------|------------|----------|---------|----------|------|--------|----------|------|
| Intersection | 8.7 | | | | | | | | | | | |
| Int Delay, s/veh | 8.7 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | ĵ. | | | 4 | | 1 | ↑ | 7 | | • | 7 |
| Traffic Vol, veh/h | 98 | 3 | 114 | 9 | 1 | 20 | 45 | 504 | 23 | 17 | 679 | 38 |
| Future Vol, veh/h | 98 | 3 | 114 | 9 | 1 | 20 | 45 | 504 | 23 | 17 | 679 | 38 |
| Conflicting Peds, #/hr | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 500 | - | - | - | - | - | 1400 | - | 0 | 600 | - | 250 |
| Veh in Median Storage, | , # - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, % | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 6 | 4 | 0 |
| Mvmt Flow | 98 | 3 | 114 | 9 | 1 | 20 | 45 | 504 | 23 | 17 | 679 | 38 |
| | | | | | | | | | | | | |
| Major/Minor N | /linor2 | | N | /linor1 | | N | Major1 | | | Major2 | | |
| | 1331 | 1330 | 679 | 1385 | 1345 | 506 | 717 | 0 | | 527 | 0 | 0 |
| Conflicting Flow All | 713 | 713 | | 594 | 594 | 500 | / 1 / | 0 | 0 | 0Z1 | 0 | 0 |
| Stage 1 | 618 | 617 | - | 791 | 751 | | - | - | | - | - | - |
| Stage 2 | 7.1 | 6.5 | - 6 2 | 7.1 | 6.5 | 6.2 | 4.1 | - | - | 4.16 | - | - |
| Critical Hdwy Stg 1 | | 5.5 | 6.2 | | 5.5 | 0.2 | 4.1 | - | - | 4.10 | - | - |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | - | 6.1 | | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.1 3.5 | | 3.3 | 6.1 | 5.5 | 3.3 | 2.2 | - | - | 2.254 | - | - |
| Follow-up Hdwy | 133 | 4 | | 3.5 | 152 | 570 | | - | - | | - | - |
| Pot Cap-1 Maneuver | 426 | 156 | 455 | 122 495 | 153 496 | 5/0 | 893 | - | - | 1020 | - | - |
| Stage 1 | | 438 | - | | | - | - | - | - | - | - | - |
| Stage 2 | 480 | 484 | - | 386 | 421 | - | - | - | - | - | - | - |
| Platoon blocked, % | 101 | 114 | 155 | 0E | 1/2 | E40 | 002 | - | - | 1020 | - | - |
| Mov Cap-1 Maneuver | 121 | 146 | 455 | 85 or | 143 | 569 | 893 | - | - | 1020 | - | - |
| Mov Cap-2 Maneuver | 121 | 146 | - | 85 | 143 | - | - | - | - | - | - | - |
| Stage 1 | 405 | 431 | - | 470 | 471 | - | - | - | - | - | - | - |
| Stage 2 | 438 | 460 | - | 282 | 414 | - | - | - | - | - | - | - |
| | | | | | | | | | | | | |
| Approach | EB | | | WB | | | NB | | | SB | | |
| HCM Control Delay, s | 56.6 | | | 25.8 | | | 0.7 | | | 0.2 | | |
| HCM LOS | F | | | D | | | | | | | | |
| | | | | | | | | | | | | |
| Minor Lane/Major Mvm | t | NBL | NBT | MRD | RI n1 | EBLn2V | //RI n1 | SBL | SBT | SBR | | |
| Capacity (veh/h) | | 893 | | | | 432 | | 1020 | 301 | אשכ | | |
| HCM Lane V/C Ratio | | | - | - | 121 | 0.271 | 203 | | - | - | | |
| | | 0.05 9.2 | - | - | | | 25.8 | | - | - | | |
| HCM Control Delay (s) HCM Lane LOS | | | - | - | 104.6 | 16.4 | | 8.6 | - | - | | |
| | | A 0.2 | - | - | F | C 1.1 | D | A | - | - | | |
| HCM 95th %tile Q(veh) | | U.Z | - | - | 4.8 | 1.1 | 0.5 | 0.1 | - | - | | |

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|-------------------------|-------|----------|------|-------|----------|------|-------|----------|-------------|----------|----------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ች | ₽ | | | 4 | | ሻ | 1 | 7 | ሻ | | 7 |
| Traffic Volume (vph) | 98 | 3 | 114 | 9 | 1 | 20 | 45 | 504 | 23 | 17 | 679 | 38 |
| Future Volume (vph) | 98 | 3 | 114 | 9 | 1 | 20 | 45 | 504 | 23 | 17 | 679 | 38 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Storage Length (m) | 50.0 | | 0.0 | 0.0 | | 0.0 | 140.0 | | 0.0 | 60.0 | | 25.0 |
| Storage Lanes | 1 | | 0 | 0 | | 0 | 1 | | 1 | 1 | | 1 |
| Taper Length (m) | 7.5 | | | 7.5 | | | 7.5 | | | 7.5 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 1.00 | | | | 0.98 | | | | | | | |
| Frt | | 0.854 | | | 0.910 | | | | 0.850 | | | 0.850 |
| Flt Protected | 0.950 | | | | 0.985 | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1729 | 1554 | 0 | 0 | 1605 | 0 | 1729 | 1750 | 1547 | 1631 | 1750 | 1547 |
| Flt Permitted | 0.738 | | | | 0.895 | | 0.362 | | | 0.456 | | |
| Satd. Flow (perm) | 1338 | 1554 | 0 | 0 | 1458 | 0 | 659 | 1750 | 1547 | 783 | 1750 | 1547 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | 114 | | | 20 | | | | 23 | | | 23 |
| Link Speed (k/h) | | 50 | | | 50 | | | 60 | | | 60 | |
| Link Distance (m) | | 201.1 | | | 305.1 | | | 207.2 | | | 300.4 | |
| Travel Time (s) | | 14.5 | | | 22.0 | | | 12.4 | | | 18.0 | |
| Confl. Peds. (#/hr) | 2 | | | | | 2 | | | | | | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Heavy Vehicles (%) | 0% | 0% | 0% | 0% | 0% | 0% | 0% | 4% | 0% | 6% | 4% | 0% |
| Adj. Flow (vph) | 98 | 3 | 114 | 9 | 1 | 20 | 45 | 504 | 23 | 17 | 679 | 38 |
| Shared Lane Traffic (%) | ,, | | | • | | | | | | | 0.7 | |
| Lane Group Flow (vph) | 98 | 117 | 0 | 0 | 30 | 0 | 45 | 504 | 23 | 17 | 679 | 38 |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | Perm | Perm | NA | Perm |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | • | | 8 | | | 2 | _ | 2 | 6 | | 6 |
| Detector Phase | 4 | 4 | | 8 | 8 | | 2 | 2 | 2 | 6 | 6 | 6 |
| Switch Phase | | • | | | | | _ | _ | _ | | | J |
| Minimum Initial (s) | 5.0 | 5.0 | | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 33.5 | 33.5 | | 33.5 | 33.5 | | 27.4 | 27.4 | 27.4 | 27.4 | 27.4 | 27.4 |
| Total Split (s) | 35.0 | 35.0 | | 35.0 | 35.0 | | 85.0 | 85.0 | 85.0 | 85.0 | 85.0 | 85.0 |
| Total Split (%) | 29.2% | 29.2% | | 29.2% | 29.2% | | 70.8% | 70.8% | 70.8% | 70.8% | 70.8% | 70.8% |
| Maximum Green (s) | 29.5 | 29.5 | | 29.5 | 29.5 | | 79.6 | 79.6 | 79.6 | 79.6 | 79.6 | 79.6 |
| Yellow Time (s) | 3.6 | 3.6 | | 3.6 | 3.6 | | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 |
| All-Red Time (s) | 1.9 | 1.9 | | 1.9 | 1.9 | | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 1.7 | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.5 | 5.5 | | | 5.5 | | 5.4 | 5.4 | 5.4 | 5.4 | 5.4 | 5.4 |
| Lead/Lag | 0.0 | 0.0 | | | 0.0 | | О. Т | 5.4 | 5.4 | 5.4 | 0.4 | 5.4 |
| Lead-Lag Optimize? | | | | | | | | | | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None | | None | None | | Max | Max | Max | Max | Max | Max |
| Walk Time (s) | 7.0 | 7.0 | | 7.0 | 7.0 | | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Flash Dont Walk (s) | 21.0 | 21.0 | | 21.0 | 21.0 | | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 |
| Pedestrian Calls (#/hr) | 21.0 | 21.0 | | 21.0 | 21.0 | | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 | 0 |
| Act Effct Green (s) | 13.0 | 13.0 | | U | 13.0 | | 82.6 | 82.6 | 82.6 | 82.6 | 82.6 | 82.6 |
| . , | | | | | | | | | | | | |
| Actuated g/C Ratio | 0.12 | 0.12 | | | 0.12 | | 0.77 | 0.77 | 0.77 | 0.77 | 0.77 | 0.77 |
| v/c Ratio | 0.60 | 0.40 | | | 0.15 | | 0.09 | 0.37 | 0.02 | 0.03 | 0.50 | 0.03 |

| | • | - | \rightarrow | • | ← | • | ~ | † | / | - | ļ | 4 |
|------------------------|------|-------|---------------|-----|----------|-----|----------|----------|----------|------|-------|------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 58.5 | 12.4 | | | 23.0 | | 4.1 | 5.1 | 1.5 | 3.7 | 6.4 | 2.1 |
| Queue Delay | 0.0 | 0.0 | | | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 58.5 | 12.4 | | | 23.0 | | 4.1 | 5.1 | 1.5 | 3.7 | 6.4 | 2.1 |
| LOS | Е | В | | | С | | Α | Α | Α | Α | Α | Α |
| Approach Delay | | 33.4 | | | 23.0 | | | 4.9 | | | 6.2 | |
| Approach LOS | | С | | | С | | | Α | | | Α | |
| Queue Length 50th (m) | 18.9 | 0.6 | | | 1.8 | | 1.8 | 26.5 | 0.0 | 0.7 | 41.5 | 0.6 |
| Queue Length 95th (m) | 35.2 | 15.7 | | | 10.0 | | 5.7 | 51.1 | 2.0 | 2.7 | 79.6 | 3.3 |
| Internal Link Dist (m) | | 177.1 | | | 281.1 | | | 183.2 | | | 276.4 | |
| Turn Bay Length (m) | 50.0 | | | | | | 140.0 | | | 60.0 | | 25.0 |
| Base Capacity (vph) | 370 | 512 | | | 418 | | 510 | 1356 | 1204 | 607 | 1356 | 1204 |
| Starvation Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.26 | 0.23 | | | 0.07 | | 0.09 | 0.37 | 0.02 | 0.03 | 0.50 | 0.03 |
| Intersection Summary | | | | | | | | | | | | |

