# patersongroup

### **Consulting Engineers**

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July 11, 2018 - Revised September 3, 2019 File: PH3333-LET.01-REV.02

Mr. Abdo El-Arab 6175 Rockdale Road Vars, ON K0A 3H0

Attention: Mr. Abdo El-Arab

Subject: Water Supply Assessment for a

**Proposed Site Plan Approval** 

6175 Rockdale Road

Vars, Ontario

Geotechnical Engineering Environmental Engineering Archaeological Studies Hydrogeology Geological Engineering Materials Testing Building Science

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#### INTRODUCTION

Further to your request, this firm has conducted a Water Supply Assessment in support of site plan approval of a proposed re-development of the commercial property located at 6175 Rockdale Road, Vars, Ontario. The purpose of these works has been to determine the suitability of the water supply aquifer underlying the site to service a re-development of the existing commercial layout.

#### DESCRIPTION OF PROPOSED DEVELOPMENT

The subject property is located at the southeast corner of Rockdale Road and Russland Road/Highway Lane in Vars, Ontario. The property consists of approximately 0.9 ha. over two lots. The lot is occupied by two commercial businesses which are serviced by an on site sewage system and a drilled well. The businesses consist of an Esso fuel station and a used car sales lot. There are two parcels at the existing development with the municipal address of 6175 Rockdale Road.

The land is to be re-developed with a new configuration with an upgraded Esso fuel station and convenience store. A drive-through serving only prepared food will be incorporated using paper service only. The existing drilled well will be retained for use. A portable hose for hand washing of cars only will be installed in the well. The well will not be used as a drinking water supply. Washrooms will be key access only to restrict access to non-drinking water. The drive-through / store will only serve pre-packaged food and drinks. There is no preparation of food or dishwashing required on-site. As such, no potable water supply is necessary for drive-through operations. Refer to Figure 1 below showing the proposed site location.

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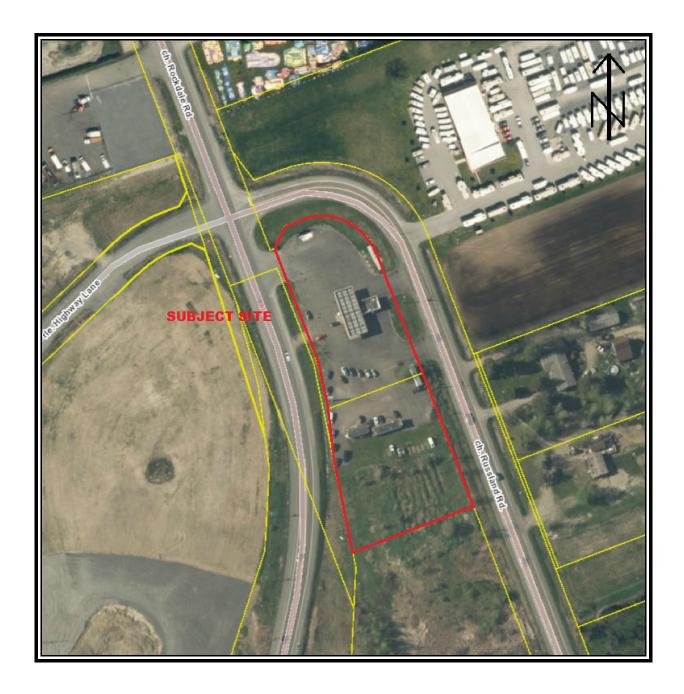


Figure 1: Key Plan

### FIELDWORK PROGRAM

As a means to demonstrate the adequacy of the overburden aquifer underlying the subject lands, with respect to water quality and quantity, a shallow dug well was constructed by Maurice Cayer Ltd on March 16, 2018. The dug well (TW 1) was constructed adjacent to the northwest corner of the subject site and is located greater than 30 m from the proposed fuel tanks and the proposed sewage system. The Ministry of Environment, Conservation

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and Parks (MECP) Water Well Record (WWR) indicates the well extends 4.9 m below the existing ground surface. The inside diameter of the well is 1.2 m and consisted of three tiles of 1.8 m height. See Paterson Drawing PH3333-3 for the approximate location of TW 1.

The tiles were set into limestone bedrock to a depth of approximately 1.2 m. Bedrock was encountered at 4.3 m depth and the casing extends down to approximately 5.3 m depth. The overburden material around the well casing consisted of a yellow sand to grey sand with some clay. A copy of the WWR can be found attached.

There is an existing drilled well on the site that is located west of the existing fuel bar and convenience store, and is located at the west edge of the asphalt parking area. The well is fully accessible with the 150 mm diameter steel casing extending approximately 200 - 300 mm above the existing ground surface. Due to the poor quality of water supply from the existing drilled well and the known poor water quality of the bedrock aquifer in the area, the owner elected to proceed with the installation of a dug well.

The ground surface surrounding the well is to be mounded appropriately to shed melt water away from it, and it is recommended to dump/stockpile snow away from the well. Existing grading is already designed to shed road water away for the well location along Russland Road. Four bollards should be placed around the well for additional protection and the locations of the bollards are to be determined at the time of construction. The site plan currently indicates evenly spaced bollards around the well, however, alternate spacing may be used at the time of construction to appropriately protect the well.

As a means to evaluate the water supply aquifer intercepted by the new well (TW 1), the well was subjected to a 6 hour constant rate pumping test. The pumping test was conducted on May 1, 2018 under the full-time supervision of Paterson.

Maurice Cayer Ltd. was retained to supply a submersible pump and generator for the pumping test. The submersible pump was placed approximately 0.3 m off the base of the well. The discharge hose was directed to the adjacent ditch along Russland Road in a downgradient direction based upon the slope of the existing landscaping and ditch. The discharge location was approximately 24 m downgradient of the well with the discharged water heading southward along Russland Road.

The pumping test (May 1, 2018) was carried out at a pumping rate of 22.5 L/min for a duration of 6 hours. Thereafter the pumping rate was lowered to 9 L/min for an additional 2.5 hours to determine if the turbidity level could be reduced. Additional pumping was performed on May 9, 2018, in an attempt, to reduce the turbidity level and to recover a bacteriological sample. During the pumping test, the pumping rate was periodically measured using the timed volume correlation method. The pump rate was maintained within 5% of the selected pump rate. The static water level was recorded and an electronic datalogger (Schlumberger Micro-Diver) was installed in the test well prior to the start of the

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pumping test. The data logger recorded water levels at 15 second intervals. In addition, manual water level readings were taken at periodic intervals during the test.

Recovery data was collected for the well following the completion of the pumping. The well was noted to have achieved approximately 95% recovery approximately 85 minutes after the completion of the first pumping test. Further development of the well was performed and the water level was monitored for several days after the completion of the pumping.

Groundwater samples were collected at 3 hours and 8.5 hours after the start of pumping. Prior to collection of the groundwater samples, the free chlorine residual was tested and found to be within a range of 7.7 mg/L at the 3 hour mark and dropped to 0.06 mg/L by the end of the 8.5 hour period. The additional pumping, carried out on May 9, 2018, extended for a period of 7 hours, after which the free chlorine residual was verified to be non-detectable. The water samples were submitted for comprehensive testing of bacteriological, chemical and physical water quality parameters consistent with the standard 'Subdivision Supply' suite of parameters and additional parameters for VOCs and PHCs F1-F2.

An additional sample was taken of the raw water from the existing drilled well. There is no WWR available at the time of writing this report.

All samples were collected unfiltered and unchlorinated and were placed directly into clean bottles supplied by the analytical laboratory. Samples were placed immediately into a cooler with ice and were transported directly to the Eurofins laboratory in Ottawa. All samples were received by the laboratory within 24 hours of collection.

Furthermore, a series of field testing of the pumped water were carried out at the well head. The parameters tested at the well head included: pH, total dissolved solids, conductivity, turbidity and temperature.

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### **AQUIFER ANALYSIS**

### **Water Quantity**

Pumping test data was analyzed using AquiferTest Pro (v. 2016.1) aquifer analysis software package by Schlumberger Water Services. Drawdown data was measured using an electronic water level tape and an electronic datalogger unit was also used to monitor drawdown in the test well.

TABLE 1:SUMMARY OF WATER SUPPLY AQUIFER CHARACTERISTICS OF TW1					
AQUIFER PARAMETER	RESULT OF ANALYSIS				
Transmissivity (m²/day)	1.33 x 10 <sup>2</sup>				
Pumping Rate (L/min)	22.5				
Pre-test Static Water Level (m)	2.08				
Post-test Static Water level (m)	2.83				
Available Drawdown (s) (m)	3.41				
% Drawdown During Pumping Test	22.0				
Specific Capacity (L/min/m drawdown)	30.0				

The drawdown data was analyzed using the Theis with Jacob Correction, and the Papadopulos & Cooper methods of analysis. Aquifer transmissivity is estimated to be approximately 133 m<sup>2</sup>/day.

