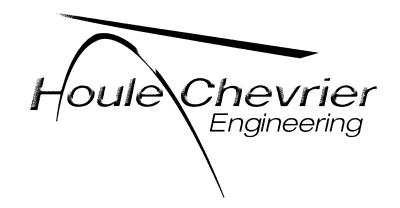
HYDROGEOLOGICAL ASSESSMENT HIGHLAND PARK CEMETERY VISITATION CENTER 2037 MCGEE SIDE ROAD OTTAWA, ONTARIO



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REPORT ON

HYDROGEOLOGICAL ASSESSMENT HIGHLAND PARK CEMETERY VISITATION CENTER 2037 MCGEE SIDE ROAD OTTAWA, ONTARIO

Submitted to:

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DISTRIBUTION:

9 Copies - Novatech Engineering Consultants Ltd. 2 Copies - Pinecrest Remembrance Services Ltd.

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1.0 INTRODUCTION

1.1 Background and Project Scope

Houle Chevrier Engineering Ltd. (HCEL) was retained by Novatech Engineering Consultants Ltd. on behalf of Pinecrest Remembrance Services Ltd. to conduct a hydrogeological investigation for a new water supply well to service a proposed visitation centre to be constructed at the Highland Park Cemetery located at 2037 McGee Side Road on Lot 11, Concession 2 in Huntley Township, Ottawa, Ontario.

The Highland Park Cemetery (hereafter referred to as 'the subject site') is comprised of a 48.6 hectare (120 acre) parcel of land to the northeast of the intersection of John Cavanaugh Drive and McGee Side Road (see Site Location Map, Figure 1). One small administration building is currently located in the southeast portion of the subject site. The existing administration building is serviced by a private drinking water well and an onsite septic disposal system.

The proposed development will consist of the construction of a new visitation centre building, approximately 1,400 square metres in size that will be serviced with on-site septic disposal system and private water supply well. The visitation centre building will be slab on grade construction and will be situated within the ringed roadway at the centre of the site (see Figure 1).

The objectives of this investigation are as follows:

- To investigate the potential quantity and quality of groundwater available from a drilled test well on the subject site for potential domestic supply;
- To assess the potential for impact on the receiving aquifer(s) and any nearby surface water features from on-site septic disposal systems. This will include predictions on nitrate concentrations at the property boundaries.

1.2 Land Use in the Vicinity of the Site

Land use within 500 metres of the drinking water well was reviewed for concerns related to groundwater quality. Land use in the vicinity of the site consists of agricultural land use, scattered rural residential and industrial/commercial land use. Specific land uses near the site boundaries are summarized below:

Site Boundary	Land Use
Southwest	 Industrial/commercial land use, including one (1) church (institutional land use).
Northwest	Agricultural land use.
Northeast	 Agricultural land use, including one (1) rural farm;
Southeast	 McGee Side Road, followed by agricultural land use, fragment woodlands and scattered rural residential.

Potential impacts to groundwater quality from adjacent land within 500 metres of the subject site boundary are not anticipated. No large scale water takings capable of causing adverse impacts to groundwater quantity were identified within 500 metres of the onsite test well.

A Phase I Environmental Site Assessment (ESA), entitled "Phase I Environmental Site Assessment, Highland Park Cemetery, 2037 McGee Side Road, Ottawa, Ontario" and dated February 2010, was prepared by Houle Chevrier Engineering Ltd. for the subject site. The Phase I ESA indicated that no actual or potential issues of environmental concern were identified at the subject site or vicinity. Based on the results of the Phase I ESA, no further environmental investigation was recommended.

1.3 Overview of Local Geological Setting

1.3.1 Topography

The topography of the site is relatively flat. Topographic mapping data, provided by Novatech Engineering Consultants Ltd., indicates that the topography in the vicinity of the proposed visitation center building generally slopes downward from the south to the north.

1.3.2 Drainage

The majority of the site appears to be well drained based on observations made during site visits. The drainage of the subject site is assumed to be influenced by the natural topography of the site and is anticipated to be generally to the north based on topographic mapping. A drainage ditch runs along the southeastern boundary of the subject site along McGee Side Road.

1.3.3 Regional Surficial and Bedrock Geology

Surficial geology maps (Urban Geology of the National Capital Region) of the area indicate that the overburden deposits on the majority of the site range in thickness from about 1 to 10 metres. The overburden thickness in the immediate vicinity in the well is indicated to range from 3 to 5 metres. The surficial geology of the subject site is indicated to consist of sensitive silty clay of marine origin and/or glacial till. Surficial deposits in areas surrounding the subject site are indicated to be offshore marine sediments consisting of marine deposits composed of silt and clay and nearshore marine sediments composed of sands or sands and gravel.

Bedrock geology maps indicate that the surficial deposits on the site are underlain by interbedded limestone and shale of the Verulam Formation. Bedrock aquifer maps indicate that the Verulam Formation is capable of supplying sufficient water for domestic use. The water is indicated to be of variable quality and may be sulphurous and saline.

Reference information for the Urban Geology of the National Capital Region is provided in Section 7.0 and Appendix A of this report.

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2.0 **GROUNDWATER IMPACT ASSESSMENT**

2.1 Field Procedure

A geotechnical investigation, entitled "Geotechnical Investigation, Highland Park Cemetery Visitation Centre, 2037 McGee Side Road, Ottawa, Ontario" and dated March 2010, was prepared by Houle Chevrier Engineering Ltd. to determine the subsurface conditions at the subject site.

The field work for the geotechnical investigation was carried out between February 8 and 9, 2010. During that time, six (6) boreholes, numbered 101 to 106, inclusive, were advanced in the area of the proposed building to depths ranging from 3.8 to 4.5 metres. In addition, two (2) test pits, numbered 101 and 102, were advanced in the area of the septic leaching bed; and, seven (7) test pits, numbered 103 to 109, were excavated in the area of the proposed parking lot and access roadways. Samples of the groundwater were recovered from boreholes 102 and 105 on June 3, 2010 and were submitted to Exova Accutest laboratory for analysis of nitrate concentrations.

The approximate locations of the boreholes and test pits advanced as part of the geotechnical investigation are shown on the Test Well, Borehole and Test Pit Location Plan, Figure 2. An aerial photograph of the overall area of the subject site is provided on the Site Plan, Figure 3. Descriptions of the subsurface conditions logged in the boreholes and test pits are provided in the geotechnical report.

2.2 **Soil and Groundwater Conditions**

A surficial layer of topsoil, generally ranging in thickness from about 0.1 metres to 0.3 metres, was encountered in all of the boreholes and test pits. Topsoil on the subject site was generally determined to be underlain by deposits silty clay, sandy silt and glacial till. A detailed discussion on the subsurface conditions can be found in the aforementioned geotechnical report.

Measured groundwater levels in the well screens installed in boreholes 102, 105, and 106 ranged from 1.7 to 1.9 metres below ground surface on February 19, 2010. No groundwater inflow was observed in the test pits during the short period that they were left open following excavation.

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The groundwater levels may be higher during wet periods of the year such as the early spring or following periods of precipitation.

2.3 Background Nitrate Concentration

Water samples were collected from the monitoring wells installed in boreholes 102 and 105 on June 3, 2010, and submitted to Exova Accutest for analysis of nitrates. The laboratory report of analysis are provided in Appendix B.

The results of the laboratory analysis indicate that the background nitrate concentration in the overburden soils in the vicinity of the proposed building were below the laboratory method of detection.

2.4 Nitrate Dilution Calculation

Calculations were carried out to assess the potential impact of septic effluent on the properties adjoining the proposed development using a nitrate dilution model. The Thornthwaite Water Balance method was used to estimate the net potential infiltration based on local climatic data available from Environment Canada for the Ottawa International Airport in Ottawa, Ontario.

The nitrate concentration at the site boundaries was calculated using the following information:

- A water surplus value of 312.4 millimetres was provided by Environment Canada obtained for the Ottawa International Airport in Ottawa, Ontario between 1983 to 2002 for soil with a water holding capacity of 280 millimetres (silty clay). A copy of the water surplus data is provided in Appendix C;
- A conservative infiltration factor of 0.45 was calculated using Table 2 of Section 4-62 of the MOE document titled "MOEE Hydrogeological Technical Requirements for Land Development Applications" dated April 1995.
 - A topography factor of 0.20 was used because the site has a gentle downward slope from the south to the north.
 - A soil factor of 0.15 based was chosen based on the existing overburden deposits (combinations of silty clay, sandy silt and glacial till).
 - A cover factor of 0.10 was chosen for this site since the subject site consists primarily of grassed landscaped areas.
- The area for potential infiltration was estimated to be approximately 44.9 hectares based on the total site area minus estimated hard surfaced parking areas, access roadways and roof tops (conservative estimate of 36,500 m² of hard surfaced areas).

Based on the above information, an expected volume of effluent of 6,000 litres per day for the proposed new building and an estimated 900 litres per day for the existing building on the subject site (total septic flow for the subject site of 6,900 litres per day) and an effluent nitrate concentration of 40 mg/L, the nitrate concentration at the site boundaries was calculated to be 1.53 mg/L (refer to the calculation in Appendix D). This is below the acceptable nitrate impact requirement of 2.5 mg/L established by the MOE for commercial sites. The value is considered to be conservative since some of the water runoff from hard surfaced areas (driveways, roofs, road, etc.) will be contained on the subject site and will infiltrate through native and imported soils.

3.0 GROUNDWATER SUPPLY INVESTIGATION

3.1 Field Procedures

A field investigation was carried out in accordance with the MOE August 1996 document "Procedure D-5-5, Technical Guideline for Private Wells: Water Supply Assessment" to determine the quantity and quality of groundwater available for domestic water supply.

One (1) new test well (Test Well TW1) was drilled by Capital Water Supply Ltd. of Stittsville, Ontario under Well Contractor License No. 1558 on February 18, 2010.

The approximate location of the test well is shown on the Test Well, Borehole and Test Pit Location Plan, Figure 2. An aerial photograph of the overall area of the subject site and area of proposed development are provided on the Site Plan, Figure 3. The MOE Water Well Record for the test wells is provided in Appendix E and the geographical reference for the test well is provided in the MOE Water Well Record.

3.1.1 Test Well Construction

Well grouting inspections were carried out by HCEL staff during the sealing of the well casing in the test well. The well casing for the test well was sealed into the bedrock by placing approximately 0.42 m³ of cement and bentonite grout. HCEL staff was not present for the remainder of the drilling of the test well.

The construction details of the test well are summarized below:

Test Well	Depth to Bedrock	Depth of Casing	Total Well Depth
	(m BGS)	(m BGS)	(m BGS)
TW1	3.35	6.40	138.67

The well driller reported that some water was present in the test well but was insufficient to support pumping of the test well. The well driller brought a cable tool drill rig onsite to further develop the test well. The cable tool drill rig was successful in developing the test well such that sufficient quantity of water was obtained to carry out pumping of the test well.

3.1.2 Preliminary Water Sampling

A two (2) hour pump test was carried out by Capital Water Supply on February 19, 2010, for completion of the MOE Water Well Record. The well was pumped at a rate of 18.2 litres per minute for approximately two (2) hours. A preliminary water sample was collected from the test well following the two (2) hour pump test. The preliminary groundwater sample was collected and prepared/preserved in the field using established sampling protocols and submitted to Exova Accutest Laboratories (Exova) in Ottawa, Ontario for chemical, physical and bacteriological analyses as listed in the MOE guideline titled "Technical Guideline for Private Wells: Water Supply Assessment", dated August 1996. The laboratory reports of analysis for the preliminary water sampling are provided in Appendix F and summarized in Table 1 following the text of this report.

Additional pumping was conducted on the test well prior to re-sampling to confirm the exceedances noted in the preliminary water sample. The test well was pumped at a rate of approximately 22.5 litres per minute for approximately eight (8) hours on March 5, 2010. Following the eight (8) hours of additional pumping, a water sample was collected and submitted to Exova Accutest for analysis of parameters that were noted to be exceeded in the preliminary water sample. The laboratory reports of analysis for the supplementary sampling are provided in Appendix G.

Additional pumping of the test well was carried out over the period of March 16 to 18, 2010, in an effort to further develop the test well. Water samples were collected on March 16 and March 18 and submitted to Exova Accutest for analysis of fluoride. The laboratory reports of analysis for the supplementary sampling of fluoride are provided in Appendix G.

The results of the initial rounds of water sampling indicated that several health related, aesthetic and operational guideline parameters exceeded the limits provided in the Ontario Drinking Water Standards (ODWS). The exceedances of the preliminary water sample and subsequent retesting are summarized below:

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			7	
Date	Parameter Exceeded	Concentration	ODWS Limit	Notes
	Total Coliform	<10 ct/100 mL	0 ct/100 mL	Exceedance due to elevated detection limit
Feb. 19, 2010	Escherichia Coli	<10 ct/100 mL	0 ct/100 mL	Exceedance due to elevated detection limit
	Colour	17 TCU	5 TCU	-
	Fluoride	3.17 mg/L	1.5 mg/L	-
	Hydrogen Sulphide	1	0.05 mg/L	Elevated Detection Limit
	Turbidity	>100 NTU	5 NTU	Elevated turbidity due to cable tool drill rig
Feb. 19, 2010	Sodium	125 mg/L	20 mg/L	Exceeds warning level for persons on sodium restricted diets only
	Iron	1.54 mg/L	0.3 mg/L	-
	Manganese	0.06 mg/L	0.05 mg/L	-
	Organic Nitrogen	0.18 mg/L	0.15 mg/L	-
	Fluoride	2.71 mg/L	1.5 mg/L	-
Mar. 5, 2010	Hydrogen Sulphide	3.80 mg/L	0.05 mg/L	-
	Turbidity	36.7 NTU	5 NTU	-
Mar. 16, 2010	Fluoride	2.94 mg/L	1.5 mg/L	-
Mar. 18, 2010	Fluoride	3.32 mg/L	1.5 mg/L	-

Notes: Bold: Health related parameter

3.1.3 Test Well Rehabilitation

Due to the observed concentrations of fluoride in the test well, rehabilitation options were investigated to improve the water quality of the well. The test well was hydro-fractured on April 30, 2010 by Outaouais Well Fracturing. The test well was hydro-fractured from a depth of approximately 6.4 metres below ground surface to a depth of 78.0 metres below ground surface.

An additional eight (8) hours of pumping was carried out on May 5, 2010, at a pumping rate of approximately 22.5 litres per minute. A water sample was collected from the test well following the eight (8) hours of pumping and submitted to Exova Accutest laboratory for analysis of fluoride. The laboratory report of analysis for the post hydro-fracturing water sample is provided in Appendix H.

The results of the May 5, 2010 water sample analysis indicated that the fluoride concentration in the test well was reduced by approximately 40 percent as a result of the hydro-fracturing activities. The fluoride concentrations in the test well samples collected prior to and after hydro-fracturing are summarized below:

Sample Date	Pre Hydro Fracturing Fluoride Concentration	Post Hydro Fracturing Fluoride Concentration
February 19, 2010	3.17 mg/L	_
March 5, 2010	2.71 mg/L	_
March 16, 2010	2.94 mg/L	-
March 18, 2010	3.32 mg/L	-
May 5, 2010	-	1.93 mg/L

Based on the Ministry of Environment document "Technical Support Document for Ontario Drinking Water Standards, Objectives and Guidelines" dated June 2006, fluoride concentrations in the range of 1.5 to 2.4 mg/L should be addressed through local boards of health to raise public and professional awareness to control excessive exposure to fluoride from other sources.

Once the concentration of fluoride in the test well following the hydro fracturing was reduced to a concentration within the range of 1.5 to 2.4 mg/L, a six (6) hour pump test was carried out on the test well to demonstrate that:

- fluoride concentrations in the test well will remain within the 1.5 to 2.4 mg/L range with continued well development;
- the quality of the water meets the Ministry of Environment Regulations, Standards, Guidelines and Objectives; and,
- the test well is capable of supplying a sufficient quantity of water for the intended future use.

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3.1.4 Pumping Test

A pumping test for the onsite test well was conducted on May 18, 2010. A six (6) hour duration constant discharge rate pumping test was conducted on the test well at a flow rate of approximately 22.5 litres per minute. During the pumping test, water level measurements were taken at regular intervals using an electric water level tape and on a continuous basis using an electronic data logger. After the pump was shut off, water level data was collected until a minimum of 95 percent of the drawdown in water level had recovered in the test well. The water level measurements for the drawdown and recovery data for the pumping test are provided in Appendix I.

3.1.5 Water Sampling

Groundwater samples were collected from the test well after three hours of pumping and again in the last hour of the pump test to characterize groundwater quality. Total chlorine tests were performed to ensure that chlorine levels were at 0.0 mg/L prior to sampling for bacteriological testing. The temperature, conductivity, total dissolved solids, pH, turbidity and total chlorine levels of the groundwater were measured at periodic intervals during the pumping tests and are summarized in Table 2. The groundwater samples were collected and prepared/preserved in the field using established sampling protocols and submitted to Exova Accutest Laboratories (Exova) in Ottawa, Ontario for chemical, physical and bacteriological analyses as listed in the MOE guideline titled "Technical Guideline for Private Wells: Water Supply Assessment", dated August 1996. The results of the analyses are summarized in Table 3 and the laboratory reports of analysis are provided in Appendix J.

Corrective actions were undertaken to address microbiological exceedances detected in the test well in water samples collected during the six (6) hour pump test. Supplementary water sampling for microbiological analysis was carried out on June 9, 2010, following the corrective actions. The results of the supplementary microbiological water sampling are summarized in Table 3. The laboratory reports of analysis for the supplementary sampling are provided in Appendix K. Field measurements for chlorine and turbidity taken during additional pumping following the corrective actions are summarized in Table 4.

The local Medical Officer of Health was notified of the fluoride and sodium concentrations and the address of the property by facsimile on June 7, 2010. A response letter from the local

Medical Officer of Health, dated June 9, 2010 indicates that advisory information regarding fluoride and sodium concentrations in the water supply should be provided to users of the well water for consumption purposes. A copy of the facsimile sent to the local Medical Officer of Health and the response letter received are provided in Appendix L.

3.2 Water Quality

3.2.1 General

The results of the chemical, physical and bacteriological analyses on the water samples collected during the six (6) hour pump test are summarized in Table 3. All water quality results reported in the following sections are based on the water testing results after the hydrofracturing of the well was completed. No water quality results prior to the hydro-fracturing are discussed in the following sections.

3.2.2 Health Related Parameters - Onsite Test Wells

Health related exceedances of the Ontario Drinking Water Standards (ODWS) were limited to microbiological parameters and fluoride. A summary of health related exceedances and subsequent re-sampling results are summarized below:

Sample Date	Parameter	Concentration	ODWS Maximum Acceptable Concentration
	Total Coliform	6 ct/100 mL - 3 hour sample 6 ct/100 mL - 6 hour sample	0 ct/100 mL
May 18, 2010	Fluoride	1.68 mg/L - 3 hour sample 2.12 mg/L - 6 hour sample	1.5/2.4 mg/L ¹
	Sodium	123 mg/L - 3 hour sample 177 mg/L - 6 hour sample	20/200 mg/L ²
June 9, 2010	Total Coliform	0 ct/100 mL - Retest B3 0 ct/100 mL - Retest B4	0 ct/100 mL

Notes:

As previously noted, the MOE Technical Support for ODWS document indicates that naturally occurring fluoride concentrations in the range of 1.5 to 2.4 mg/L can be addressed through local boards of health. When contacted, the local medical officer of health indicated that fluoride

^{1.} Naturally occurring fluoride concentrations in the range of 1.5 to 2.4 mg/L can be address through local boards of health.

^{2.} Sodium concentration does not exceed aesthetic objective and exceeds warning level of 20 mg/L for persons on sodium restricted diets only.

concentrations in the test well were acceptable provided that advisory information is provided to users of the well water.

The following corrective actions were carried out to address the total coliform exceedance in the May 18, 2010 sample:

- The test well was chlorinated on June 4, 2010 by HCEL staff using approximately 8 litres of 6 % sodium hypochlorite solution (bleach);
- After approximately 87 hours of contact time, the test well was pumped at a flow rate of approximately 22.5 litres per minute for approximately sixteen (16) hours on June 8 and approximately eight (8) hours on June 9, 2010;
- On June 9, 2010, the total chlorine concentration was confirmed by HCEL staff to be non-detectable as indicated by four (4) consecutive total chlorine measurements taken approximately five (5) minutes apart using a HACH Total Chlorine test kit (model CN-66T),
- On June 9, 2010, the level of turbidity of the water from the test well was confirmed to be below 5.0 NTU in the field as indicated by four (4) consecutive turbidity measurements taken approximately five (5) minutes apart using a Hanna Instruments Portable Turbidity Meter (model HI 93703-11), and;
- Following confirmation of low levels of turbidity and the absence of total chlorine concentrations, two (2) water samples were collected on June 9, 2010 in laboratory supplied bottles by HCEL approximately five (5) minutes apart and submitted to Exova Laboratories for analysis of total coliform bacteria.

The results of the re-sampling for total coliform on June 9, 2010, of the test well indicated that total coliform bacteria concentrations had been reduced to 0 ct/100 mL in both of the re-test samples. Based on the absence of total coliform bacteria in the retest samples taken on June 9, 2010, no further corrective actions for the test well are required and it is considered that it has been satisfactorily demonstrated that the water quality available at the site is free from bacteriological exceedances of the ODWS.

3.2.3 Aesthetic Objectives and Operational Guidelines

Aesthetic and operational related exceedances of the Ontario Drinking Water Standards (ODWS) were limited to hydrogen sulphide, total dissolved solids, turbidity and hardness. A summary of aesthetic objective and operational guideline related exceedances for the onsite test well are summarized below:

Sample Date	Exceedance	Concentration of Exceedance	ODWS Criteria
	Hydrogen Sulphide	0.17 mg/L - 3 hour sample 0.75 mg/L - 6 hour sample	0.05 mg/L
May 18,	Total Dissolved Solids	520 mg/L - 3 hour sample 683 mg/L - 6 hour sample	500 mg/L
2010	Turbidity	11.2 NTU - 3 hour sample 22.9 mg/L - 6 hour sample	5.0 NTU
	Hardness	128 mg/L as CaCO ₃ - 3 hour sample 121 mg/L as CaCO ₃ - 6 hour sample	100 mg/L as CaCO₃

Hydrogen Sulphide

The concentration of hydrogen sulphide in the test well exceeded the Ontario Drinking Water Standards (ODWS) aesthetic objective of 0.05 mg/L. The concentration of hydrogen sulphide in the test well ranged from 0.17 to 0.75 mg/L.

Elevated concentrations of hydrogen sulphide are typically characterized by an unpleasant odour (rotten egg smell) and, when in present in association with iron, can produce black stains on laundered items and black deposits on pipes and fixtures.

The Ministry of Environment document entitled "Technical Support Document for Ontario Drinking Water Standards, Objectives and Guidelines" indicates that low levels of hydrogen sulphide can be removed effectively from most well water by aeration. Hydrogen sulphide can also be effectively treated through the use of activated charcoal filters, chlorination, manganese greensand filters and other forms of oxidizing treatment. Based on the relatively low levels of hydrogen sulphide in the water samples collected during the pumping test, the water is considered to be reasonably treatable by aeration for the hydrogen sulphide exceedance.

Total Dissolved Solids

The level of Total Dissolved Solids (TDS) in the water sample from the test well exceeded the ODWS aesthetic objective of 500 milligrams per litre. As per Table 3 in the Appendix of the MOE Guideline D-5-5, rationale must be provided that corrosion, encrustation or taste problems will not occur when there are exceedances of the aesthetic objective for TDS.

To determine the potential for corrosion and/or encrustation of the groundwater, the Langelier Index (LI) and the Ryznar Stability Index (RSI) were calculated for the six (6) hour water sample obtained from test well on May 18, 2010. These values are based on the TDS, temperature, pH, alkalinity (as CaCO3), calcium (as CaCO3), chloride and sulphate levels observed in the sample. The six (6) hour laboratory results and the field temperature measured after six (6) hours of pumping of the test well were used for the purposes of the calculation.