Intersection Summary

Area Type: Other

Cycle Length: 120

Actuated Cycle Length: 106.6

Natural Cycle: 70

Control Type: Semi Act-Uncoord Maximum v/c Ratio: 0.60

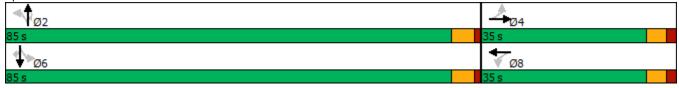
Intersection Signal Delay: 9.8

Intersection Capacity Utilization 61.0%

Intersection LOS: A ICU Level of Service B

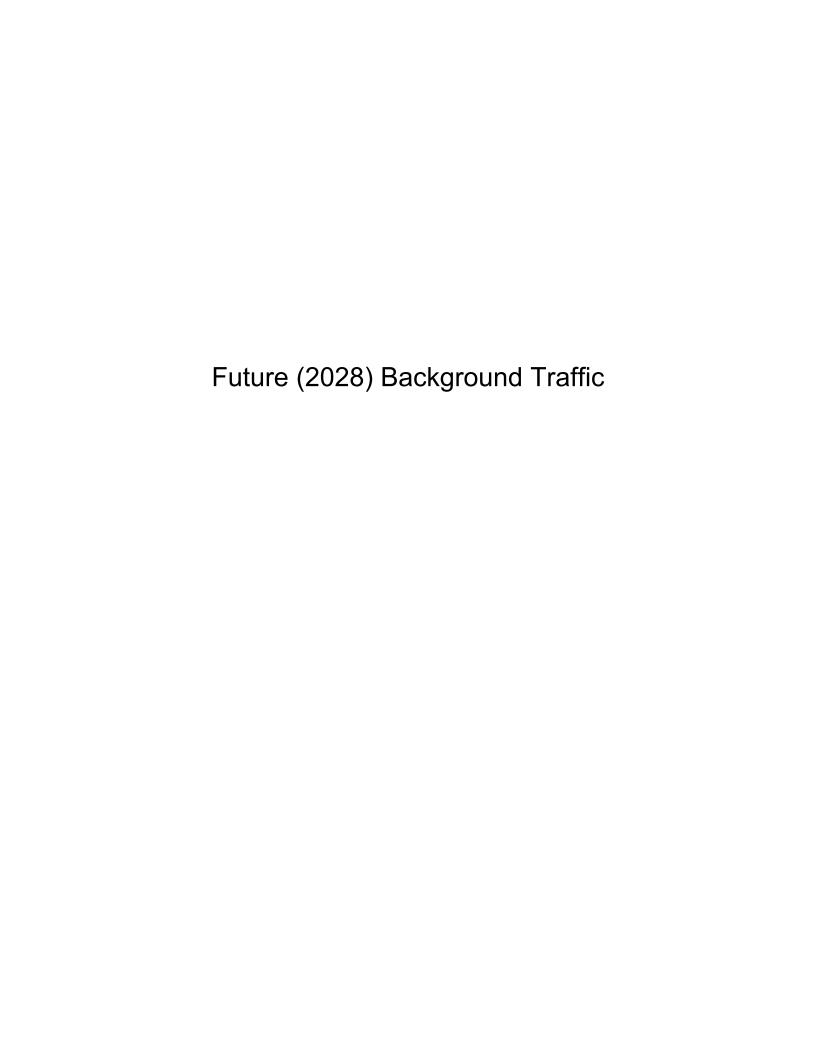
Analysis Period (min) 15

Splits and Phases: 1: Fallowfield & O'Keefe Court/Cobble Hill



| Intersection | | | | | | |
|------------------------------|-------|-------|---------|------|--------|------|
| Int Delay, s/veh | 1.3 | | | | | |
| | | EDD | MDI | MOT | ND | NIDD |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | f) | | | 4 | ¥ | |
| Traffic Vol, veh/h | 178 | 0 | 26 | 32 | 0 | 14 |
| Future Vol, veh/h | 178 | 0 | 26 | 32 | 0 | 14 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, | # 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, % | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 178 | 0 | 26 | 32 | 0 | 14 |
| | | | | | | |
| | | | | | | |
| | ajor1 | | /lajor2 | Λ | Minor1 | |
| Conflicting Flow All | 0 | 0 | 178 | 0 | 262 | 178 |
| Stage 1 | - | - | - | - | 178 | - |
| Stage 2 | - | - | - | - | 84 | - |
| Critical Hdwy | - | - | 4.1 | - | 6.4 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.4 | - |
| Follow-up Hdwy | _ | - | 2.2 | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | - | - | 1410 | - | 731 | 870 |
| Stage 1 | _ | - | - | _ | 858 | - |
| Stage 2 | _ | - | - | _ | 944 | - |
| Platoon blocked, % | _ | _ | | _ | 711 | |
| Mov Cap-1 Maneuver | | _ | 1410 | _ | 717 | 870 |
| Mov Cap-1 Maneuver | - | | 1410 | - | 717 | 070 |
| | - | - | - | - | 858 | |
| Stage 1 | - | - | - | - | | - |
| Stage 2 | - | - | - | - | 926 | - |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 3.4 | | 9.2 | |
| HCM LOS | - 0 | | J.7 | | Α.Σ | |
| TIOWI LOO | | | | | А | |
| | | | | | | |
| Minor Lane/Major Mvmt | 1 | VBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | 870 | - | | 1410 | |
| HCM Lane V/C Ratio | | 0.016 | - | | 0.018 | - |
| HCM Control Delay (s) | | 9.2 | - | - | | 0 |
| HCM Lane LOS | | Α | - | - | Α | A |
| HCM 95th %tile Q(veh) | | 0 | _ | - | 0.1 | - |
| 1.5111 75111 751110 (2(1011) | | U | | | 0.1 | |

| Intersection | | | | | | |
|--------------------------|--------|-------|---------|----------|---------|------|
| Int Delay, s/veh | 0.2 | | | | | |
| | | | | | 0== | 0.5. |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | | 7 | | ^ | | - 7 |
| Traffic Vol, veh/h | 0 | 17 | 0 | 575 | 798 | 7 |
| Future Vol, veh/h | 0 | 17 | 0 | 575 | 798 | 7 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 0 | - | - | - | 250 |
| Veh in Median Storage, | # 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, % | 0 | 0 | 0 | 3 | 4 | 0 |
| Mvmt Flow | 0 | 17 | 0 | 575 | 798 | 7 |
| | | | | | | |
| NA - 1/NA1 NA | ! | | 1-!1 | | 4-! | |
| | linor2 | | /lajor1 | | /lajor2 | |
| Conflicting Flow All | - | 798 | - | 0 | - | 0 |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | 6.2 | - | - | - | - |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | 3.3 | - | - | - | - |
| Pot Cap-1 Maneuver | 0 | 389 | 0 | - | - | - |
| Stage 1 | 0 | - | 0 | - | - | - |
| Stage 2 | 0 | - | 0 | - | - | - |
| Platoon blocked, % | | | | - | - | - |
| Mov Cap-1 Maneuver | - | 389 | - | - | - | - |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | _ | - | - | - | _ | - |
| Stage 2 | _ | | _ | _ | _ | _ |
| 3 - | | | | | | |
| | | | . LID | | 0.5 | |
| Approach | EB | | NB | | SB | |
| HCM Control Delay, s | 14.7 | | 0 | | 0 | |
| HCM LOS | В | | | | | |
| | | | | | | |
| Minor Lane/Major Mvmt | | NBT E | RI n1 | SBT | SBR | |
| Capacity (veh/h) | | וטוו | 389 | 301 | JUIC | |
| HCM Lane V/C Ratio | | • | 0.044 | • | - | |
| HCM Control Delay (s) | | - | 14.7 | - | - | |
| HCM Lane LOS | | • | | - | - | |
| HCM 95th %tile Q(veh) | | - | В | - | - | |
| nulyi yaiti %ille Utven) | | - | 0.1 | - | - | |



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|-------------------------|-------|----------------|------|-------|----------|------|-------|----------|-------------|----------|----------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | (î | | | 4 | | ሻ | 1 | 7 | ሻ | ^ | 7 |
| Traffic Volume (vph) | 27 | 6 | 32 | 39 | 7 | 42 | 116 | 646 | 9 | 8 | 876 | 88 |
| Future Volume (vph) | 27 | 6 | 32 | 39 | 7 | 42 | 116 | 646 | 9 | 8 | 876 | 88 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Storage Length (m) | 50.0 | | 0.0 | 0.0 | | 0.0 | 140.0 | | 0.0 | 60.0 | | 25.0 |
| Storage Lanes | 1 | | 0 | 0 | | 0 | 1 | | 1 | 1 | | 1 |
| Taper Length (m) | 7.5 | | | 7.5 | | | 7.5 | | | 7.5 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | | 0.98 | | | 1.00 | | | | 0.98 | 1.00 | | 0.98 |
| Frt | | 0.874 | | | 0.936 | | | | 0.850 | | | 0.850 |
| Flt Protected | 0.950 | | | | 0.978 | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1729 | 1498 | 0 | 0 | 1626 | 0 | 1729 | 1733 | 992 | 1544 | 1750 | 1547 |
| Flt Permitted | 0.678 | | | | 0.839 | | 0.289 | | | 0.394 | | |
| Satd. Flow (perm) | 1234 | 1498 | 0 | 0 | 1394 | 0 | 526 | 1733 | 969 | 640 | 1750 | 1512 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | 32 | | | 36 | | | | 23 | | | 40 |
| Link Speed (k/h) | | 50 | | | 50 | | | 60 | | | 60 | |
| Link Distance (m) | | 201.1 | | | 305.1 | | | 207.2 | | | 300.4 | |
| Travel Time (s) | | 14.5 | | | 22.0 | | | 12.4 | | | 18.0 | |
| Confl. Peds. (#/hr) | | | 1 | 1 | | | 1 | | 1 | 1 | | 1 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Heavy Vehicles (%) | 0% | 0% | 5% | 3% | 14% | 0% | 0% | 5% | 56% | 12% | 4% | 0% |
| Adj. Flow (vph) | 27 | 6 | 32 | 39 | 7 | 42 | 116 | 646 | 9 | 8 | 876 | 88 |
| Shared Lane Traffic (%) | | | | 0, | • | | | 0.0 | , | | 0.0 | |
| Lane Group Flow (vph) | 27 | 38 | 0 | 0 | 88 | 0 | 116 | 646 | 9 | 8 | 876 | 88 |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | Perm | Perm | NA | Perm |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | _ | 2 | 6 | | 6 |
| Detector Phase | 4 | 4 | | 8 | 8 | | 2 | 2 | 2 | 6 | 6 | 6 |
| Switch Phase | | | | | | | _ | _ | _ | | | J |
| Minimum Initial (s) | 5.0 | 5.0 | | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 33.5 | 33.5 | | 33.5 | 33.5 | | 27.4 | 27.4 | 27.4 | 27.4 | 27.4 | 27.4 |
| Total Split (s) | 33.5 | 33.5 | | 33.5 | 33.5 | | 86.5 | 86.5 | 86.5 | 86.5 | 86.5 | 86.5 |
| Total Split (%) | 27.9% | 27.9% | | 27.9% | 27.9% | | 72.1% | 72.1% | 72.1% | 72.1% | 72.1% | 72.1% |
| Maximum Green (s) | 28.0 | 28.0 | | 28.0 | 28.0 | | 81.1 | 81.1 | 81.1 | 81.1 | 81.1 | 81.1 |
| Yellow Time (s) | 3.6 | 3.6 | | 3.6 | 3.6 | | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 |
| All-Red Time (s) | 1.9 | 1.9 | | 1.9 | 1.9 | | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 1.7 | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.5 | 5.5 | | | 5.5 | | 5.4 | 5.4 | 5.4 | 5.4 | 5.4 | 5.4 |
| Lead/Lag | 0.0 | 3.3 | | | 0.0 | | Э. т | 5.4 | 5.4 | 5.4 | Э. т | 5.4 |
| Lead-Lag Optimize? | | | | | | | | | | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None | | None | None | | Max | Max | Max | Max | Max | Max |
| Walk Time (s) | 7.0 | 7.0 | | 7.0 | 7.0 | | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Flash Dont Walk (s) | 21.0 | 21.0 | | 21.0 | 21.0 | | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 |
| Pedestrian Calls (#/hr) | 0 | 0 | | 21.0 | 21.0 | | 0 | 0 | 15.0 | 15.0 | 0 | 0 |
| Act Effct Green (s) | 9.5 | 9.5 | | U | 9.5 | | 88.1 | 88.1 | 88.1 | 88.1 | 88.1 | 88.1 |
| . , | | | | | | | | | | | | |
| Actuated g/C Ratio | 0.09 | 0.09 | | | 0.09 | | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 |
| v/c Ratio | 0.25 | 0.23 | | | 0.56 | | 0.26 | 0.44 | 0.01 | 0.01 | 0.60 | 0.07 |