The pumping test results show that test well TW1 has a high yield. Drawdown at a pumping rate of 22.5 L/min for 6 hours was 0.75 m and was used for the analysis. 95% recovery was achieved approximately 85 minutes after the end of pumping. Additional pumping was completed subsequent to the 6 hour period in an attempt to reduce turbidity with further development for a total of 8.5 hours. The total volume of water pumped during the 8.5 hour pumping event was approximately 9,450 L. The proposed daily sewage design flow is 9,145 L. As the pumped volume exceeded the maximum daily sewage design flow with minimal drawdown (0.03 m) from the 2.0 hour to the 8.5 hour mark, the well is considered adequate in regards to quantity. Additionally, Part 8 of the Ontario Building Code typically overestimates the daily sewage design flows. As the washroom is based upon keyed access, it is not expected that the design flows will be achieved.

As the pumping test was completed on a dug well, the well storage of the existing dug well must be considered. The well storage of the existing dug well is approximately 3,639 L, equating to 2.6 well volumes being removed from the well prior to the termination of the pumping test.

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The suitability of the aquifer to supply the proposed re-development was assessed based upon the methodology provided in MOECC Procedure D-5-5 (MOEE, 1996) and the proposed sewage daily design flows of 9,145 L/day. The usage of the water supply is proposed to be for the Service Station consisting of the gas bar at 560 L/day per gas nozzle (total of 12 nozzles), the convenience store at 155 m² at 5 L/day and two staff at 75 L/day. The water supply is intended to be used for hand washing and toilet supply only. The owner intends on importing bottled water for drinking purposes.

Based on the information summarized in Table 1, it is readily apparent that the new water supply well has intercepted a strong water supply aquifer which has more than sufficient quantity to service a fuel service station's needs of pump servicing, hand washing and bathroom facilities. The transmissivity aquifer parameter suggests a strong aquifer which is able to transmit significant quantities of water relatively quickly. It should be noted that the overburden aquifer's quantity may vary seasonally.

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### **Water Quality**

### Field Data

Turbidity, electrical conductivity, total dissolved solids, pH and temperature were measured at the wellhead during the pumping test. The measurements and time intervals for each of these parameters are summarized on the graphical representation in Figure 2. In addition, chlorine test strips and a Hach Colorimeter II were used to measure the chlorine residual level. No chlorine residual was detected in the discharge water prior to the collection of the bacteriological water sample recovered at the end of the May 9 pumping event.

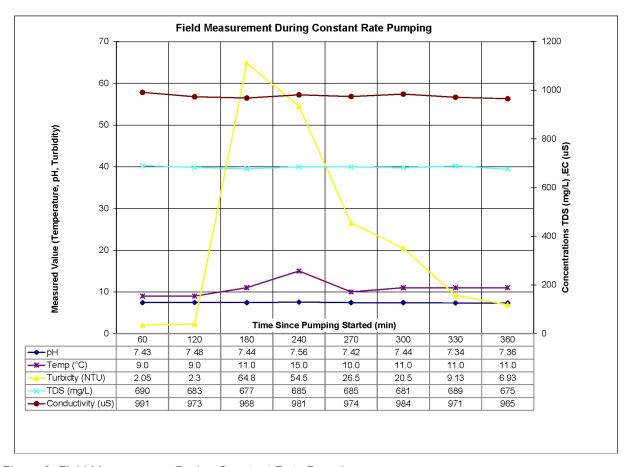


Figure 2: Field Measurement During Constant Rate Pumping

### Laboratory Data

The laboratory water quality, from the standard subdivision package, obtained from the pumping test of TW 1 is provided in Table 2 below and the full laboratory analyses reports that include the VOCs and PHC results can be found attached. The existing drilled well on the property was sampled to determine a comparison of the groundwater aquifer quality and the overburden aquifer quality with the sample WS#3 taken from the existing service station bathroom tap. There is no water treatment system within the existing Service

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Station.

The initial pumping test of TW1 contained a free chlorine residual at the completion of the pumping test and bacteriological testing was not performed on samples WS#1 or WS#2. Subsequent pumping to reduce turbidity and the free chlorine residual was performed with the bacteriological analysis results shown in Table 3 under WS#4.

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		OD	WS	TW	Existing		
PARAMETER	UNITS					Drilled Well	
TANAMETER	ONTO	LIMIT	TYPE	1-May-18	1-May-18	1-May-18	
				WS#1 (3hr)	WS#2 (8.5hr)	WS#3	
MICROBIOLOGICAL	Т	1	1				
Escherichia Coli (E.Coli)	ct/100mL	0	MAC	-	-	-	
Total Coliforms	ct/100mL	0	MAC	-	-	-	
GENERAL CHEMICAL -	HEALTH REL		1				
Fluoride	mg/L	1.5(2.4)	MAC	0.15	<0.10	<0.10	
N-NO2 (Nitrite)	mg/L	1	MAC	<0.10	<0.10	<0.10	
N-NO3 (Nitrate)	mg/L	10	MAC	0.35	0.22	<0.10	
Turbidity (Laboratory)	NTU	1.0 (5.0)	MAC/AO	18.2	9	8.8	
Turbidity (Field)	NTU	1.0 (5.0)	MAC/AO	45.2	17.4	-	
N-NH3 (Ammonia)	mg/L			0.03	0.10	1.2	
Total Kjeldahl Nitrogen	mg/L			0.5	0.5	1.6	
GENERAL CHEMICAL - A	ESTHETIC R	ELATED					
Hardness (as CaCO3)	mg/L	100	OG	568	551	582	
Ion Balance	unitless			0.92	0.9	0.9	
Total Dissolved Solids	mg/L	500	AO	1,480	1,490	1,850	
Alkalinity (as CaCO3)	mg/L	500	OG	330	418	503	
Chloride	mg/L	250	AO	567	554	607	
Colour	TCU	5	AO	<2	2	5	
Conductivity	uS/cm			2,270	2,290	2,850	
pH	unitless	6.5-8.5	AO	7.82	7.79	7.74	
Sulphide	mg/L	0.05	AO	0.03	<0.02	0.47	
Sulphate	mg/L	500	AO	54	82	53	
Calcium	mg/L			196	191	177	
Iron	mg/L	0.3	AO	0.36	0.22	0.77	
Potassium	mg/L			14	7	9	
Magnesium	mg/L			19	18	34	
Manganese	mg/L	0.05	AO	0.5	0.42	1.22	
Sodium	mg/L	200	AO	236	275	313	
Phenols	mg/L			<0.001	<0.001	<0.001	
Tannin & Lignin	mg/L			<0.1	0.1	0.5	
Dissolved Organic Carbon	mg/L	5	AO	3.3	3.7	7.1	

<sup>1.</sup> ODWS identifies the following types of parameters:

MAC=Maximum Allowable Concentration

AO = Aesthetic Objective

**OG= Operational Guideline** 

2. Shaded Concentration Indicates an Exceedance of the ODWS Objective

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TABLE 3: GROUNDWATER GEOCHEMISTRY (TW 1)								
	, ,							
PARAMETER	UNITS	LIMIT	TYPE	TW # 1 9-May-18 WS#4 (7 hr)				
MICROBIOLOGICAL								
Escherichia Coli (E.Coli)	ct/100mL	0	MAC	0				
Total Coliforms	ct/100mL	0	MAC	0				
GENERAL CHEMICAL - HEALTH RELATED								
Fluoride	mg/L	1.5(2.4)	MAC	-				
N-NO2 (Nitrite)	mg/L	1	MAC	-				
N-NO3 (Nitrate)	mg/L	10	MAC	<del>-</del>				
Turbidity (Laboratory)	NTU	1.0 (5.0)	MAC/AO	-				
Turbidity (Field)	NTU	1.0 (5.0)	MAC/AO	1.2				
N-NH3 (Ammonia)	mg/L			-				
Total Kjeldahl Nitrogen	mg/L			-				
GENERAL CHEMICAL - AL	STHETIC RI	LATED						
Hardness (as CaCO3)	mg/L	100	OG	-				
Ion Balance	unitless			-				
Total Dissolved Solids	mg/L	500	AO	-				
Alkalinity (as CaCO3)	mg/L	500	OG	<del>-</del>				
Chloride	mg/L	250	AO	<del>-</del>				
Colour	TCU	5	AO	-				
Conductivity	uS/cm			<del>-</del>				
рН	unitless	6.5-8.5	AO	<del>-</del>				
Sulphide	mg/L	0.05	AO	-				
Sulphate	mg/L	500	AO	-				
Calcium	mg/L			<del>-</del>				
Iron	mg/L	0.3	AO	-				
Potassium	mg/L			-				
Magnesium	mg/L			-				
Manganese	mg/L	0.05	AO	-				
Sodium	mg/L	200	AO	-				
Phenols	mg/L			-				
Tannin & Lignin	mg/L			-				
Dissolved Organic Carbon	mg/L	5	AO	-				
1. ODWS identifies the follo		paramete	rs:					
MAC=Maximum Allowabl		•						
AO = Aesthetic Objective								
OG= Operational Guidelin	е							
2. Shaded Concentration Indicates an Exceedance of the ODWS Objective								

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Two water samples were recovered during the initial pumping test of the well and submitted for laboratory analyses. The laboratory groundwater geochemistry results can be found attached.