The LI was calculated to be 0.55 and the RSI was calculated to be 7.2 for the test well. Information from the American Water Works Association indicates that the desired range of LI and RSI values to prevent corrosion and scaling is an LI greater than 0 and an RSI between 5.0 and 7.0. The results and our interpretations of the calculations are:

- The LI is in the desired range (slightly greater than zero (0)) and the water is considered to have a slight but tolerable scaling potential.
- The RSI is slightly outside the desired range of 5.0 to 7.0 and the water is considered to have a slight but tolerable corrosive potential.

Therefore, the degree of corrosion and scaling of plumbing should be acceptable. Additionally, based on our experience of carrying out resident interviews of homeowners with high TDS concentrations in their drinking water, we do not anticipate any discernable taste problems due to the TDS exceedance.

As per MOE Guideline D-5-5, we have shown that corrosion and encrustation are not expected to be of concern based on the LI and RSI calculations and we do not anticipate any discernable taste problems. Furthermore, a conventional water softener could be installed. The use of a conventional water softener will not reduce the total TDS, but will reduce the concentrations of calcium and magnesium, which are contributing factors to corrosion and encrustation.

Turbidity

The level of turbidity reported on the laboratory reports of analysis for the three (3) and six (6) hour water samples collected on May 18, 2010, ranged from 11.2 to 22.9 NTU and exceeded the ODWS aesthetic objective of 5.0 NTU. Additionally, field measurements of the turbidity during the pumping test ranged from 6.83 to 34.54 NTU.

Elevated levels of turbidity encountered in the test well are likely the result of the hydrofracturing activities previously conducted on the test well (refer to section 3.1.3 of this report).

Additional pumping of the test well was carried out on June 8 and June 9, 2010, to address microbiological exceedances. Field turbidity measurements were taken on June 9, 2010, to confirm that turbidity levels reduced to levels below the ODWS aesthetic objective. Four (4) consecutive field turbidity measurements were taken approximately five (5) minutes apart. The results of the field turbidity testing are provided in Table 4.

As indicated in Table 4, the level of turbidity as measured in the field ranged from 1.95 to 2.76 NTU. Therefore, based on the field turbidity measurements made on June 9, 2010, the water from the test well currently meets the ODWS aesthetic objective for turbidity.

Hardness

The concentration of hardness in the water samples obtained from the test well ranged from 121 to 128 mg/L as CaCO3 and exceeded the operational guideline of 80 to 100 mg/L of CaCO3 as specified in the ODWS.

Water having a hardness level above 80 to 100 mg/L as CaCO3 is often softened for domestic use. The MOE Procedure D-5-5 document states that water having a hardness value more than 300 mg/L is considered "very hard". The Ontario Ministry of the Environment publication entitled "Ontario Drinking Water Objectives", states that waters with hardness in excess of 500 mg/L are considered to be unacceptable for most domestic purposes. Most water supply wells within rural eastern Ontario are equipped with water softeners.

The level of hardness in the test well is within the treatable limits provided in MOE Procedure D-5-5 document using conventional water softeners.

Water softening by conventional sodium ion exchange may introduce relatively high concentrations of sodium into the drinking water which may be of concern to persons on a sodium restricted diet. The use of potassium chloride in the water softener (which adds potassium to the water instead of sodium) could be considered as a means of keeping sodium concentrations in the water at background levels. Consideration could also be given to providing a bypass of the water softener for drinking water purposes.

3.3 Water Quantity

A pumping test was carried out on the onsite test well to determine the characteristics of the water supply aquifer. Water level measurements were taken using an electronic water level tape and an electronic data logger in the test well during the pumping and recovery portions of the pumping test. The drawdown and recovery data and graphs for the water levels in the test wells during pumping are provided in Appendix I. The drawdown data contained in Appendix I was measured with reference to the top of the well casings.

Please note that the discharge rate on the drawdown data and graph sheets for the pumping tests are listed as variable because the recovery period, where the discharge rate is zero, is included in the same data set as the drawdown data. However, the actual discharge rate during the pumping of the test wells was at a constant rate.

The specific details of the pumping tests carried out on the test well are summarized below. All depths provided are in metres below ground surface (m BGS):

Parameter	Test Well
Pumping Duration (minutes)	381
Flow Rate (L/min)	22.8
Static Water Level (m BGS)	8.26
Well Depth (m BGS)	138.67
Available Drawdown (m)	130.09
Water Level at End of Pumping (m BGS)	28.64
Observed Drawdown at End of Pumping (m)	20.38
Drawdown Utilized (%)	15.7
Specific Capacity (m³/day•m)	1.6

As per MOE Procedure D-5-5, the test well was pumped at a flow rate greater than 13.7 litres per minute over a minimum of 6 hours. The maximum drawdown observed was 20.38 metres which is equivalent to approximately 15.7 percent of the available drawdown in the test well.

Novatech Engineering Consultants Ltd.

Based on these results, the onsite test well is capable of supplying water at a rate greater than 22.8 litres per minute for a period greater than six (6) hours. This is considered more than sufficient for proposed development use.

Based on the results of the drawdown and recovery data for the pumping test on the test well, the transmissivity was determined based on Theis analyses using Aquifer Test Pro 4.2.1.0, a commercially available software program from Waterloo Hydrogeologic Inc. The results of the Aquifer Test Pro 4.2.1.0 analysis are provided in Appendix M. The results of the analysis are summarized below:

Data Source	Transmissivity (m²/day)
Test Well	1.3
Typical Aquifer Parameters	15.7

The typical aquifer parameters transmissivity value was calculated as the arithmetic mean from the average transmissivity values for the Nepean-March-Oxford Hydrogeologic Unit. Rockcliffe Hydrogeologic Unit and Ottawa Group Hydrogeologic Unit provided in the MOE document entitled "The Hydrogeology of Southern Ontario, Second Edition" and dated April 2003.

The results of the Theis analysis indicate that the calculated transmissivity of the water supply aquifer available at the subject site is less than the typical aquifer transmissivity for local aquifers in the Ottawa area. Although the calculated transmissivity is less than typical transmissivity, there is sufficient water available at the site. This conclusion is based on:

- the flow rate during the pumping tests (22.8 litres per minute);
- the duration of the pumping tests (greater than 6 hours);
- the drawdown observed in the water wells (maximum of 15.7 percent drawdown after 6 hours of pumping), and;
- the water level in the well recovered by 95 percent of the drawdown approximately 130 minutes after the pump was shut off.

3.4 Ontario Ministry of Environment Water Well Records

The MOE Water Well Records for a 1.5 kilometre radius surrounding the subject site were obtained to determine the characteristics of existing private wells in the vicinity of the subject site. A total of one hundred and twenty two (122) well records were obtained and these records are provided in Appendix N. One hundred and five (105) of the well records were for drilled wells completed in the bedrock, twelve (12) of the well records were for wells completed in the overburden and five (5) of the well records were for unknown well types.

The well characteristics for the water well records are summarized below:

Parameter	Minimum	Maximum
Depth Water Found (m)	7.6	147.8
Pumping Rate (litres per minute)	4.5	682
Total Well Depth (m)	3.7	154.2

The depth to water found, pumping rate and total well depth of the onsite test well are within the ranges of depth to water found, pumping rate and total well depth for private wells in the vicinity of the subject site.

4.0 CONCLUSIONS

The subject site is considered suitable for development based on the results of the hydrogeological assessment. The quality and quantity of groundwater is sufficient to service proposed development.

Following hydro-fracturing and chlorination of the test well, water quality at the site is suitable for the intended use since:

- Education and notification measures can be put in place to address fluoride concentrations that range between 1.5 and 2.4 mg/l.
- Notification can be provided to indicate sodium concentrations exceeding the ODWS warning level of 20mg/l.
- A combination of reasonably available treatment measures (as indicated by MOE Procedure D-5-5 document), including aeration and conventional water softeners can be utilized to address hydrogen sulphide, total dissolved solids and hardness.
- The local medical officer of health has been notified of the sodium and fluoride concentrations found in the test well and concurred that education and notification to the users of the well for consumption purposes is an acceptable approach.
- The pump test indicated that the onsite test well is capable of sustaining short term yields greater than 22.8 litres per minute for a minimum period of six (6) hours. The maximum observed drawdown during the pumping test was approximately 15.7 percent of the available drawdown in the test well. The quantity of water pumped during the six (6) hour pumping test is greater than the calculated daily design flow for the proposed septic system to service the development. Therefore, the quantity of water available from the test well is sufficient to service the proposed development.
- The results of the nitrate dilution calculation indicate that the expected nitrate concentration at the boundaries of the subject site is expected to be approximately 1.5 mg/L, which is below the allowable nitrate concentration at the site boundaries. Therefore, no significant impacts from onsite disposal of septic effluent are anticipated on the water supply aguifer due to the proposed development.

6.0 LIMITATIONS OF REPORT

This report was prepared for Novatech Engineering Consultants (Novatech) and Pinecrest Remembrance Services Ltd. (Pinecrest) and is intended for the exclusive use of Novatech and Pinecrest. This report may not be relied upon by any other person or entity without the express written consent of HCEL, Novatech and Pinecrest. Nothing in this report is intended to provide a legal opinion.

The investigation undertaken by HCEL with respect to this report and any conclusions or recommendations made in this report reflect the best judgments of HCEL based on the site conditions observed during the investigations undertaken at the date(s) identified in the report and on the information available at the time the report was prepared. This report has been prepared for the application noted and it is based, in part, on visual observations made at the site, subsurface investigations at discrete locations and depths and laboratory analyses of specific chemical parameters and material during a specific time interval, all as described in the report. Unless otherwise stated, the findings contained in this report cannot be extrapolated or extended to previous or future site conditions, portions of the site that were unavailable for direct investigation, subsurface locations on the site that were not investigated directly, or chemical parameters, materials or analysis which were not addressed.

Should new information become available during future work, including excavations, borings or other studies, HCEL should be requested to review the information and, if necessary, re-assess the conclusions presented herein.

We trust that this report is sufficient for your requirements. If you have any questions concerning this information or if we can be of further assistance to you on this project, please call.

Yours truly,

HOULE CHEVRIER ENGINEERING LTD.

James McEwen, B.Sc., B.Eng.

Hydrogeologist

Mike Grinnell, P.Eng. Senior Environmental Engineer

Andrew Chevrier, M.Eng., P.Eng.

Principal



7.0 REFERENCES

Geological Survey of Canada. <u>Urban Geology of the National Capital Region</u> (http://gsc.nrcan.gc.ca/urbgeo/natcap/index e.php). November 5, 2007. (Refer to Appendix M for full Bibliography for this reference source).

Ontario Ministry of the Environment. <u>Manual of Policy, Procedures and Guidelines for Private</u> Sewage Disposal Systems. May 1982.

Ontario Ministry of the Environment. <u>Procedure D-5-5, Technical Guideline for Private Wells:</u> Water Supply Assessment. August 1996.

Ontario Ministry of the Environment. <u>Procedure D-5-4, Technical Guideline for Individual On-Site Sewage Systems: Water Quality Impact Risk Assessment</u>. August 1996.

Ontario Ministry of the Environment. <u>Ontario Drinking Water Quality Standards</u>, Safe Drinking Water Act, 2002, Ontario Regulation 169/03 as amended by Ontario Regulation 327/08. 2008.

Ontario Ministry of the Environment. <u>Technical Support Document for Ontario Drinking Water Standards, Objectives and Guidelines</u>. June 2006.

S.N. Singer, C.K. Cheng, and M.G. Scafe. Ontario Ministry of the Environment. <u>The Hydrogeology of Southern Ontario</u>, Second Edition. 2003.

Table 1 - Summary of Preliminary Water Test Results

Our Ref: 10-025-2

Count ct/100mL ct/0 Ct/100mL ct/0 Ct/100mL ct/0 Sarbon mg/L 269 mg/L 271 mg/L c0.19 mg/L c0.10 mg/L c0.01	PARAMETER	SEND	19-Feb-10	26-Feb-10	26-Feb-10	6-Mar-10	ONTARIO DRINKING WATER STANDARD	TYPE OF STANDARD
Opinio Coli CVI (100mL CVI (1	Total Coliforms	ct/100mL	012	O	C			
Coliforms	Escherichia Coli	0418mL	Š) :	>	> C	•	
Coliforms c4100mL <10	Heterotrophic Plate Count	ct/mL	65		B	> C	-	MAC
Streptococcus ct/100mL <10 - 10 - 10 - 10 - 10 - 10 - 10 - 10	Faecal Coliforms	ct/100mL	0.5	8	B 1	D) (ş	8
y as CaCO3 mg/L 269	Faecal Streptococcus	ct/100mL	× 45	1		> 5	ŧ	8
## Start			·		ı	,	8	8
## ## ## ## ## ## ## ## ## ## ## ## ##	Alkalinity as CaCO3	ma/L	269					
trivity FCU FCU FCU FCU FCU FCU FCU FC	Chloride	J/bu	20	ı	1	1) 9
### definition of the control of the	Colour	2	} •	1	8	. (550	8
Organic Carbon mg/L 1.4	Conductivity	mS/cm	747	1	8	7	Ω	Ş
Sulphide mg/L 3.17	Dissolved Organic Carbon	7/m	: 4		£	\$	8 8	8
Suphride Mg/L 1 1 1 1 1 1 1 1 1	Fluoride	- Z			9		0	2
with teaching mg/L 0.19 3.80 vitrate) mg/L <0.10 - vitrate) mg/L <0.05 - Lignin mg/L 27 - Lignin mg/L 27 - Lignin mg/L 27 - Lignin mg/L 1.0 - ND - CALC) mg/L 1.0 - mg/L 1.0 - - ddah I Nitrogen mg/L 1.7 - mg/L 1.5 - - mg/L 0.06 - - mg/L 0.06 - - mg/L 0.06 - </th <td>Hydrogen Sulphide</td> <td></td> <td>; ;</td> <td>9</td> <td>8</td> <td>Z</td> <td>w.</td> <td>S & C</td>	Hydrogen Sulphide		; ;	9	8	Z	w.	S & C
with the point of the	N-NH3 (Ammonia)	\$ 8		Ē	ı	8	0.05	\$
Mitrate) mg/L <0.10	N-NO (Airme)) () ()		š	ŧ	8	6
Lignin mg/L 0.005	N NOS (Nitropo)		2 9	•	8	ı	Š	MAC
Lignin		ě	<0.10		8	1	٤	MAC
Lignin mg/L 27			8.3G	8	3	ı	0.5-0 8.5-0 8.5	8
Lignin mg/L 27 Lignin mg/L 1.0 ND - CALC) mg/L 486 Gahl Nitrogen MTU 710 Sas CaCO3 mg/L 0.93 mg/L 17 mg/L 9 mg/L 4 mg/L 126 mg/L 164 Mg/L 0.06 Sas CaCO3 mg/L 164 Mg/L 164		mg/L	0.005	3	ŧ	8	8	8
NTU	Sulphate	mg/L	27	8	8	1	S	Ş
ND - CALC) mg/L 486	Tammin & Lignin	J/6m	0.		8	8) :) ,
MTU MG/L 0.37	TDS (COND - CALC)	766	486	3	\$	1	S	8
s as CaCO3 mg/L 80 36.7 nce mg/L 17	Total Kjeldahl Nitrogen	7/bu	0.37	3	9	ı	>	?
s as CaCO3 mg/L 80	Turbidity	2	8	8	8	7.98.	L.	, 🚭
mg/L 17	Hardness as CaCO3	mg/L	8	ē	8	•	2	2 8
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ium mg/L 9	Calcium]/gw	17	g	\$	ı	i 8	} {
mg/L 126	Magnesium	J/Su	ග		\$	8	8) (
mg/L 1.54	Potassium	786	4	9	9	1	1	
ganese mg/L 1.54 <0.03 mg/L 0.06 <0.01	Sodium) DE	8	8	ŧ	ı	2000	. §
mg/L	CO	J/6w	Š	ı	\$	<0.03	(f)	: \$
	Manganese	mg/L	90.0	1	1	\$0.01 10.02	? 5	§ &
- 25	Organic Nitrogen ⁽⁵⁾	mg/l-	8.0		8	8) C	2 8

NOTES

^{1.} MAC = Maximum Acceptable Concentration
2. OG = Operational Guideline
3. AO = Aesthetic Objective
4. The total of Nitrate and Nitrite should not exceed 10 mg/litre
5. The aesthetic Objective for sodium is 200 mg/litre. The local medical officer of health should be notified when the sodium concentration exceeds 20 mg/litre for persons on sodium restricted diets.
6. Organic Nitrogen = Total Kjeldahl Nitrogen - N-NH3 and should not exceed 0.15 mg/litre.
7. '' signifies no value provided in the ODWS guideline.

July 2010

Table 1 (Continued) - Summary of Preliminary Water Test Results

Our Ref: 10-025-2

				ONTARIO	
PARAMETER	2	16-Mar-10	18-War-10	DRINKING	7EQ
				WATER	STANDARD
Feshorishis Celi	ct/100mL	e		0	MACm
	Tung :	ı	8	0	MAC
	ce 1mL	ē	9	1	3
	ct/100mL	2	ı	ŧ	8
raecal Streptococcus	ct/100mL	8	1	9	ξ
Alkalinity as CaCO3	3		00.000/000000		
Chlorido	5	8	ı	30-500	00(5)
	7/8ú	8	8	250	AO(3)
: :	3	В	3	2	8
Conductivity	ms/cm	ą	8	. 8	
Dissolved Organic Carbon	mg/L	В	t	20	A
Fluoride	mg/L	8	888		28
Hydrogen Sulphide	mg/L	•	1	5:- 2:-0	3 <
N-NH3 (Ammonia)	J/ow	8	I	3	?
N-NO2 (Nitrite)	- J	5		0 1(4)	
N-NO3 (Nitrate)	mg/L	ŧ	ı	10(4)	
盂		ı		0 0	Ž.
Phenois	mo/L	ā) (0.0-0.0	3
Subject) M	1	į	2 2	. <
Tamin & Lignin	a more	ŧ		200	₹
TDS (COND - CALC)	1/8m	ŧ	3 8	- 05	. \$
Total Kjeldahi Nitrogen) Ма	8	ŧ	9	?
Turbidity	, <u>2</u>	â	ı	· (c	. 8
Hardness as CaCO3	Ž	ē	ŧ	80-100	2 8
Ion Balance)	\$	ı	2)
Calcium	Ž	\$	ł		B :
Magnesium	mg/	1	ı	ı (8
Potassium	Jõn M	Ē	\$: 6
Modium	mg/L	8	ı	(9)000	Ş
Lo.	m W	4	1	0.3	Q Q
Manganese	J S	B	ŧ	0.05	8
Organic Nitrogen(1)	mg/L	ı		0.15	90

MAC = Maximum Acceptable Concentration
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^{6.} Organic Nitrogen = Total Kjeldahl Nitrogen - N-NH3 and should not exceed 0.15 mg/litre. 7. '-' signifies no value provided in the ODWS guideline.

Table 2 - Summary of Field Parameter Measurements - Six Hour Pump Test

Our Ref: 10-025-2

|--|

Table 3 - Summary of Water Test Results - Six Hour Pump Test

PARAMETER	STIND	18-May-10 3 Hour Sample	18-May-10 6 Hour Sample	6/9/2010 Refest B3	6/9/2010 Refest B4	ONTARIO DRINKING WATER STANDARD	TYPEOF
Total Coliforms	ct/100mL	œ	e				
Escherichia Coli	ct/100mL	0 0	• •	>	0	0	
Heterotrophic Plate Count	ct/1ml	20	> <	•		0	MAC
Faecal Coliforms	ct/100ml	•	- 0	1		E E	8
Faecal Strentococcus	04/400ml)	>			5	8
200000000000000000000000000000000000000	3000		0		ı	1	8
Alkalinity as CaCO3	1/500	1000	4				
Chloride		757	238		,	30-500	000
	mg/L	82	130		8	250	AO ⁽³⁾
Conductivity	3 5	₹	\$*	2	,	S.	, Q
Dissiling	ma/cm	800	1050		•) (?
Dissolved Organic Carbon	mg/L	1.7	6.				. (
Fluoride	mg/L	3.68	2.2) ·	2
Hydrogen Sulphide	mg/L	0.17	0.75	1		0. 1	MAC
N-NH3 (Ammonia)	mg/L	0.26	0.32			o 5 5	8
N-NO2 (Nitrite)	mg/L	<0.10	<0.10		•	. (4)	8
N-NO3 (Nitrate)	ma/l.	\$0.10	3 0 0				MAC
급)	822	200				MAC
Phenois	ma/L	0000	2000	,		က် လ လ	90
Sulphate	ma/l	A5.0	0.00			\$	
Tannin & Lignin	ma/L	2 6	0 7		,	200	AO
TDS (COND - CALC)	ma/L	820	÷ &			\$	e
Total Kjeldahl Nitrogen	mg/L	0.25	38		,	33	Q Q
Turbidity	Z N	?	22.8		•	: 4	. (
Hardness as CaCO3	mg/L	128	ž		•	0 1	2
Ion Balance)	1.8	101		:	3	စ္ခ
Calcium	mg/L	30	27			1	B
Magnesium	mg/L	33			ı	1	ş
Potassium	mg/L	9) ıc		•	\$	8
Sodium	mg/l-	2	6	1	1	(8)	. (
Lou	mo/L	0.16	. «C			S	Ş Ş
Manganese	ma/L	0 0	8 6			? (\$0
Organic Nitrogen ⁽⁶⁾	ma/l	00 0	90.0	•	1	S :	AO
	m /2	W.VV	0.00		TO THE REAL PROPERTY OF THE PERSON NAMED AND THE PE	0.15	ဗ

- MAC = Maximum Acceptable Concentration
 OB = Operational Guideline

- AO = Aesthetic Objective
 The total of Nitrate and Nitrite should not exceed 10 mg/litre
 The aesthetic objective for sodium is 200 mg/litre. The local medical officer of health should be notified when the sodium concentration exceeds 20 mg/itre for persons on sodium restricted diets.

 6. Organic Nitrogen = Total Kjeldahl Nitrogen - N-NH3 and should not exceed 0.15 mg/litre.

 7. 'signifies no value provided in the ODWS guideline.