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|------------------------|------|-------|---------------|-----|----------|-----|-------|----------|----------|------|-------|------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 48.3 | 20.6 | | | 41.6 | | 4.6 | 4.4 | 0.4 | 2.8 | 6.2 | 1.7 |
| Queue Delay | 0.0 | 0.0 | | | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 48.3 | 20.6 | | | 41.6 | | 4.6 | 4.4 | 0.4 | 2.8 | 6.2 | 1.7 |
| LOS | D | С | | | D | | Α | Α | Α | Α | Α | Α |
| Approach Delay | | 32.1 | | | 41.6 | | | 4.4 | | | 5.8 | |
| Approach LOS | | С | | | D | | | Α | | | Α | |
| Queue Length 50th (m) | 5.1 | 1.1 | | | 10.0 | | 4.4 | 30.8 | 0.0 | 0.3 | 52.4 | 1.5 |
| Queue Length 95th (m) | 13.3 | 10.4 | | | 24.9 | | 12.7 | 59.8 | 0.5 | 1.4 | 104.1 | 5.2 |
| Internal Link Dist (m) | | 177.1 | | | 281.1 | | | 183.2 | | | 276.4 | |
| Turn Bay Length (m) | 50.0 | | | | | | 140.0 | | | 60.0 | | 25.0 |
| Base Capacity (vph) | 329 | 423 | | | 398 | | 441 | 1452 | 816 | 536 | 1467 | 1274 |
| Starvation Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.08 | 0.09 | | | 0.22 | | 0.26 | 0.44 | 0.01 | 0.01 | 0.60 | 0.07 |

Intersection Summary

Area Type: Other

Cycle Length: 120

Actuated Cycle Length: 105.1

Natural Cycle: 90

Control Type: Semi Act-Uncoord

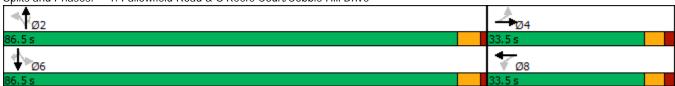
Maximum v/c Ratio: 0.60

Intersection Signal Delay: 7.8
Intersection Capacity Utilization 81.1%

Intersection LOS: A ICU Level of Service D

Analysis Period (min) 15

Splits and Phases: 1: Fallowfield Road & O'Keefe Court/Cobble Hill Drive



| Intersection | | | | | | |
|--|--------|-------|--------|------|---------|------|
| Int Delay, s/veh | 1.5 | | | | | |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | ĵ. | | | 4 | W | |
| Traffic Vol, veh/h | 31 | 0 | 25 | 173 | 0 | 23 |
| Future Vol, veh/h | 31 | 0 | 25 | 173 | 0 | 23 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | _ | - | _ | - | 0 | - |
| Veh in Median Storage, | # 0 | _ | _ | 0 | 0 | _ |
| Grade, % | 0 | _ | _ | 0 | 0 | _ |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, % | 3 | 0 | 0 | 6 | 0 | 0 |
| Mymt Flow | 31 | 0 | 25 | 173 | 0 | 23 |
| IVIVIII(I IOVV | JI | U | 25 | 173 | U | 23 |
| | | | | | | |
| | lajor1 | N | Major2 | Λ | /linor1 | |
| Conflicting Flow All | 0 | 0 | 31 | 0 | 254 | 31 |
| Stage 1 | - | - | - | - | 31 | - |
| Stage 2 | - | - | - | - | 223 | - |
| Critical Hdwy | - | - | 4.1 | - | 6.4 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.4 | - |
| Follow-up Hdwy | - | - | 2.2 | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | - | - | 1595 | - | 739 | 1049 |
| Stage 1 | - | - | - | - | 997 | - |
| Stage 2 | - | - | - | - | 819 | - |
| Platoon blocked, % | - | - | | - | | |
| Mov Cap-1 Maneuver | - | - | 1595 | - | 726 | 1049 |
| Mov Cap-2 Maneuver | - | - | - | - | 726 | - |
| Stage 1 | - | - | _ | - | 997 | - |
| Stage 2 | - | - | _ | - | 805 | _ |
| The grade of the g | | | | | | |
| | | | \4/D | | ND | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 0.9 | | 8.5 | |
| HCM LOS | | | | | Α | |
| | | | | | | |
| Minor Lane/Major Mvmt | | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | 1049 | - | - | 1595 | - |
| HCM Lane V/C Ratio | | 0.022 | - | - | 0.016 | - |
| HCM Control Delay (s) | | 8.5 | - | - | 7.3 | 0 |
| HCM Lane LOS | | А | - | - | Α | A |
| HCM 95th %tile Q(veh) | | 0.1 | - | - | 0 | - |
| | | | | | | |

| Intersection | | | | | | |
|---|-----------|-------|-----------------------|---------------|----------|------|
| Int Delay, s/veh | 0.1 | | | | | |
| | | EDD | ND | NET | ODT | 000 |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | | 7 | | ^ | ↑ | 7 |
| Traffic Vol, veh/h | 0 | 13 | 0 | 773 | 949 | 8 |
| Future Vol, veh/h | 0 | 13 | 0 | 773 | 949 | 8 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 0 | - | - | - | 250 |
| Veh in Median Storage, | , # 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, % | 0 | 0 | 0 | 6 | 4 | 0 |
| Mvmt Flow | 0 | 13 | 0 | 773 | 949 | 8 |
| | | | | | | |
| N A = 1 = 1/N A1 = = | 4' | | 1-1-1 | | 4-1-0 | |
| | /linor2 | | Major1 | | /lajor2 | |
| Conflicting Flow All | - | 949 | - | 0 | - | 0 |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | 6.2 | - | - | - | - |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | 3.3 | - | - | - | - |
| Pot Cap-1 Maneuver | 0 | 319 | 0 | - | - | - |
| Stage 1 | 0 | - | 0 | - | - | - |
| Stage 2 | 0 | - | 0 | - | - | - |
| Platoon blocked, % | | | | | _ | _ |
| Mov Cap-1 Maneuver | _ | 319 | _ | _ | _ | _ |
| Mov Cap-2 Maneuver | _ | | _ | _ | _ | _ |
| Stage 1 | | | | | | _ |
| Stage 2 | - | - | _ | _ | - | _ |
| Staye 2 | - | - | - | - | - | - |
| | | | | | | |
| Approach | EB | | NB | | SB | |
| | | | | | 0 | |
| | 16.8 | | 0 | | U | |
| HCM Control Delay, s HCM LOS | 16.8 C | | 0 | | U | |
| HCM Control Delay, s | | | 0 | | 0 | |
| HCM Control Delay, s HCM LOS | С | NPT | | CDT | | |
| HCM Control Delay, s HCM LOS Minor Lane/Major Mvml | С | NBT E | EBLn1 | SBT | SBR | |
| HCM Control Delay, s HCM LOS Minor Lane/Major Mvmt Capacity (veh/h) | С | - | EBLn1 319 | SBT - | | |
| HCM Control Delay, s HCM LOS Minor Lane/Major Mvml Capacity (veh/h) HCM Lane V/C Ratio | С | - | EBLn1 319 0.041 | SBT - - | | |
| HCM Control Delay, s HCM LOS Minor Lane/Major Mvml Capacity (veh/h) HCM Lane V/C Ratio HCM Control Delay (s) | С | - | 319 0.041 16.8 | - | | |
| HCM Control Delay, s HCM LOS Minor Lane/Major Mvml Capacity (veh/h) HCM Lane V/C Ratio | C t | - | EBLn1 319 0.041 | - | | |

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|-------------------------|-------|----------|------|-------|----------|------|-------|---------|-------------|-------|----------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ች | f) | | | 4 | | ሻ | | 7 | * | | 7 |
| Traffic Volume (vph) | 98 | 3 | 114 | 9 | 1 | 20 | 45 | 661 | 23 | 17 | 757 | 38 |
| Future Volume (vph) | 98 | 3 | 114 | 9 | 1 | 20 | 45 | 661 | 23 | 17 | 757 | 38 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Storage Length (m) | 50.0 | | 0.0 | 0.0 | | 0.0 | 140.0 | | 0.0 | 60.0 | | 25.0 |
| Storage Lanes | 1 | | 0 | 0 | | 0 | 1 | | 1 | 1 | | 1 |
| Taper Length (m) | 7.5 | | | 7.5 | | | 7.5 | | | 7.5 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 1.00 | | | | 0.98 | | | | | | | |
| Frt | | 0.854 | | | 0.910 | | | | 0.850 | | | 0.850 |
| Flt Protected | 0.950 | | | | 0.985 | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1729 | 1554 | 0 | 0 | 1605 | 0 | 1729 | 1750 | 1547 | 1631 | 1750 | 1547 |
| Flt Permitted | 0.738 | | | | 0.895 | | 0.324 | | | 0.372 | | |
| Satd. Flow (perm) | 1338 | 1554 | 0 | 0 | 1458 | 0 | 590 | 1750 | 1547 | 639 | 1750 | 1547 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | 114 | | | 20 | | | | 23 | | | 23 |
| Link Speed (k/h) | | 50 | | | 50 | | | 60 | | | 60 | |
| Link Distance (m) | | 201.1 | | | 305.1 | | | 207.2 | | | 300.4 | |
| Travel Time (s) | | 14.5 | | | 22.0 | | | 12.4 | | | 18.0 | |
| Confl. Peds. (#/hr) | 2 | | | | | 2 | | | | | | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Heavy Vehicles (%) | 0% | 0% | 0% | 0% | 0% | 0% | 0% | 4% | 0% | 6% | 4% | 0% |
| Adj. Flow (vph) | 98 | 3 | 114 | 9 | 1 | 20 | 45 | 661 | 23 | 17 | 757 | 38 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 98 | 117 | 0 | 0 | 30 | 0 | 45 | 661 | 23 | 17 | 757 | 38 |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | Perm | Perm | NA | Perm |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | 2 | 6 | | 6 |
| Detector Phase | 4 | 4 | | 8 | 8 | | 2 | 2 | 2 | 6 | 6 | 6 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 33.5 | 33.5 | | 33.5 | 33.5 | | 27.4 | 27.4 | 27.4 | 27.4 | 27.4 | 27.4 |
| Total Split (s) | 34.0 | 34.0 | | 34.0 | 34.0 | | 86.0 | 86.0 | 86.0 | 86.0 | 86.0 | 86.0 |
| Total Split (%) | 28.3% | 28.3% | | 28.3% | 28.3% | | 71.7% | 71.7% | 71.7% | 71.7% | 71.7% | 71.7% |
| Maximum Green (s) | 28.5 | 28.5 | | 28.5 | 28.5 | | 80.6 | 80.6 | 80.6 | 80.6 | 80.6 | 80.6 |
| Yellow Time (s) | 3.6 | 3.6 | | 3.6 | 3.6 | | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 |
| All-Red Time (s) | 1.9 | 1.9 | | 1.9 | 1.9 | | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 |
| Lost Time Adjust (s) | 0.0 | 0.0 | | | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.5 | 5.5 | | | 5.5 | | 5.4 | 5.4 | 5.4 | 5.4 | 5.4 | 5.4 |
| Lead/Lag | | | | | | | | | | | | |
| Lead-Lag Optimize? | | | | | | | | | | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None | | None | None | | Max | Max | Max | Max | Max | Max |
| Walk Time (s) | 7.0 | 7.0 | | 7.0 | 7.0 | | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Flash Dont Walk (s) | 21.0 | 21.0 | | 21.0 | 21.0 | | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 |
| Pedestrian Calls (#/hr) | 0 | 0 | | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Act Effct Green (s) | 13.1 | 13.1 | | | 13.1 | | 83.7 | 83.7 | 83.7 | 83.7 | 83.7 | 83.7 |
| Actuated g/C Ratio | 0.12 | 0.12 | | | 0.12 | | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 |
| v/c Ratio | 0.60 | 0.40 | | | 0.15 | | 0.10 | 0.49 | 0.02 | 0.03 | 0.56 | 0.03 |