The water quality of the subject water supply well meets all the Ontario Drinking Water Standards maximum acceptable concentrations (MAC). Furthermore, the water meets all the aesthetic objectives (AO) and operational guidelines (OG) with the exception of the following:

hardness;
TDS;
chloride;
iron;
manganese; and
sodium.

Exceedances of the above parameters are typical of the water supply in the subject aquifer. Each of these groundwater parameters are discussed in detail below.

#### Hardness

Hardness, expressed as calcium carbonate, an operational guideline, does not appear in the ODWS. Rather, it appears in the Technical Support Documents for Drinking Water Standards, Objectives and Guidelines (Technical Support Documents) as a parameter with an operational guideline of 100 mg/L. At the measured concentration of 568 and 551 mg/L, the water is considered to be hard to very hard, however it is exceeding the reasonable treatable limit of 500 mg/L, specified in Table 3 of the MOECC guidance document Procedure D-5-5 (1996), by a small margin. The hardness concentration can be treated using modern conventional water softener technologies.

#### **TDS**

Total dissolved solids (TDS) refers to the concentration of inorganic substances dissolved in water. The main constituents are typically chloride, sulphates, calcium, magnesium and bicarbonates. Water with a TDS concentration above 500 mg/L of TDS may not be palatable. Procedure D-5-5 does not provide a 'treatability limit' for TDS, but it does require written rationale that corrosion, encrustation or taste problems will not occur.

The Langelier Saturation Index (Langelier, 1936) is used to predict the calcium carbonate stability of water. It indicates whether the water will precipitate, dissolve or be in equilibrium with calcium carbonate.

The results of the Langelier calculation (LSI = 0.8) indicate the water is super saturated

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and tends to precipitate a scale layer of calcium carbonate (scale forming and non-corrosive). See attached Langelier calculations for further details.

The presence of TDS in drinking water contributes to the palatability of the water and is strictly an aesthetic parameter. Generally, water with TDS levels in excess of 1,200 mg/L is considered to be unacceptable, however, the palatability of the water is dependant upon the user. The TDS level in the subject water supply was measured to be 1,490 mg/L, which may impact the taste of the drinking water to some users. If desired, a point-of-use reverse osmosis treatment unit can be used to reduce the TDS levels at a designated drinking water tap. However, the proposed usage of the water supply is currently for hand washing and bathroom usage.

#### Chloride

Chloride (CI), an aesthetic parameter, was detected in the laboratory test sample at a concentration of 567 and 554 mg/L, which exceeds the ODWS aesthetic objective of 250 mg/L. The World Health Organization prepared a document "Chloride in Drinking-water" dated 1996 that concludes chloride concentrations in excess of 250 mg/L may potentially provide a detectable taste in the water. Consumers may become accustomed to chloride concentrations that exceed 250 mg/L. WHO noted that they would not be proposing limits for chlorides in drinking water. If desired, a reverse osmosis system would be able to reduce chloride levels.

#### Iron

An iron concentration of 0.36 and 0.22 mg/L was measured at the 3 and 8.5 hour interval, which is slightly above and below the aesthetic objectives in the ODWO. Concentrations exceeding the aesthetic objective of 0.3 mg/L may contribute to staining of plumbing fixtures and laundry. As per D-5-5, the results are below the level considered to be reasonably treatable. A conventional water softener can be used to reduce the levels of iron.

### Manganese

The manganese concentration results of 0.5 and 0.42 mg/L is above the aesthetic objectives in the ODWO. Concentrations exceeding the aesthetic objective of 0.05 mg/L may contribute to staining of plumbing fixtures and laundry. As per D-5-5, the results are well below the level considered to be reasonably treatable (1.0 mg/L). A conventional water softener can be used to reduce the levels of manganese.

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### Sodium

Sodium (Na), an aesthetic parameter, was detected in the laboratory test sample at a concentration of 236 and 275 mg/L, which exceeds the ODWS aesthetic objective of 200 mg/L. Although sodium is not toxic and no maximum acceptable concentration has been set, concentrations above 20 mg/L require that the Medical Officer of Health be notified of the water quality results, so that this information may be passed on to local physicians for use in treatment of those requiring a sodium-restricted diet.

### **Turbidity**

Turbidity, which is generally an aesthetic parameter, was detected in the laboratory test samples at values of 18.2 and 9.0 NTU at the 3 and 8.5 hour tests. The field results showed that turbidity increased around the 2.0 to 6.5 hour period of the initial test. Continued pumping showed a steady decrease towards the end of the pumping test. Field tests initially showed values of 1.15 to 2.05 NTU during the second pumping test over a seven hour period.

The ODWS maximum acceptable concentration for turbidity in drinking water entering the distribution system is 1 NTU. The Aesthetic Objective for turbidity in drinking water reaching the consumer is 5 NTU. In accordance with Procedure D-5-5, Table 2 does not reflect a maximum concentration considered reasonably treatable for turbidity. Rather, Procedure D-5-5 indicates that "particular care must be taken during testing to ensure that the bacteria requirements of Table 1 are met." Based on the test results, the bacteria requirements of Table 1 of D-5-5 have been met (E.Coli = 0 and Total Coliforms = 0).

It should be noted that the field turbidity testing indicated that the turbidly level reduced significantly during the pumping event. The field turbidity of 70.3 and 17.4 NTU was measured at the well head at approximately the 6 hour and 8.5 hour interval, respectively. Approximately 1 week after completion of the pumping test, the turbidity level was measured at 1.15 to 2.05 NTU. The high turbidity levels are related to sediment being mobilized and flushing into the well from the initial well construction. Further development of the well is expected to further reduce the turbidity levels.

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### **EXISTING DRILLED WATER WELL SUPPLY**

The existing drilled water well supply at the subject site is currently used for only hand washing and bathroom needs. When comparing the existing drilled well water supply to the proposed supply (TW 1), the existing drilled water well samples show exceedances for the same categories (Turbidity, Hardness, TDS, Chloride, Iron, Manganese and Sodium) as the proposed water well supply and also for Dissolved Organic Carbon (DOC) and Hydrogen Sulphide. The higher concentration of hydrogen sulphide was found in the existing drilled supply well. It was noted that the existing drilled supply has been in use for many years and is exhibiting worse water quality than the proposed water supply. There is no treatment system in place and the Service Station bathroom has a distinct odour of hydrogen sulphide (rotten eggs). This odour is common in other drilled wells in the area. Table 2 provides a comparison of the existing supply and TW 1 results.

The existing drilled water well supply will be retained for use. A portable hose for hand washing of cars only will be installed in this well.

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### **CONCLUSIONS**

Based on the information contained within the body of this report, the following conclusions can be drawn:

- The water supply aquifer intercepted by TW 1 is considered to be adequate to support the proposed service station in the long term. However, seasonal variations of water quality and quantity in shallow aquifers may occur. It is recommended that the dug well water supply be used for hand washing and toilet use only. Disinfection (Ultraviolet treatment) is recommended and signs indicating the water is to be used for hand washing and toilet use only must be posted. Access to the bathroom will be restricted by key access through a request to an employee and is not considered a public supply.
- 2. The preferred water supply aquifer intercepted by TW 1 contains a water supply that contains only elevated concentrations of aesthetic parameters (Hardness, TDS, chloride, iron, manganese and sodium). Some of the concentrations are above the reasonable treatable limits of D-5-5, but they can be removed by readily available water conditioning equipment.
- 3. A water softener is recommended to facilitate the removal of the hardness, iron and manganese concentrations.
- 4. Turbidity had reduced to below 2 NTU during the further development of the well and it is expected to reduce upon further development of the well.
- 5. The sodium concentrations were measured to be above the 20 mg/L reporting limit and, as such, the Medical Officer of Health for the City of Ottawa should be informed to assist area physicians in the treatment of local residents on sodium reduced diets. However, the water supply is not to be used as a potable water supply.
- 6. The results of the water supply assessment have provided satisfactory evidence that the water supply aquifer underlying the subject lands can support the redeveloped property with respect to water quality and quantity for the proposed usage of hand washing and toilet flushing.
- 7. The existing drilled well is to be maintained as per O.Reg 903.

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We trust that this satisfies your present requirements. Should you have any questions regarding this submission, please do not hesitate to contact the undersigned.

Yours truly,

### PATERSON GROUP INC.

Michael S. Killam, P. Eng.