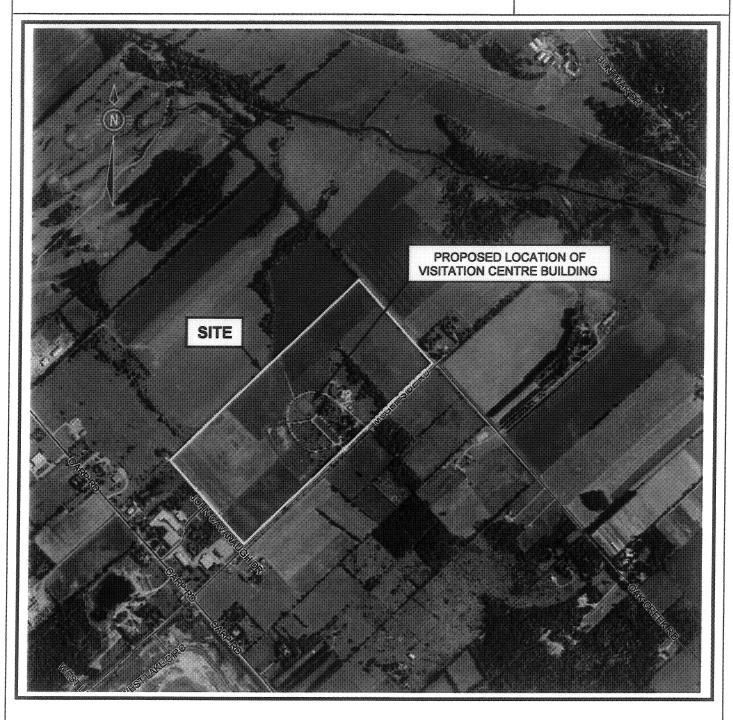
Table 4 - Summary of Field Parameter Measurements - Supplemental Sampling

Our ref: 10-025-2

Date Additional Pumping (hrs:min) Turbidity (NTU) Total Chlorine (mg/L) Total Chlorine (mg/L) Photes 9-Jun-10 24:07 2.76 0.0 - - 24:16 2.19 0.0 Collected Supplemental Sample TW1 - B3 24:22 1.95 0.0 Collected Supplemental Sample TW1 - B4						
24:00 2.00 0.0 24:07 2.19 0.0 0.0 24:22 1.95 0.0	Date	Approximate Time Since Start of	Trickidite, Astron			
24:00 24:07 24:16 24:16 24:22 24:22 1.95 0.0		Additional Pumping (hrs.:min)		lotal Chlorine (mg/L)	Notes	
24:07 2.76 0.0 24:16 2.19 0.0 24:22 1.95 0.0		24:00	2.00	0.0		
2.19 0.0 1.95 0.0	9-Jun-10	24:07	2.76	0.0		
0.0		24:22	2.70	0.0	Collected Supplemental Samnia TW1 - p	6
			GS.1	0.0	Collected Supplemental Sample TW1 - B) et

SITE LOCATION MAP

FIGURE 1

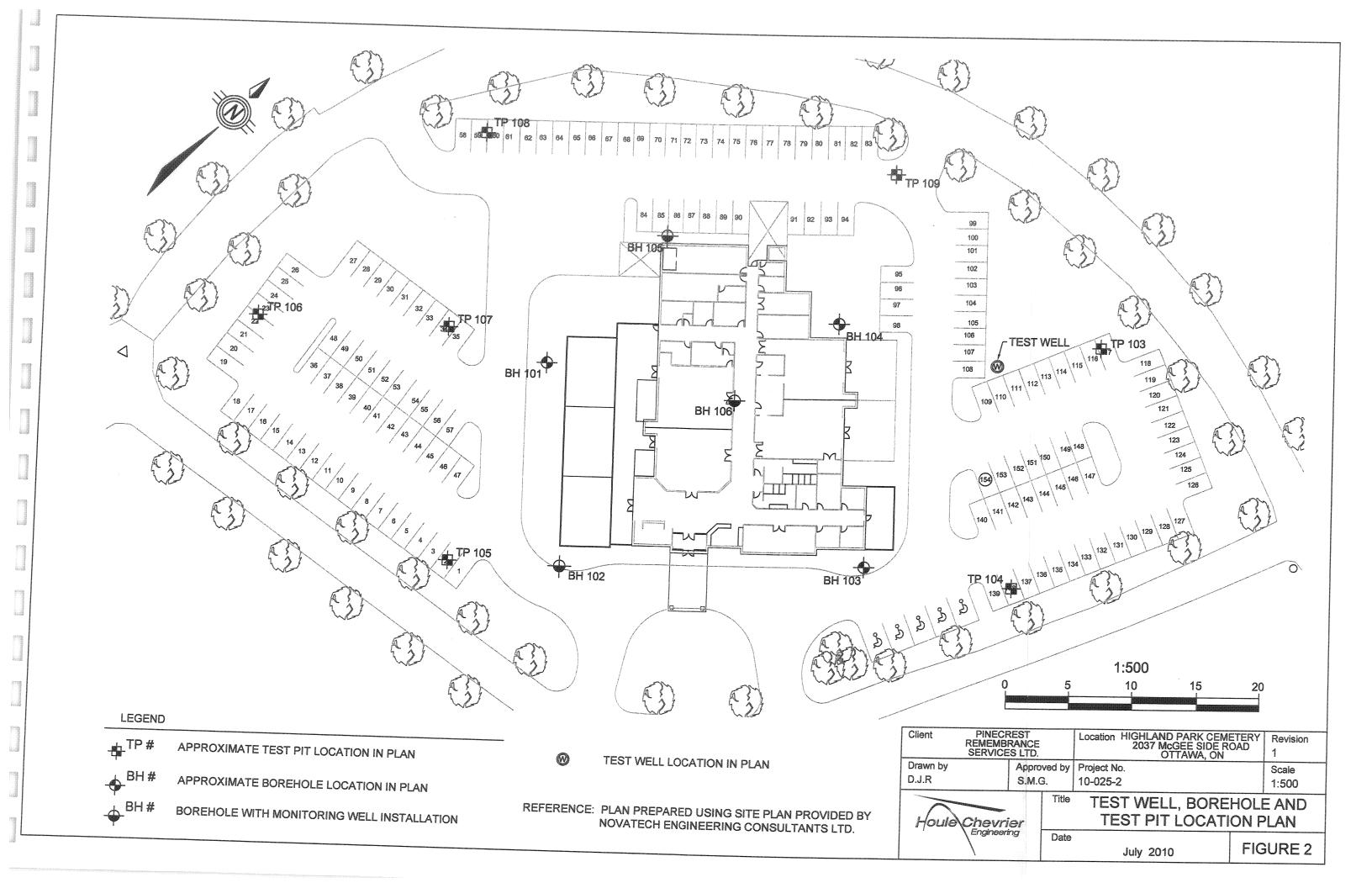


N.T.S



Date: July 2010

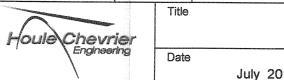
Project: 10-025





REFERENCE: PLAN PREPARED USING OTTAWA E-MAPS.

Client PINECF REMEMB SERVICE	RANCE	Location	HIGHLAND PARK CEMETARY 2037 McGEE SIDE ROAD OTTAWA, ON	Revision 0
Drawn by	Approved by	Project N	O.	Scale
D.J.R	\$.M.G.	10-025-2	2	1:1000



SITE	PLAN
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July 2010

FIGURE 3

APPENDIX A URBAN GEOLOGY OF THE NATIONAL CAPITAL REGION BIBLIOGRAPHY REFERENCES

Urban Geology of the National Capital Area Bibliography

Aylsworth, J.M., Lawrence D.E., and Evans, S.G.

1997: Landslide and settlement problems in sensitive marine clay, Ottawa Valley; Geological Association of Canada, Mineralogical Association of Canada, Joint Annual Meeting, 1997, Ottawa, Field Trip B1, 63 p.

Baer, A.J., Poole, W.H., Sanford, B.V.

1971: Rivière Gatineau, Québec-Ontario; Geological Survey of Canada, Map 1334A, scale 1: 1 000 000.

Bally, A.W.

1989: Phanerozoic basins of North America, in The geology of North America- An overview, Bally, A.W. and Palmer, A.R. eds., The Geology of North America, v. A, GSA, Boulder, Colorado, Chapt. 15.

Bally, A.W., Scotese, C.R., Ross, M.I.

1989: North America; Plate-tectonic setting and tectonic elements, in The geology of North America- An overview, Bally,A.W. and Palmer, A.R. eds., The Geology of North America, v. A, GSA, Boulder, Colorado, Chapt. 1.

Bélanger, J.R.

1998 Urban Geology of Canada's National Capital Area, in Karrow, P.F. and White O.L., Urban Geology of Canadian Cities; Geological Association of Canada, Special Paper 42, p365-384.

Bélanger, J. R. and Harrison, J.E.

1980 Regional Geoscience Information: Ottawa-Hull; Geological Survey of Canada, paper 77-11, 18p.

Fulton, R.J.

1989: Foreword to the Quaternary Geology of Canada and Greenland; in Geology of Canada and Greenland, R.J. Fulton, (ed.); Geological Survey of Canada, Geology of Canada no. 1.

Fulton, R.J. and Richard S.H.

1987: Chronology of late Quaternary events in the Ottawa region; in Quaternary Geology of the Ottawa Region, Ontario and Québec, Fulton, R.J., (ed.), Geological Survey of Canada, paper 86-23.

Gadd, N.R.

1987: Geological setting and Quaternary deposits of the Ottawa region, in Quaternary Geology of the Ottawa Region, Ontario and Québec, Fulton, R.J., (ed.), Geological Survey of Canada, paper 86-23.

Hoffman, P.F.

1989: Precambrian geology and tectonic history of North America, in The geology of North America- An overview, Bally,A.W. and Palmer, A.R. eds., The Geology of North America, v. A, GSA, Boulder, Colorado, Chapt. 16.

Hogarth, D.,D.

1962: A guide to the geology of the Gatineau-Lièvre district, Can. Field-Naturalist, Vol. 76, pp. 1-55

Johnson, D.K., Armstrong, D.K., Sanford, B.V., Telford, P.G., and Rutka, M.A. 1992: Paleozoic and Mesozoic Geology of Ontario, in Geology of Ontario, OGS Special Vol. 4, Part 2, Chapt. 20.

Livingstone, K.W.

1974: Geology, Arnprior, Ontario; Geological Survey of Canada, Map 1363A, scale 1:50 000.

MacDonald, G.

1967: Geology of the Ottawa Region: a Compilation, Department of geology, Carleton University, Ottawa, Geological Series 67-1, scale 1:250 000.

McLennan, S.M.

1992: Continental Crust, in Encyclopedia of Earth System Science, V.1, Academic Press, Orlando.

Rast, N.

1989: The evolution of the Appalachian chain, in The geology of North America- An overview, Bally, A.W. and Palmer, A.R. eds., The Geology of North America, v. A, GSA, Boulder, Colorado, Chapt. 12.

Reinhardt, E.W.

1973: Geology, Carleton Place, Ontario; Geological Survey of Canada, Map 1362A, scale 1:50 000.

Richard, S.H.

1990: Surficial Geology - Géologie de surface, Carleton Place, Ontario, Geological Survey of Canada, Map 1681A, scale 1:50 000.

1984: Surficial Geology - Géologie de surface, Arnprior, Ontario-Québec, Geological Survey of Canada, Map 1599A, scale 1:50 000.

1984: Surficial Geology - Géologie de surface, Lachute-Arundel, Québec-Ontario, Geological Survey of Canada Map 1577A, scale 1:100 000

1984: Géologie de surface, Buckingham, Québec-Ontario, Geological Survey of Canada Map 1670A, scale 1:50 000.

1982: Surficial Geology, Kemptville, Ontario, Geological Survey of Canada Map, 1492A, scale 1:50 000.

1982: Surficial Geology, Ottawa, Ontario-Québec / Géologie de Surface, Ottawa, Ontario-Québec, Geological Survey of Canada, map, 1506A, scale 1:50 000.

1982: Surficial Geology, Winchester, Ontario / Géologie De Surface, Winchester, Ontario, Geological Survey of Canada, "A" Series Map , 1491A, scale 1:50 000.

1982: Surficial Geology, Russell, Ontario / Géologie De Surface, Russell, Ontario, Geological Survey of Canada, "A" Series Map , 1507A, scale 1:50 000.

St-Onge, DA.

1997: Surficial geology, Quyon, Quebec-Ontario (31F/09) / Géologie de surface, Quyon, Québec-Ontario (31F/09); Geological Survey of Canada, Open File D3500, scale 1:50 000.

Williams, D.A.

1991: Paleozoic Geology of the Ottawa-St. Lawrence Lowland, Southern Ontario; Ont. Geol. Surv., O.F. Report 5770.

Williams, D.A., Rae, A.M., and Wolf, R.R.

1984: Paleozoic Geology of the Ottawa Area, Southern Ontario; Ont, Geol. Surv., Map P.2716, scale 1:50 000.

1985: Paleozoic Geology of the Russell-Thurso Area, Southern Ontario; Ont, Geol. Surv., Map P.2717, scale 1:50 000.

Williams, D.A., and Wolf, R.R.

1984: Paleozoic Geology of the Carleton Place Area, Southern Ontario; Ont, Geol. Surv., Map P.2725, scale 1:50 000.

1985: Paleozoic Geology of the Winchester Area, Southern Ontario; Ont, Geol. Surv., Map P.2722, scale 1:50 000.

Williams, D.A., Wolf, R.R., and Rae, A.M.

1984: Paleozoic Geology of the Arnprior-Quyon Area, Southern Ontario; Ont, Geol. Surv., Map P.2726, scale 1:50 000.

APPENDIX B

NITRATE CONCENTRATIONS EXOVA ACCUTEST REPORT OF ANALYSIS

EXUVA ACCUTEST

REPORT OF ANALYSIS



Report Number: Date: Date Submitted: Client: Houle Chevrier Engineering 180 Wescar Lane, R.R. #2 Carp, ON K0A 1L0 Attention: Mr. James McEwen

Project:

1012419 2010-06-07 2010-06-03

10-025-2

P.O. Number:

Chain of Custody Number: 122500

	_	_				_,	
						UNITS	mg/L
Water	GUIDELINE	COURTINE	ODWSOG			LIMII	10.0
					14,61	TPE	MAC
Matrix:							
. ≥							
	802539	2010-06-03	BH105			0 4 0 7	
	\vdash	2010-06-03	_			<0.10	
					MRL	0	<u>;</u>
		Sam	Š		UNITS	ma/L	i ħ :
000271					PARAMETER		
dy Nulliber.							
Circuit of Custody Nulliber: 122500						N-NO3 (Nitrate)	
įĹ					:	ż	

MRL = Method Reporting Limit INC = Incomplete AO = Aesthetic Objective OG = Operational Guideline MAC = Maximum Allowable Concentration IMAC = Interim Maximum Allowable Concentration Comment:

Ewart McRobbie Inorganic Lab Supervisor APPROVAL;

APPENDIX C

OTTAWA INTERNATIONAL AIRPORT WATER SURPLUS DATA ENVIRONMENT CANADA

	ment Canada	a
Water S	urplus Data	
(1983-20	02)	
		·
Soil Type:		Silty Clay
		280 millimetres
	THE PERSON AND THE PE	
Year	Surplus (mm)	
1983	337.1	
1984	386.7	
1985	258.8	
1986	460.4	
1987	240.6	
1988	287.3	
1989	203.9	
1990	353.9	
1991	335.8	
1992	308.7	And the second of the second o
1993	467.7	
1994	335.6	
1995	298.6	
1996	374.3	
1997	341.4	
1998	223.8	
1999	150.9	
2000	329.3	
2001	215.5	
2002	338.6	
vg. Surplu	ıs (mm) (1983-2	2003) 312.

APPENDIX D NITRATE DILUTION CALCULATION

APPENDIX D

NITRATE DILUTION CALCULATION

Average Water Surplus for 1983-2002 (Ottawa International Airport) = 312.4 millimetres

Potential Area for Infiltration = Site Area - Hard Surface Areas

=
$$485,619 \text{ m}^2 - 36,500 \text{ m}^2$$
 (Estimated Hard Surface Areas) = $449,119 \text{ m}^2$

Volume of Available Annual Infiltration

Annual expected volume of effluent based on 6,900 litres of effluent per day

= 1 x 6,900 litres/day x
$$\frac{1}{1000 \text{ litres/m}^3}$$
 x 365 days/year = 2,518.5 m³

Concentration of Nitrate at Site Boundaries

=
$$\frac{2,518.5 \text{ m}^3 \times 40 \text{ mg/litre}}{63,137 \text{ m}^3 + 2,518.5 \text{ m}^3}$$
 = 1.53 mg/litre

APPENDIX E ONSITE TEST WELL WATER WELL RECORD

3 1000	s (Street Number) ar: Litine n I Location (Street	Name)		Municipality Carep Tolenship	Province Ontario	Postal Code	Telephone No. (Well Owner Inc. area code)
nty/Olstrict/	Municipality Leading Zorie Easting	North		ile at Carleton- City/Town/Village Carro Municipal Plan and Sub		Prov On One	tario	stal Code
neral Colour	***************************************	immon Material	O.	ert Materials ner Materials nerticusour congresses Materials of the congress		rai Description	3* Fiv	Oapen (m/n) n To
**************************************	Lines			Clayera			3.3	
					21 8 2 5 7 5 4 JF 2 5 3	Haranga Proces		
upth Set at (i tour	To	Amular Sp. Type of Sealant (Material and T) ad Coment &	Used (pe)	Volume Placed (m/h²)	After test of well yield, a Clear and sand fo Other, specify If pumping discontinues	oe Tene (min	Water Level Tim (m/ll) (mi	
					Pump intake set at (m	Leve	8.46 8.58 4 9.27 2	30. 300
ible Tool sary (Conve sary (Revers	se) _{/ [C} Driving	ond Public Damest	dk 🔲 Test Ho	rcial Not used al Dewatering le Monitoring	Pumping rate (Vmin / 6 18 , 20 Duration of pumping 2 hrs+ m	4 in 5	3 10,87 4 11,57 5	25.68 24.89
ning r percussion har, specify	☐ Diggin	g Imgation Industrie Cither, s	al Control	& Air Conditioning	Final water level end of 2.7 , 8.4 If flowing give rate (l/m	in/GPM) 15	16.89 15	18.12
toe Operation (Garania) Con	en Hole OR Minterel Iventized, Floregless, nords, Plestia, Steel)	Thickness (anvin) F	Depth (m/fl) from To .45 5.40	Water Supply Replacement Well Test Hole Recharge Well	Recommended pump 50, 95 Recommended pump (Imin / GPM)	25	18,92 20 20,35 26 22,15 30	14.46
				Dewstering Well Deservation and/or Monitoring Hole Alteration (Construction)	18,20 Well production (Vinin) Disinfected?	50	24,13 40 25,10 50	10.43
scio	Metadal	Record - Screen	Depth (m/ft)	Abandoned, insufficient Supply Abandoned, Poor Water Quality Abandoned, other,	Yes No	Map of Well Loc elow following instruct		
vin) (**ass.	ic, Galvenized, Slee			specify Other, specify	Lagran Santonia	Alon a chiais Vian aca ing bi		n b
found at D		er]FreshJUn		ole Diameter (m/li) Diameter To (cmin))	ge det :
(m/ff) [] found at D	Ges ⊡Other, spepth Kind of Wat	er: ☐Fresh ☐Un		6,40 15,86 136,54 15,23	Language de la companya de la compa	timm, sittellederte viindelist.		
	Gas Other, sp Well Contract Well Contractor		nnician Informati Wei	Gra Contractor's Licence No.				

APPENDIX F

PRELIMINARY WATER TEST RESULTS EXOVA ACCUTEST REPORTS OF ANALYSES

i

EXOVO I

1003373 2010-02-22 2010-02-19

Report Number: Date: Date Submitted:

Client: Houle Chevrier Engineering 180 Wescar Lane, R.R. #2 Carp, ON KOA 1L0 Attention: Mr. James McEwen

Project:

10-025

P.O. Number: Matrix:

Water Chain of Custody Number: 105725

			-		STINI	CFU/100mL	
Water	GUIDELINE		ODWSOG		LIMIT	0 0	
					TYPE	MAC MAC	
Matrix:							
2005	7.17902	2010-02-19 TW/1 SA1				0 10 410 410 410 410 410 410 410 410 410	
H		Sample Date:		-	MR		
	ć	Samp	5		UNITS	CFU/100mL CFU/100mL CFU/100mL CFU/100mL	
				DADAMETED	ns - Alchiel ER	Faecal Streptococcus	
					Total Colifor	Faecal Streg	

MRL = Method Reporting Limit INC = Incomplete AO = Aesthetic Objective OG = Operational Guideline MAC = Maximum Allowable Concentration IMAC = Interim Maximum Allowable Concentration Comment: APPROVAL:

Dragana Dzeletovic

Microbiology Analyst



Client: Houle Chevrier Engineering

1

180 Wescar Lane, R.R. #2

Carp, ON K0A 1L0

Attention: Mr. James McEwen

Report Number: Date: Date Submitted:

1003389 2010-03-01 2010-02-19

10-025

Project:

P.O. Number: Matrix:

UNITS mg/L mg/L TCU mg/L mg/L mg/L mg/L mg/L mg/L NTU mg/L mg/L mg/L mg/L GUIDELINE ODWSOG 1.0 10.0 6.5-8.5 500 250 5 5 1.5 0.05 200 0.3 0.05 500 200 0.0 Water TYPE AO AO MAC MAC OG 8 8 8 8 9 90 999 9 2010-02-19 TW1 SA1 777948 269 56 17 747 1.4 3.17 Sample Date: Sample ID: LAB ID: 1 2 5 0.5 0.1 1 0.02 0.1 0.001 0.5 5 0.1 1 0.01 1 1 1 1 0.03 0.03 MR mg/L mg/L TCU uS/cm mg/L mg/L mg/L mg/L mg/L mg/L mg/L ng/L ng/L mg/L mg/L mg/L mg/L PARAMETER Total Dissolved Solids (COND - CALC) Chain of Custody Number: 105725 Dissolved Organic Carbon Total Kjeldahl Nitrogen Hardness as CaCO3 N-NH3 (Ammonia) N-NO2 (Nitrite) Alkalinity as CaCO3 Hydrogen Sulphide Tannin & Lignin N-NO3 (Nitrate) lon Balance Conductivity Magnesium Manganese Potassium Sulphate Turbidity Sodium Chloride Fluoride Calcium **Phenols** Colour <u>r</u>on

MRL = Method Reporting Limit INC = Incomplete AO = Aesthetic Objective OG = Operational Guideline MAC = Maximum Allowable Concentration IMAC = Interim Maximum Allowable Concentration Comment

777948: Sediment was not included in Metals analysis. H2S MRL elevated due to sample turbidity. Tannin/Lignin MRL elevated due to sample turbidity.