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|------------------------|------|----------|-----|-----|----------|-----|-------|----------|------|------|-------|------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 59.2 | 12.5 | | | 23.2 | | 4.2 | 6.3 | 1.5 | 3.8 | 7.2 | 2.1 |
| Queue Delay | 0.0 | 0.0 | | | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 59.2 | 12.5 | | | 23.2 | | 4.2 | 6.3 | 1.5 | 3.8 | 7.2 | 2.1 |
| LOS | Е | В | | | С | | Α | Α | Α | Α | Α | Α |
| Approach Delay | | 33.8 | | | 23.2 | | | 6.0 | | | 6.9 | |
| Approach LOS | | С | | | С | | | Α | | | Α | |
| Queue Length 50th (m) | 19.1 | 0.6 | | | 1.8 | | 1.8 | 40.0 | 0.0 | 0.7 | 50.3 | 0.6 |
| Queue Length 95th (m) | 35.6 | 15.8 | | | 9.9 | | 5.8 | 76.5 | 2.0 | 2.7 | 96.4 | 3.3 |
| Internal Link Dist (m) | | 177.1 | | | 281.1 | | | 183.2 | | | 276.4 | |
| Turn Bay Length (m) | 50.0 | | | | | | 140.0 | | | 60.0 | | 25.0 |
| Base Capacity (vph) | 354 | 495 | | | 401 | | 458 | 1359 | 1206 | 496 | 1359 | 1206 |
| Starvation Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.28 | 0.24 | | | 0.07 | | 0.10 | 0.49 | 0.02 | 0.03 | 0.56 | 0.03 |
| Intersection Summary | | | | | | | | | | | | |

Intersection Summary

Area Type: Other

Cycle Length: 120

Actuated Cycle Length: 107.7

Natural Cycle: 75

Control Type: Semi Act-Uncoord

Maximum v/c Ratio: 0.60

Intersection Signal Delay: 10.0 Intersection LOS: B
Intersection Capacity Utilization 63.5% ICU Level of Service B

Analysis Period (min) 15

Splits and Phases: 1: Fallowfield Road & O'Keefe Court/Cobble Hill Drive



| Intersection | | | | | | |
|------------------------|-------|-------|--------|-------|-----------------|--------|
| Int Delay, s/veh | 1.3 | | | | | |
| | | EE5 | 11/5: | 14/5= | | NES |
| | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | f) | | | 4 | ¥ | |
| Traffic Vol, veh/h | 178 | 0 | 26 | 32 | 0 | 14 |
| Future Vol, veh/h | 178 | 0 | 26 | 32 | 0 | 14 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, | # 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, % | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 178 | 0 | 26 | 32 | 0 | 14 |
| | | | | | | |
| N.A. '. 'N.A'. N.A. | | | 4 ' 0 | | | |
| | ajor1 | | Major2 | | Minor1 | |
| Conflicting Flow All | 0 | 0 | 178 | 0 | 262 | 178 |
| Stage 1 | - | - | - | - | 178 | - |
| Stage 2 | - | - | - | - | 84 | - |
| Critical Hdwy | - | - | 4.1 | - | 6.4 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.4 | - |
| Follow-up Hdwy | - | - | 2.2 | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | - | - | 1410 | - | 731 | 870 |
| Stage 1 | - | - | - | - | 858 | - |
| Stage 2 | - | - | - | - | 944 | - |
| Platoon blocked, % | - | - | | - | | |
| Mov Cap-1 Maneuver | _ | - | 1410 | - | 717 | 870 |
| Mov Cap-2 Maneuver | - | _ | - | - | 717 | - |
| Stage 1 | - | - | - | - | 858 | - |
| Stage 2 | _ | _ | _ | _ | 926 | _ |
| Jugo Z | | | | | ,20 | |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 3.4 | | 9.2 | |
| HCM LOS | | | | | Α | |
| | | | | | | |
| Minor Lane/Major Mvmt | ı | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | 870 | LDI | LDIX | 1410 | וטיי |
| Capacity (venin) | | | - | - | | |
| UCM Land V/C Datic | | 0.016 | - | - | 0.018 | - |
| HCM Control Dolay (c) | | | | | 7 / | () |
| HCM Control Delay (s) | | 9.2 | - | - | 7.6 | 0 |
| | | | - | - | 7.6 A 0.1 | 0 A |

| Intersection | | | | | | |
|------------------------|--------------|-------|---------|----------|---------|------|
| Int Delay, s/veh | 0.2 | | | | | |
| | | ED.5 | NS | | 057 | 055 |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | | 7 | | ^ | | - 7 |
| Traffic Vol, veh/h | 0 | 17 | 0 | 736 | 878 | 7 |
| Future Vol, veh/h | 0 | 17 | 0 | 736 | 878 | 7 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 0 | - | - | - | 250 |
| Veh in Median Storage | , # 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, % | 0 | 0 | 0 | 3 | 4 | 0 |
| Mvmt Flow | 0 | 17 | 0 | 736 | 878 | 7 |
| | | | | | | |
| N A ' ' /N A' N | A ' 0 | | 1 1 1 | | 4 ' 0 | |
| | /linor2 | | /lajor1 | | /lajor2 | |
| Conflicting Flow All | - | 878 | - | 0 | - | 0 |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | 6.2 | - | - | - | - |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | 3.3 | - | - | - | - |
| Pot Cap-1 Maneuver | 0 | 350 | 0 | - | - | - |
| Stage 1 | 0 | - | 0 | - | - | - |
| Stage 2 | 0 | - | 0 | - | - | - |
| Platoon blocked, % | | | | - | - | - |
| Mov Cap-1 Maneuver | - | 350 | - | - | - | - |
| Mov Cap-2 Maneuver | _ | - | _ | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | _ | _ | _ | _ | _ | _ |
| Jugo Z | | | | | | |
| | | | | | | |
| Approach | EB | | NB | | SB | |
| HCM Control Delay, s | 15.8 | | 0 | | 0 | |
| HCM LOS | С | | | | | |
| | | | | | | |
| Minor Lane/Major Mvm | + | NBT E | DI n1 | SBT | SBR | |
| | l | | | SBI | SBK | |
| Capacity (veh/h) | | - | 000 | - | - | |
| HCM Lane V/C Ratio | | | 0.049 | - | - | |
| HCM Control Delay (s) | | - | | - | - | |
| HCM Lane LOS | | - | С | - | - | |
| HCM 95th %tile Q(veh) | | _ | 0.2 | - | _ | |



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|-------------------------|-------|-------|------|-------|----------|------|-------|----------|-------|----------|----------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | £ | | | 4 | | , j | | 7 | * | † | 7 |
| Traffic Volume (vph) | 30 | 6 | 32 | 39 | 7 | 42 | 119 | 573 | 9 | 8 | 675 | 88 |
| Future Volume (vph) | 30 | 6 | 32 | 39 | 7 | 42 | 119 | 573 | 9 | 8 | 675 | 88 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Storage Length (m) | 50.0 | | 0.0 | 0.0 | | 0.0 | 140.0 | | 0.0 | 60.0 | | 25.0 |
| Storage Lanes | 1 | | 0 | 0 | | 0 | 1 | | 1 | 1 | | 1 |
| Taper Length (m) | 7.5 | | | 7.5 | | | 7.5 | | | 7.5 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | | 0.98 | | | 1.00 | | 1.00 | | 0.98 | 1.00 | | 0.98 |
| Frt | | 0.874 | | | 0.936 | | | | 0.850 | | | 0.850 |
| Flt Protected | 0.950 | | | | 0.978 | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1729 | 1498 | 0 | 0 | 1626 | 0 | 1729 | 1733 | 992 | 1544 | 1750 | 1547 |
| Flt Permitted | 0.680 | | | | 0.839 | | 0.379 | | | 0.430 | | |
| Satd. Flow (perm) | 1238 | 1498 | 0 | 0 | 1394 | 0 | 689 | 1733 | 969 | 698 | 1750 | 1512 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | 32 | | | 36 | | | | 23 | | | 51 |
| Link Speed (k/h) | | 50 | | | 50 | | | 60 | | | 60 | |
| Link Distance (m) | | 201.1 | | | 305.1 | | | 207.2 | | | 300.4 | |
| Travel Time (s) | | 14.5 | | | 22.0 | | | 12.4 | | | 18.0 | |
| Confl. Peds. (#/hr) | | | 1 | 1 | | | 1 | | 1 | 1 | | 1 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Heavy Vehicles (%) | 0% | 0% | 5% | 3% | 14% | 0% | 0% | 5% | 56% | 12% | 4% | 0% |
| Adj. Flow (vph) | 30 | 6 | 32 | 39 | 7 | 42 | 119 | 573 | 9 | 8 | 675 | 88 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 30 | 38 | 0 | 0 | 88 | 0 | 119 | 573 | 9 | 8 | 675 | 88 |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | Perm | Perm | NA | Perm |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | 2 | 6 | | 6 |
| Detector Phase | 4 | 4 | | 8 | 8 | | 2 | 2 | 2 | 6 | 6 | 6 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 33.5 | 33.5 | | 33.5 | 33.5 | | 27.4 | 27.4 | 27.4 | 27.4 | 27.4 | 27.4 |
| Total Split (s) | 34.0 | 34.0 | | 34.0 | 34.0 | | 86.0 | 86.0 | 86.0 | 86.0 | 86.0 | 86.0 |
| Total Split (%) | 28.3% | 28.3% | | 28.3% | 28.3% | | 71.7% | 71.7% | 71.7% | 71.7% | 71.7% | 71.7% |
| Maximum Green (s) | 28.5 | 28.5 | | 28.5 | 28.5 | | 80.6 | 80.6 | 80.6 | 80.6 | 80.6 | 80.6 |
| Yellow Time (s) | 3.6 | 3.6 | | 3.6 | 3.6 | | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 |
| All-Red Time (s) | 1.9 | 1.9 | | 1.9 | 1.9 | | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 |
| Lost Time Adjust (s) | 0.0 | 0.0 | | | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.5 | 5.5 | | | 5.5 | | 5.4 | 5.4 | 5.4 | 5.4 | 5.4 | 5.4 |
| Lead/Lag | | | | | | | | | | | | |
| Lead-Lag Optimize? | | | | | | | | | | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None | | None | None | | Max | Max | Max | Max | Max | Max |
| Walk Time (s) | 7.0 | 7.0 | | 7.0 | 7.0 | | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Flash Dont Walk (s) | 21.0 | 21.0 | | 21.0 | 21.0 | | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 |
| Pedestrian Calls (#/hr) | 0 | 0 | | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Act Effct Green (s) | 9.4 | 9.4 | | | 9.4 | | 87.4 | 87.4 | 87.4 | 87.4 | 87.4 | 87.4 |
| Actuated g/C Ratio | 0.09 | 0.09 | | | 0.09 | | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 |
| v/c Ratio | 0.27 | 0.23 | | | 0.56 | | 0.21 | 0.39 | 0.01 | 0.01 | 0.46 | 0.07 |