### Attachments:

- MECP Water Well Record
- Eurofins Certificate of Analysis
- AquiferTest Pro Pumping Test Analysis Reports
- Langelier Saturation Index Calculation
- Paterson Drawing PH3333-1
- Paterson Drawing PH3333-2
- Paterson Drawing PH3333-3



Ministry of the Environment Well Record Tag#: A 238439 (ow) and Climate Change Regulation 903 Ontario Water Resources Act 238439 Measurements recorded in: ☐ Metric ☐ Imperial Page **Well Owner's Information** Last Name / Organization E-mail Address First Name ABDO Mailing Address (Street Number/N EL-Arab by Well Owner Municipality Province Telephone No. (inc. area code) 6175 ROCKdale Road KIGA3 406/13/8/35/35/25 ottawa **Well Location** Address of Well Location (Street Number/Name) Concession County/District/Municipality OTTOWO Postal Code KON3HO Ontario UTM Coordinates Zone Easting Municipal Plan and Sublot Number Other NAD | 8 | 3 | 18 | 18 | 18 | 5 | 02 | 08 | 8 | 3 |

NAD | 8 | 3 | 18 | 18 | 18 | 5 | 02 | 08 | 8 | 3 |

Overburden and Bedrock Materials/Abandonment Sealing Record (see instructions on the back of this form) Depth (m/ft) General Description From 0 **Results of Well Yield Testing** Annular Space Type of Sealant Used Volume Placed After test of well yield, water was: Depth Set at (m/ft)
From To Time | Water Level (m3/ft3) Clear and sand free (m/ft) (min) (m/ft) Other, specify seolants If pumping discontinued, give reason: 8-8 Level 3 1 1 8.8 Pump intake set at (m/ft) 7 2 7 **Method of Construction** Well Use 4 Commercial Diamond Public Not used Duration of pumping Jetting Rotary (Conventional) Domestic Municipal Dewatering 5 ☐ Rotary (Reverse) ☐ Driving ☐ Livestock Test Hole ☐ Monitoring Final water level end of pumping (m/j) ☐ Boring Digging ☐ Irrigation Cooling & Air Conditioning 4 10 ☐ Industrial Air percussion Other, specify Other, specify 15 15 **Construction Record - Casing** Status of Well 20 20 Open Hole OR Material (Galvanized, Fibreglass, Concrete, Plastic, Steel) Water Supply Inside Wall Depth (m/ft) Diamete (cm/in) Thickness Replacement Well 25 From To (cm/in) Test Hole 30 8.0 18 +2 Recharge Well concrete Dewatering Well 40 40 Observation and/or Monitoring Hole Well production (I/min (GPM) 50 Alteration (Construction) 7, 60 60 Yes Abandoned. Insufficient Supply **Map of Well Location Construction Record - Screen** Abandoned, Poor Water Quality Please provide a map below following instructions on the back. Depth (m/ft) Abandoned, other, reland RD (cm/in) specify Other, specify **Water Details Hole Diameter** Water found at Depth Depth (m/ft) Kind of Water: Fresh Untested Diameter 14 (m/tt) Gas Other, specify From Water found at Depth Kind of Water: Fresh Untested (m/ft) Gas Other, specify Water found at Depth Kind of Water: Fresh Untested **Well Contractor and Well Technician Information** Business Name of Well Contractor 1 | 5 Municipality Comment est Casselman Business E-mail Address Well owner's information Ministry Use Only Date Package Delivered 20180366 Name of Well Technician (Last Name, First Name) package delivered Date Work Completed tor Date Submitted 20180366 No Received © Queen's Printer for Ontario, 2014

# CERTIFICATE OF WELL COMPLIANCE

I, Regean Cayer	_ DO HEREBY CERTIFY that I am licensed
to drill water wells in the Province of Oniario, and the	nat I have supervised the drilling of a well on the
property of ABDO EL-A sab	(Name of Landowner), located at
6175 Rockdale Road Vage	On (Legal Description, Lot/Plan No.)
property of ABDO EL-Arab  (4175 Rockdale Road Voya in the Township of Osgoode Lot 27 Ca	ONC 6 KOA 3HO
I CERTIFY FURTHER that, I am aware of	the well drilling requirements the guidelines
recommendations and regulations of the Ministry of	the Environment governing well installations in
the Province of Ontario, and the standards	specified in any subdivision agreement and
hydrogeological report applicable to this site and T	ownship Standards
AND DO HEREBY CERTIFY THAT the said v	well has been drilled, cased, prouted (cement or
bentonite) as applicable and constructed in strict co	onformity with the standards required
	with the standards required.
SIGNED 4: 9	2010
SIGNED this 9 day of April 3	\$ <u>078</u> .
Maurice Cayer 150 Well Driller/ Company	
Well Driller/ Company	
The Engineer on behalf of the landowner set out ab	ove CERTIFIES that he/she has inspected the
well and it was constructed in accordance with the	specifications in O.Reg.903, this report and the
Hydrogeological Report with regards to casing leng	th and grouting requirements.
SIGNED this 23rd day of April	20.0
day of April	OFESSIONAL
	73/04/18 FF 100221103
W. Leilla	M S KILLAM #
Engineer	100221103
	NCE OF ONT PRI
	NCE OF ON



### **Environment Testing**

Client: Paterson Group

154 Colonnade Rd. South

Nepean, ON K2E 7T7

Attention: Mr. Mike Killam

PO#: 10449

Invoice to: Paterson Group

Report Number: 1806662
Date Submitted: 2018-05-02
Date Reported: 2018-05-10
Project: PH 3333
COC #: 197584

				Lab I.D. Sample Matrix Sample Type Sampling Date Sample I.D.	1356872 Water 2018-05-01 WS #1	1356873 Water 2018-05-01 WS #2	1356874 Water 2018-05-01 WS #3
Group	Analyte	MRL	Units	Guideline			
Calculations	Hardness as CaCO3	1	mg/L	OG 100	568*	551*	582*
	Ion Balance	0.01			0.92	0.90	0.90
	TDS (COND - CALC)	1	mg/L	AO 500	1480*	1490*	1850*
General Chemistry	Alkalinity as CaCO3	5	mg/L	OG 500	330	418	503*
	Chlorine (free)	0.04	mg/L			0.17	
	Cl	1	mg/L	AO 250	567*	554*	607*
	Colour	2	TCU	AO 5	<2	2	5
	Conductivity	5	uS/cm		2270	2290	2850
	F	0.10	mg/L	MAC 1.5	0.15	<0.10	<0.10
	N-NO2	0.10	mg/L	MAC 1.0	<0.10	<0.10	<0.10
	N-NO3	0.10	mg/L	MAC 10.0	0.35	0.22	<0.10
	рН	1.00		6.5-8.5	7.82	7.79	7.74
	SO4	1	mg/L	AO 500	54	82	53
	Turbidity	0.1	NTU	AO 5.0	18.2*	9.0*	8.8*
Metals	Ca	1	mg/L		196	191	177
	Fe	0.03	mg/L	AO 0.3	0.36*	0.22	0.77*
	K	1	mg/L		14	7	9
	Mg	1	mg/L		19	18	34
	Mn	0.01	mg/L	AO 0.05	0.50*	0.42*	1.22*
	Na	2	mg/L	AO 200	236*	275*	313*
Nutrients	Total Kjeldahl Nitrogen	0.1	mg/L		0.5	0.5	1.6
Others	F1 (C6-C10)	20	ug/L		<20	<20	
	F2 (C10-C16)	20	ug/L		60	<20	
Phenols	Phenols	0.001	mg/L		<0.001	<0.001	<0.001
Subcontract	DOC	0.5	mg/L	AO 5	3.3	3.7	7.1*

#### Guideline = ODWSOG

Results relate only to the parameters tested on the samples submitted. Methods references and/or additional QA/QC information available on request.