APPROVAL:

Inorganic Lab Supervisor Ewan McRobbie

APPENDIX G PRE-HYDRO FRACTURING SUPPLEMENTAL WATER SAMPLING EXOVA ACCUTEST REPORTS OF ANALYSIS



Client: Houle Chevrier Engineering 180 Wescar Lane, R.R. #2

Carp, ON K0A 1L0

Attention: Mr. James McEwen

Report Number: Date: Date Submitted:

1004426 2010-03-08 2010-03-05

10-025 P.O. Number: Matrix: Project: Chain of Custody Number: 109910

					UNITS	CFU/100mL	CFU/100mL															
Water	GUIDELINE		908MG0		LIMIT																	
					TYPE	MAC	MAC															
Matrix:																						
	780975	2010-03-05 TW1			ľ	0 0	<u> </u>	n c	- c	-79.	 			*******								
H		Sample Date: Sample ID:			MAL																	
	(Samp		TIMIT	1400	CFU/100mL	CFU/100mL	CF11/100ml	CFU/100mL													
				_																		
				PARAMETER																		
					ns	Soli	Plate Count	ıms	Faecal Streptococcus													
					Total Coliforms	Escherichia (Heterotrophic	Faecal Colifc	Faecal Strep													

MRL = Method Reporting Limit INC = Incomplete AO = Aesthetic Objective OG = Operational Guideline MAC = Maximum Allowable Concentration IMAC = Interim Maximum Allowable Concentration Comment:

APPROVAL:

Dragana Dzeletovic

Microbiology Analyst



Client: Houle Chevrier Engineering 180 Wescar Lane, R.R. #2 Carp, ON K0A 1L0

Attention: Mr. James McEwen

1004438 2010-03-08 2010-03-05 Report Number: Date: Date Submitted:

Project:

10-025

UNITS MRL CODWSOG	MRL 7010-03-05 Converged	MRI
MRL TW1 DDWSOG	MRI	MRL TW1 DDWSOG
MRL MRL MRL MRL MRL MRL MRC 15 MRC 15 MRC 10 0.05 MRC 1.0 0.05 MRC 1.0 MRC	MRL	MRL
MRL	MRL	MRL
MRL 2 <2 AO 5 0.1 2.71 AO 5 0.01 3.80 0.01 3.6.7 AO 0.05 0.03 <0.03 0.001 <0.01 0.01 <0.01 0.01 <0.001 0.01 <0.001 0.01 <0.001 0.01 <0.001 0.01 <0.001 0.002	MRL	MRL
2	2 <2 0.1 2.71 MAC 1.5 0.01 3.80 0.01 3.80 0.03 <0.03 <0.03 <0.003 <0.003 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001	2
0.01 3.67 0.03 4.03 0.01 36.7 MAC 1.0 0.03 <0.03 0.01 <0.01 <0.05 0.01 <0.05	0.01 3.87 AO 0.05 0.05 0.01 36.7 AO 0.05 0.01 0.01 0.01 0.01 0.01 0.01 0.01	0.01 3.87 0.03 4.003 0.03 <0.03 <0.05 0.01 <0.01 <0.01 <0.05 0.01 <0.01 <0.05 0.01 <0.05
0.01 3.80 AO 0.05 0.03 co.03 c	0.01 3.80 MAC 0.05 0.03 0.003 0.01 0.01 0.005 0.005 0.00	0.01 3.80 0.03 <0.03
0.01 36.7 MAC 1.0 0.03 <0.03 AO 0.3 0.01 <0.01 <0.05 AO 0.05	0.01 36.7 MAC 1.0 0.03 <0.03 AO 0.3 0.01 <0.01 <0.05 AO 0.05 AO 0.05	0.01 36.7 MAC 1.0 0.03 <0.03 0.01 <0.01 0.01 <0.05 AO 0.05 AO 0.05
0.03 < <0.03	0.03 < <0.03 0.01 < <0.01 < <0.05 0.05	0.03 < <0.03 0.01 < <0.01 0.01 < <0.04 AO
0.00 AO AO O O O O O O O O O O O O O O O O	0.00 AOO 0.05	0.00 AOO 0.005

MRL = Method Reporting Limit INC = Incomplete AO = Aesthetic Objective OG = Operational Guideline MAC = Maximum Allowable Concentration IMAC = Interim Maximum Allowable Concentration Comment:

APPROVAL:

Ewan McRobbie

Inorganic Lab Supervisor

EXCVQ |

Client: Houle Chevrier Engineering 180 Wescar Lane, R.R. #2

Carp, ON K0A 1L0

Attention: Mr. James McEwen

1005237 2010-03-17 2010-03-16 Report Number: Date: Date Submitted:

Project:

10-025

P.O. Number:

Г	Т				
				UNITS	J/Gm
SHIDE INF		ODWSOG		LIMIT	رن ت
				TYPE	MAC
L	-			\downarrow	
-	16	E)	+	+	
783200	2010-03-	TW1-SA			2.94
LAB ID:	ple Date:	ımple ID:	MD	MINI.	.
	Sam	S _S	OTINIT	2 3	J.Biu
			AETER		
			PARA		
				Flioride	
	783200	783200 2010-03-16	783200 2010-03-16 TW1-SA3	LAB ID: 783200 CulpELINE Sample Date: 2010-03-16 CulpELINE CulpELINE	LAB ID: 783200 TR3200 TR3200 TR3200 GUIDELINE Sample ID: Sample ID: TW1-SA3 TW1-SA3 ODWSOG PARAMETER UNITS MRL TYPE LIMIT

MRL = Method Reporting Limit INC = Incomplete AO = Aesthetic Objective OG = Operational Guideline MAC = Maximum Allowable Concentration IMAC = Interim Maximum Allowable Concentration Comment:

Inorganic Lab Supervisor APPROVAL:

Ewan McRobbie

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1005393 2010-03-19 2010-03-18

Report Number: Date: Date Submitted: Project: Client: Houle Chevrier Engineering 180 Wescar Lane, R.R. #2 Attention: Mr. James McEwen Carp, ON K0A 1L0

Chain of Custody Number: 109912

10-025

P.O. Number: Matrix:

UNITS mg/L Water GUIDELINE ODWSOG 1.5 TYPE 2010-03-18 TW1-SA4 3.32 LAB ID: Sample Date: Sample ID: MRL 0.1 UNITS mg/L PARAMETER Fluoride

MRL = Method Reporting Limit INC = Incomplete AO = Aesthetic Objective OG = Operational Guideline MAC = Maximum Allowable Concentration IMAC = Interim Maximum Allowable Concentration Comment:

APPENDIX H POST-HYDRO FRACTURING WATER TEST RESULTS EXOVA ACCUTEST REPORT OF ANALYSIS

REPORT OF ANY VSIS

EXOVO IIII

Report Number: Date: Date Submitted: Client: Houle Chevrier Engineering 180 Wescar Lane, R.R. #2 Carp, ON K0A 1L0

Attention: Mr. James McEwen

Project:

1009701 2010-05-06 2010-05-05

10-029

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						ONITS	
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	Water	DELLIN				<u> </u>	
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P.O. Number:	<u>.</u>						
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	794479	2010-0	TW1-S			1.93	
	-				_		
	LAB ID:	nple Da	Sample ID:		MR	0.1	
		San	Ο̈́		UNITS	mg/L	
					5	ı.	
					3		
20925					PARAMETER		
er: 1					PAR		
Numk							
ustody							
Chain of Custody Number: 120925						Fluoride	
Cha					į	Ī Ĭ	

MRL = Method Reporting Limit INC = Incomplete AO = Aesthetic Objective OG = Operational Guideline MAC = Maximum Allowable Concentration IMAC = Interim Maximum Allowable Concentration Comment:

Inorganic Lab Supervisor APPROVAL:

Ewan McRobbie

APPENDIX I WATER LEVEL DRAWDOWN AND RECOVERY DATA



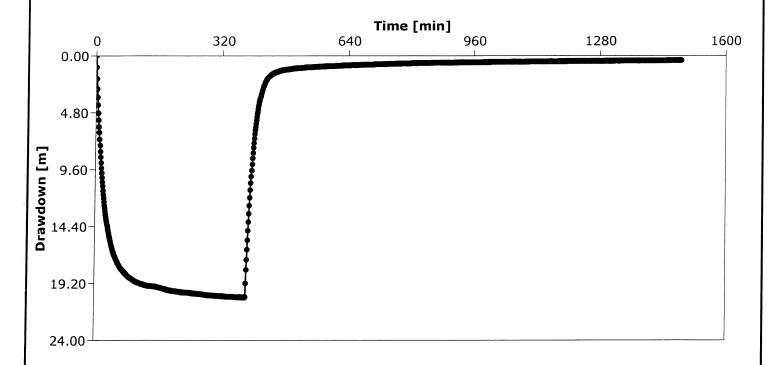
ruiii	unu	I CSL	milai	V3I3	Report

Project: Highland Park Hydrogeological Assessment

Number: 10-025-2

Client: Pinecrest Remembrance Services Ltd.

Location: 2037 McGee Side Road, Ottawa, Ontario	Pumping Test: Pumping Test 1	Pumping Well: TW1
Test Conducted by:		Test Date: 5/27/2010
Analysis Performed by: JM	Drawdown vs. Time	Analysis Date: 5/27/2010
Aquifer Thickness:	Discharge: variable, average rate 0.0043434 [m³/mir	3]





				_
Pumping	Toet -	Water	امدم ا	Data

Page 1 of 27

Project: Highland Park Hydrogeological Assessment

Number: 10-025-2

Client: Pinecrest Remembrance Services Ltd.

Location: 2037 McGee Side Road, Ottawa, Ontario

Pumping Test: Pumping Test 1

Pumping Well: TW1

Test Conducted by:

Test Date: 5/27/2010

Discharge: variable, average rate 0.0043434 [m³/min]

Radial Distance to PW [m]: 0.15

Time (min) Water Level (m) Drawdown (m) 1 0 8.58 0.00 2 1 9.53 0.95 3 2 10.50 1.92 4 3 11.35 2.77 5 4 12.07 3.49 6 5 12.75 4.17 7 6 13.40 4.82 8 7 14.00 5.42 9 8 14.56 5.98 10 9 15.06 6.48 11 10 15.61 7.03 12 11 16.14 7.56 13 12 16.65 8.07 14 13 17.13 8.55 15 14 17.60 9.02 16 15 18.04 9.46 17 16 18.46 9.88 18 17 18.86 10.28 19 18 19.24 <t< th=""><th colspan="3">Observation Well: TW1a</th><th>Static Water Level [m]: 8.58</th></t<>	Observation Well: TW1a			Static Water Level [m]: 8.58
1 0 8.58 0.00 2 1 9.53 0.95 3 2 10.50 1.92 4 3 11.35 2.77 5 4 12.07 3.49 6 5 12.75 4.17 7 6 13.40 4.82 8 7 14.00 5.42 9 8 14.56 5.98 10 9 15.06 6.48 11 10 15.61 7.03 12 11 16.65 8.07 13 12 16.65 8.07 14 13 17.13 8.55 15 14 17.60 9.02 16 15 18.04 9.46 17 16 18.46 9.88 18 17 18.86 10.28 19 18 19.24 10.66 20 19 19.60 11.			l l	
3 2 10.50 1.92 4 3 11.35 2.77 5 4 12.07 3.49 6 5 12.75 4.17 7 6 13.40 4.82 8 7 14.00 5.42 9 8 14.56 5.98 10 9 15.06 6.48 11 10 15.61 7.03 12 11 16.14 7.56 13 12 16.65 8.07 14 13 17.13 8.55 15 14 17.60 9.02 16 15 18.04 9.46 17 16 18.46 9.88 18 17 18.86 10.28 19 18 19.24 10.66 20 19 19.60 11.02 21 20 19.96 11.38 22 21 20.28	1			
4 3 11.35 2.77 5 4 12.07 3.49 6 5 12.75 4.17 7 6 13.40 4.82 8 7 14.00 5.42 9 8 14.56 5.98 10 9 15.06 6.48 11 10 15.61 7.03 12 11 16.14 7.56 13 12 16.65 8.07 14 13 17.13 8.55 15 14 17.60 9.02 16 15 18.04 9.46 17 16 18.46 9.88 18 17 18.86 10.28 19 18 19.24 10.66 20 19 19.60 11.02 21 20 19.96 11.38 22 21 20.28 11.70 23 22 20.60	2	1	9.53	0.95
5 4 12.07 3.49 6 5 12.75 4.17 7 6 13.40 4.82 8 7 14.00 5.42 9 8 14.56 5.98 10 9 15.06 6.48 11 10 15.61 7.03 12 11 16.14 7.56 13 12 16.65 8.07 14 13 17.13 8.55 15 14 17.60 9.02 16 15 18.04 9.46 17 16 18.46 9.88 18 17 18.86 10.28 19 18 19.24 10.66 20 19 19.60 11.02 21 20 19.96 11.38 22 21 20.28 11.70 23 22 26.60 12.02 24 23 20.90	3	2	10.50	1.92
6 5 12.75 4.17 7 6 13.40 4.82 8 7 14.00 5.42 9 8 14.56 5.98 10 9 15.06 6.48 11 10 15.61 7.03 12 11 16.14 7.56 13 12 16.65 8.07 14 13 17.13 8.55 15 14 17.60 9.02 16 15 18.04 9.46 17 16 18.46 9.88 18 17 18.86 10.28 19 18 19.24 10.66 20 19 19.60 11.02 21 20 19.96 11.38 22 21 20.28 11.70 23 22 20.60 12.02 24 23 20.90 12.32 25 24 21.18 <td></td> <td></td> <td>11.35</td> <td></td>			11.35	
6 5 12.75 4.17 7 6 13.40 4.82 8 7 14.00 5.42 9 8 14.56 5.98 10 9 15.06 6.48 11 10 15.61 7.03 12 11 16.14 7.56 13 12 16.65 8.07 14 13 17.13 8.55 15 14 17.60 9.02 16 15 18.04 9.46 17 16 18.46 9.88 18 17 18.86 10.28 19 18 19.24 10.66 20 19 19.60 11.02 21 20 19.96 11.38 22 21 20.28 11.70 23 22 20.60 12.02 24 23 20.90 12.32 25 24 21.18 <td>5</td> <td>4</td> <td>12.07</td> <td>3.49</td>	5	4	12.07	3.49
7 6 13.40 4.82 8 7 14.00 5.42 9 8 14.56 5.98 10 9 15.06 6.48 11 10 15.61 7.03 12 11 16.14 7.56 13 12 16.65 8.07 14 13 17.13 8.55 15 14 17.60 9.02 16 15 18.04 9.46 17 16 18.46 9.88 18 17 18.86 10.28 19 18 19.24 10.66 20 19 19.60 11.02 21 20 19.96 11.38 22 21 20.28 11.70 23 22 20.60 12.02 24 23 20.90 12.32 25 24 21.18 12.60 26 25 21.45<	6	5	12.75	4.17
9 8 14.56 5.98 10 9 15.06 6.48 11 10 15.61 7.03 12 11 16.14 7.56 13 12 16.65 8.07 14 13 17.13 8.55 15 14 17.60 9.02 16 15 18.04 9.46 17 16 18.46 9.88 18 17 18.86 10.28 19 18 19.24 10.66 20 19 19.60 11.02 21 20 19.96 11.38 22 21 20.28 11.70 23 22 20.60 12.02 24 23 20.90 12.32 25 24 21.18 12.60 26 25 21.45 12.87 27 26 21.70 13.12 28 27 21.95 13.37 29 28 22.18 13.60 30 29 22.40 13.82 31 30 22.61 14.03 32 31 22.81 14.23 33 32 23.01 14.43 34 33 23.20 14.62 35 34 23.98 15.40 39 38 15.40 40 39 24.13 15.55 41 40 24.27 15.69 42 41 15.83 43 42 24.53 15.95 44 43 24.64 16.06 45 24.88 16.30 47 46 24.99 16.41	7	6	13.40	4.82
10 9 15.06 6.48 11 10 15.61 7.03 12 11 16.14 7.56 13 12 16.65 8.07 14 13 17.13 8.55 15 14 17.60 9.02 16 15 18.04 9.46 17 16 18.46 9.88 18 17 18.86 10.28 19 18 19.24 10.66 20 19 19.60 11.02 21 20 19.96 11.38 22 21 20.28 11.70 23 22 20.60 12.02 24 23 20.90 12.32 25 24 21.18 12.60 26 25 21.45 12.87 27 26 21.70 13.12 28 27 21.95 13.37 29 28 <	8	7	14.00	5.42
11 10 15.61 7.03 12 11 16.14 7.56 13 12 16.65 8.07 14 13 17.13 8.55 15 14 17.60 9.02 16 15 18.04 9.46 17 16 18.46 9.88 18 17 18.86 10.28 19 18 19.24 10.66 20 19 19.60 11.02 21 20 19.96 11.38 22 21 20.28 11.70 23 22 20.60 12.02 24 23 20.90 12.32 25 24 21.18 12.60 26 25 21.45 12.87 27 26 21.70 13.12 28 27 21.95 13.37 29 28 22.18 13.60 30 29	9	8	14.56	5.98
12 11 16.14 7.56 13 12 16.65 8.07 14 13 17.13 8.55 15 14 17.60 9.02 16 15 18.04 9.46 17 16 18.46 9.88 18 17 18.86 10.28 19 18 19.24 10.66 20 19 19.60 11.02 21 20 19.96 11.38 22 21 20.28 11.70 23 22 20.60 12.02 24 23 20.90 12.32 25 24 21.18 12.60 26 25 21.45 12.87 27 26 21.70 13.12 28 27 21.95 13.37 29 28 22.18 13.60 30 29 22.40 13.82 31 30	10	9	15.06	6.48
13 12 16.65 8.07 14 13 17.13 8.55 15 14 17.60 9.02 16 15 18.04 9.46 17 16 18.46 9.88 18 17 18.86 10.28 19 18 19.24 10.66 20 19 19.60 11.02 21 20 19.96 11.38 22 21 20.28 11.70 23 22 20.60 12.02 24 23 20.90 12.32 25 24 21.18 12.60 26 25 21.45 12.87 27 26 21.70 13.12 28 27 21.95 13.37 29 28 22.18 13.60 30 29 22.40 13.82 31 30 22.61 14.03 32 31	11	10	15.61	7.03
14 13 17.13 8.55 15 14 17.60 9.02 16 15 18.04 9.46 17 16 18.46 9.88 18 17 18.86 10.28 19 18 19.24 10.66 20 19 19.60 11.02 21 20 19.96 11.38 22 21 20.28 11.70 23 22 20.60 12.02 24 23 20.90 12.32 25 24 21.18 12.60 26 25 21.45 12.87 27 26 21.70 13.12 28 27 21.95 13.37 29 28 22.18 13.60 30 29 22.40 13.82 31 30 22.61 14.03 32 31 32.261 14.03 33 32	12	11	16.14	7.56
14 13 17.13 8.55 15 14 17.60 9.02 16 15 18.04 9.46 17 16 18.46 9.88 18 17 18.86 10.28 19 18 19.24 10.66 20 19 19.60 11.02 21 20 19.96 11.38 22 21 20.28 11.70 23 22 20.60 12.02 24 23 20.90 12.32 25 24 21.18 12.60 26 25 21.45 12.87 27 26 21.70 13.12 28 27 21.95 13.37 29 28 22.18 13.60 30 29 22.40 13.82 31 30 22.61 14.03 32 31 32.281 14.23 33 32	13	12	16.65	8.07
15 14 17.60 9.02 16 15 18.04 9.46 17 16 18.46 9.88 18 17 18.86 10.28 19 18 19.24 10.66 20 19 19.60 11.02 21 20 19.96 11.38 22 21 20.28 11.70 23 22 20.60 12.02 24 23 20.90 12.32 25 24 21.18 12.60 26 25 21.45 12.87 27 26 21.70 13.12 28 27 21.95 13.37 29 28 22.18 13.60 30 29 22.40 13.82 31 30 22.61 14.03 32 31 22.81 14.23 33 32 23.01 14.43 34 33		13	17.13	8.55
16 15 18.04 9.46 17 16 18.46 9.88 18 17 18.86 10.28 19 18 19.24 10.66 20 19 19.60 11.02 21 20 19.96 11.38 22 21 20.28 11.70 23 22 20.60 12.02 24 23 20.90 12.32 25 24 21.18 12.60 26 25 21.45 12.87 27 26 21.70 13.12 28 27 21.95 13.37 29 28 22.18 13.60 30 29 22.40 13.82 31 30 22.61 14.03 32 31 32 14.43 34 33 23.20 14.62 35 34 23.37 14.79 36 35				9.02
17 16 18.46 9.88 18 17 18.86 10.28 19 18 19.24 10.66 20 19 19.60 11.02 21 20 19.96 11.38 22 21 20.28 11.70 23 22 20.60 12.02 24 23 20.90 12.32 25 24 21.18 12.60 26 25 21.45 12.87 27 26 21.70 13.12 28 27 21.95 13.37 29 28 22.18 13.60 30 29 22.40 13.82 31 30 22.61 14.03 32 31 22.81 14.23 33 32 23.01 14.43 34 33 23.20 14.62 35 34 23.37 14.79 36 35				9.46
18 17 18.86 10.28 19 18 19.24 10.66 20 19 19.60 11.02 21 20 19.96 11.38 22 21 20.28 11.70 23 22 20.60 12.02 24 23 20.90 12.32 25 24 21.18 12.60 26 25 21.45 12.87 27 26 21.70 13.12 28 27 21.95 13.37 29 28 22.18 13.60 30 29 22.40 13.82 31 30 22.61 14.03 32 31 22.81 14.23 33 32 23.01 14.43 34 33 23.20 14.62 35 34 23.37 14.79 36 35 23.54 14.96 37 36			18.46	9.88
19 18 19.24 10.66 20 19 19.60 11.02 21 20 19.96 11.38 22 21 20.28 11.70 23 22 20.60 12.02 24 23 20.90 12.32 25 24 21.18 12.60 26 25 21.45 12.87 27 26 21.70 13.12 28 27 21.95 13.37 29 28 22.18 13.60 30 29 22.40 13.82 31 30 22.61 14.03 32 31 22.81 14.23 33 32 23.01 14.43 34 33 23.20 14.62 35 34 23.37 14.79 36 35 23.54 14.96 37 36 23.69 15.11 38 37			18.86	10.28
20 19 19.60 11.02 21 20 19.96 11.38 22 21 20.28 11.70 23 22 20.60 12.02 24 23 20.90 12.32 25 24 21.18 12.60 26 25 21.45 12.87 27 26 21.70 13.12 28 27 21.95 13.37 29 28 22.18 13.60 30 29 22.40 13.82 31 30 22.61 14.03 32 31 22.81 14.23 33 32 23.01 14.43 34 33 23.20 14.62 35 34 23.37 14.79 36 35 23.54 14.96 37 36 23.69 15.11 38 37 23.84 15.26 39 38			19.24	10.66
21 20 19.96 11.38 22 21 20.28 11.70 23 22 20.60 12.02 24 23 20.90 12.32 25 24 21.18 12.60 26 25 21.45 12.87 27 26 21.70 13.12 28 27 21.95 13.37 29 28 22.18 13.60 30 29 22.40 13.82 31 30 22.61 14.03 32 31 22.81 14.23 33 32 23.01 14.43 34 33 23.20 14.62 35 34 23.37 14.79 36 35 23.54 14.96 37 36 23.69 15.11 38 37 23.84 15.26 39 38 23.98 15.40 40 39			19.60	11.02
22 21 20.28 11.70 23 22 20.60 12.02 24 23 20.90 12.32 25 24 21.18 12.60 26 25 21.45 12.87 27 26 21.70 13.12 28 27 21.95 13.37 29 28 22.18 13.60 30 29 22.40 13.82 31 30 22.61 14.03 32 31 22.81 14.23 33 32 23.01 14.43 34 33 23.20 14.62 35 34 23.37 14.79 36 35 23.54 14.96 37 36 23.69 15.11 38 37 23.84 15.26 39 38 23.98 15.40 40 39 24.13 15.55 41 40			19.96	
23 22 20.60 12.02 24 23 20.90 12.32 25 24 21.18 12.60 26 25 21.45 12.87 27 26 21.70 13.12 28 27 21.95 13.37 29 28 22.18 13.60 30 29 22.40 13.82 31 30 22.61 14.03 32 31 22.81 14.23 33 32 23.01 14.43 34 33 23.20 14.62 35 34 23.37 14.79 36 35 23.54 14.96 37 36 23.69 15.11 38 37 23.84 15.26 39 38 23.98 15.40 40 39 24.13 15.55 41 40 24.27 15.69 42 41				
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25 24 21.18 12.60 26 25 21.45 12.87 27 26 21.70 13.12 28 27 21.95 13.37 29 28 22.18 13.60 30 29 22.40 13.82 31 30 22.61 14.03 32 31 22.81 14.23 33 32 23.01 14.43 34 33 23.20 14.62 35 34 23.37 14.79 36 35 23.54 14.96 37 36 23.69 15.11 38 37 23.84 15.26 39 38 23.98 15.40 40 39 24.13 15.55 41 40 24.27 15.69 42 41 24.41 15.83 43 42 24.53 15.95 44 43				
26 25 21.45 12.87 27 26 21.70 13.12 28 27 21.95 13.37 29 28 22.18 13.60 30 29 22.40 13.82 31 30 22.61 14.03 32 31 22.81 14.23 33 32 23.01 14.43 34 33 23.20 14.62 35 34 23.37 14.79 36 35 23.54 14.96 37 36 23.69 15.11 38 37 23.84 15.26 39 38 23.98 15.40 40 39 24.13 15.55 41 40 24.27 15.69 42 41 24.41 15.83 43 42 24.53 15.95 44 43 24.64 16.06 45 44				
27 26 21.70 13.12 28 27 21.95 13.37 29 28 22.18 13.60 30 29 22.40 13.82 31 30 22.61 14.03 32 31 22.81 14.23 33 32 23.01 14.43 34 33 23.20 14.62 35 34 23.37 14.79 36 35 23.54 14.96 37 36 23.69 15.11 38 37 23.84 15.26 39 38 23.98 15.40 40 39 24.13 15.55 41 40 24.27 15.69 42 41 24.41 15.83 43 42 24.53 15.95 44 43 24.64 16.06 45 44 24.77 16.19 46 45				
28 27 21.95 13.37 29 28 22.18 13.60 30 29 22.40 13.82 31 30 22.61 14.03 32 31 22.81 14.23 33 32 23.01 14.43 34 33 23.20 14.62 35 34 23.37 14.79 36 35 23.54 14.96 37 36 23.69 15.11 38 37 23.84 15.26 39 38 23.98 15.40 40 39 24.13 15.55 41 40 24.27 15.69 42 41 24.41 15.83 43 42 24.53 15.95 44 43 24.64 16.06 45 44 24.77 16.19 46 45 24.88 16.30 47 46 24.99 16.41 48 47 25.09 16.51 49 48 25.20 16.62				
29 28 22.18 13.60 30 29 22.40 13.82 31 30 22.61 14.03 32 31 22.81 14.23 33 32 23.01 14.43 34 33 23.20 14.62 35 34 23.37 14.79 36 35 23.54 14.96 37 36 23.69 15.11 38 37 23.84 15.26 39 38 23.98 15.40 40 39 24.13 15.55 41 40 24.27 15.69 42 41 24.41 15.83 43 42 24.53 15.95 44 43 24.64 16.06 45 44 24.77 16.19 46 45 24.88 16.30 47 46 24.99 16.41 48 47 25.09 16.51 49 48 25.20 16.62 <td></td> <td></td> <td></td> <td></td>				
30 29 22.40 13.82 31 30 22.61 14.03 32 31 22.81 14.23 33 32 23.01 14.43 34 33 23.20 14.62 35 34 23.37 14.79 36 35 23.54 14.96 37 36 23.69 15.11 38 37 23.84 15.26 39 38 23.98 15.40 40 39 24.13 15.55 41 40 24.27 15.69 42 41 24.41 15.83 43 42 24.53 15.95 44 43 24.64 16.06 45 44 24.77 16.19 46 45 24.88 16.30 47 46 24.99 16.41 48 47 25.09 16.51 49 48 25.20 16.62				
31 30 22.61 14.03 32 31 22.81 14.23 33 32 23.01 14.43 34 33 23.20 14.62 35 34 23.37 14.79 36 35 23.54 14.96 37 36 23.69 15.11 38 37 23.84 15.26 39 38 23.98 15.40 40 39 24.13 15.55 41 40 24.27 15.69 42 41 24.41 15.83 43 42 24.53 15.95 44 43 24.64 16.06 45 44 24.77 16.19 46 45 24.88 16.30 47 46 24.99 16.41 48 47 25.09 16.51 49 48 25.20 16.62				13.82
32 31 22.81 14.23 33 32 23.01 14.43 34 33 23.20 14.62 35 34 23.37 14.79 36 35 23.54 14.96 37 36 23.69 15.11 38 37 23.84 15.26 39 38 23.98 15.40 40 39 24.13 15.55 41 40 24.27 15.69 42 41 24.41 15.83 43 42 24.53 15.95 44 43 24.64 16.06 45 44 24.77 16.19 46 45 24.88 16.30 47 46 24.99 16.41 48 47 25.09 16.51 49 48 25.20 16.62		30	22.61	14.03
33 32 23.01 14.43 34 33 23.20 14.62 35 34 23.37 14.79 36 35 23.54 14.96 37 36 23.69 15.11 38 37 23.84 15.26 39 38 23.98 15.40 40 39 24.13 15.55 41 40 24.27 15.69 42 41 24.41 15.83 43 42 24.53 15.95 44 43 24.64 16.06 45 44 24.77 16.19 46 45 24.88 16.30 47 46 24.99 16.41 48 47 25.09 16.51 49 48 25.20 16.62			22.81	
34 33 23.20 14.62 35 34 23.37 14.79 36 35 23.54 14.96 37 36 23.69 15.11 38 37 23.84 15.26 39 38 23.98 15.40 40 39 24.13 15.55 41 40 24.27 15.69 42 41 24.41 15.83 43 42 24.53 15.95 44 43 24.64 16.06 45 44 24.77 16.19 46 45 24.88 16.30 47 46 24.99 16.41 48 47 25.09 16.51 49 48 25.20 16.62				
35 34 23.37 14.79 36 35 23.54 14.96 37 36 23.69 15.11 38 37 23.84 15.26 39 38 23.98 15.40 40 39 24.13 15.55 41 40 24.27 15.69 42 41 24.41 15.83 43 42 24.53 15.95 44 43 24.64 16.06 45 44 24.77 16.19 46 45 24.88 16.30 47 46 24.99 16.41 48 47 25.09 16.51 49 48 25.20 16.62			23.20	14.62
36 35 23.54 14.96 37 36 23.69 15.11 38 37 23.84 15.26 39 38 23.98 15.40 40 39 24.13 15.55 41 40 24.27 15.69 42 41 24.41 15.83 43 42 24.53 15.95 44 43 24.64 16.06 45 44 24.77 16.19 46 45 24.88 16.30 47 46 24.99 16.41 48 47 25.09 16.51 49 48 25.20 16.62			23.37	14.79
37 36 23.69 15.11 38 37 23.84 15.26 39 38 23.98 15.40 40 39 24.13 15.55 41 40 24.27 15.69 42 41 24.41 15.83 43 42 24.53 15.95 44 43 24.64 16.06 45 44 24.77 16.19 46 45 24.88 16.30 47 46 24.99 16.41 48 47 25.09 16.51 49 48 25.20 16.62			23.54	14.96
39 38 23.98 15.40 40 39 24.13 15.55 41 40 24.27 15.69 42 41 24.41 15.83 43 42 24.53 15.95 44 43 24.64 16.06 45 44 24.77 16.19 46 45 24.88 16.30 47 46 24.99 16.41 48 47 25.09 16.51 49 48 25.20 16.62		36	23.69	15.11
39 38 23.98 15.40 40 39 24.13 15.55 41 40 24.27 15.69 42 41 24.41 15.83 43 42 24.53 15.95 44 43 24.64 16.06 45 44 24.77 16.19 46 45 24.88 16.30 47 46 24.99 16.41 48 47 25.09 16.51 49 48 25.20 16.62	38	37	23.84	15.26
41 40 24.27 15.69 42 41 24.41 15.83 43 42 24.53 15.95 44 43 24.64 16.06 45 44 24.77 16.19 46 45 24.88 16.30 47 46 24.99 16.41 48 47 25.09 16.51 49 48 25.20 16.62	39	38	23.98	15.40
42 41 24.41 15.83 43 42 24.53 15.95 44 43 24.64 16.06 45 44 24.77 16.19 46 45 24.88 16.30 47 46 24.99 16.41 48 47 25.09 16.51 49 48 25.20 16.62	40	39	24.13	15.55
43 42 24.53 15.95 44 43 24.64 16.06 45 44 24.77 16.19 46 45 24.88 16.30 47 46 24.99 16.41 48 47 25.09 16.51 49 48 25.20 16.62	41	40	24.27	15.69
44 43 24.64 16.06 45 44 24.77 16.19 46 45 24.88 16.30 47 46 24.99 16.41 48 47 25.09 16.51 49 48 25.20 16.62	42	41	24.41	15.83
44 43 24.64 16.06 45 44 24.77 16.19 46 45 24.88 16.30 47 46 24.99 16.41 48 47 25.09 16.51 49 48 25.20 16.62			24.53	15.95
45 44 24.77 16.19 46 45 24.88 16.30 47 46 24.99 16.41 48 47 25.09 16.51 49 48 25.20 16.62			24.64	16.06
46 45 24.88 16.30 47 46 24.99 16.41 48 47 25.09 16.51 49 48 25.20 16.62			24.77	16.19
47 46 24.99 16.41 48 47 25.09 16.51 49 48 25.20 16.62	46	45	24.88	16.30
48 47 25.09 16.51 49 48 25.20 16.62		46	24.99	16.41
49 48 25.20 16.62			_ 	16.51
		48	25.20	16.62
			25.29	16.71
51 50 25.39 16.81			25.39	16.81