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|------------------------|------|----------|------------|-----|----------|-----|----------|----------|------|------|----------|------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 48.8 | 20.5 | | | 41.4 | | 3.7 | 4.0 | 0.4 | 2.8 | 4.5 | 1.5 |
| Queue Delay | 0.0 | 0.0 | | | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 48.8 | 20.5 | | | 41.4 | | 3.7 | 4.0 | 0.4 | 2.8 | 4.5 | 1.5 |
| LOS | D | С | | | D | | Α | Α | Α | Α | Α | Α |
| Approach Delay | | 33.0 | | | 41.4 | | | 3.9 | | | 4.2 | |
| Approach LOS | | С | | | D | | | Α | | | Α | |
| Queue Length 50th (m) | 5.7 | 1.1 | | | 9.9 | | 4.3 | 25.3 | 0.0 | 0.3 | 32.6 | 1.1 |
| Queue Length 95th (m) | 14.4 | 10.3 | | | 24.7 | | 11.5 | 49.7 | 0.5 | 1.4 | 63.9 | 4.7 |
| Internal Link Dist (m) | | 177.1 | | | 281.1 | | | 183.2 | | | 276.4 | |
| Turn Bay Length (m) | 50.0 | | | | | | 140.0 | | | 60.0 | | 25.0 |
| Base Capacity (vph) | 338 | 432 | | | 407 | | 577 | 1451 | 815 | 584 | 1465 | 1274 |
| Starvation Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.09 | 0.09 | | | 0.22 | | 0.21 | 0.39 | 0.01 | 0.01 | 0.46 | 0.07 |

Intersection Summary

Area Type: Other

Cycle Length: 120

Actuated Cycle Length: 104.4

Natural Cycle: 70

Control Type: Semi Act-Uncoord

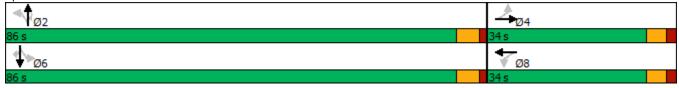
Maximum v/c Ratio: 0.56 Intersection Signal Delay: 7.3

Intersection LOS: A ICU Level of Service C

Intersection Capacity Utilization 70.1%

Analysis Period (min) 15

Splits and Phases: 1: Fallowfield Road & O'Keefe Court/Cobble Hill Drive



Synchro 10 Report Lanes, Volumes, Timings March 2020

| Intersection | | | | | | |
|------------------------|-----------|-------|-----------|--------|-----------|-------|
| Int Delay, s/veh | 1.6 | | | | | |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | | LDK | WDL | ₩ 4 | NDL W | NDK |
| Traffic Vol, veh/h | 31 | 0 | 28 | 173 | 0 | 26 |
| Future Vol, veh/h | 31 | 0 | 28 | 173 | 0 | 26 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | riee - | None | riee - | None | Stop - | None |
| | - | | | | | |
| Storage Length | | - | - | - | 0 | - |
| Veh in Median Storage, | | - | - | 0 | 0 | - |
| Grade, % | 0 | 100 | 100 | 0 | 0 | 100 |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, % | 3 | 0 | 0 | 6 | 0 | 0 |
| Mvmt Flow | 31 | 0 | 28 | 173 | 0 | 26 |
| | | | | | | |
| Major/Minor N | 1ajor1 | 1 | Major2 | N | Minor1 | |
| Conflicting Flow All | 0 | 0 | 31 | 0 | 260 | 31 |
| Stage 1 | - | - | - | - | 31 | - |
| Stage 2 | - | _ | _ | _ | 229 | _ |
| Critical Hdwy | - | - | 4.1 | - | 6.4 | 6.2 |
| Critical Hdwy Stg 1 | _ | _ | - 1.1 | _ | 5.4 | - 0.2 |
| Critical Hdwy Stg 2 | - | | _ | _ | 5.4 | _ |
| Follow-up Hdwy | _ | | 2.2 | _ | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | - | _ | 1595 | - | 733 | 1049 |
| • | - | - | 1373 | - | 997 | 1049 |
| Stage 1 | | - | - | | 814 | |
| Stage 2 | - | - | - | - | δ14 | - |
| Platoon blocked, % | - | - | 1505 | - | 710 | 1040 |
| Mov Cap-1 Maneuver | - | - | 1595 | - | 719 | 1049 |
| Mov Cap-2 Maneuver | - | - | - | - | 719 | - |
| Stage 1 | - | - | - | - | 997 | - |
| Stage 2 | - | - | - | - | 799 | - |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 1 | | 8.5 | |
| HCM LOS | U | | | | Α | |
| TOW LOS | | | | | | |
| | | | | | | |
| Minor Lane/Major Mvmt | t I | VBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | 1049 | - | | 1595 | - |
| HCM Lane V/C Ratio | | 0.025 | - | - | 0.018 | - |
| HCM Control Delay (s) | | 8.5 | - | - | 7.3 | 0 |
| HCM Lane LOS | | Α | - | - | Α | Α |
| HCM 95th %tile Q(veh) | | 0.1 | - | - | 0.1 | - |
| | | | | | | |

| Intersection | | | | | | |
|------------------------|---------|-------|---------|----------|----------|------|
| Int Delay, s/veh | 0.1 | | | | | |
| | | EDD | ND | NOT | CDT | CDD |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | | 7 | | ^ | ^ | 7 |
| Traffic Vol, veh/h | 0 | 15 | 0 | 702 | 737 | 13 |
| Future Vol, veh/h | 0 | 15 | 0 | 702 | 737 | 13 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 0 | - | - | - | 250 |
| Veh in Median Storage, | , # 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, % | 0 | 0 | 0 | 6 | 4 | 0 |
| Mvmt Flow | 0 | 15 | 0 | 702 | 737 | 13 |
| | | | | | | |
| | | _ | | _ | | |
| | /linor2 | | /lajor1 | | /lajor2 | |
| Conflicting Flow All | - | 737 | - | 0 | - | 0 |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | 6.2 | - | - | - | - |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | 3.3 | - | - | - | - |
| Pot Cap-1 Maneuver | 0 | 422 | 0 | - | - | - |
| Stage 1 | 0 | - | 0 | - | - | - |
| Stage 2 | 0 | - | 0 | _ | - | _ |
| Platoon blocked, % | _ | | _ | _ | _ | _ |
| Mov Cap-1 Maneuver | | 422 | | _ | _ | _ |
| Mov Cap 1 Maneuver | _ | - | _ | _ | _ | _ |
| Stage 1 | | | | | | |
| Stage 2 | | | _ | | _ | _ |
| Staye 2 | - | - | - | - | - | - |
| | | | | | | |
| Approach | EB | | NB | | SB | |
| HCM Control Delay, s | 13.8 | | 0 | | 0 | |
| HCM LOS | В | | | | | |
| | _ | | | | | |
| Minor Lang/Major Mumi | + | NDT | DI n1 | CDT | CDD | |
| Minor Lane/Major Mvmi | l | NBT E | | SBT | SBR | |
| Capacity (veh/h) | | - | | - | - | |
| HCM Lane V/C Ratio | | | 0.036 | - | - | |
| HCM Control Delay (s) | | - | | - | - | |
| HCM Lane LOS | | - | В | - | - | |
| HCM 95th %tile Q(veh) | | - | 0.1 | - | - | |

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|-------------------------|-------|-------|------|-------|----------|------|-------|---------|-------|----------|----------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | £ | | | 4 | | Ĭ | | 7 | * | † | 7 |
| Traffic Volume (vph) | 107 | 3 | 114 | 9 | 1 | 20 | 52 | 504 | 23 | 17 | 689 | 38 |
| Future Volume (vph) | 107 | 3 | 114 | 9 | 1 | 20 | 52 | 504 | 23 | 17 | 689 | 38 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Storage Length (m) | 50.0 | | 0.0 | 0.0 | | 0.0 | 140.0 | | 0.0 | 60.0 | | 25.0 |
| Storage Lanes | 1 | | 0 | 0 | | 0 | 1 | | 1 | 1 | | 1 |
| Taper Length (m) | 7.5 | | | 7.5 | | | 7.5 | | | 7.5 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 1.00 | | | | 0.98 | | | | | | | |
| Frt | | 0.854 | | | 0.910 | | | | 0.850 | | | 0.850 |
| Flt Protected | 0.950 | | | | 0.985 | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1729 | 1554 | 0 | 0 | 1605 | 0 | 1729 | 1750 | 1547 | 1631 | 1750 | 1547 |
| Flt Permitted | 0.738 | | | | 0.898 | | 0.355 | | | 0.454 | | |
| Satd. Flow (perm) | 1338 | 1554 | 0 | 0 | 1463 | 0 | 646 | 1750 | 1547 | 780 | 1750 | 1547 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | 114 | | | 20 | | | | 23 | | | 23 |
| Link Speed (k/h) | | 50 | | | 50 | | | 60 | | | 60 | |
| Link Distance (m) | | 201.1 | | | 305.1 | | | 207.2 | | | 300.4 | |
| Travel Time (s) | | 14.5 | | | 22.0 | | | 12.4 | | | 18.0 | |
| Confl. Peds. (#/hr) | 2 | | | | | 2 | | | | | | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Heavy Vehicles (%) | 0% | 0% | 0% | 0% | 0% | 0% | 0% | 4% | 0% | 6% | 4% | 0% |
| Adj. Flow (vph) | 107 | 3 | 114 | 9 | 1 | 20 | 52 | 504 | 23 | 17 | 689 | 38 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 107 | 117 | 0 | 0 | 30 | 0 | 52 | 504 | 23 | 17 | 689 | 38 |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | Perm | Perm | NA | Perm |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | 2 | 6 | | 6 |
| Detector Phase | 4 | 4 | | 8 | 8 | | 2 | 2 | 2 | 6 | 6 | 6 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 33.5 | 33.5 | | 33.5 | 33.5 | | 27.4 | 27.4 | 27.4 | 27.4 | 27.4 | 27.4 |
| Total Split (s) | 35.0 | 35.0 | | 35.0 | 35.0 | | 85.0 | 85.0 | 85.0 | 85.0 | 85.0 | 85.0 |
| Total Split (%) | 29.2% | 29.2% | | 29.2% | 29.2% | | 70.8% | 70.8% | 70.8% | 70.8% | 70.8% | 70.8% |
| Maximum Green (s) | 29.5 | 29.5 | | 29.5 | 29.5 | | 79.6 | 79.6 | 79.6 | 79.6 | 79.6 | 79.6 |
| Yellow Time (s) | 3.6 | 3.6 | | 3.6 | 3.6 | | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 |
| All-Red Time (s) | 1.9 | 1.9 | | 1.9 | 1.9 | | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 |
| Lost Time Adjust (s) | 0.0 | 0.0 | | | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.5 | 5.5 | | | 5.5 | | 5.4 | 5.4 | 5.4 | 5.4 | 5.4 | 5.4 |
| Lead/Lag | | | | | | | | | | | | |
| Lead-Lag Optimize? | | | | | | | | | | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None | | None | None | | Max | Max | Max | Max | Max | Max |
| Walk Time (s) | 7.0 | 7.0 | | 7.0 | 7.0 | | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Flash Dont Walk (s) | 21.0 | 21.0 | | 21.0 | 21.0 | | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 |
| Pedestrian Calls (#/hr) | 0 | 0 | | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Act Effct Green (s) | 13.8 | 13.8 | | | 13.8 | | 82.6 | 82.6 | 82.6 | 82.6 | 82.6 | 82.6 |
| Actuated g/C Ratio | 0.13 | 0.13 | | | 0.13 | | 0.77 | 0.77 | 0.77 | 0.77 | 0.77 | 0.77 |
| v/c Ratio | 0.62 | 0.39 | | | 0.15 | | 0.10 | 0.37 | 0.02 | 0.03 | 0.51 | 0.03 |