<sup>\* =</sup> Guideline Exceedence



### **Environment Testing**

Client: Paterson Group

154 Colonnade Rd. South

Nepean, ON K2E 7T7

Attention: Mr. Mike Killam

PO#: 10449

Invoice to: Paterson Group

 Report Number:
 1806662

 Date Submitted:
 2018-05-02

 Date Reported:
 2018-05-10

 Project:
 PH 3333

 COC #:
 197584

<b>Q</b>	Analida	MDI	Units	Lab I.D. Sample Matrix Sample Type Sampling Date Sample I.D.  Guideline	1356872 Water 2018-05-01 WS #1	1356873 Water 2018-05-01 WS #2	1356874 Water 2018-05-01 WS #3
Group Subcontract	Analyte N-NH3	<b>MRL</b> 0.01	mg/L	Guideline	0.03	0.10	
Subcontract	IN-INFIO	0.01			0.03	0.10	1.20
-	S2-	0.04	mg/L mg/L	AO 0.05	0.03	<0.02	0.47*
_	Tannin & Lignin	0.02	mg/L	AO 0.05	<0.1	0.1	0.47
VOCs	1,1,1,2-tetrachloroethane	0.1	ug/L		<0.5	<0.5	0.5
VOCS	1,1,1-trichloroethane	0.5	ug/L ug/L		<0.4	<0.4	
-	1,1,2,2-tetrachloroethane	0.4	ug/L ug/L		<0.5	<0.5	
-	1,1,2-trichloroethane	0.5	ug/L ug/L		<0.4	<0.4	
-	1,1-dichloroethane	0.4	ug/L ug/L		<0.4	<0.4	
_	1,1-dichloroethylene	0.4	ug/L ug/L	MAC 14	<0.5	<0.5	
_	1,2-dichlorobenzene	0.3	ug/L ug/L	MAC 200	<0.4	<0.4	
-	1,2-dichloroethane	0.4	ug/L	IMAC 5	<0.2	<0.2	
-	1,2-dichloropropane	0.5	ug/L	1141/10-0	<0.5	<0.5	
-	1,3,5-trimethylbenzene	0.3	ug/L		<0.3	<0.3	
-	1,3-dichlorobenzene	0.4	ug/L		<0.4	<0.4	
-	1,3-Dichloropropylene (cis+trans)	0.3	ug/L		<0.3	<0.3	
	1,4-dichlorobenzene	0.4	ug/L	MAC 5	<0.4	<0.4	
-	Acetone	30	ug/L		<30	<30	
-	Benzene	0.5	ug/L	MAC 1	<0.5	<0.5	
	Bromodichloromethane	0.3	ug/L	-	32.0	8.8	
	Bromoform	0.4	ug/L		1.8	1.5	
	Bromomethane	0.5	ug/L		<0.5	<0.5	
	c-1,2-Dichloroethylene	0.4	ug/L		<0.4	<0.4	
	c-1,3-Dichloropropylene	0.2	ug/L		<0.2	<0.2	
	Carbon Tetrachloride	0.2	ug/L	MAC 2	<0.2	<0.2	

Guideline = ODWSOG

\* = Guideline Exceedence

Results relate only to the parameters tested on the samples submitted. Methods references and/or additional QA/QC information available on request.



### **Environment Testing**

Client: Paterson Group

154 Colonnade Rd. South

Nepean, ON K2E 7T7

Attention: Mr. Mike Killam

PO#: 10449

Invoice to: Paterson Group

 Report Number:
 1806662

 Date Submitted:
 2018-05-02

 Date Reported:
 2018-05-10

 Project:
 PH 3333

 COC #:
 197584

				Lab I.D. Sample Matrix Sample Type Sampling Date Sample I.D.	1356872 Water 2018-05-01 WS #1	1356873 Water 2018-05-01 WS #2	1356874 Water 2018-05-01 WS #3
Group	Analyte	MRL	Units	Guideline			
VOCs	Chloroethane	0.2	ug/L		<0.2	<0.2	
	Chloroform	0.5	ug/L		54.8	9.6	
	Dibromochloromethane	0.3	ug/L		12.9	5.7	
	Dichlorodifluoromethane	0.5	ug/L		<0.5	<0.5	
	Dichloromethane	4.0	ug/L	MAC 50	<4.0	<4.0	
	Ethylbenzene	0.5	ug/L	MAC 140	<0.5	<0.5	
	Ethylene Dibromide	0.2	ug/L		<0.2	<0.2	
	Hexane	5	ug/L		<5	<5	
	m/p-xylene	0.4	ug/L		<0.4	<0.4	
	Methyl Ethyl Ketone (MEK)	10	ug/L		<10	<10	
	Methyl Isobutyl Ketone (MIBK)	10	ug/L		<10	<10	
	Methyl Tert Butyl Ether (MTBE)	2	ug/L	AO 15	<2	<2	
	Monochlorobenzene	0.5	ug/L	MAC 80	<0.5	<0.5	
	o-xylene	0.4	ug/L		<0.4	<0.4	
	Styrene	0.5	ug/L		<0.5	<0.5	
	t-1,2-Dichloroethylene	0.4	ug/L		<0.4	<0.4	
	t-1,3-Dichloropropylene	0.2	ug/L		<0.2	<0.2	
	Tetrachloroethylene	0.3	ug/L	MAC 10	<0.3	<0.3	
	Toluene	0.5	ug/L	MAC 60	<0.5	<0.5	
	Trichloroethylene	0.3	ug/L	MAC 5	<0.3	<0.3	
	Trichlorofluoromethane	0.5	ug/L		<0.5	<0.5	
	Vinyl Chloride	0.2	ug/L	MAC 1	<0.2	<0.2	
	Xylene; total	0.5	ug/L	MAC 90	<0.5	<0.5	
OCs Surrogates	1,2-dichloroethane-d4	0	%		103	105	
(%REC)	4-bromofluorobenzene	0	%		117	121	

Guideline = ODWSOG

\* = Guideline Exceedence

Results relate only to the parameters tested on the samples submitted. Methods references and/or additional QA/QC information available on request.



**Environment Testing** 

Client: Paterson Group

154 Colonnade Rd. South

Nepean, ON K2E 7T7

Attention: Mr. Mike Killam

PO#: 10449

Invoice to: Paterson Group

 Report Number:
 1806662

 Date Submitted:
 2018-05-02

 Date Reported:
 2018-05-10

 Project:
 PH 3333

 COC #:
 197584

Group	Analyte	MRL	Units	Lab I.D. Sample Matrix Sample Type Sampling Date Sample I.D.  Guideline	1356872 Water 2018-05-01 WS #1	1356873 Water 2018-05-01 WS #2	1356874 Water 2018-05-01 WS #3
· ·						0.5	
VOCs Surrogates (%	Toluene-d8	0	%		83	85	

Guideline = ODWSOG

\* = Guideline Exceedence

Results relate only to the parameters tested on the samples submitted. Methods references and/or additional QA/QC information available on request.



**Environment Testing** 

Client: Paterson Group

154 Colonnade Rd. South

Nepean, ON K2E 7T7

Attention: Mr. Mike Killam

PO#: 23839

Invoice to: Paterson Group Report Number: 1807217 Date Submitted: 2018-05-09 Date Reported: 2018-05-11 Project: PH3333 COC #: 82891

Group	Analyte	MRL	Units	Lab I.D. Sample Matrix Sample Type Sampling Date Sample I.D. Guideline	1358331 Water 2018-05-09 WS#3
Others	Escherichia Coli	0	ct/100mL	MAC 0	0
	Total Coliforms	0	ct/100mL	MAC 0	0

Guideline = ODWSOG

\* = Guideline Exceedence

Results relate only to the parameters tested on the samples submitted. Analytical Method: AMBCOLM1

additional QA/QC information available on request.

### 154 Colonnade Road South Ottawa, ON

patersongroup K2E 7J5

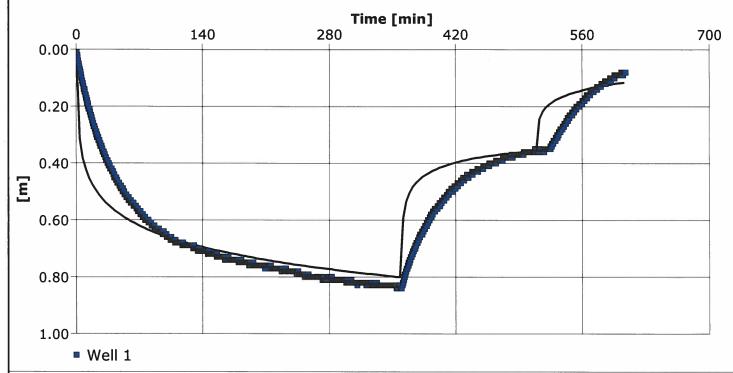
**Pumping Test Analysis Report** 

Project: Vars Esso

Number: PH3333

Client: Abdo El Arab

Location: 6175 Rockdale Road, Vars	Pumping Test: Pumping Test with full data	Pumping Well: Well 1
Test Conducted by: MK		Test Date: 01/05/2018
Analysis Performed by: MK	Theis with Jacob Correction	Analysis Date: 28/05/2018
Aquifer Thickness: 4.30 m	Discharge: variable, average rate 17.824 [l/s]	
Pumping rate was reduced to lower turbidity	. Part of recovery consists of pumping at a lower output.	