Pumping Test - Water Level Data

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Project: Highland Park Hydrogeological Assessment

Number: 10-025-2

Client: Pinecrest Remembrance Services Ltd.

	Time [min]	Water Level [m]	Drawdown [m]		
52	51	25.48	16.90		
53	52	25.56	16.98		
54	53	25.64	17.06		
55	54	25.72	17.14		
56	55	25.78	17.20		
57	56	25.85	17.27		
58	57	25.92	17.34		
59	58	25.99	17.41		
60	59	26.07	17.49		
61	60	26.12	17.54		
62	61	26.17	17.59		
63	62	26.22	17.64		
64	63	26.28	17.70		
65	64	26.33	17.75		
66	65	26.39	17.81		
67	66	26.45	17.87		
68	67	26.49	17.91		
69	68	26.52	17.94		
70	69	26.58	18.00		
71	70	26.64	18.06		
72	71	26.67	18.09		
73	72	26.71	18.13		
74	73	26.75	18.17		
75	74	26.79	18.21		
76	75	26.83	18.25		
77	76	26.87	18.29		
78	77	26.90	18.32		
79	78	26.94	18.36		
80	79	26.99	18.41		
81	80	27.01	18.43		
82	81	27.05	18.47		
83	82	27.08	18.50		
84	83	27.10	18.52		
85	84	27.15	18.57		
86	85	27.18	18.60		
87	86	27.20	18.62		
88	87	27.24	18.66		
89	88	27.26	18.68		
90	89	27.29	18.71		
91	90	27.31	18.73		
92	91	27.34	18.76		
93	92	27.36	18.78		
94	93	27.39	18.81		
95	94	27.42	18.84		
96	95	27.44	18.86		
97	96	27.47	18.89		
98	97	27.49	18.91		
99	98	27.51	18.93		
100	99	27.54	18.96		
101	100	27.56	18.98		
102	101	27.57	18.99		
	102	27.59	19.01		
103		07.64	10.02		
103 104	103	27.61	19.03		
	103 104	27.63	19.05		
104					



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Project: Highland Park Hydrogeological Assessment

Number: 10-025-2

		\	
	Time	Water Level [m]	Drawdown [m]
100	[min] 107	27.67	19.09
108		27.70	19.12
109	108	27.70	19.12
110	109	27.73	19.15
111	110		
112	111	27.72	19.14 19.16
113	112	27.74	
114	113	27.75	19.17
115	114	27.77	19.19
116	115	27.78	19.20
117	116	27.80	19.22
118	117	27.81	19.23
119	118	27.82	19.24
120	119	27.83	19.25
121	120	27.85	19.27
122	121	27.86	19.28
123	122	27.88	19.30
124	123	27.89	19.31
125	124	27.89	19.31
126	125	27.90	19.32
127	126	27.91	19.33
128	127	27.92	19.34
129	128	27.93	19.35
130	129	27.93	19.35
131	130	27.94	19.36
132	131	27.95	19.37
133	132	27.97	19.39
134	133	27.98	19.40
135	134	27.97	19.39
136	135	27.99	19.41
137	136	28.00	19.42
138	137	28.01	19.43
139	138	28.01	19.43
140	139	28.01	19.43
141	140	28.01	19.43
142	141	28.01	19.43
143	142	28.02	19.44
144	143	28.02	19.44
145	144	28.02	19.44
146	145	28.03	19.45
147	146	28.02	19.44
148	147	28.02	19.44
149	148	28.03	19.45
150	149	28.04	19.46
151	150	28.04	19.46
152	151	28.04	19.46
153	152	28.06	19.48
154	153	28.05	19.47
155	154	28.05	19.47
156	155	28.06	19.48
157	156	28.07	19.49
158	157	28.08	19.50
159	158	28.08	19.50
160	159	28.09	19.51
161	160	28.09	19.51
162	161	28.11	19.53
1	162	28.12	19.54



Pumping	Test -	Water	Level	Data
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Project: Highland Park Hydrogeological Assessment

Number: 10-025-2

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	Time	Water Level [m]	Drawdown [m]
164	[min] 163	28.12	19.54
165	164	28.13	19.55
	165	28.14	19.56
166		28.15	19.57
	166	28.15	19.57
168	167	28.17	19.59
169	168	28.17	19.59
170	169		19.60
171	170	28.18	19.61
172	171		19.61
173	172	28.19	19.64
174	173	28.22	
175	174	28.22	19.64
176	175	28.23	19.65
177	176	28.23	19.65
178	177	28.25	19.67
179	178	28.25	19.67
180	179	28.26	19.68
181	180	28.28	19.70
182	181	28.28	19.70
183	182	28.30	19.72
184	183	28.31	19.73
185	184	28.32	19.74
186	185	28.34	19.76
187	186	28.34	19.76
188	187	28.35	19.77
189	188	28.36	19.78
190	189	28.36	19.78
191	190	28.37	19.79
192	191	28.39	19.81
193	192	28.38	19.80
194	193	28.39	19.81
195	194	28.39	19.81
196	195	28.40	19.82
197	196	28.41	19.83
198	197	28.41	19.83
199	198	28.43	19.85
200	199	28.42	19.84
201	200	28.42	19.84
202	201	28.42	19.84
203	202	28.41	19.83
204	203	28.44	19.86
205	204	28.43	19.85
206	205	28,44	19.86
207	206	28.45	19.87
208	207	28.44	19.86
209	208	28.45	19.87
210	209	28.46	19.88
211	210	28.47	19.89
212	210	28.47	19.89
	212	28.49	19.91
213	212	28.49	19.91
214		28.49	19.91
215	214		19.91
216	215	28.49	
217	216	28.50	19.92
218	217	28.52	19.94
219	218	28.53	19.95



Pumping	Test -	Water	Level	Data
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		, , , , , , , , , , , , , , , , , , , ,	
	Time	Water Level [m]	Drawdown [m]
220	[min] 219	28.53	19.95
221	220	28.54	19.96
222	221	28.52	19.94
223	222	28.54	19.96
223	223	28.54	19.96
225	224	28.52	19.94
226	225	28.55	19.97
	226	28.54	19.96
227	227	28.55	19.97
228	228	28.56	19.98
229	229	28.56	19.98
230		28.56	19.98
231	230	28.55	19.97
232	231	28.54	19.96
233	232	<u> </u>	
234	233	28.55	19.97
235	234	28.55	19.97
236	235	28.55	19.97
237	236	28.56	19.98
238	237	28.57	19.99
239	238	28.57	19.99 19.98
240	239	28.56	
241	240	28.56	19.98
242	241	28.56	19.98
243	242	28.58	20.00
244	243	28.59	20.01
245	244	28.57	19.99
246	245	28.59	20.01
247	246	28.60	20.02
248	247	28.60	20.02
249	248	28.61	20.03
250	249	28.61	20.03
251	250	28.62	20.04
252	251	28.62	20.04
253	252	28.63	20.05
254	253	28.62	20.04
255	254	28.64	20.06
256	255	28.63	20.05
257	256	28.64	20.06
258	257	28.65	20.07
259	258	28.64	20.06
260	259	28.65	20.07
261	260	28.66	20.08
262	261	28.66	20.08
263	262	28.67	20.09
264	263	28.67	20.09
265	264	28.68	20.10
266	265	28.68	20.10
267	266	28.68	20.10
268	267	28.69	20.11
269	268	28.69	20.11
270	269	28.69	20.11
271	270	28.69	20.11
272	271	28.70	20.12
273	272	28.70	20.12
274	273	28.70	20.12
		28.70	20.12



Pumping Test	Water	Level Data
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	Time [min]	Water Level [m]	Drawdown [m]
276	275	28.70	20.12
277	276	28.72	20.14
278	277	28.72	20.14
279	278	28.73	20.15
280	279	28.73	20.15
281	280	28.74	20.16
282	281	28.74	20.16
283	282	28.75	20.17
284	283	28.76	20.18
285	284	28.76	20.18
286	285	28.76	20.18
287	286	28.76	20.18
288	287	28.76	20.18
289	288	28.77	20.19
290	289	28.77	20.19
291	290	28.78	20.20
292	291	28.78	20.20
293	292	28.77	20.19
293	292	28.77	20.19
295	294	28.78	20.20
296	295	28.77	20.19
	296	28.79	20.21
297		28.80	20.22
298	297	28.80	20.22
299	298	28.80	20.22
300	299 300	28.80	20.22
301	300	28.81	20.22
302	302	28.81	20.23
303	303	28.81	20.23
	304	28.81	20.23
305		28.81	20.23
306	305 306	28.82	20.24
307	307	28.82	20.24
308		28.82	20.24
310	308	28.82	20.24
		28.82	20.24
311	310 311	28.83	20.25
312		28.82	20.24
313	312 313	28.83	20.25
314	314	28.84	20.26
315		28.84	20.26
316	315 316	28.85	20.27
	317	28.85	20.27
318		28.85	20.27
319	318 319	28.85	20.27
320		28.85	20.27
321	320	28.86	20.28
322	321 322	28.86	20.28
323	323	28.85	20.27
324	324	28.85	20.27
325	325	28.86	20.28
326		28.87	20.29
327	326	28.86	20.29
328	327	28.88	20.30
329	328	28.87	20.29
330	329	 	20.29
331	330	28.88	20.30



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		<u> </u>	
	Time [min]	Water Level [m]	Drawdown [m]
332	331	28.88	20.30
333	332	28.89	20.31
334	333	28.89	20.31
335	334	28.90	20.32
336	335	28.90	20.32
337	336	28.89	20.31
338	337	28.90	20.32
339	338	28.89	20.31
340	339	28.90	20.32
341	340	28.90	20.32
342	341	28.91	20.33
343	342	28.91	20.33
344	343	28.91	20.33
345	344	28.90	20.32
346	345	28.91	20.33
347	346	28.91	20.33
348	347	28.91	20.33
349	348	28.90	20.32
350	349	28.91	20.33
351	350	28.91	20.33
352	351	28.91	20.33
353	352	28.92	20.34
354	353	28.93	20.35
355	354	28.92	20.34
356	355	28.92	20.34
357	356	28.92	20.34
358	357	28.93	20.35
359	358	28.94	20.36
360	359	28.94	20.36
361	360	28.94	20.36
362	361	28.93	20.35
363	362	28.94	20.36
364	363	28.93	20.35
365	364	28.95	20.37
366	365	28.95	20.37
367	366	28.95	20.37
368	367	28.94	20.36
369	368	28.93	20.35
370	369	28.93	20.35
371	370	28.94	20.36
372	371	28.94	20.36
373	372	28.93	20.35
374	373	28.94	20.36
375	374	28.95	20.37
376	375	28.96	20.38
377	376	28.95	20.37
378	377	28.95	20.37
379	378	28.94	20.36
380	379	28.96	20.38
381	380	28.96	20.38
382	381	28.94	20.36
383	382	27.78	19.20
384	383	26.64	18.06
385	384	25.75	17.17
386	385	24.92	16.34
	386	24.12	15.54



Pumping Test	- Water	Level Data
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	\			
	Time [min]	Water Level [m]	Drawdown [m]	
388	387	23.34	14.76	
389	388	22.60	14.02	
390	389	21.88	13.30	
391	390	21.21	12.63	
392	391	20.55	11.97	
393	392	19.91	11.33	_
394	393	19.31	10.73	
395	394	18.76	10.18	
396	395	18.23	9.65	
397	396	17.72	9.14	
398	397	17.23	8.65	
399	398	16.77	8.19	
400	399	16.34	7.76	_
401	400	15.93	7.35	
402	401	15.54	6.96	_
403	402	15.18	6.60	
404	403	14.84	6.26	_
	404	14.60	6.02	_
405		14.31	5.73	
406	405	 	5.45	_
407	406	14.03		_
408	407	13.76	5.18	
409	408	13.52	4.94	_
410	409	13.30	4.72	
411	410	13.08	4.50	
412	411	12.88	4.30	
413	412	12.69	4.11	
414	413	12.51	3.93	
415	414	12.34	3.76	
416	415	12.19	3.61	
417	416	12.05	3.47	_
418	417	11.92	3.34	
419	418	11.79	3.21	
420	419	11.65	3.07	
421	420	11.55	2.97	
422	421	11.43	2.85	
423	422	11.32	2.74	
424	423	11.22	2.64	
425	424	11.12	2.54	
426	425	11.04	2.46	
427	426	10.97	2.39	_
428	427	10.88	2.30	_
429	428	10.82	2.24	_
430	429	10.74	2.16	_
431	430	10.69	2.11	_
432	431	10.63	2.05	_
433	432	10.58	2.00	_
	433	10.53	1.95	
434	434	10.46	1.88	_
435		10.43	1.85	_
436	435		1.80	_
437	436	10.38		_
438	437	10.34	1.76	
439	438	10.31	1.73	_
440	439	10.28	1.70	
441	440	10.27	1.69	
442	441	10.25	1.67	
443	442	10.21	1.63	



Pumping Test - Wa	ater Level Data
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	Time [min]	Water Level [m]	Drawdown [m]		
444		10.18	1.60		
445	5 444	10.16	1.58		
446	445	10.14	1.56		
447	7 446	10.12	1.54		
448	3 447	10.10	1.52		
449	9 448	10.08	1.50		
450	449	10.06	1.48		
451	450	10.05	1.47		
452		10.02	1.44		
453		10.01	1.43		
454		9.99	1.41		
455		9.98	1.40		
456		9.97	1.39		
457			1.38		
		9.96	-		
458		9.94	1.36		
459		9.93	1.35		
460	_ 	9.92	1.34		
461		9.91	1.33		
462	461	9.89	1.31		
463	462	9.88	1.30		
464	463	9.87	1.29		
465	464	9.86	1.28		
466	465	9.86	1.28		
467	466	9.85	1.27		
468	467	9.84	1.26		
469	468	9.82	1.24		
470	469	9.81	1.23		
471	470	9.81	1.23		
472	471	9.80	1.22		
			<u> </u>		
473	472	9.80	1.22		
474	473	9.79	1.21		
475	474	9.78	1.20		
476	475	9.77	1.19		
477	476	9.77	1.19		
478	477	9.76	1.18		
479	478	9.76	1.18		
480	479	9.75	1.17		
481	480	9.74	1.16		
482	481	9.74	1.16		
483	482	9.74	1.16		
484	483	9.74	1.16		
485	484	9.73	1.15		
486	485	9.73	1.15		
487	486	9.72	1.14		
488	487	9.72	1.14		
489	488	9.71	1.13		
490	489	9.71	1.13		
491	490	9.70	1.12		
492	491	9.70	1.12		
493	492	9.69	1.11		
494	493	9.69	1.11		
495	494	9.68	1.10		
496	495	9.68	1.10		
497	496	9.68	1.10		
498	497	9.67	1.09		



Pumping Test - Water Level Data

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		\	
	Time [min]	Water Level [m]	Drawdown [m]
500		9.65	1.07
501		9.65	1.07
502	_ 	9.64	1.06
503		9.64	1.06
504		9.64	1.06
505		9.63	1.05
506		9.63	1.05
507	 	9.62	1.03
508		9.61	1.03
509		9.62	1.03
510		9.61	1.03
511		9.61	1.03
512		9.60	1.02
513		9.60	1.02
514		9.60	1.02
515		9.60	1.02
516	-	9.60	1.02
517		9.61	1.03
518		9.60	1.02
519	518	9.60	1.02
520	519	9.59	
521	520	·	1.01
522		9.58	1.00
523	521 522	9.58 9.58	1.00
	 	· · · · · · · · · · · · · · · · · · ·	1.00
524	523 524	9.58	1.00
525 526	525	9.57	0.99
527	 	9.57	0.99
528	526 527	9.57 9.57	0.99
529	528		0.99
530	529	9.56 9.55	0.98
531	530	9.57	
532	531	9.56	0.99
533	532	9.55	0.98
534	533	9.55	0.97
535	534	9.54	0.96
536	535	9.54	0.96
537	536	9.55	0.97
538	537	9.55	
539	538	9.55	0.97 0.97
540	539	9.54	0.96
541	540	9.53	0.95
542	541	9.54	0.96
543	542	9.54	0.96
544	543	9.54	0.96
545	543	9.54	
546	545	9.54	0.96
547	546	9.54	0.96 0.96
548	547	9.54	0.96
549	548	9.54	
	549		0.96
550 551	550	9.52	0.94
552	551	9.53	0.95
553		9.51	0.93
	552	9.51	0.93
554 555	553 554	9.50	0.92
333	JJ4	9.51	0.93