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|------------------------|------|----------|-----|-----|----------|-----|-------|----------|------|------|-------|------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 59.1 | 12.0 | | | 22.6 | | 4.5 | 5.4 | 1.7 | 3.9 | 6.9 | 2.2 |
| Queue Delay | 0.0 | 0.0 | | | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 59.1 | 12.0 | | | 22.6 | | 4.5 | 5.4 | 1.7 | 3.9 | 6.9 | 2.2 |
| LOS | Е | В | | | С | | Α | Α | Α | Α | Α | Α |
| Approach Delay | | 34.5 | | | 22.6 | | | 5.2 | | | 6.6 | |
| Approach LOS | | С | | | С | | | Α | | | Α | |
| Queue Length 50th (m) | 20.7 | 0.6 | | | 1.8 | | 2.2 | 27.5 | 0.0 | 0.7 | 44.2 | 0.6 |
| Queue Length 95th (m) | 38.1 | 15.7 | | | 9.8 | | 6.8 | 53.4 | 2.1 | 2.8 | 85.1 | 3.4 |
| Internal Link Dist (m) | | 177.1 | | | 281.1 | | | 183.2 | | | 276.4 | |
| Turn Bay Length (m) | 50.0 | | | | | | 140.0 | | | 60.0 | | 25.0 |
| Base Capacity (vph) | 368 | 510 | | | 417 | | 497 | 1346 | 1195 | 600 | 1346 | 1195 |
| Starvation Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.29 | 0.23 | | | 0.07 | | 0.10 | 0.37 | 0.02 | 0.03 | 0.51 | 0.03 |

Intersection Summary

Area Type: Other

Cycle Length: 120

Actuated Cycle Length: 107.3

Natural Cycle: 70

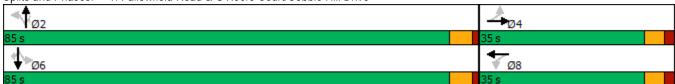
Control Type: Semi Act-Uncoord Maximum v/c Ratio: 0.62

Intersection Signal Delay: 10.3
Intersection Capacity Utilization 67.6%

Intersection LOS: B
ICU Level of Service C

Analysis Period (min) 15

Splits and Phases: 1: Fallowfield Road & O'Keefe Court/Cobble Hill Drive



| Intersection | | | | | | |
|-------------------------------------|----------|-----------------|---------|------|-----------------|--------|
| Int Delay, s/veh | 1.8 | | | | | |
| | | EDD. | WDI | WDT | NDI | NDD |
| | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | } | ^ | 0.0 | 4 | ¥ | 00 |
| Traffic Vol, veh/h | 178 | 0 | 33 | 32 | 0 | 23 |
| Future Vol, veh/h | 178 | 0 | 33 | 32 | 0 | 23 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, # | # 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, % | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 178 | 0 | 33 | 32 | 0 | 23 |
| | | | | | | |
| NA - ' / NA' NA | -!1 | | 4-! | | A'1 | |
| | ajor1 | | /lajor2 | | Minor1 | |
| Conflicting Flow All | 0 | 0 | 178 | 0 | 276 | 178 |
| Stage 1 | - | - | - | - | 178 | - |
| Stage 2 | - | - | - | - | 98 | - |
| Critical Hdwy | - | - | 4.1 | - | 6.4 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.4 | - |
| Follow-up Hdwy | - | - | 2.2 | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | - | - | 1410 | - | 718 | 870 |
| Stage 1 | - | - | - | - | 858 | - |
| Stage 2 | - | - | - | - | 931 | - |
| Platoon blocked, % | - | - | | - | | |
| Mov Cap-1 Maneuver | _ | - | 1410 | - | 701 | 870 |
| Mov Cap-2 Maneuver | - | _ | - | _ | 701 | - |
| Stage 1 | _ | | _ | _ | 858 | _ |
| Stage 2 | | | | | 909 | _ |
| Jiago Z | - | _ | | | 707 | _ |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 3.9 | | 9.3 | |
| HCM LOS | | | | | Α | |
| | | | | | | |
| Minor Lane/Major Mvmt | N | NBLn1 | EBT | EBR | WBL | WBT |
| • | ı ı | | LDI | LDIX | | וטייי |
| Capacity (veh/h) HCM Lane V/C Ratio | | 870 | - | - | 1410 | - |
| | | 0.026 | - | - | 0.023 | - |
| | | 0.0 | | | | |
| HCM Control Delay (s) | | 9.3 | - | - | 7.6 | 0 |
| | | 9.3 A 0.1 | - | - | 7.6 A 0.1 | 0 A |

| Intersection | | | | | | |
|---|-----------------|-------|------------------------------------|-------------|--------------------|----------|
| Int Delay, s/veh | 0.2 | | | | | |
| | | EDD | NDI | NDT | CDT | CDD |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | | 7 | | ^ | 700 | 7 |
| Traffic Vol, veh/h | 0 | 23 | 0 | 582 | 798 | 17 |
| Future Vol, veh/h | 0 | 23 | 0 | 582 | 798 | 17 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | _ 0 | _ 0 | _ 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 0 | - | - | - | 250 |
| Veh in Median Storage | | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, % | 0 | 0 | 0 | 3 | 4 | 0 |
| Mvmt Flow | 0 | 23 | 0 | 582 | 798 | 17 |
| | | | | | | |
| Major/Minor N | /liner? | Λ. | Najor1 | | /aior? | |
| | /linor2 | | /lajor1 | | /lajor2 | |
| Conflicting Flow All | - | 798 | - | 0 | - | 0 |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | 6.2 | - | - | - | - |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | 3.3 | - | - | - | - |
| Pot Cap-1 Maneuver | 0 | 389 | 0 | - | - | - |
| Stage 1 | 0 | - | 0 | - | - | - |
| Stage 2 | 0 | - | 0 | - | - | - |
| Platoon blocked, % | - | | - | - | _ | _ |
| Mov Cap-1 Maneuver | _ | 389 | _ | _ | _ | _ |
| Mov Cap-2 Maneuver | _ | - | _ | _ | _ | _ |
| Stage 1 | _ | _ | | | _ | |
| | | - | - | - | - | - |
| | | | | - | - | - |
| Stage 2 | - | - | - | | | |
| | - | - | - | | | |
| | EB | - | NB | | SB | |
| Stage 2 Approach | EB | _ | | | | |
| Stage 2 Approach HCM Control Delay, s | EB 14.8 | | NB 0 | | SB 0 | |
| Stage 2 Approach | EB | | | | | |
| Stage 2 Approach HCM Control Delay, s HCM LOS | EB 14.8 B | | 0 | | 0 | |
| Stage 2 Approach HCM Control Delay, s HCM LOS Minor Lane/Major Mvm | EB 14.8 B | NBT E | 0 EBLn1 | SBT | | |
| Stage 2 Approach HCM Control Delay, s HCM LOS Minor Lane/Major Mvm Capacity (veh/h) | EB 14.8 B | NBT E | 0 EBLn1 389 | SBT_ | 0 | |
| Stage 2 Approach HCM Control Delay, s HCM LOS Minor Lane/Major Mvm Capacity (veh/h) HCM Lane V/C Ratio | EB 14.8 B | NBT E | 0 EBLn1 389 0.059 | | 0 SBR | |
| Stage 2 Approach HCM Control Delay, s HCM LOS Minor Lane/Major Mvm Capacity (veh/h) | EB 14.8 B | NBT E | 0 EBLn1 389 | - | 0 SBR | |
| Stage 2 Approach HCM Control Delay, s HCM LOS Minor Lane/Major Mvm Capacity (veh/h) HCM Lane V/C Ratio HCM Control Delay (s) HCM Lane LOS | EB 14.8 B | NBT E | 0 EBLn1 389 0.059 | - | 0 SBR - | |
| Stage 2 Approach HCM Control Delay, s HCM LOS Minor Lane/Major Mvm Capacity (veh/h) HCM Lane V/C Ratio HCM Control Delay (s) | EB 14.8 B | NBT E | 0 EBLn1 389 0.059 14.8 | - - - | 0 SBR - - | |



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|--|-------|-------|------|-------------|----------|------|-------|------------|-------|----------|----------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | £ | | | 4 | | Ĭ | | 7 | * | † | 7 |
| Traffic Volume (vph) | 30 | 6 | 32 | 39 | 7 | 42 | 119 | 646 | 9 | 8 | 881 | 88 |
| Future Volume (vph) | 30 | 6 | 32 | 39 | 7 | 42 | 119 | 646 | 9 | 8 | 881 | 88 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Storage Length (m) | 50.0 | | 0.0 | 0.0 | | 0.0 | 140.0 | | 0.0 | 60.0 | | 25.0 |
| Storage Lanes | 1 | | 0 | 0 | | 0 | 1 | | 1 | 1 | | 1 |
| Taper Length (m) | 7.5 | | | 7.5 | | | 7.5 | | | 7.5 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | | 0.98 | | | 1.00 | | | | 0.98 | 1.00 | | 0.98 |
| Frt | | 0.874 | | | 0.936 | | | | 0.850 | | | 0.850 |
| Flt Protected | 0.950 | | | | 0.978 | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1729 | 1498 | 0 | 0 | 1626 | 0 | 1729 | 1733 | 992 | 1544 | 1750 | 1547 |
| Flt Permitted | 0.679 | | | | 0.839 | | 0.286 | | | 0.394 | | |
| Satd. Flow (perm) | 1236 | 1498 | 0 | 0 | 1394 | 0 | 521 | 1733 | 969 | 640 | 1750 | 1512 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | 32 | | | 36 | | | | 23 | | | 40 |
| Link Speed (k/h) | | 50 | | | 50 | | | 60 | | | 60 | |
| Link Distance (m) | | 201.1 | | | 305.1 | | | 207.2 | | | 300.4 | |
| Travel Time (s) | | 14.5 | | | 22.0 | | | 12.4 | | | 18.0 | |
| Confl. Peds. (#/hr) | | | 1 | 1 | | | 1 | | 1 | 1 | | 1 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Heavy Vehicles (%) | 0% | 0% | 5% | 3% | 14% | 0% | 0% | 5% | 56% | 12% | 4% | 0% |
| Adj. Flow (vph) | 30 | 6 | 32 | 39 | 7 | 42 | 119 | 646 | 9 | 8 | 881 | 88 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 30 | 38 | 0 | 0 | 88 | 0 | 119 | 646 | 9 | 8 | 881 | 88 |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | Perm | Perm | NA | Perm |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | _ |
| Permitted Phases | 4 | | | 8 | | | 2 | | 2 | 6 | | 6 |
| Detector Phase | 4 | 4 | | 8 | 8 | | 2 | 2 | 2 | 6 | 6 | 6 |
| Switch Phase | F 0 | F 0 | | F 0 | F 0 | | F 0 | F 0 | F 0 | F 0 | F 0 | F 0 |
| Minimum Initial (s) | 5.0 | 5.0 | | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 33.5 | 33.5 | | 33.5 | 33.5 | | 27.4 | 27.4 | 27.4 | 27.4 | 27.4 | 27.4 |
| Total Split (s) | 33.5 | 33.5 | | 33.5 | 33.5 | | 86.5 | 86.5 | 86.5 | 86.5 | 86.5 | 86.5 |
| Total Split (%) | 27.9% | 27.9% | | 27.9% | 27.9% | | 72.1% | 72.1% | 72.1% | 72.1% | 72.1% | 72.1% |
| Maximum Green (s) | 28.0 | 28.0 | | 28.0 | 28.0 | | 81.1 | 81.1 | 81.1 | 81.1 | 81.1 | 81.1 |
| Yellow Time (s) | 3.6 | 3.6 | | 3.6 | 3.6 | | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 |
| All-Red Time (s) | 1.9 | 1.9 | | 1.9 | 1.9 | | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 |
| Lost Time Adjust (s) | 0.0 | 0.0 | | | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.5 | 5.5 | | | 5.5 | | 5.4 | 5.4 | 5.4 | 5.4 | 5.4 | 5.4 |
| Lead/Lag | | | | | | | | | | | | |
| Lead-Lag Optimize? Vehicle Extension (s) | 3.0 | 3.0 | | 2.0 | 3.0 | | 2.0 | 2 0 | 2 0 | 2 0 | 3.0 | 2.0 |
| Recall Mode | | | | 3.0 None | | | 3.0 | 3.0 Max | 3.0 | 3.0 | | 3.0 |
| | None | None | | None | None | | Max | | Max | Max | Max | Max |
| Walk Time (s) | 7.0 | 7.0 | | 7.0 | 7.0 | | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Flash Dont Walk (s) | 21.0 | 21.0 | | 21.0 | 21.0 | | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 |
| Pedestrian Calls (#/hr) | 0 | 0 | | 0 | 0 | | 07.0 | 07.0 | 07.0 | 07.0 | 07.0 | 07.0 |
| Act Effet Green (s) | 9.4 | 9.4 | | | 9.4 | | 87.9 | 87.9 | 87.9 | 87.9 | 87.9 | 87.9 |
| Actuated g/C Ratio | 0.09 | 0.09 | | | 0.09 | | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 |
| v/c Ratio | 0.27 | 0.23 | | | 0.56 | | 0.27 | 0.44 | 0.01 | 0.01 | 0.60 | 0.07 |