Calculation using Theis with Jacob Correction

Observation Well	Transmissivity	Hydraulic Conductivity Storage coefficient		Storage coefficient Radial Distance to PW	
	[m²/d]	[m/d]		[m]	
Well 1	1.64 × 10 <sup>3</sup>	3.80 × 10 <sup>2</sup>		0.6	

### 154 Colonnade Road South Ottawa, ON patersongroup K2E 7J5

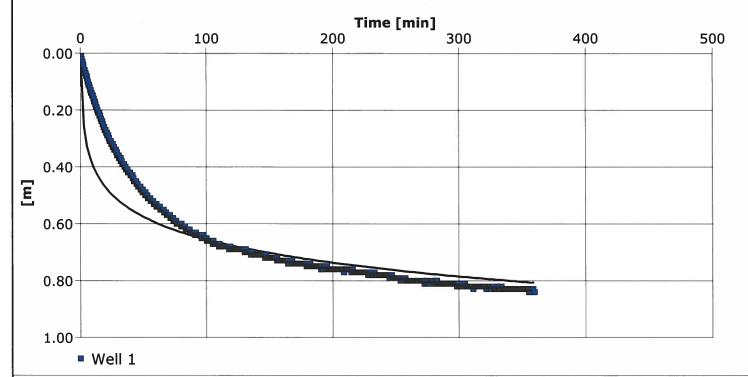
Pumping Test Analysis Report

Project: Vars Esso

Number: PH3333

Client: Abdo El Arab

Location: 6175 Rockdale Road, Vars	Pumping Test: Pumping Test with full data	Pumping Well: Well 1
Test Conducted by: MK		Test Date: 01/05/2018
Analysis Performed by: MK	Papadopulos & Cooper	Analysis Date: 30/05/2018
Aquifer Thickness: 4.30 m	Discharge: variable, average rate 17.824 [l/s]	
Pumping rate was reduced to lower turbidity. Part	recovery consists of pumping at a lower output.	



### Calculation using Theis with Jacob Correction

Observation Well	Transmissivity	Hydraulic Conductivity	rdraulic Conductivity Storage coefficient		
	[m²/d]	[m/d]		[m]	
Well 1	1.07 × 10 <sup>3</sup>	2.49 × 10 <sup>2</sup>		0.6	

### 154 Colonnade Road South Ottawa, ON patersongroup K2E 7J5

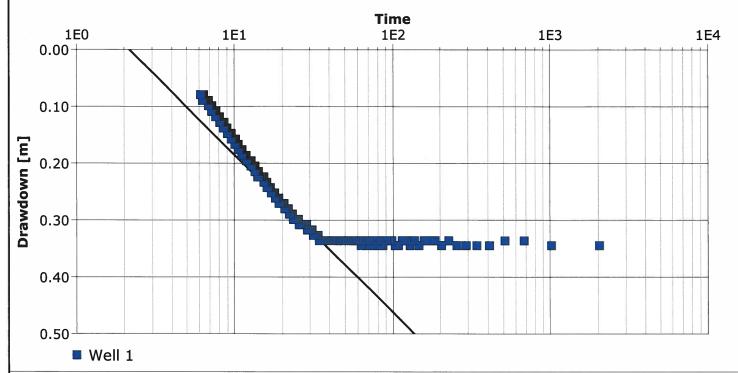
Project: Vars Esso

**Pumping Test Analysis Report** 

Number: PH3333

Client: Abdo El Arab

Location: 6175 Rockdale Road, Vars	Pumping Test: Pumping Test with full data	Pumping Well: Well 1	
Test Conducted by: MK		Test Date: 01/05/2018	
Analysis Performed by:	Theis Recovery	Analysis Date: 31/05/2018	
Aquifer Thickness: 4.30 m	Discharge: variable, average rate 17.824 [l/s]		
Pumping rate was reduced to lower turbidity. I	Part of recovery consists of pumping at a lower output.		



### Calculation using THEIS & JACOB

Observation Well	Transmissivity	Hydraulic Conductivity	Radial Distance to PW	
	[m²/d]	[m/d]	[m]	
Well 1	1.02 × 10 <sup>3</sup>	2.36 × 10 <sup>2</sup>	0.6	

### 154 Colonnade Road South Ottawa, ON patersongroup K2E 7J5

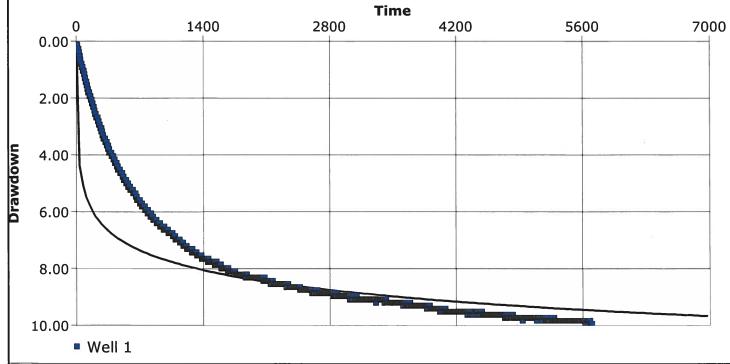
Project: Vars Esso

**Pumping Test Analysis Report** 

Number: PH3333

Client: Abdo El Arab

Location: 6175 Rockdale Road, Vars	Pumping Test: Pumping Test with full data	Pumping Well: Well 1
Test Conducted by: MK		Test Date: 01/05/2018
Analysis Performed by: MK	Theis with Jacob Correction (6 hours)	Analysis Date: 31/05/2018
Aquifer Thickness: 4.30 m	Discharge: variable, average rate 17.824 [l/s]	
Pumping rate was reduced to lower turbidity	Part of recovery consists of numping at a lower output	



Calculation using Theis with Jacob Correction

Observation Well	Transmissivity	Hydraulic Conductivity	Storage coefficient	Radial Distance to PW
	[m²/d]	[m/d]		[m]
Well 1	1.61 × 10 <sup>3</sup>	3.73 × 10 <sup>2</sup>		0.6

### 154 Colonnade Road South Ottawa, ON

patersongroup K2E 7J5

**Pumping Test Analysis Report** 

Project: Vars Esso

Number: PH3333

				Client: Abdo	El Arab				
Loca	ation: 6175 Rockdale Roa	ad, Vars	Pumping Test: F	Pumping Test with full dat	ta Pump	ing Well:	Well 1		
Tes	t Conducted by: MK				Test I	Date: 01/0	5/2018		
Aqu	ifer Thickness: 4.30 m	F:	Discharge: varia	ible, average rate 17.824	[l/s]				
Pun	ping rate was reduced to	lower turbidity. Part of	recovery consist	s of pumping at a lower o	output.				
	Analysis Name	Analysis Performed by	Analysis Date	Method name	Well	1	Γ [m²/d]	K [m/d]	s
1	Theis with Jacob Correction	nMK	28/05/2018	Theis with Jacob Correction	nWell 1	1	1.64 × 10 <sup>3</sup>	3.80 × 10 <sup>2</sup>	
2	Papadopulos & Cooper	мк	30/05/2018	Theis with Jacob Correction	nWell 1	1	1.07 × 10 <sup>3</sup>	2.49 × 10 <sup>2</sup>	
3	Theis Recovery		31/05/2018	Theis Recovery	Well 1	1	1.02 × 10 <sup>3</sup>	2.36 × 10 <sup>2</sup>	
4	Theis with Jacob Correction	nMKhours)	31/05/2018	Theis with Jacob Correction	nWell 1	1	1.61 × 10 <sup>3</sup>	3.73 × 10 <sup>2</sup>	
ši.	<u>*</u>		•		Α	verage 1	1.33 × 10 <sup>3</sup>	3.10 × 10 <sup>2</sup>	