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	\				
	Time [min]	Water Level [m]	Drawdown [m]		
556	555	9.51	0.93		
557	556	9.50	0.92		
558	557	9.50	0.92		
559	558	9.50	0.92		
560	559	9.50	0.92		
561	560	9.50	0.92		
562	561	9.50	0.92		
563	562	9.50	0.92		
564	563	9.49	0.91		
565	564	9.49	0.91		
566	565	9.49	0.91		
567	566	9.49	0.91		
568	567	9.49	0.91		
569	568	9.49	0.91		
570	569	9.48	0.90		
571	570	9.48	0.90		
572	571	9.47	0.89		
573	572	9.46	0.88		
574	573	9.47	0.89		
575	574	9.46	0.88		
576	575	9.46	0.88		
577	576	9.46	0.88		
578	577	9.45	0.87		
579	578	9.47	0.89		
580	579	9.46	0.88		
581	580	9.46	0.88		
582	581	9.46	0.88		
583	582	9.45	0.87		
584	583	9.46	0.88		
585	584	9.46	0.88		
586	585	9.45	0.87		
587	586	9.45	0.87		
588	587	9.45	0.87		
589	588	9.45	0.87		
590	589	9.44	0.86		
591	590	9.45	0.87		
592	591	9.45	0.87		
593	592	9.44	0.86		
594	593	9.44	0.86		
595	594	9.45	0.87		
596	595	9.44	0.86		
597	596	9.44	0.86		
598	597	9.44	0.86		
599	598	9.43	0.85		
600	599	9.43	0.85		
601	600	9.44	0.86		
602	601	9.43	0.85		
603	602	9.43	0.85		
604	603	9.43	0.85		
605	604	9.43	0.85		
606	605	9.43	0.85		
607	606	9.43	0.85		
608	607	9.42	0.84		
609	608	9.42	0.84		
610	609	9.41	0.83		
611	610	9.41	0.83		



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	Time [min]	Water Level [m]	Drawdown [m]		
612	2 611	9.41	0.83		
613	3 612	9.41	0.83		
614	4 613	9.42	0.84		
615	5 614	9.41	0.83		
616	615	9.41	0.83		
617	7 616	9.40	0.82		
618	617	9.41	0.83		
619	618	9.41	0.83		
620	619	9.40	0.82		
621		9.40	0.82		
622		9.40	0.82		
623	·	9.39	0.81		
624		9.40	0.82		
625		9.40	0.82		
626		9.38	0.80		
					
627		9.39	0.81		
628		9.39	0.81		
629		9.39	0.81		
630		9.38	0.80		
631		9.39	0.81		
632		9.37	0.79		
633	632	9.37	0.79		
634	633	9.37	0.79		
635	634	9.37	0.79		
636	635	9.37	0.79		
637	636	9.37	0.79		
638	637	9.37	0.79		
639	638	9.38	0.80		
640	639	9.38	0.80		
641	640	9.38	0.80		
642	641	9.38	0.80		
643	642	9.37	0.79		
644	643	9.37	0.79		
645	644	9.37	0.79		
646	645	9.36	0.78		
647	646	9.36	0.78		
648	647	9.35	0.77		
649	648	9.35	0.77		
650	649	9.35	0.77		
					
651	650	9.35	0.77		
652	651	9.36	0.78		
653	652	9.36	0.78		
654	653	9.36	0.78		
655	654	9.37	0.79		
656	655	9.36	0.78		
657	656	9.36	0.78		
658	657	9.36	0.78		
659	658	9.35	0.77		
660	659	9.35	0.77		
661	660	9.34	0.76		
662	661	9.36	0.78		
663	662	9.35	0.77		
664	663	9.35	0.77		
665	664	9.35	0.77		
666	665	9.35	0.77		



Pumping Test - Water Level Data

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	Time [min]	Water Level [m]	Drawdown [m]
668	667	9.35	0.77
669	668	9.34	0.76
670	669	9.35	0.77
671	670	9.33	0.75
672	671	9.34	0.76
673	672	9.33	0.75
674	673	9.34	0.76
675	674	9.33	0.75
676	675	9.34	0.76
677	676	9.33	0.75
678	677	9.33	0.75
679	678	9.33	0.75
680	679	9.33	0.75
681	680	9.34	0.76
682	681	9.32	0.74
683	682	9.33	0.75
684	683	9.33	0.75
685	684	9.33	0.75
686	685	9.33	0.75
687	686	9.31	0.73
688	687	9.31	0.73
689	688	9.32	0.74
690	689	9.32	0.74
691	690	9.31	0.73
692	691	9.31	0.73
693	692	9.31	0.73
694	693	9.30	0.72
695	694	9.31	0.73
696	695	9.31	0.73
697	696	9.31	0.73
698	697	9.30	0.72
699	698	9.30	0.72
700	699	9.31	0.73
701	700	9.30	0.72
702	701	9.30	0.72
702	702	9.30	0.72
704	703	9.30	0.72
705	704	9.29	0.71
706	705	9.30	0.72
707	706	9.29	0.71
708	707	9.29	0.71
709	707	9.29	0.71
710	709	9.29	0.71
711	710	9.29	0.71
712	711	9.29	0.71
713	712	9.28	0.70
714	713	9.28	0.70
714	713	9.28	0.70
		9.29	0.71
716	715 716	9.28	0.71
717	716	9.28	0.70
718		9.28	0.70
719	718 719	9.27	0.70
720			0.70
721	720 721	9.28	0.70
722			
723	722	9.27	0.69



Pumping '	Test - \	Nater	Level	Data
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			j
	Time	Water Level	Drawdown
724	[min] 723	[m] 9.27	[m] 0.69
725	724	9.27	0.69
726	725	9.27	0.69
			0.69
727	726	9.27	
728	727	9.27	0.69
729	728	9.26	0.68
730	729	9.27	0.69
731	730	9.27	0.69
732	731	9.27	0.69
733	732	9.27	0.69
734	733	9.27	0.69
735	734	9.28	0.70
736	735	9.27	0.69
737	736	9.27	0.69
738	737	9.26	0.68
739	738	9.26	0.68
740	739	9.26	0.68
741	740	9.26	0.68
742	741	9.26	0.68
743	742	9.26	0.68
744	743	9.26	0.68
745	744	9.26	0.68
746	745	9.25	0.67
747	746	9.26	0.68
748	747	9.26	0.68
749	748	9.24	0.66
750	749	9.25	0.67
751	750	9.25	0.67
752	751	9.25	0.67
753	752	9.25	0.67
754	753	9.25	0.67
755	754	9.25	0.67
756	755	9.25	0.67
757	756	9.25	0.67
758	757	9.25	0.67
759	758	9.25	0.67
760	759	9.23	0.65
761	760	9.23	0.65
762	761	9.23	0.65
763	762	9.23	0.65
764	763	9.25	0.67
765	764	9.23	0.65
766	765	9.24	0.66
767	766	9.24	0.66
768	767	9.23	0.65
769	768	9.23	0.65
770	769	9.23	0.65
771	770	9.23	0.65
772	771	9.24	0.66
773	772	9.24	0.66
774	773	9.23	0.65
775	774	9.22	0.64
776	775	9.22	0.64
777	776	9.22	0.64
778	777	9.22	0.64
	778	9.22	0.64



Pumping	Test -	Water	Level	Data
1 UIIIDIIIU	1631 -	vvalei		Data

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	\				
	Time [min]	Water Level [m]	Drawdown [m]		
780	0 779	9.21	0.63		
78	1 780	9.23	0.65		
782	2 781	9.23	0.65		
783	782	9.23	0.65		
784	4 783	9.22	0.64		
785	5 784	9.23	0.65		
786	785	9.22	0.64		
787	7 786	9.22	0.64		
788	3 787	9.22	0.64		
789	788	9.21	0.63		
790	789	9.22	0.64		
791	790	9.22	0.64		
792	791	9.22	0.64		
793	792	9.22	0.64		
794	793	9.21	0.63		
795	794	9.22	0.64		
796		9.22	0.64		
797		9.22	0.64		
798		9.21	0.63		
799		9.22	0.64		
800		9.20	0.62		
801		9.20	0.62		
802		9.20	0.62		
803		9.20	0.62		
804		9.20	0.62		
805		9.20	0.62		
806	805	9.20	0.62		
807	806	9.20	0.62		
	807	9.20	0.62		
808 809	808	9.20	0.62		
810	809	9.20	0.62		
811	810	9.21	0.63		
812	811	9.20	0.62		
813	812	9.20	0.62		
814	813	9.20	0.62		
815	814	9.20	0.62		
	815	9.20			
816		 	0.62		
817	816	9.20	0.62		
818	817	9.20	0.62		
819	818 819	9.20	0.62		
820		9.19	0.61		
821	820	9.20	0.62		
822	821	9.20	0.62		
823	822	9.20	0.62		
824	823	9.20	0.62		
825	824	9.20	0.62		
826	825	9.20	0.62		
827	826	9.20	0.62		
828	827	9.19	0.61		
829	828	9.19	0.61		
830	829	9.19	0.61		
831	830	9.19	0.61		
832	831	9.19	0.61		
833	832	9.19	0.61		
834 835	833 834	9.19 9.19	0.61 0.61		



Pumping Test - Water Level Data

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	Time [min]	Water Level [m]	Drawdown [m]		
836	835	9.19	0.61		
837	836	9.18	0.60		
838	837	9.18	0.60		
839	838	9.18	0.60		
840	839	9.18	0.60		
841	840	9.18	0.60		
842	841	9.18	0.60		
843	842	9.18	0.60		
844	843	9.18	0.60		
845	844	9.18	0.60		
846	845	9.18	0.60		
847	846	9.18	0.60		
848	847	9.18	0.60		
849	848	9.17	0.59		
850	849	9.17	0.59		
851	850	9.17	0.59		
852	851	9.17	0.59		
853	852	9.17	0.59		
854	853	9.17	0.59		
855	854	9.17	0.59		
856	855	9.17	0.59		
857	856	9.17	0.59		
858	857	9.17	0.59		
859	858	9.17	0.59		
860	859	9.17	0.59		
861	860	9.17	0.59		
862	861	9.17	0.59		
863	862	9.17	0.59		
864	863	9.16	0.58		
865	864	9.17	0.59		
866	865	9.16	0.58		
867	866	9.16	0.58		
868	867	9.16	0.58		
869	868	9.17	0.59		
870	869	9.17	0.59		
871	870	9.16	0.58		
872	871	9.16	0.58		
873	872	9.16	0.58		
874	873	9.16	0.58		
875	874	9.16	0.58		
876	875	9.16	0.58		
877	876	9.17	0.59		
878	877	9.15	0.57		
879	878	9.15	0.57		
880	879	9.15	0.57		
881	880	9.16	0.58		
882	881	9.15	0.57		
883	882	9.16	0.58		
884	883	9.16	0.58		
885	884	9.15	0.57		
886	885	9.14	0.56	\neg	
887	886	9.16	0.58		
888	887	9.15	0.57		
889	888	9.14	0.56		
890	889	9.14	0.56	\neg	
891	890	9.14	0.56	コ	



Pumping	Test -	Water	Level	Data
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	\				
	Time [min]	Water Level [m]	Drawdown [m]		
892	891	9.15	0.57		
893	892	9.14	0.56		
894	893	9.14	0.56		
895	894	9.14	0.56		
896	895	9.14	0.56		
897	896	9.14	0.56		
898	897	9.14	0.56		
899	898	9.15	0.57		
900	899	9.15	0.57		
901	900	9.15	0.57		
902	901	9.15	0.57		
903	902	9.15	0.57		
904	903	9.14	0.56		
905	904	9.14	0.56		
906	905	9.14	0.56		
907	906	9.14	0.56		
908	907	9.14	0.56		
909	908	9.13	0.55		
910	909	9.13	0.55		
911	910	9.13	0.55		
912	911	9.14	0.56		
913	912	9.14	0.56		
914	913	9.14	0.56		
915	914	9.13	0.55		
916	915	9.16	0.58		
917	916	9.14	0.56		
918	917	9.14	0.56		
919	918	9.13	0.55		
920	919	9.13	0.55		
921	920	9.13	0.55		
922	921	9.13	0.55		
923	922	9.13	0.55		
924	923	9.12	0.54		
925	924	9.13	0.55		
926	925	9.13	0.55		
927	926	9.13	0.55		
928	927	9.13	0.55		
929	928	9.13	0.55		
930	929	9.12	0.54		
931	930	9.12	0.54		
932	931	9.12	0.54		
933	932	9.12	0.54		
934	933	9.13	0.55		
935	934	9.12	0.54		
936	935	9.12	0.54		
937	936	9.12	0.54		
938	937	9.12	0.54		
939	938	9.12	0.54		
940	939	9.12	0.54		
941	940	9.13	0.55		
942	941	9.11	0.53		
943	942	9.12	0.54		
944	943	9.11	0.53		
945	944	9.11	0.53		
946	945	9.11	0.53		
	946	9.11	0.53		



Pumping	Test -	Water	Level	Data
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		\	
	Time [min]	Water Level [m]	Drawdown [m]
94		9.11	0.53
94		9.12	0.54
950		9.12	0.54
95		9.11	0.53
95		9.12	0.54
953		9.12	0.54
954		9.12	0.54
955	5 954	9.12	0.54
956	955	9.11	0.53
957	7 956	9.11	0.53
958	957	9.11	0.53
959	958	9.11	0.53
960	959	9.11	0.53
961	960	9.11	0.53
962	961	9.11	0.53
963	962	9.11	0.53
964	963	9.11	0.53
965	964	9.11	0.53
966	965	9.11	0.53
967	966	9.11	0.53
968	967	9.11	0.53
969	968	9.12	0.54
970	969	9.11	0.53
971	970	9.11	0.53
972	971	9.11	0.53
973	972	9.12	0.54
974		9.11	0.53
975	974	9.12	0.54
976	975	9.11	0.53
977	976	9.11	0.53
978	977	9.11	0.53
979	978	9.11	0.53
980	979	9.11	0.53
981	980	9.11	0.53
982	981	9.11	0.53
983	982	9.11	0.53
984	983	9.10	0.52
985	984	9.10	0.52
986	985	9.11	0.53 0.53
987 988	986 987	9.11	0.53
989	988	9.11	0.53
990	989	9.10	0.52
991	990	9.11	0.53
992	991	9.11	0.53
993	992	9.11	0.53
994	993	9.11	0.53
995	994	9.11	0.53
996	995	9.10	0.52
997	996	9.10	0.52
998	997	9.10	0.52
999	998	9.10	0.52
1000	999	9.11	0.53
	1000	9.10	0.52
1001	1000		0.02
1001	1001	9.10	0.52



Pumping	Test -	Water	Level	Data
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<u> </u>			i
]	Time [min]	Water Level [m]	Drawdown
1004	1003	9.10	[m] 0.52
1005	1003	9.10	0.52
1005	1004	9.10	0.52
1007	1006	9.10	0.52
1007	1007	9.09	0.52
1009	1007		
	1008	9.10	0.52
1010	1010	9.10	0.52
1011	1010	9.10	0.52
		9.10	0.52
1013	1012 1013	9.10	0.52
1014	1013		
		9.09	0.51
1016	1015	9.10	0.52
1017	1016	9.09	0.51
1018	1017	9.10	0.52
1019	1018	9.09	0.51
1020	1019	9.09	0.51
1021	1020	9.09	0.51
1022	1021	9.09	0.51
1023	1022	9.09	0.51
1024	1023	9.09	0.51
1025	1024	9.09	0.51
1026	1025	9.09	0.51
1027	1026	9.09	0.51
1028	1027	9.09	0.51
1029	1028	9.09	0.51
1030	1029	9.09	0.51
1031	1030	9.09	0.51
1032	1031	9.09	0.51
1033	1032	9.09	0.51
1034	1033	9.09	0.51
1035	1034	9.09	0.51
1036	1035	9.09	0.51
1037	1036	9.08	0.50
1038	1037	9.08	0.50
1039	1038	9.08	0.50
1040	1039	9.08	0.50
1041	1040	9.08	0.50
1042	1041	9.09	0.51
1043	1042	9.09	0.51
1044	1043	9.09	0.51
1045	1044	9.08	0.50
1046	1045	9.08	0.50
1047	1046	9.08	0.50
1048	1047	9.08	0.50
1049	1048	9.08	0.50
1050	1049	9.08	0.50
1051	1050	9.08	0.50
1052	1051	9.08	0.50
1053	1052	9.08	0.50
1054	1053	9.08	0.50
1055	1054	9.08	0.50
1056	1055	9.08	0.50
1057	1056	9.07	0.49
1058	1057	9.08	0.50
1059	1058	9.07	0.49



Pumping Tes	st - Water	Level Data
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	Time	Water Level	Drawdown
1060	[min] 1059	[m] 9.07	[m] 0.49
1060			
1061	1060	9.08	0.50
1062	1061	9.08	0.50
1063	1062	9.07	0.49
1064	1063	9.07	0.49
1065	1064	9.07	0.49
1066	1065	9.07	0.49
1067	1066	9.07	0.49
1068	1067	9.07	0.49
1069	1068	9.08	0.50
1070	1069	9.08	0.50
1071	1070	9.08	0.50
1072	1071	9.09	0.51
1073	1072	9.09	0.51
1074	1073	9.09	0.51
1075	1074	9.09	0.51
1076	1075	9.07	0.49
1077	1076	9.08	0.50
1078	1077	9.07	0.49
1079	1078	9.07	0.49
1080	1079	9.08	0.50
1081	1080	9.09	0.51
1082	1081	9.09	0.51
1083	1082	9.09	0.51
1084	1083	9.08	0.50
1085	1084	9.08	0.50
1086	1085	9.08	0.50
1087	1086	9.08	0.50
1088	1087	9.09	0.51
1089	1088	9.08	0.50
1090	1089	9.08	0.50
1091	1090	9.07	0.49
1092	1091	9.07	0.49
1093	1092	9.08	0.50
1094	1093	9.08	0.50
1095	1094	9.07	0.49
1096	1095	9.06	0.48
1097	1096	9.07	0.49
1098	1097	9.07	0.49
1099	1098	9.07	0.49
1100	1099	9.08	0.50
1101	1100	9.06	0.48
1102	1101	9.07	0.49
1103	1102	9.07	0.49
1104	1103	9.07	0.49
1105	1104	9.07	0.49
1106	1105	9.06	0.48
1107	1106	9.07	0.49
1108	1107	9.06	0.48
1109	1108	9.06	0.48
1110	1109	9.06	0.48
1111	1110	9.07	0.49
1112	1111	9.06	0.48
1113	1112	9.06	0.48
1114	1113	9.06	0.48
	1114	9.06	0.48