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|------------------------|------|----------|-----|-----|----------|-----|-------|----------|------|----------|----------|------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 49.2 | 20.6 | | | 41.6 | | 4.8 | 4.4 | 0.4 | 2.8 | 6.3 | 1.7 |
| Queue Delay | 0.0 | 0.0 | | | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 49.2 | 20.6 | | | 41.6 | | 4.8 | 4.4 | 0.4 | 2.8 | 6.3 | 1.7 |
| LOS | D | С | | | D | | Α | Α | Α | Α | Α | Α |
| Approach Delay | | 33.2 | | | 41.6 | | | 4.4 | | | 5.8 | |
| Approach LOS | | С | | | D | | | Α | | | Α | |
| Queue Length 50th (m) | 5.7 | 1.1 | | | 10.0 | | 4.6 | 30.5 | 0.0 | 0.3 | 52.6 | 1.5 |
| Queue Length 95th (m) | 14.3 | 10.4 | | | 24.9 | | 13.3 | 59.8 | 0.5 | 1.4 | 105.3 | 5.2 |
| Internal Link Dist (m) | | 177.1 | | | 281.1 | | | 183.2 | | | 276.4 | |
| Turn Bay Length (m) | 50.0 | | | | | | 140.0 | | | 60.0 | | 25.0 |
| Base Capacity (vph) | 330 | 423 | | | 398 | | 436 | 1452 | 816 | 536 | 1466 | 1274 |
| Starvation Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.09 | 0.09 | | | 0.22 | | 0.27 | 0.44 | 0.01 | 0.01 | 0.60 | 0.07 |

Intersection Summary

Area Type: Other

Cycle Length: 120

Actuated Cycle Length: 104.9

Natural Cycle: 90

Control Type: Semi Act-Uncoord

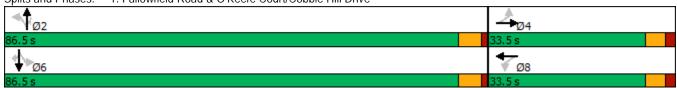
Maximum v/c Ratio: 0.60

Intersection Signal Delay: 7.9
Intersection Capacity Utilization 81.5%

Intersection LOS: A ICU Level of Service D

Analysis Period (min) 15

Splits and Phases: 1: Fallowfield Road & O'Keefe Court/Cobble Hill Drive



| Intersection | | | | | | |
|---------------------------------------|----------|----------|---------|------|----------|--------|
| Int Delay, s/veh | 1.6 | | | | | |
| | | FDD | WDI | MDT | NDI | NDD |
| | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | } | | -00 | 4 | ¥ | 2/ |
| Traffic Vol, veh/h | 31 | 0 | 28 | 173 | 0 | 26 |
| Future Vol, veh/h | 31 | 0 | 28 | 173 | 0 | 26 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, # | | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, % | 3 | 0 | 0 | 6 | 0 | 0 |
| Mvmt Flow | 31 | 0 | 28 | 173 | 0 | 26 |
| | | | | | | |
| Major/Minor Ma | ajor1 | ١ | /lajor2 | N | Minor1 | |
| Conflicting Flow All | 0 | 0 | 31 | 0 | 260 | 31 |
| Stage 1 | - | - | - | - | 31 | - |
| Stage 2 | _ | _ | _ | _ | 229 | _ |
| Critical Hdwy | - | - | 4.1 | | 6.4 | 6.2 |
| Critical Hdwy Stg 1 | - | - | 4.1 | - | 5.4 | 0.2 |
| Critical Hdwy Stg 2 | - | - | - | | 5.4 | - |
| Follow-up Hdwy | - | - | 2.2 | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | - | - | 1595 | - | 733 | 1049 |
| • | - | - | | - | 997 | 1049 |
| Stage 1 | - | - | - | | 814 | - |
| Stage 2 | - | - | - | - | δ14 | - |
| Platoon blocked, % | - | - | 1505 | - | 710 | 1040 |
| Mov Cap-1 Maneuver | - | - | 1595 | - | 719 | 1049 |
| Mov Cap-2 Maneuver | - | - | - | - | 719 | - |
| Stage 1 | - | - | - | - | 997 | - |
| Stage 2 | - | - | - | - | 799 | - |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 1 | | 8.5 | |
| HCM LOS | | | | | A | |
| | | | | | , , | |
| | | IDI. | | E55 | 11/5: | 14/5- |
| Minor Lane/Major Mvmt | 1 | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | 1049 | - | | 1595 | - |
| HCM Lane V/C Ratio | | 0.025 | - | - | 0.018 | - |
| | | 8.5 | - | - | , | 0 |
| | | Α | - | - | Α | Α |
| HCM 95th %tile Q(veh) | | 0.1 | - | - | 0.1 | - |
| HCM Control Delay (s) HCM Lane LOS | | 8.5 A | - | - | 7.3 A | 0 A |

| Intersection | | | | | | |
|--|-------------------|----------|--|-------------|-------------------|-------------|
| Int Delay, s/veh | 0.1 | | | | | |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| | EBL | | NDL | | | |
| Lane Configurations | 0 | 7 | 0 | ^ | ↑ | 12 |
| Traffic Vol, veh/h | 0 | 15 | 0 | 776 | 949 | 13 |
| Future Vol, veh/h | 0 | 15 | 0 | 776 | 949 | 13 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 0 | - | - | - | 250 |
| Veh in Median Storage | | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, % | 0 | 0 | 0 | 6 | 4 | 0 |
| Mvmt Flow | 0 | 15 | 0 | 776 | 949 | 13 |
| | | | | | | |
| Major/Minor N | Minor2 | | Noior1 | Λ. | /oior? | |
| | | | /lajor1 | | /lajor2 | |
| Conflicting Flow All | - | 949 | - | 0 | - | 0 |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | 6.2 | - | - | - | - |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | 3.3 | - | - | - | - |
| Pot Cap-1 Maneuver | 0 | 319 | 0 | - | - | - |
| Stage 1 | 0 | - | 0 | - | - | - |
| Stage 2 | 0 | - | 0 | - | - | - |
| Platoon blocked, % | | | | - | - | - |
| Mov Cap-1 Maneuver | - | 319 | - | - | - | - |
| Mov Cap-2 Maneuver | | | | | | |
| | _ | - | - | _ | - | - |
| | - | | - | - | - | - - |
| Stage 1 | - - | | | - | | - |
| | - - - | | - | - - | - | - - - |
| Stage 1 Stage 2 | - | | - | - - - | - | - - - |
| Stage 1 Stage 2 Approach | - - - EB | | - | - | - | - |
| Stage 1 Stage 2 Approach HCM Control Delay, s | EB 16.8 | | - | - | - | - |
| Stage 1 Stage 2 Approach | EB | | - - NB | - | SB | - |
| Stage 1 Stage 2 Approach HCM Control Delay, s | EB 16.8 | | - - NB | - | SB | - |
| Stage 1 Stage 2 Approach HCM Control Delay, s HCM LOS | EB 16.8 | | - - NB 0 | - | - - SB 0 | |
| Stage 1 Stage 2 Approach HCM Control Delay, s HCM LOS Minor Lane/Major Mvm | EB 16.8 | | - - NB 0 | SBT | SB | |
| Stage 1 Stage 2 Approach HCM Control Delay, s HCM LOS Minor Lane/Major Mvm Capacity (veh/h) | EB 16.8 | NBT E | NB 0 | SBT | SB 0 | |
| Stage 1 Stage 2 Approach HCM Control Delay, s HCM LOS Minor Lane/Major Mvm Capacity (veh/h) HCM Lane V/C Ratio | EB 16.8 C | NBT E | NB 0 EBLn1 319 0.047 | SBT | SB 0 | |
| Stage 1 Stage 2 Approach HCM Control Delay, s HCM LOS Minor Lane/Major Mvm Capacity (veh/h) HCM Lane V/C Ratio HCM Control Delay (s) | EB 16.8 C | NBT E | NB 0 EBLn1 319 0.047 16.8 | SBT | SB 0 | |
| Stage 1 Stage 2 Approach HCM Control Delay, s HCM LOS Minor Lane/Major Mvm Capacity (veh/h) HCM Lane V/C Ratio | EB 16.8 C | NBT E | NB 0 EBLn1 319 0.047 | SBT | SB 0 | |