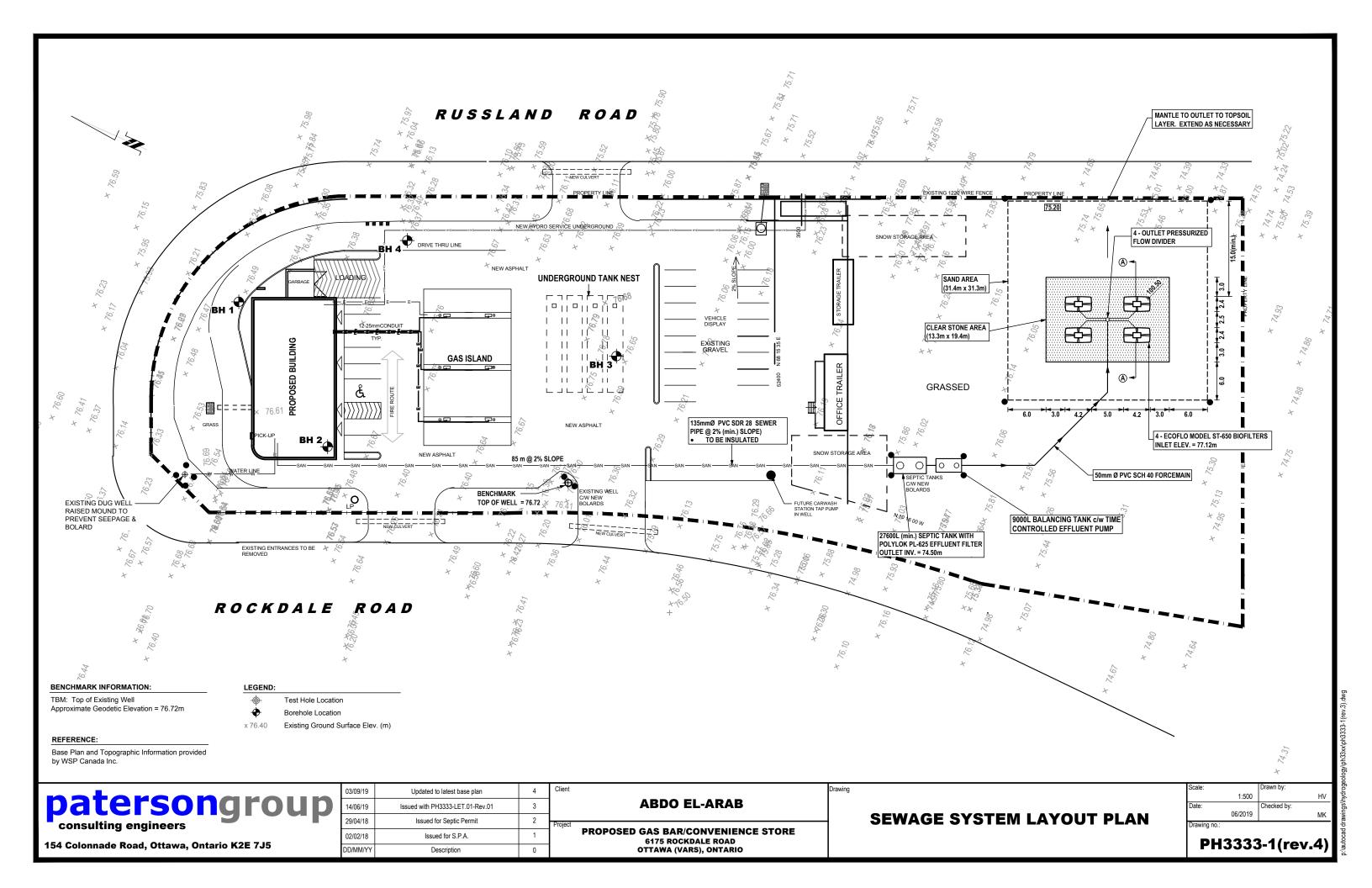
## patersongroup

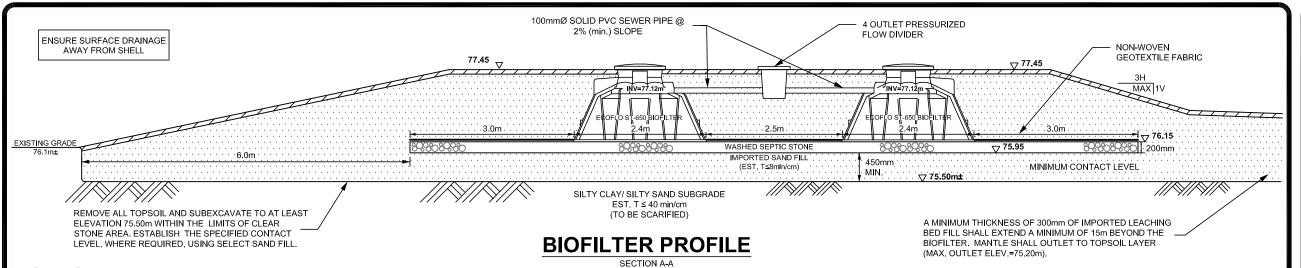
### 6175 Rockdale Road PH3333

ΓW1	inputs		
pН	7.79	A	0.22
TDS	1490	В	2.40
Hardness	551	С	2.34
Alkalinity	418	D	2.62
Temp.	9		
		pHs =	6.957722445

Langelier Saturation Index (LSI) Calcu	lation (Langelier, 1936)
pHs = (9.3 + A + B) - (C + D) Where:	A = (Log10 [TDS] - 1) / 10 B = -13.12 x Log10 (oC + 273) + 34.55 C = Log10 [Ca2+ as CaCO3] - 0.4 D = Log10 [alkalinity as CaCO3]
Γ	LSI = 0.8

		LOI =	0.0	
LSI	Effect			
0.5 to 2	Water is super saturated and tends to precipitate a scale layer	er of calcium carbonate (scale	forming but non-corrosive)	
0 to 0.5	Water is super saturated and tends to precipitate a scale layer	r of calcium carbonate (slightl	y scale forming and corrosive)	
0	Water is saturated (in equilibrium) with calcium carbonate. A scale layer of calcium carbonate is neither precipitated nor dissolved.			
0 to -0.5	Water is under saturated and tends to dissolve solid calcium c	carbonate (slightly corrosivebu	it non-scale forming).	
-0.5 to -2	Water is under saturated and tends to dissolve solid calcium c	carbonate (seriously corrosive	).	





### **NOTES:**

#### 1) ESTIMATE OF DAILY SEWAGE FLOW (Q)

THE PROPOSED DEVELOPMENT WILL CONSIST OF A GAS BAR WITH A CONVENIENCE STORE AND A TAKE-OUT RESTAURANT WITH PAPER SERVICE ONLY

GAS BAR: 12 NOZZLES @ 560L/DAY = 6720 L/DAY CONVENIENCE STORE: 155 m<sup>2</sup> x 5 L/DAY = 775 L/DAY TAKE OUT RESTAURANT: 74m²/9.25m² X 190 L/DAY/m² = 1527 L/DAY = 150 L/DAY + 2 STAFF @ 75 L/DAY TOTAL SEWAGE FLOW = 9145 L/DAY

DESIGN SEWAGE FLOW = 9200 L/DAY

#### 2) SUBGRADE CONDITIONS

SOILS INFORMATION GATHERED BY PATERSON GROUP INC. ON JULY 17, 2017 TH 2 FLEV 75.21m

1111, LLLV.	14.57111	1112, LLL	7. 70.21111	1110, LLL	v. 75.00m
0-0.19 0.19-0.35 0.35-1.35	TOPSOIL SILTY SAND SILTY CLAY SOME SAND	0-0.25 0.25-1.35	TOPSOIL SILTY CLAY SOME SAND	0-0.05 0.05-1.35	TOPSOIL SILTY SAND, SOME CLA
- GWL. @ 0.5	i8m DEPTH	- GWL @ 0.	.80m DETPH	- DRY UPC	ON COMPLETION

### GREASE TRAP

THE KITCHEN FLOW FROM THE TAKE-OUT RESTAURANT MUST OUTLET INTO AN INTERIOR GREASE TRAP TO BE DESIGNED BY MECHANICAL ENGINEER

TH 3 FLEV 75.88m

#### TANKAGE

TH 1 FLEV 7/107m

#### General

- ALL TANKS SHALL CONSIST OF PRECAST CONCRETE TANKS CONFORMING TO CSA-B66
- THE ACTUAL TANK CONFIGURATION MAY DIFFER FROM THAT SHOWN PROVIDED THE MINIMUM SPECIFIED WORKING CAPACITY OF THE TANK MEET THE DESIGN REQUIREMENTS.

ALL SEPTIC TANKS MUST BE CERTIFIED TO WITHSTAND ALL APPLICABLE LOADS.

- CONTRACTOR TO PROVIDE SHOP DRAWINGS FOR REVIEW TANKS SHALL BE BEDDED ON A LAYER OF OPSS GRANULAR A COMPACTED TO AT LEAST 95%
- OF ITS SPMDD.
- TANKS SHALL BE CONNECTED USING 100 mmØ SDR35 PVC SEWER PIPE WITH WATERTIGHT 6) CONNECTIONS
- BACKFILL TANKS USING OPSS GRANULAR B TYPE 1 BACKFILL OR CLEAN SAND FILL. PLACE BACKFILL IN UNIFORM LAYERS NOT EXCEEDING 300 mm THICKNESS AND COMPACT TO AT LEAST 90% OF SPMDD.
- FINAL GRADING SHALL BE SHAPED TO ENSURE THAT SURFACE WATER IS DIRECTED AWAY
- WORK AREA SHALL BE COVERED WITH A LAYER OF TOPSOIL OF AT LEAST 100mm IN

#### Septic Tank

- INSTALL A 27,600 L (min.) PRECAST CONCRETE SEPTIC TANK
- INSTALL POLYLOK PL-625 EFFLUENT FILTER ON OUTLET PIPE. EFFLUENT FILTER TO BE INSTALLED WITH BOTTOM PIPE SUPPORT AND EXTENDED HANDLE.
- EFLUENT FILTER TO BE INSTALLED ACCORDING TO MANUFACTURER'S GUIDELINES
- EFFLUENT FILTER TO BE CENTRED OVER ACCESS OPENING.
- A 600mmØ ULTRA RIB RISERS AND INSULATED COVER ASSEMBLY SHALL BE INSTALLED OVER TANK ACCESS OPENINGS
- RISERS SHALL EXTEND TO AT LEAST 50mm ABOVE FINISHED GRADE.
- PIPE CONNECTIONS AT TANK SHALL BE WATERTIGHT.