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Time	L		· · · · · · · · · · · · · · · · · · ·	
1116		1	I	
1117	1116	 		
1118 1117 9.06 0.48 1119 1118 9.06 0.48 1120 1119 9.06 0.48 1121 1120 9.06 0.48 1122 1121 9.06 0.48 1123 1122 9.06 0.48 1124 1125 9.06 0.48 1125 1124 9.06 0.48 1126 1125 9.06 0.48 1127 1126 9.06 0.48 1128 1127 9.06 0.48 1129 1128 9.06 0.48 1129 1128 9.06 0.48 1130 1129 9.06 0.48 1131 1130 9.06 0.48 1133 1132 9.06 0.48 1133 1133 9.06 0.48 1133 1133 9.06 0.48 1133 1133 9.06 0.48	<u></u>			
1119 1118 9.06 0.48 1120 1119 9.06 0.48 1121 1120 9.06 0.48 1122 1121 9.06 0.48 1123 1122 9.06 0.48 1124 1123 9.06 0.48 1125 1124 9.06 0.48 1127 1126 9.06 0.48 1127 1128 9.06 0.48 1128 1127 9.06 0.48 1129 1128 9.06 0.48 1130 1129 9.06 0.48 1131 1130 9.06 0.48 1131 1130 9.06 0.48 1131 1130 9.06 0.48 1133 1132 9.06 0.48 1133 1133 9.06 0.48 1133 1133 9.06 0.48 1134 1133 9.06 0.48		 		
1120 1119 9.06 0.48 1121 1120 9.06 0.48 1122 1121 9.06 0.48 1123 1122 9.06 0.48 1124 1123 9.06 0.48 1125 1124 9.06 0.48 1126 1125 9.06 0.48 1127 1126 9.06 0.48 1128 1127 9.06 0.48 1129 1128 9.06 0.48 1130 1129 9.06 0.48 1131 1130 9.06 0.48 1132 1131 9.06 0.48 1133 1132 9.06 0.48 1133 1131 9.06 0.48 1133 1132 9.06 0.48 1133 1134 9.06 0.48 1133 1135 9.06 0.48 1137 1136 9.06 0.48				
1121 1120 9.06 0.48 1122 1121 9.06 0.48 1123 1122 9.06 0.48 1124 1123 9.06 0.48 1125 1124 9.06 0.48 1126 1125 9.06 0.48 1127 1126 9.06 0.48 1129 1128 9.06 0.48 1129 1128 9.06 0.48 1130 1129 9.06 0.48 1131 1130 9.06 0.48 1132 1131 9.06 0.48 1133 1132 9.06 0.48 1133 1132 9.06 0.48 1133 1133 9.06 0.48 1133 1133 9.06 0.48 1133 1134 9.06 0.48 1134 1133 9.06 0.48 1137 1136 9.06 0.48		 		
11122 1121 9.06 0.48 1123 1122 9.06 0.48 1124 1123 9.06 0.48 1125 1124 9.06 0.48 1126 1125 9.06 0.48 1127 1126 9.06 0.48 1128 1127 9.06 0.48 1130 1129 9.06 0.48 1131 1130 9.06 0.48 1131 1130 9.06 0.48 1131 1130 9.06 0.48 1132 1131 9.06 0.48 1133 1132 9.06 0.48 1133 1133 9.06 0.48 1134 1133 9.06 0.48 1135 1134 9.06 0.48 1136 1135 9.06 0.48 1137 1136 9.06 0.48 1138 1137 9.06 0.48	-			
11123 11124 11123 9.06 0.48 11125 1124 9.06 0.48 1125 1124 9.06 0.48 1127 1126 9.06 0.48 1127 1126 9.06 0.48 1129 1128 9.06 0.48 1130 1129 9.06 0.48 1131 1130 9.06 0.48 1132 1131 9.06 0.48 1133 1132 9.06 0.48 1133 1133 9.06 0.48 1133 1133 9.06 0.48 1133 1133 9.06 0.48 1135 1134 9.06 0.48 1135 1134 9.06 0.48 1137 1136 9.06 0.48 1137 1136 9.06 0.48 1139 1138 9.06 0.48 1140 1139 9.06 0.48<				
1124 1125 1124 9.06 0.48 1126 1124 9.06 0.48 1127 1126 9.06 0.48 1128 1127 9.06 0.48 1129 1128 9.06 0.48 1130 1129 9.06 0.48 1131 1130 9.06 0.48 1132 1131 9.06 0.48 1133 1132 9.06 0.48 1133 1133 9.06 0.48 1134 1133 9.06 0.48 1135 1134 9.06 0.48 1136 1135 9.06 0.48 1137 1136 9.06 0.48 1137 1136 9.06 0.48 1137 1136 9.06 0.48 1137 1136 9.06 0.48 1139 1139 9.06 0.48 1140 1139 9.06 0.48		<u> </u>		
1125 1124 9.06 0.48 1126 1125 9.06 0.48 1127 1126 9.06 0.48 1129 1128 9.06 0.48 1130 1129 9.06 0.48 1131 1130 9.06 0.48 1132 1131 9.06 0.48 1133 1132 9.06 0.48 1134 1133 9.06 0.48 1135 1134 9.06 0.48 1136 1135 9.06 0.48 1137 1136 9.06 0.48 1138 1137 9.06 0.48 1139 1138 9.06 0.48 1139 1138 9.06 0.48 1140 1139 9.06 0.48 1141 1140 9.06 0.48 1141 1140 9.06 0.48 1141 1140 9.06 0.48	<u> </u>			
1126 1125 9.06 0.48 1127 1126 9.06 0.48 1128 1127 9.06 0.48 1129 1128 9.06 0.48 1130 1129 9.06 0.48 1131 1130 9.06 0.48 1132 1131 9.06 0.48 1133 1132 9.06 0.48 1133 1132 9.06 0.48 1134 133 9.06 0.48 1135 1134 9.06 0.48 1135 1134 9.06 0.48 1137 1136 9.06 0.48 1137 1136 9.06 0.48 1137 1138 9.06 0.48 1139 1138 9.06 0.48 1140 1139 9.06 0.48 1141 1140 9.06 0.48 1141 1141 9.06 0.48				
11127 1126 9.06 0.48 1128 1127 9.06 0.48 1129 1128 9.06 0.48 1130 1129 9.06 0.48 1131 1130 9.06 0.48 1132 1131 9.06 0.48 1133 1132 9.06 0.48 1133 1133 9.06 0.48 1134 1133 9.06 0.48 1135 19.06 0.48 1136 1135 9.06 0.48 1137 1136 9.06 0.48 1137 1136 9.06 0.48 1137 1138 9.06 0.48 1139 1138 9.06 0.48 1140 1139 9.06 0.48 1141 1140 9.06 0.48 1141 1140 9.06 0.48 1142 1141 9.06 0.48 1143				+
1128 1127 9.06 0.48 1129 1128 9.06 0.48 1130 1129 9.06 0.48 1131 1130 9.06 0.48 1132 1131 9.06 0.48 1133 1132 9.06 0.48 1134 1133 9.06 0.48 1135 1134 9.06 0.48 1136 1135 9.06 0.48 1137 1136 9.06 0.48 1138 1137 9.06 0.48 1139 1138 9.06 0.48 1139 1138 9.06 0.48 1140 1139 9.06 0.48 1141 1140 9.06 0.48 1141 1140 9.06 0.48 1141 1141 9.06 0.48 1141 1141 9.06 0.48 1142 1141 9.06 0.48				
1129 1128 9.06 0.48 1130 1129 9.06 0.48 1131 1130 9.06 0.48 1132 1131 9.06 0.48 1133 1132 9.06 0.48 1134 1133 9.06 0.48 1135 1134 9.06 0.48 1136 1135 9.06 0.48 1137 1136 9.06 0.48 1137 1136 9.06 0.48 1139 1138 9.06 0.48 1140 1139 9.06 0.48 1141 1140 9.06 0.48 1141 1140 9.06 0.48 1141 1140 9.06 0.48 1142 1141 19.06 0.48 1143 1142 9.05 0.47 1144 1143 9.06 0.48 1145 1144 9.06 0.48				
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1137 1136 9.06 0.48 1138 1137 9.06 0.48 1139 1138 9.06 0.48 1140 1139 9.06 0.48 1141 1140 9.06 0.48 1142 1141 9.06 0.48 1143 1142 9.05 0.47 1144 1143 9.06 0.48 1145 1144 9.06 0.48 1145 1144 9.06 0.48 1145 1144 9.06 0.48 1146 1145 9.05 0.47 1148 1147 9.05 0.47 1148 1147 9.05 0.47 1149 1148 9.06 0.48 1150 1149 9.06 0.48 1151 1150 9.06 0.48 1152 1151 9.05 0.47 1153 1152 9.05 0.47			9.06	
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1139 1138 9.06 0.48 1140 1139 9.06 0.48 1141 1140 9.06 0.48 1142 1141 9.06 0.48 1143 1142 9.05 0.47 1144 1143 9.06 0.48 1145 1144 9.06 0.48 1146 1145 9.05 0.47 1147 1146 9.05 0.47 1148 1147 9.05 0.47 1149 1148 9.06 0.48 1150 1149 9.06 0.48 1151 1150 9.06 0.48 1151 1150 9.06 0.48 1152 1151 9.05 0.47 1153 1152 9.05 0.47 1154 1153 9.06 0.48 1155 1154 9.06 0.48 1155 1154 9.06 0.48	1137			0.48
1140 1139 9.06 0.48 1141 1140 9.06 0.48 1142 1141 9.06 0.48 1143 1142 9.05 0.47 1144 1143 9.06 0.48 1145 1144 9.06 0.48 1146 1145 9.05 0.47 1147 1146 9.05 0.47 1148 1147 9.05 0.47 1149 1148 9.06 0.48 1150 1149 9.06 0.48 1151 1150 9.06 0.48 1152 1151 9.05 0.47 1153 1152 9.05 0.47 1154 1153 9.06 0.48 1155 1154 9.06 0.48 1155 1154 9.06 0.48 1155 1154 9.06 0.48 1155 1154 9.06 0.48	1138	1137	9.06	
1141 1140 9.06 0.48 1142 1141 9.06 0.48 1143 1142 9.05 0.47 1144 1143 9.06 0.48 1145 1144 9.06 0.48 1146 1145 9.05 0.47 1147 1146 9.05 0.47 1148 1147 9.05 0.47 1149 1148 9.06 0.48 1150 1149 9.06 0.48 1151 1150 9.06 0.48 1152 1151 9.05 0.47 1153 1152 9.05 0.47 1153 1152 9.05 0.47 1154 1153 9.06 0.48 1155 1154 9.06 0.48 1155 1154 9.06 0.48 1155 1155 9.05 0.47 1157 1156 9.04 0.46	1139		9.06	0.48
1142 1141 9.06 0.48 1143 1142 9.05 0.47 1144 1143 9.06 0.48 1145 1144 9.06 0.48 1146 1145 9.05 0.47 1147 1146 9.05 0.47 1148 1147 9.05 0.47 1149 1148 9.06 0.48 1150 1149 9.06 0.48 1151 1150 9.06 0.48 1152 1151 9.05 0.47 1153 1152 9.05 0.47 1153 1152 9.05 0.47 1154 1153 9.06 0.48 1155 1154 9.06 0.48 1155 1154 9.06 0.48 1155 1154 9.06 0.48 1155 1155 9.05 0.47 1157 1156 9.04 0.46	1140		9.06	0.48
1143 1142 9.05 0.47 1144 1143 9.06 0.48 1145 1144 9.06 0.48 1146 1145 9.05 0.47 1147 1146 9.05 0.47 1148 1147 9.05 0.47 1149 1148 9.06 0.48 1150 1149 9.06 0.48 1151 1150 9.06 0.48 1152 1151 9.05 0.47 1153 1152 9.05 0.47 1154 1153 9.06 0.48 1155 1154 9.06 0.48 1155 1154 9.06 0.48 1155 1154 9.06 0.48 1155 1154 9.06 0.48 1157 1156 9.05 0.47 1157 1156 9.04 0.46 1158 1157 9.06 0.48	1141	1140	9.06	0.48
1144 1143 9.06 0.48 1145 1144 9.06 0.48 1146 1145 9.05 0.47 1147 1146 9.05 0.47 1148 1147 9.05 0.47 1149 1148 9.06 0.48 1150 1149 9.06 0.48 1151 1150 9.06 0.48 1152 1151 9.05 0.47 1153 1152 9.05 0.47 1153 1152 9.05 0.47 1154 1153 9.06 0.48 1155 1154 9.06 0.48 1155 1154 9.06 0.48 1155 1155 9.05 0.47 1157 1156 9.04 0.46 1158 1157 9.06 0.48 1159 1158 9.05 0.47 1160 1159 9.05 0.47	1142	1141	9.06	0.48
1145 1144 9.06 0.48 1146 1145 9.05 0.47 1147 1146 9.05 0.47 1148 1147 9.05 0.47 1149 1148 9.06 0.48 1150 1149 9.06 0.48 1151 1150 9.06 0.48 1152 1151 9.05 0.47 1153 1152 9.05 0.47 1153 1152 9.05 0.47 1154 1153 9.06 0.48 1155 1154 9.06 0.48 1155 1154 9.06 0.48 1155 1154 9.06 0.48 1157 1156 9.04 0.46 1158 1157 9.06 0.48 1159 1158 9.05 0.47 1160 1159 9.05 0.47 1161 1160 9.05 0.47	1143		9.05	0.47
1146 1145 9.05 0.47 1147 1146 9.05 0.47 1148 1147 9.05 0.47 1149 1148 9.06 0.48 1150 1149 9.06 0.48 1151 1150 9.06 0.48 1152 1151 9.05 0.47 1153 1152 9.05 0.47 1154 1153 9.06 0.48 1155 1154 9.06 0.48 1155 1154 9.06 0.48 1155 1154 9.06 0.48 1157 1156 9.04 0.46 1158 1157 9.06 0.48 1159 1158 9.05 0.47 1160 1159 9.05 0.47 1161 1160 9.05 0.47 1162 1161 9.05 0.47 1163 1162 9.05 0.47	1144	1143	9.06	0.48
1147 1148 9.05 0.47 1148 1147 9.05 0.47 1149 1148 9.06 0.48 1150 1149 9.06 0.48 1151 1150 9.06 0.48 1152 1151 9.05 0.47 1153 1152 9.05 0.47 1154 1153 9.06 0.48 1155 1154 9.06 0.48 1155 1154 9.06 0.48 1157 1156 9.04 0.46 1158 1157 9.06 0.48 1159 1158 9.05 0.47 1160 1159 9.05 0.47 1161 1160 9.05 0.47 1162 1161 9.05 0.47 1163 1162 9.05 0.47 1164 1163 9.05 0.47 1165 1164 9.05 0.47	1145	1144	9.06	0.48
1148 1147 9.05 0.47 1149 1148 9.06 0.48 1150 1149 9.06 0.48 1151 1150 9.06 0.48 1152 1151 9.05 0.47 1153 1152 9.05 0.47 1154 1153 9.06 0.48 1155 1154 9.06 0.48 1156 1155 9.05 0.47 1157 1156 9.04 0.46 1158 1157 9.06 0.48 1159 1158 9.05 0.47 1160 1159 9.05 0.47 1161 1160 9.05 0.47 1162 1161 9.05 0.47 1163 1162 9.05 0.47 1164 1163 9.05 0.47 1165 1164 9.05 0.47 1166 1165 9.06 0.48	1146	1145	9.05	0.47
1149 1148 9.06 0.48 1150 1149 9.06 0.48 1151 1150 9.06 0.48 1152 1151 9.05 0.47 1153 1152 9.05 0.47 1154 1153 9.06 0.48 1155 1154 9.06 0.48 1156 1155 9.05 0.47 1157 1156 9.04 0.46 1158 1157 9.06 0.48 1159 1158 9.05 0.47 1160 1159 9.05 0.47 1161 1160 9.05 0.47 1162 1161 9.05 0.47 1163 1162 9.05 0.47 1164 1163 9.05 0.47 1165 1164 9.05 0.47 1166 1165 9.06 0.48 1167 1166 9.05 0.47	1147	1146	9.05	0.47
1150 1149 9.06 0.48 1151 1150 9.06 0.48 1152 1151 9.05 0.47 1153 1152 9.05 0.47 1154 1153 9.06 0.48 1155 1154 9.06 0.48 1156 1155 9.05 0.47 1157 1156 9.04 0.46 1158 1157 9.06 0.48 1159 1158 9.05 0.47 1160 1159 9.05 0.47 1161 1160 9.05 0.47 1162 1161 9.05 0.47 1163 1162 9.05 0.47 1164 1163 9.05 0.47 1165 1164 9.05 0.47 1166 1165 9.06 0.48 1167 1166 9.05 0.47 1168 1167 9.05 0.47	1148	1147	9.05	0.47
1151 1150 9.06 0.48 1152 1151 9.05 0.47 1153 1152 9.05 0.47 1154 1153 9.06 0.48 1155 1154 9.06 0.48 1156 1155 9.05 0.47 1157 1156 9.04 0.46 1158 1157 9.06 0.48 1159 1158 9.05 0.47 1160 1159 9.05 0.47 1161 1160 9.05 0.47 1162 1161 9.05 0.47 1163 1162 9.05 0.47 1164 1163 9.05 0.47 1165 1164 9.05 0.47 1166 1165 9.06 0.48 1167 1168 9.05 0.47 1168 1167 9.05 0.47 1169 1168 9.05 0.47	1149	1148	9.06	0.48
1152 1151 9.05 0.47 1153 1152 9.05 0.47 1154 1153 9.06 0.48 1155 1154 9.06 0.48 1156 1155 9.05 0.47 1157 1156 9.04 0.46 1158 1157 9.06 0.48 1159 1158 9.05 0.47 1160 1159 9.05 0.47 1161 1160 9.05 0.47 1162 1161 9.05 0.47 1163 1162 9.05 0.47 1164 1163 9.05 0.47 1165 1164 9.05 0.47 1166 1165 9.06 0.48 1167 1168 9.05 0.47 1168 1167 9.05 0.47 1169 1169 9.05 0.47 1170 1169 9.05 0.47	1150	1149	9.06	0.48
1153 1152 9.05 0.47 1154 1153 9.06 0.48 1155 1154 9.06 0.48 1156 1155 9.05 0.47 1157 1156 9.04 0.46 1158 1157 9.06 0.48 1159 1158 9.05 0.47 1160 1159 9.05 0.47 1161 1160 9.05 0.47 1162 1161 9.05 0.47 1163 1162 9.05 0.47 1164 1163 9.05 0.47 1165 1164 9.05 0.47 1166 1165 9.06 0.48 1167 1168 9.05 0.47 1168 1167 9.05 0.47 1169 1169 9.05 0.47 1170 1169 9.05 0.47	1151	1150	9.06	0.48
1154 1153 9.06 0.48 1155 1154 9.06 0.48 1156 1155 9.05 0.47 1157 1156 9.04 0.46 1158 1157 9.06 0.48 1159 1158 9.05 0.47 1160 1159 9.05 0.47 1161 1160 9.05 0.47 1162 1161 9.05 0.47 1163 1162 9.05 0.47 1164 1163 9.05 0.47 1165 1164 9.05 0.47 1166 1165 9.06 0.48 1167 1166 9.05 0.47 1168 1167 9.05 0.47 1169 1169 9.05 0.47	1152	1151	9.05	0.47
1155 1154 9.06 0.48 1156 1155 9.05 0.47 1157 1156 9.04 0.46 1158 1157 9.06 0.48 1159 1158 9.05 0.47 1160 1159 9.05 0.47 1161 1160 9.05 0.47 1162 1161 9.05 0.47 1163 1162 9.05 0.47 1164 1163 9.05 0.47 1165 1164 9.05 0.47 1166 1165 9.06 0.48 1167 1168 9.05 0.47 1168 1167 9.05 0.47 1169 1169 9.05 0.47	1153	1152	9.05	0.47
1156 1155 9.05 0.47 1157 1156 9.04 0.46 1158 1157 9.06 0.48 1159 1158 9.05 0.47 1160 1159 9.05 0.47 1161 1160 9.05 0.47 1162 1161 9.05 0.47 1163 1162 9.05 0.47 1164 1163 9.05 0.47 1165 1164 9.05 0.47 1166 1165 9.06 0.48 1167 1168 9.05 0.47 1168 1167 9.05 0.47 1169 9.05 0.47 1170 1169 9.05 0.47	1154	1153	9.06	0.48
1157 1156 9.04 0.46 1158 1157 9.06 0.48 1159 1158 9.05 0.47 1160 1159 9.05 0.47 1161 1160 9.05 0.47 1162 1161 9.05 0.47 1163 1162 9.05 0.47 1164 1163 9.05 0.47 1165 1164 9.05 0.47 1166 1165 9.06 0.48 1167 1166 9.05 0.47 1168 1167 9.05 0.47 1169 1169 9.05 0.47	1155	1154	9.06	0.48
1158 1157 9.06 0.48 1159 1158 9.05 0.47 1160 1159 9.05 0.47 1161 1160 9.05 0.47 1162 1161 9.05 0.47 1163 1162 9.05 0.47 1164 1163 9.05 0.47 1165 1164 9.05 0.47 1166 1165 9.06 0.48 1167 1166 9.05 0.47 1168 1167 9.05 0.47 1169 1169 9.05 0.47 1170 1169 9.05 0.47	1156	1155	9.05	0.47
1159 1158 9.05 0.47 1160 1159 9.05 0.47 1161 1160 9.05 0.47 1162 1161 9.05 0.47 1163 1162 9.05 0.47 1164 1163 9.05 0.47 1165 1164 9.05 0.47 1166 1165 9.06 0.48 1167 1166 9.05 0.47 1168 1167 9.05 0.47 1169 1169 9.05 0.47 1170 1169 9.05 0.47	1157	1156	9.04	0.46
1160 1159 9.05 0.47 1161 1160 9.05 0.47 1162 1161 9.05 0.47 1163 1162 9.05 0.47 1164 1163 9.05 0.47 1165 1164 9.05 0.47 1166 1165 9.06 0.48 1167 1166 9.05 0.47 1168 1167 9.05 0.47 1169 1169 9.05 0.47 1170 1169 9.05 0.47	1158	1157	9.06	0.48
1161 1160 9.05 0.47 1162 1161 9.05 0.47 1163 1162 9.05 0.47 1164 1163 9.05 0.47 1165 1164 9.05 0.47 1166 1165 9.06 0.48 1167 1166 9.05 0.47 1168 1167 9.05 0.47 1169 1169 9.05 0.47 1170 1169 9.05 0.47	1159	1158	9.05	0.47
1162 1161 9.05 0.47 1163 1162 9.05 0.47 1164 1163 9.05 0.47 1165 1164 9.05 0.47 1166 1165 9.06 0.48 1167 1166 9.05 0.47 1168 1167 9.05 0.47 1169 1169 9.05 0.47 1170 1169 9.05 0.47	1160	1159	9.05	0.47
1163 1162 9.05 0.47 1164 1163 9.05 0.47 1165 1164 9.05 0.47 1166 1165 9.06 0.48 1167 1166 9.05 0.47 1168 1167 9.05 0.47 1169 1168 9.05 0.47 1170 1169 9.05 0.47	1161	1160	9.05	0.47
1164 1163 9.05 0.47 1165 1164 9.05 0.47 1166 1165 9.06 0.48 1167 1166 9.05 0.47 1168 1167 9.05 0.47 1169 1168 9.05 0.47 1170 1169 9.05 0.47	1162	1161	9.05	0.47
1165 1164 9.05 0.47 1166 1165 9.06 0.48 1167 1166 9.05 0.47 1168 1167 9.05 0.47 1169 1168 9.05 0.47 1170 1169 9.05 0.47	1163	1162	9.05	0.47
1166 1165 9.06 0.48 1167 1166 9.05 0.47 1168 1167 9.05 0.47 1169 1168 9.05 0.47 1170 1169 9.05 0.47	1164	1163	9.05	0.47
1167 1166 9.05 0.47 1168 1167 9.05 0.47 1169 1168 9.05 0.47 1170 1169 9.05 0.47	1165	1164	9.05	0.47
1168 1167 9.05 0.47 1169 1168 9.05 0.47 1170 1169 9.05 0.47	1166	1165	9.06	0.48
1168 1167 9.05 0.47 1169 1168 9.05 0.47 1170 1169 9.05 0.47	1167	1166	9.05	0.47
1169 1168 9.05 0.47 1170 1169 9.05 0.47				
1170 1169 9.05 0.47			<u> </u>	
11/1 11/0 9.05 0.47	1171	1170	9.05	0.47
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Number: 10-025-2

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	Time	Water Level	Drawdown
1172	[min]	[m] 9.05	[m] 0.47
	1171 1172	9.05	0.47
1173	1173	9.05	0.47
1174			
1175	1174	9.05	0.47
1176	1175	9.05	
1177	1176	9.04	0.46
1178	1177	9.05	0.47
1179	1178	9.05	0.47
1180	1179	9.05	0.47
1181	1180	9.05	0.47
1182	1181	9.05	0.47
1183	1182	9.04	0.46
1184	1183	9.05	0.47
1185	1184	9.05	0.47
1186	1185	9.05	0.47
1187	1186	9.05	0.47
1188	1187	9.04	0.46
1189	1188	9.04	0.46
1190	1189	9.05	0.47
1191	1190	9.05	0.47
1192	1191	9.04	0.46
1193	1192	9.05	0.47
1194	1193	9.04	0.46
1195	1194	9.04	0.46
1196	1195	9.04	0.46
1197	1196	9.04	0.46
1198	1197	9.04	0.46
1199	1198	9.04	0.46
1200	1199	9.04	0.46
1201	1200	9.04	0.46
1202	1201	9.04	0.46
1203	1202	9.04	0.46
1204	1203	9.03	0.45
1205	1204	9.04	0.46
1206	1205	9.04	0.46
1207	1206	9.04	0.46
1207	1207	9.04	0.46
1209	1208	9.03	0.45
1210	1209	9.03	0.45
1211	1210	9.04	0.46
1212	1211	9.04	0.46
1213	1212	9.04	0.46
1214	1213	9.03	0.45
		 	0.45
1215	1214	9.03	0.45
1216	1215	9.04	0.46
1217	1216	9.04	0.46
1218	1217	9.04	
1219	1218	9.04	0.46
1220	1219	9.04	0.46
1221	1220	9.04	0.46
1222	1221	9.03	0.45
1223	1222	9.04	0.46
1224	1223	9.03	0.45
1225	1224	9.03	0.45
1226	1225	9.04	0.46
1227	1226	9.03	0.45



Pumping Test - Water Level Dat	Pumping	Test -	Water	Level	Data
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Number: 10-025-2

		\	<u> </u>
	Time [min]	Water Level [m]	Drawdown [m]
1228		9.03	0.45
1229		9.03	0.45
1230			0.45
		9.03	
1231		9.03	0.45
1232		9.03	0.45
1233		9.03	0.45
1234		9.03	0.45
1235		9.03	0.45
1236	. 	9.04	0.46
1237		9.04	0.46
1238		9.03	0.45
1239		9.03	0.45
1240		9.03	0.45
1241		9.03	0.45
1242		9.03	0.45
1243		9.03	0.45
1244		9.03	0.45
1245		9.03	0.45
1246		9.03	0.45
1247		9.03	0.45
1248		9.03	0.45
1249	1248	9.03	0.45
1250	1249	9.03	0.45
1251	1250	9.03	0.45
1252	1251	9.03	0.45
1253	1252	9.03	0.45
1254	1253	9.03	0.45
1255	1254	9.02	0.44
1256	1255	9.03	0.45
1257	1256	9.03	0.45
1258	1257	9.03	0.45
1259	1258	9.03	0.45
1260	1259	9.03	0.45
1261	1260	9.03	0.45
1262	1261	9.03	0.45
1263	1262	9.03	0.45
1264	1263	9.03	0.45
1265	1264	9.03	0.45
1266	1265	9.03	0.45
1267	1266	9.03	0.45
1268	1267	9.03	0.45
1269	1268	9.02	0.44
1270	1269	9.02	0.44
1271	1270	9.03	0.45
1272	1271	9.02	0.44
1273	1272	9.03	0.45
1274	1273	9.02	0.44
1275	1274	9.03	0.45
1276	1275	9.03	0.45
1277	1276	9.03	0.45
1278	1277	9.02	0.44
1279	1278	9.02	0.44
1280	1279	9.03	0.45
1281	1280	9.03	0.45
1282	1281	9.03	0.45
1283	1282	9.03	0.45



Pumping Test -	Water L	_evel	Data
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Project: Highland Park Hydrogeological Assessment