| | • | - | • | • | ← | • | 4 | † | <i>></i> | / | ţ | 4 |
|-------------------------|-------|-------|------|-------|----------|------|-------|----------|-------------|----------|----------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ň | £ | | | 4 | | * | | 7 | ř | + | 7 |
| Traffic Volume (vph) | 107 | 3 | 114 | 9 | 1 | 20 | 52 | 661 | 23 | 17 | 767 | 38 |
| Future Volume (vph) | 107 | 3 | 114 | 9 | 1 | 20 | 52 | 661 | 23 | 17 | 767 | 38 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Storage Length (m) | 50.0 | | 0.0 | 0.0 | | 0.0 | 140.0 | | 0.0 | 60.0 | | 25.0 |
| Storage Lanes | 1 | | 0 | 0 | | 0 | 1 | | 1 | 1 | | 1 |
| Taper Length (m) | 7.5 | | | 7.5 | | | 7.5 | | | 7.5 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 1.00 | | | | 0.99 | | | | | | | |
| Frt | | 0.854 | | | 0.910 | | | | 0.850 | | | 0.850 |
| Flt Protected | 0.950 | | | | 0.985 | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1729 | 1554 | 0 | 0 | 1607 | 0 | 1729 | 1750 | 1547 | 1631 | 1750 | 1547 |
| Flt Permitted | 0.738 | | | | 0.873 | | 0.280 | | | 0.346 | | |
| Satd. Flow (perm) | 1340 | 1554 | 0 | 0 | 1424 | 0 | 510 | 1750 | 1547 | 594 | 1750 | 1547 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | 111 | | | 20 | | | | 39 | | | 39 |
| Link Speed (k/h) | | 50 | | | 50 | | | 60 | | | 60 | |
| Link Distance (m) | | 201.1 | | | 305.1 | | | 207.2 | | | 300.4 | |
| Travel Time (s) | | 14.5 | | | 22.0 | | | 12.4 | | | 18.0 | |
| Confl. Peds. (#/hr) | 2 | | | | | 2 | | | | | | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Heavy Vehicles (%) | 0% | 0% | 0% | 0% | 0% | 0% | 0% | 4% | 0% | 6% | 4% | 0% |
| Adj. Flow (vph) | 107 | 3 | 114 | 9 | 1 | 20 | 52 | 661 | 23 | 17 | 767 | 38 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 107 | 117 | 0 | 0 | 30 | 0 | 52 | 661 | 23 | 17 | 767 | 38 |
| Turn Type | Perm | NA | | Perm | NA | | Perm | NA | Perm | Perm | NA | Perm |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | | 2 | | 2 | 6 | | 6 |
| Detector Phase | 4 | 4 | | 8 | 8 | | 2 | 2 | 2 | 6 | 6 | 6 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 33.5 | 33.5 | | 33.5 | 33.5 | | 27.4 | 27.4 | 27.4 | 27.4 | 27.4 | 27.4 |
| Total Split (s) | 33.5 | 33.5 | | 33.5 | 33.5 | | 36.5 | 36.5 | 36.5 | 36.5 | 36.5 | 36.5 |
| Total Split (%) | 47.9% | 47.9% | | 47.9% | 47.9% | | 52.1% | 52.1% | 52.1% | 52.1% | 52.1% | 52.1% |
| Maximum Green (s) | 28.0 | 28.0 | | 28.0 | 28.0 | | 31.1 | 31.1 | 31.1 | 31.1 | 31.1 | 31.1 |
| Yellow Time (s) | 3.6 | 3.6 | | 3.6 | 3.6 | | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 |
| All-Red Time (s) | 1.9 | 1.9 | | 1.9 | 1.9 | | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 |
| Lost Time Adjust (s) | 0.0 | 0.0 | | | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.5 | 5.5 | | | 5.5 | | 5.4 | 5.4 | 5.4 | 5.4 | 5.4 | 5.4 |
| Lead/Lag | | | | | | | | | | | | |
| Lead-Lag Optimize? | | | | | | | | | | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None | | None | None | | Max | Max | Max | Max | Max | Max |
| Walk Time (s) | 7.0 | 7.0 | | 7.0 | 7.0 | | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Flash Dont Walk (s) | 21.0 | 21.0 | | 21.0 | 21.0 | | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 |
| Pedestrian Calls (#/hr) | 0 | 0 | | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Act Effct Green (s) | 9.4 | 9.4 | | | 9.4 | | 35.8 | 35.8 | 35.8 | 35.8 | 35.8 | 35.8 |
| Actuated g/C Ratio | 0.18 | 0.18 | | | 0.18 | | 0.68 | 0.68 | 0.68 | 0.68 | 0.68 | 0.68 |
| v/c Ratio | 0.45 | 0.32 | | | 0.10 | | 0.15 | 0.56 | 0.02 | 0.04 | 0.65 | 0.04 |
| | 0.70 | 0.02 | | | 0,11 | | 0.10 | 0.00 | 0.02 | 0.07 | 0.00 | 0.07 |

| | • | → | • | • | • | • | 4 | † | ~ | - | ļ | 1 |
|------------------------|------|----------|-----|-----|-------|-----|-------|----------|------|------|--------|------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 24.9 | 7.5 | | | 11.4 | | 6.7 | 9.0 | 1.5 | 5.5 | 11.4 | 2.2 |
| Queue Delay | 0.0 | 0.0 | | | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 24.9 | 7.5 | | | 11.4 | | 6.7 | 9.0 | 1.5 | 5.5 | 11.4 | 2.2 |
| LOS | С | Α | | | В | | Α | Α | Α | Α | В | Α |
| Approach Delay | | 15.8 | | | 11.4 | | | 8.6 | | | 10.8 | |
| Approach LOS | | В | | | В | | | Α | | | В | |
| Queue Length 50th (m) | 8.8 | 0.5 | | | 0.8 | | 1.7 | 31.9 | 0.0 | 0.5 | 41.0 | 0.0 |
| Queue Length 95th (m) | 20.0 | 10.3 | | | 5.9 | | 6.9 | 71.7 | 1.5 | 2.8 | #103.7 | 2.8 |
| Internal Link Dist (m) | | 177.1 | | | 281.1 | | | 183.2 | | | 276.4 | |
| Turn Bay Length (m) | 50.0 | | | | | | 140.0 | | | 60.0 | | 25.0 |
| Base Capacity (vph) | 713 | 878 | | | 767 | | 346 | 1188 | 1063 | 403 | 1188 | 1063 |
| Starvation Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | | | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.15 | 0.13 | | | 0.04 | | 0.15 | 0.56 | 0.02 | 0.04 | 0.65 | 0.04 |

Intersection Summary

Area Type: Other

Cycle Length: 70

Actuated Cycle Length: 52.7

Natural Cycle: 75

Control Type: Semi Act-Uncoord

Maximum v/c Ratio: 0.65

Intersection Signal Delay: 10.6 Intersection LOS: B
Intersection Capacity Utilization 67.6% ICU Level of Service C

Analysis Period (min) 15

Queue shown is maximum after two cycles.

Splits and Phases: 1: Fallowfield Road & O'Keefe Court/Cobble Hill Drive



^{# 95}th percentile volume exceeds capacity, queue may be longer.

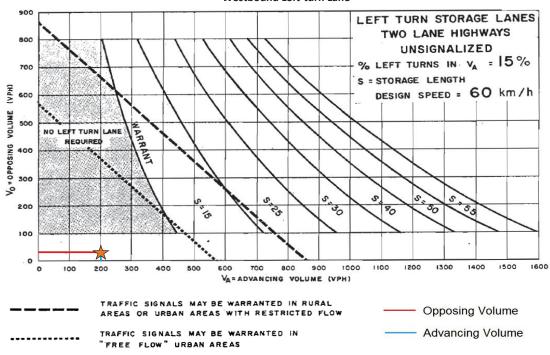
| Intersection | | | | | | |
|------------------------|-------|-------|--------|------|---------|--------|
| Int Delay, s/veh | 1.8 | | | | | |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | ĵ. | | | 4 | W | ,,,,,, |
| Traffic Vol, veh/h | 178 | 0 | 33 | 32 | 0 | 23 |
| Future Vol, veh/h | 178 | 0 | 33 | 32 | 0 | 23 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | _ | - | _ | - | 0 | - |
| Veh in Median Storage, | # 0 | _ | _ | 0 | 0 | _ |
| Grade, % | 0 | _ | _ | 0 | 0 | _ |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, % | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 178 | 0 | 33 | 32 | 0 | 23 |
| IVIVIII(I IOVV | 170 | U | 33 | 32 | U | 23 |
| | | | | | | |
| | ajor1 | N | Major2 | Λ | /linor1 | |
| Conflicting Flow All | 0 | 0 | 178 | 0 | 276 | 178 |
| Stage 1 | - | - | - | - | 178 | - |
| Stage 2 | - | - | - | - | 98 | - |
| Critical Hdwy | - | - | 4.1 | - | 6.4 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.4 | - |
| Follow-up Hdwy | - | - | 2.2 | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | - | - | 1410 | - | 718 | 870 |
| Stage 1 | - | - | - | - | 858 | - |
| Stage 2 | - | - | - | - | 931 | - |
| Platoon blocked, % | - | - | | - | | |
| Mov Cap-1 Maneuver | - | - | 1410 | - | 701 | 870 |
| Mov Cap-2 Maneuver | - | - | - | - | 701 | - |
| Stage 1 | - | - | - | - | 858 | - |
| Stage 2 | _ | - | _ | _ | 909 | _ |
| Olago 2 | | | | | , , , | |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 3.9 | | 9.3 | |
| HCM LOS | | | | | Α | |
| | | | | | | |
| Minor Lane/Major Mvmt | | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | 870 | - | | 1410 | - |
| HCM Lane V/C Ratio | | 0.026 | - | - | 0.023 | - |
| HCM Control Delay (s) | | 9.3 | - | - | 7.6 | 0 |
| HCM Lane LOS | | Α | - | - | Α | A |
| HCM 95th %tile Q(veh) | | 0.1 | - | - | 0.1 | - |
| | | | | | | |

| Intersection | | | | | | |
|------------------------|--------|-------|---------|------------|---------|-----------|
| Int Delay, s/veh | 0.2 | | | | | |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| | EBL | | NDL | | | |
| Lane Configurations | 0 | 77 | 0 | ↑ ↑ | 070 | 17 |
| Traffic Vol, veh/h | 0 | 23 | 0 | 743 | 878 | 17 |
| Future Vol, veh/h | 0 | 23 | 0 | 743 | 878 | 17 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 0 | - | - | - | 250 |
| Veh in Median Storage | | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, % | 0 | 0 | 0 | 3 | 4 | 0 |
| Mvmt Flow | 0 | 23 | 0 | 743 | 878 | 17 |
| | | | | | | |
| Major/Minor N | Minor2 | ١ | /lajor1 | ١ | /lajor2 | |
| Conflicting Flow All | - | 878 | - | 0 | - | 0 |
| Stage 1 | _ | - | _ | - | _ | - |
| Stage 2 | _ | _ | _ | _ | _ | _ |
| Critical Hdwy | _ | 6.2 | _ | | _ | |
| Critical Hdwy Stg 1 | - | 0.2 | | - | | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| | | 3.3 | | | | |
| Follow-up Hdwy | - | | - | - | - | - |
| Pot Cap-1 Maneuver | 0 | 350 | 0 | - | - | - |
| Stage 1 | 0 | - | 0 | - | - | - |
| Stage 2 | 0 | - | 0 | - | - | - |
| Platoon blocked, % | | | | - | - | - |
| Mov Cap-1 Maneuver | - | 350 | - | - | - | - |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| | | | | | | |
| Approach | EB | | NB | | SB | |
| HCM Control Delay, s | 16 | | 0 | | 0 | |
| HCM LOS | C | | U | | U | |
| TIGIVI EUG | U | | | | | |
| | | | | | | |
| Minor Lane/Major Mvm | nt | NBT E | | SBT | SBR | |
| Capacity (veh/h) | | - | 350 | - | - | |
| HCM Lane V/C Ratio | | - | 0.066 | - | - | |
| HCM Control Delay (s) | | - | 16 | - | - | |
| HCM Lane LOS | | - | С | - | - | |
| HCM 95th %tile Q(veh) |) | - | 0.2 | - | - | |
| | | | | | | |

Appendix K – Auxiliary Lane Analyses

April 9, 2020 11

O'Keefe Court & Lusk Street - Future (2028) Total Traffic - AM Peak Hour Westbound Left-turn Lane



O'Keefe Court & Lusk Street - Future (2028) Total Traffic - PM Peak Hour Westbound Left-Turn Lane