#### **Balancing Tank**

- THE BALANCING TANK SHALL CONSIST OF A 9,000 L SINGLE COMPARTMENT PRECAST CONCRETE TANK. IF A TWO COMPARTMENT TANK IS BEING USED, 3-150 mm Ø FLOW HOLES SHALL BE INSTALLED NEAR THE BASE OF THE DIVIDER WALL OF THE BALANCING TANK.
- BALANCING TANK SHALL BE LOCATED IN SERIES AND DOWNSTREAM FROM THE SEPTIC TANK
- TANKS SHALL BE CONNECTED USING 100 mm Ø SDR35 PVC SEWER PIPE WITH WATERTIGHT CONNECTIONS USING STAINLESS STEEL LINK SEALS OR APPROVED EQUIVALENT.
- THE ACCESS OPENING IN THE TANK LID OVER THE PUMP SHALL BE 600mmø. A 750mmø ULTRA 15.1m FROM ANY DRILLED WELL RIB RISER PIPE SHALL BE CAST IN THE TANK LID AND EXTEND TO AT LEAST 50mm ABOVE • 30.1m FROM ANY DUG WELL FINISHED GRADE. A LOCKABLE INSULATED COVER SHALL BE INSTALLED ON RISER
- THE BALANCING TANK SHALL BE EQUIPPED WITH AN ALTERNATING DUPLEX PUMP SYSTEM, OR SIMILAR. THE PUMPS (2) SHALL CONSIST OF MYERS ME3F, OR EQUIVALENT, (230V, 1PH) WITH CORD LENGTH TO SUIT
- INSTALL REQUIRED FITTINGS AND PIPING FROM NEW PUMPS AND CONNECT A 50 mm Ø SCH40 PVC FORCEMAINS
- FORCEMAINS TO BE INSTALLED TO GRAVITY DRAIN AND OVERLAIN BY 50 mm THICK BY 600 mm WIDE INSULATION BOARDS
- ALL PIPING CONNECTIONS TO BE GLUED
- THE PUMPS SHALL BE OPERATED BY AN ALTERNATING DUPLEX TIME CONTROL PANEL.
- THE CONTROL PANEL SHALL ALTERNATE THE PUMPS AND THE PUMPS SHALL OPERATE EVERY 20 MINUTES WITH A RUN TIME OF 110 SECONDS AND DOSE VOLUME OF 230L.
- PUMP RUN TIME TO BE CONFIRMED IN THE FIELD
- A CONTROL SWITCH SHALL OVERRIDE THE TIMER TO MAINTAIN THE LIQUID LEVEL WITHIN THE WORKING CAPACITY OF THE TANK
- ALL ELECTRICAL WORKS MUST BE CARRIED OUT BY A QUALIFIED ELECTRICAL CONTRACTOR IN ACCORDANCE TO THE LATEST CODES, BYLAWS AND REGULATIONS.
- CONTRACTOR SHALL BE RESPONSIBLE TO OBTAIN ALL NECESSARY ELECTRICAL PERMITS AND COORDINATE ALL FLECTRICAL INSPECTIONS

#### 5) DISPOSAL FIELD SIZING REQUIREMENTS

- INSTALL ECOFLO MODEL ST-650 BIOFILTERS
- CLEAR STONE AREA REQUIRED = 9200/50 = 184m<sup>2</sup>
- CLEAR STONE AREA PROVIDED = 258 0m<sup>2</sup>
- SAND AREA REQUIRED = QT/400 =9200(40)/400 = 920m<sup>2</sup>
- SAND AREA PROVIDED = 982.8m2

#### DISPOSAL FIELD CONSTRUCTION GUIDELINES

- REMOVE ALL EXISTING TOPSOIL. WITHIN THE LIMITS OF THE SAND AREA AND SUBEXCAVATE TO AT LEAST ELEVATION 75.50m, WHICHEVER IS GREATER.
- A MINIMUM THICKNESS OF 450mm OF LEACHING BED FILL SHALL BE INSTALLED OVER A SUITABLY PREPARED SUBGRADE.
- LEACHING BED FILL SHALL BE UNIFORM SAND WITH GRADING LIMITS SIMILAR TO 100% PASSING 13.2mm SIEVE, LESS THAN 5% PASSING 0.075mm SIEVE AND HAVE A PERCOLATION RATE OF 6-8 min/cm.
- A MINIMUM THICKNESS OF 200mm OF WASHED SEPTIC STONE SHALL BE INSTALLED, WITHIN THE SPECIFIED CLEAR STONE AREA, OVER LEACHING BED FILL.
- THE ECOFLO BIOFILTERS SHALL BE INSTALLED LEVEL ON THE CLEAR STONE LAYER IN ACCORDANCE WITH THE MANUFACTURER'S RECOMMENDATIONS.
- THE CLEAR STONE LAYER, BEYOND THE BIOFILTERS, SHALL BE COVERED WITH A NON-WOVEN GEOTEXTILE FABRIC, ALL BACKEILL MATERIALS SHALL CONSIST OF PERMEABLE SAND FILL
- THE TOTAL WORK AREA SHOULD BE COVERED WITH APPROX. 100mm OF SANDY TOPSOIL AND SHALL BE VEGETATED AS SOON AS POSSIBLE.
- THE FINAL LANDSCAPED GRADING SHALL DIRECT SURFACE WATER AWAY FROM THE

THE UNDERSIDE OF THE BIOFILTER LIDS SHALL EXTEND ABOVE THE FINAL LANDSCAPED

#### 7) MINIMUM CLEARANCE DISTANCES FROM BIOFILTER

- 3.1m FROM ANY PROPERTY LINE
- 5.1m FROM ANY STRUCTURE

#### MINIMUM CLEARANCE DISTANCES FROM TANKS

- 1.5m FROM ANY PROPERTY LINE
- 1.5m FROM ANY STRUCTURE
- 15.0m FROM ANY DRILLED WELL

#### GENERAL

- CONTRACTOR SHALL BE QUALIFIED AND REGISTERED UNDER PART 8 OF THE ONTARIO BUILDING CODE.
- ALL WORK SHALL BE CARRIED OUT IN ACCORDANCE WITH THE LATEST BY-LAWS. CODES AND REGULATIONS.
- CONTRACTOR SHALL REVIEW DRAWINGS IN DETAIL AND SHALL INFORM THE CONSULTANT OF ANY ERRORS AND/OR OMISSIONS ON DESIGN DRAWINGS IMMEDIATELY.
- CONTRACTOR SHALL VISIT THE SITE AND REVIEW ALL DOCUMENTATION TO BECOME FAMILIAR WITH THE SITE AND SUBSURFACE SOIL CONDITIONS TO DETERMINE SUITABLE METHODS OF CONSTRUCTION.
- CONTRACTOR SHALL BE RESPONSIBLE FOR LAYOUT AND GRADING AS DETAILED ON THE DESIGN DRAWINGS THE CONTRACTOR IS RESPONSIBLE TO LOCATE AND PROTECT EXISTING UNDERGROUND SERVICES.
- THE MANUFACTURER PROVIDES A LIMITED WARRANTY OF THE SYSTEM COMPONENTS. THE OWNER OF THE BIOFILTER MUST SIGN A MAINTENANCE AGREEMENT WITH THE MANUFACTURER'S REPRESENTATIVE.
- THE PROPERTY OWNER IS RESPONSIBLE FOR THE ANNUAL COSTS ASSOCIATED WITH THE MAINTENANCE PROGRAM.
- THE FIRM OF PATERSON GROUP INC. HAS PROVIDED DESIGN SERVICES ONLY FOR THE SUBJECT SEWAGE SYSTEM. THE DESIGN HAS BEEN CARRIED OUT IN ACCORDANCE WITH THE MANUFACTURER'S GUIDELINES AND OUR INTERPRETATION OF PART 8 OF THE ONTARIC BUILDING CODE.
- INSPECTIONS BY THE CONSULTANT DURING THE INSTALLATION OF THE SYSTEM IS REQUIREMENT OF SOME REGULATING AUTHORITIES AND IS STRONGLY RECOMMENDED BY

14/06/19	Issued with PH3333-LET.01-Rev.01	3
29/04/19	Issued for Septic Permit	2
02/02/18	Issued for S.P.A.	1
19/07/17	Issued for Discussion Purposed	0
DD/MM/YY	DESCRIPTION	REV.

Consultant:

### patersongroup consulting engineers

Client:

**ABDO EL-ARAB** 

### **PROPOSED GAS BAR / CONVENIENCE STORE**

**6175 ROCKDALE ROAD OTTAWA (VARS), ONTARIO** 

Drawing:

### SEWAGE SYSTEM **DETAIL & NOTES**

Scale:	Drawn by:
N.T.S.	HV
Date:	Checked by:
06/2019	AVS

Drawing No.:

PH3333-2(rev.1)

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