Number: 10-025-2

1	Time	Water Level	Drawdown
100	[min]	[m]	[m]
128		9.03	0.45
128		9.02	0.44
128		9.03	0.45
128	·	9.02	0.44
128	· + · · · · · · · · · · · · · · · · · ·	9.03	0.45
1289		9.03	0.45
1290		9.02	0.44
129		9.02	0.44
1292		9.02	0.44
1293		9.01	0.43
1294		9.02	0.44
1295	1294	9.02	0.44
1296	1295	9.02	0.44
1297	1296	9.02	0.44
1298	1297	9.01	0.43
1299	1298	9.01	0.43
1300	1299	9.02	0.44
1301	1300	9.01	0.43
1302	1301	9.02	0.44
1303	1302	9.02	0.44
1304	1303	9.02	0.44
1305	1304	9.02	0.44
1306	1305	9.01	0.43
1307	1306	9.02	0.44
1308	1307	9.02	0.44
1309	1308	9.02	0.44
1310	1309	9.01	0.43
1311	1310	9.02	0.44
1312	1311	9.02	0.44
1313	1312	9.02	0.44
1314	1313	9.01	0.43
1315	1314	9.02	0.44
1316	1315	9.01	0.43
1317	1316	9.01	0.43
1318	1317	9.01	0.43
1319	1318	9.01	0.43
1320	1319	9.01	0.43
1321	1320	9.00	0.42
1322	1321	9.01	0.43
1323	1322	9.01	0.43
1324	1323	9.01	0.43
1325	1324	9.01	0.43
1326	1325	9.01	0.43
1327	1326	9.02	0.44
1328	1327	9.01	0.43
1329	1328	9.01	0.43
1330	1329	9.01	0.43
1331	1330	9.01	0.43
1332	1331	9.01	0.43
1333	1332	9.01	0.43
1334	1333	9.01	0.43
1335	1334	9.01	0.43
1336	1335	9.01	0.43
1337	1336	9.01	0.43
1338	1337	9.01	0.43
1339	1338	9.01	0.43



Pumping Test - Water Level I	Pumping	Test -	Water	Level	Data
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Project: Highland Park Hydrogeological Assessment

Number: 10-025-2

	Time	Water Level	Drawdown
1240	[min] 1339	[m] 9.01	[m] 0.43
1340			
1341	1340	9.01	0.43
1342	1341	9.01	0.43
1343	1342	9.00	0.42
1344	1343	9.01	0.43
1345	1344	9.01	0.43
1346	1345	9.01	0.43
1347	1346	9.01	0.43
1348	1347	9.01	0.43
1349	1348	9.00	0.42
1350	1349	9.00	0.42
1351	1350	9.01	0.43
1352	1351	9.00	0.42
1353	1352	9.00	0.42
1354	1353	9.00	0.42
1355	1354	9.01	0.43
1356	1355	9.01	0.43
1357	1356	9.00	0.42
1358	1357	9.00	0.42
1359	1358	9.00	0.42
1360	1359	9.00	0.42
1361	1360	9.00	0.42
1362	1361	9.00	0.42
1363	1362	9.00	0.42
1364	1363	9.01	0.43
1365	1364	9.01	0.43
1366	1365	9.00	0.42
1367	1366	9.00	0.42
1368	1367	9.01	0.43
1369	1368	9.00	0.42
1370	1369	9.00	0.42
1371	1370	9.00	0.42
1372	1371	9.00	0.42
1373	1372	9.00	0.42
1374	1373	9.01	0.43
1375	1374	9.01	0.43
1376	1375	9.01	0.43
1377	1376	9.01	0.43
1378	1377	9.00	0.42
1379	1378	9.01	0.43
1380	1379	9.01	0.43
1381	1380	9.01	0.43
1382	1381	9.00	0.42
1383	1382	9.00	0.42
1384	1383	9.00	0.42
1385	1384	9.01	0.43
1386	1385	9.00	0.42
1387	1386	9.00	0.42
1388	1387	9.00	0.42
1389	1388	9.00	0.42
1390	1389	9.00	0.42
1391	1390	9.00	0.42
1392	1391	9.00	0.42
1393	1392	9.00	0.42
1394	1393	9.00	0.42
1395	1394	9.00	0.42



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Project: Highland Park Hydrogeological Assessment

Number: 10-025-2

		\	
	Time	Water Level	Drawdown
	[min]	[m]	[m]
1396		8.99	0.41
1397		8.99	0.41
1398		9.00	0.42
1399		9.00	0.42
1400		9.00	0.42
1401	1400	9.00	0.42
1402	1401	8.99	0.41
1403	1402	8.99	0.41
1404	1403	9.00	0.42
1405	1404	8.99	0.41
1406	1405	8.99	0.41
1407	1406	9.00	0.42
1408	1407	9.00	0.42
1409	1408	9.00	0.42
1410	1409	8.99	0.41
1411	1410	8.99	0.41
1412	1411	8.99	0.41
1413	1412	8.99	0.41
1414	1413	8.99	0.41
1415	1414	8.99	0.41
1416	1415	8.99	0.41
1417	1416	8.99	0.41
1418	1417	8.99	0.41
1419	1418	8.99	0.41
1420	1419	8.99	0.41
1421	1420	8.99	0.41
1422	1421	9.00	0.42
1423	1422	9.00	0.42
1424	1423	8.99	0.41
1425	1424	8.99	0.41
1426	1425	8.99	0.41
1427	1426	8.99	0.41
1428	1427	8.99	0.41
1429	1428	8.99	0.41
1430	1429	8.99	0,41
1431	1430	8.99	0.41
1432	1431	8.99	0.41
1433	1432	8.99	0.41
1434	1433	8.99	0.41
1435	1434	8.99	0.41
1436	1435	8.99	0.41
1437	1436	8.99	0.41
1438	1437	8.99	0.41
1439	1438	8.99	0.41
1440	1439	8.99	0.41
1441	1440	8.99	0.41
1442	1441	8.98	0.41
1443	1442	8.98	0.40
1444	1443	8.99	0.41
1445	1443	8.99	0.41
1446	1444	8.98	0.40
1447	1446	8.99	0.41
1448	1447	8.98	0.40
1449	1448	8.98	0.40
1450	1449	8.97	0.39
1451	1450	8.98	0.40



Pumping Test - Wa	ter Level Data
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Project: Highland Park Hydrogeological Assessment

Number: 10-025-2

		\	
	Time [min]	Water Level [m]	Drawdown [m]
1452	1451	8.97	0.39
1453	1452	8.99	0.41
1454	1453	8.97	0.39
1455	1454	8.97	0.39
1456	1455	8.97	0.39
1457	1456	8.97	0.39
1458	1457	8.97	0.39
1459	1458	8.98	0.40
1460	1459	8.97	0.39
1461	1460	8.97	0.39
1462	1461	8.97	0.39
1463	1462	8.96	0.38
1464	1463	8.96	0.38
1465	1464	8.96	0.38
1466	1465	8.97	0.39
1467	1466	8.96	0.38
1468	1467	8.96	0.38
1469	1468	8.96	0.38
1470	1469	8.98	0.40
1471	1470	8.97	0.39
1472	1471	8.96	0.38
1473	1472	8.96	0.38
1474	1473	8.96	0.38
1475	1474	8.97	0.39
1476	1475	8.97	0.39
1477	1476	8.96	0.38
1478	1477	8.96	0.38
1479	1478	8.96	0.38
1480	1479	8.97	0.39
1481	1480	8.96	0.38
1482	1481	8.96	0.38
1483	1482	8.96	0.38
1484	1483	8.96	0.38
1485	1484	8.97	0.39
1486	1485	8.96	0.38
1487	1486	8.96	0.38

July 2010 Our ref: 10-025

APPENDIX J SIX HOUR PUMP TEST WATER TEST RESULTS EXOVA ACCUTEST REPORTS OF ANALYSES



Client: Houle Chevrier Engineering 180 Wescar Lane, R.R. #2 Carp, ON KOA 1L0 Attention: Mr. James McEwen

1010895 2010-05-21 2010-05-18 Report Number: Date: Date Submitted:

10-025-2	Water GUIDELINE
Project:	P.O. Number: Matrix:
	LAB ID: 797757 797758 Sample Date: 2010-05-18 2010-05-18
AMERICAN MIL CALIFOS MICEWER	Chain of Custody Number: 120931

10071 100000							Matrix:		Water	ter	
	(797757	797758				 -	130	GUIDELINE	
	Samp		2010-05-18	2010-05-18							
	Sa	Sample ID:	TW1-SA6	TW1-SA7				<u> </u>	č		
									5		
PARAMETER	UNITS	MR							-		
Total Coliforms	CF11/100ml	1	u	0				TYPE	1	_	UNITS
Escherichia Coli	CF1 //100ml		o c	0 0	_			MAC	 o	0	CFU/100mL
Heterotrophic Plate Count	CE1/1m		> 6	> •				MAC	 o		CFU/100mL
Faecal Coliforms	0 0 0		4,	_							
Faecal Streetococcus	CTO/100mL		0	0							
	E001/010			0							
									-		
		-									
								=-7-1			
									,		
								-			
											
											-
		•									
				_	_	_		_	_		

MRL = Method Reporting Limit INC = Incomplete AO = Aesthetic Objective OG = Operational Guideline MAC = Maximum Allowable Concentration IMAC = Interim Maximum Allowable Concentration Comment:

APPROVAL:

Krista Quantrill

Drinking Water Coordinator

Results relate only to the parameters tested on the samples submitted.

EXCVQ Accutest

Client: Houle Chevrier Engineering 180 Wescar Lane, R.R. #2

Carp, ON

K0A 1L0

Attention: Mr. James McEwen

Chain of Custody Number: 120931

Report Number: Date: Date Submitted:

1010894 2010-05-27 2010-05-18

10-025-2

Project:

P.O. Number:

							Matrix:		Water	
		LAB ID:	797755	797756					GIIDEI INE	
	Sam	Sample Date:	2010-05-18	2010-05-18					COIDELINE	
	ιχ	Sample ID:	TW1-SA6	TW1-SA7						
									ODWSOG	
PARAMETER	OTHAIL									
Alkalinity as CaCO3	CINO	MKL						TYPE	LIMIT	UNITS
Chloride	mg/L	ဌ	237	238				8	500	l/om
	mg/L	-	82	130				04	250	1/600
Colour	TCU	2	7	<2				9 9	000	1.0/L
Conductivity	mS/cm	2	800	1050		-		2	ס	3
Dissolved Organic Carbon	mg/L	0.5	1.7	1.3				(ų	-
Fluoride	mg/L	0.1	1.68	2.12	-			2 5	o ,	rng/L
Hydrogen Sulphide	mg/L	0.01	0.17	0.75						mg/L
N-NH3 (Ammonia)	mg/L	0.02	0.26	0.32				Ş	cn.0	mg/L
N-NO2 (Nitrite)	mg/L	0.1	<0.10	<0.10						:
N-NO3 (Nitrate)	mg/L	0.1	<0.10	<0.10				MAC.	0.1	mg/L
Ha)		8 22	2 6				MAC	0.01	mg/L
Phenols	ma/l	0.001	0.00	0.00					6.5-8.5	
Sulphate	, e	-	700.0	000.0						
Tannin & Lianin	111g/L	- ;	t 45	9/				AO	200	mg/L
Total Discolved Solids (OND OND O	mg/L	L.O	0.1	9.4						1
Total Kipldoh Nittons	mg/L	2	520	683				AO	200	ma/l
Total Nethalii Nitrogen	mg/L	0.1	0.25	0.38		-				l D
lurbidity	NTO	0.1	11.2	22.9				MAC	-	Ę
Hardness as CaCO3	mg/L	τ-	128	121	-			ي ا	5. 5	2 5
lon Balance		0.01	1.00	1.01				3	2	1/g:
Calcium	mg/L	~	30	27						
Magnesium	mg/L	<u>_</u>	13	13						
Potassium	mg/L	τ-	2	2						
Sodium	mg/L	2	123	177				OA	000	1/000
lron	mg/L	0.03	0.16	0.08) \ \	~ ~ ~	1/6m
Manganese	mg/L	0.01	<0.01	<0.01				2 4	30.0	118/L
	,						_	?	20.5	119/L

MRL = Method Reporting Limit INC = Incomplete AO = Aesthetic Objective OG = Operational Guideline MAC = Maximum Allowable Concentration IMAC = Interim Maximum Allowable Concentration Comment:

Inorganic Lab Supervisor APPROVAL:

Ewan McRobbie

Results relate only to the parameters tested on the samples submitted.

July 2010 Our ref: 10-025

APPENDIX K POST-HYDRO FRACTURING SUPPLEMENTAL WATER TEST RESULTS EXOVA ACCUTEST REPORTS OF ANALYSES

REFURT OF ANALYSIS



Client: Houle Chevrier Engineering 180 Wescar Lane, R.R. #2 Carp, ON K0A 1L0

1012849 2010-06-10 2010-06-09 10-11025-2 Report Number: Date: Date Submitted: P.O. Number: Project: Chain of Custody Number: 120933 Attention: Mr. James McEwen

					Matrix:		Water	
	LAB ID:	803539	803540				בוווסבו זאונ	
	Sample Date:	2010-06-09	2010-06-09				GOIDELINE	
	Sample ID:	: TW1-B3 TW1-B4	TW1-B4					
							ODWSOG	
PARAMETER	TIMIT							
Coliforms	ONI S MRL					TVPF	IMIT	OFINIT
	CE 1/100m1	c	,					20
				•	•			

	UNITS	CFU/100mL	
	LIMIT	0	
	TYPE	MAC	-
+			_
		0	
	,	0	
1.	1		
1	MR.		
LINITO	00110	CFU7100m	
2			
PARAMETER			
Ā			
	rms		
	Total Coliforms		
	Tog		

MRL = Method Reporting Limit INC = Incomplete AO = Aesthetic Objective OG = Operational Guideline MAC = Maximum Allowable Concentration IMAC = Interim Maximum Allowable Concentration Comment:



Results relate only to the parameters tested on the samples submitted.

July 2010 Our ref: 10-025

APPENDIX L

CORRESPONDANCE WITH LOCAL MEDICAL OFFICER OF HEALTH



Houle Chevrier Engineering Ltd.

180 Wescar Lane, R.R. 2, Carp, Ontario, K0A 1L0 Ph: (613) 836-1422 Fax: (613) 836-9731

Facsimile Transmission

Date Sent:

June 7, 2010

Our Ref: 10-025

To:

Jean Guy Albert

Ottawa Public Health

Fax No.:

613-580-9648

From:

James McEwen, B.Sc., B.Eng.

RE:

FLUORIDE AND SODIUM CONCENTRATIONS IN PRIVATE WELL. 2037 MCGEE

SIDE ROAD, CARP, ONTARIO

Total number of pages (including this cover page): 1

As per the Ontario Drinking Water Standards, this facsimile is to inform you of fluoride concentrations exceeding 1.5 milligrams per litre and sodium concentrations exceeding 20 mg/L that were detected during routine sampling of the private well located at the above referenced site in March 2010. The analytical results are summarized as follows:

- Feb. 19, 2010 Fluoride Concentration = 3.17 mg/L; Sodium Concentration = 125 mg/L
- March 5, 2010 Fluoride Concentration = 2.71 mg/L
- March 16, 2010 Fluoride Concentration = 2.94 mg/L
- March 18, 2010 Fluoride Concentration = 3.32 mg/L

The test well was hydro fractured on April 30, 2010 to improve the water quality. Subsequent testing is summarized as follows:

- May 5, 2010 Fluoride Concentration = 1.93 mg/L
- May 18, 2010 Fluoride Concentration = 1.68 to 2.12 mg/L; Sodium Concentration = 123 to 177 mg/L

The 2037 McGee Side Road property is occupied by the Highland Park Cemetery and owned by Pinecrest Remembrance Services Ltd. (Pinecrest). The water well is currently not connected to a building or currently in use.

We trust that this information is satisfactory. Should you have any questions or concerns regarding these sample results, please do not hesitate to call the undersigned.

Yours truly,

HOULE CHEVRIER ENGINEERING LTD.

James McEwen, B.Sc., B.Eng.

Hydrogeologist



June 9, 2010

James McEwen Houle Chevrier Engineering Ltd. 180 Wescar Lane R.R. 2 Carp, ON K0A 1L0

Dear Mr. McEwen,

Re: Drinking Water Advisory 2037 McGee Side Road, Carp

In your June 7, 2010 letter to Ottawa Public Health you indicated that the analyses of water samples taken from a well located at 2037 McGee Side Road, Carp show that the concentration of Fluoride in the water is in the range of 1.68 to 2.12 mg/L, and that the concentration of Sodium in the water is in the range of 123 to 177 mg/L. It is our understanding that the well is presently not connected to a building and that it is not in use. Should the well be activated, the below cited information must be shared with the people who will use the well water for consumption purposes.

The Maximum Acceptable Concentration for Fluoride in drinking water is 1.5 mg/L however, where water supplies contain naturally occurring Fluoride at concentrations above 1.5 mg/L but below 2.4 mg/L, the Ontario Ministry of Health recommends that people who consume the water be informed of the Fluoride concentration, and be advised to control excessive exposure to Fluoride from other sources, such as from Fluoride treatments, or from Fluoride supplements.

The health-based advisory concentration for Sodium in drinking water is 20 mg/L. People who are on a Sodium-restricted diet or suffering from hypertension, congestive heart disease or kidney disease, should consult with their physician regarding the use of the water for consumption purposes.

If you have any questions regarding this letter, please contact me at 613 580-6744 ext. 23653.

Jean-Guy Albert Program Manager

Ottawa Public Health

cc: File



July 2010 Our ref: 10-025

APPENDIX M

THEIS ANALYSIS

AQUIFER TEST PRO

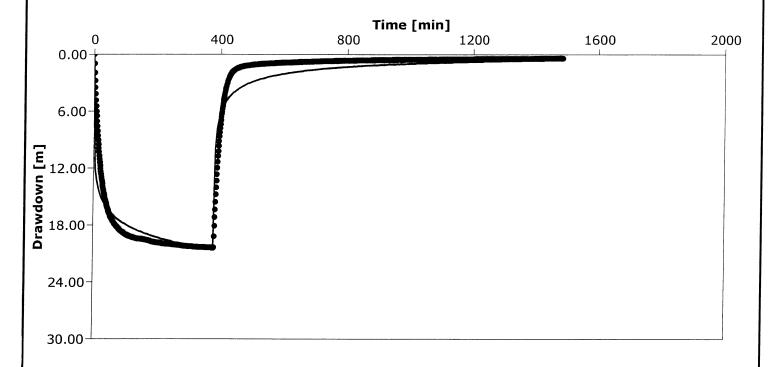


Project: Highland Park Hydrogeological Assessment

Number: 10-025-2

Client: Pinecrest Remembrance Services Ltd.

Location: 2037 McGee Side Road, Ottawa, Ontario	Pumping Test: Pumping Test 1	Pumping Well: TW1
Test Conducted by:		Test Date: 5/27/2010
Analysis Performed by: JM	Theis Analysis	Analysis Date: 5/27/2010
Aquifer Thickness:	Discharge: variable, average rate 0.0043434 [m³/min]	



Calculation after Theis				
Observation Well	Transmissivity	Storage coefficient	Radial Distance to PW	
	[m²/d]		[m]	
TW1a	1.31 × 10 ⁰	1 15 × 10 ⁻³	0.15	

July 2010 Our ref: 10-025

APPENDIX N OFFSITE PRIVATE WATER WELL RECORDS ONTARIO MINISTRY OF ENVIRONMENT

	Well Con	nputer Prin	t Out Dat	a as of Fet	Well Computer Print Out Data as of February 19 2010	© Queen's Printer, 2009	. 2009 Page: 1 / 10
TOWNSHIP CONCESSION (LOT)	UTM ¹	DATE ² CNTR ³	CASING DIA 4	WATER ^{5,6} DETAIL	STAT LVL/PUMP LVL 7 RATE 8 /TIME HR:MIN	WATER SCREEN USE^9 INFO 10	WELL # (AUDIT#) WE: THS TO WHICH FORMATION
	18 421578 5017602 ^w	2008/01 1119	00	0256 0270	008 / 083 005 / 1:0	DO	7104179 (Z61198) A072334 SAND GRVL 0040 GREN LMSN 0280
HUNTLEY TOWNSHIP CON 01(010)	18 423466 5019312 ^W	1966/06 4806	04 04	SU 0370 SU 0410 SU 0185	020 / 152 015 / 1:0	ST DO	1503027 () BLUE CLAY 0026 GREY LMSN 0416
HUNTLEY TOWNSHIP CON 01(010)	18 423525 5019433 ¹	2003/10	90 90	UK 0350 UK 0450	025 / 300 004 / 1:0	DO	1534376 (264065) BRWN SAND 0003 GREY GRNT 0460
HUNTLEY TOWNSHIP CON 01(010)	18 423525 5019433 ^L	2001/11 6574	90 90	UK 0240 UK 0460	004 / 450 005 / 8:0	DO	619 (; LOAM BLUE HARD
HUNTLEY TOWNSHIP CON 01(011)	18 423127 5019896 ^L	1987/10 1558	90 90	FR 0041	026 / 035 020 / 2:0	DO	GRNT HARD 0500 88 (25112) CLAY PCKD 0012 GREY
HUNTLEY TOWNSHIP CON 01(011)	18 421530 5018621 ^W	1982/06 3504	90	FR 0125	026 / 120 020 / 0:30	OQ	MENG 0035 GREY LMSN MGRD HARD 0070 1517897 () BLUE CLAY 0008 BLCK GRNT 0128
HUNTLEY TOWNSHIP CON 01(011)	18 423655 5020188 ^W	1975/03 1558	90 90	FR 0340	020 / 250 001 / 1:0	DO	591 () CLAY BLDR PCKD 0015
HUNTLEY TOWNSHIP CON 01(011)	18 423122 5019897 ^L	2002/10 6574	90 90	FR 0145	004 / 026 150 / 20:0	DO 0141	GRNT HARD 0398 4) PCKD 0026 BLUE
HUNTLEY TOWNSHIP CON 01(011)	18 423127 5019896 ^L	1997/11 1558	90 90	UK 0116	015 / 250 001 / 1:0	DO	1139 GREI SAND 122 (182713) LOAM STNS 0004 0110 GREY GRNT MGRD 0220 GREY
HUNTLEY TOWNSHIP CON 01(012)	18 422728 5020358 ^L	1998/12 1558	90 90 90		011 / 075 001 / 1:0	ST	1530432 (194809) 1530432 (194809) SOFT 0139 GREY GRNT HARD 0250
CON 01(012)	18 422724 5020358 ^L	2003/09	90	UK 0103	021 / 043 008 / 4:0	DO	l .
HUNTLEY TOWNSHIP CON 01 (012)	18 422728 5020358 ^L	1998/12 1558	90 90	UK 0187 UK 0137 UK 0123	015 / 100 025 / 1:0	TS	1530431 (194808) BRWN CLAY PCKD 0021 GREY CLAY STKY 0037 GREY CLAY 0045 GREY CLAY PCKD
	18 422728 5020358 ^L	1998/12 1558	90 90	UK 0275 UK 0275	004 / 275 003 / 1:0	T.S.	GREY GREY GRNT GRNT
HUNTLEY TOWNSHIP CON 01(012)	18 422728 5020358 ^L	1998/11 3323	90	FR 0220	012 / 225 010 / 1:30	DO	420 (19122) CLAY 0011

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TOWNSHIP CONCESSION (LOT)	\mathtt{UTM}^1	DATE 2 CNTR 3	CASING DIA 4	WATER ^{5,6}	STAT LVL/PUMP LVL 7 RATE 8 /TIME HR:MIN		WELL # (AUDIT#) WELL TAG # THS TO WHICH FORMATIONS EXTEN
HUNTLEY TOWNSHIP CON 01(014)	18 421631 5020432 ^W	1967/05 3601	0.5	FR 0064	012 / 018 008 / 3:0	DO	1503034 () CLAY LOAM 0
HUNTLEY TOWNSHIP CON 02(008)	18 423726 5018048 ^W	2004/09	90	0124	006 / 020 012 / 1:0	DO	1535002 (Z10644) A010620 GREY CLAY DNSE 0008 GREY CLAY SOFT 0018 GREY SAND 0020 GREY GRVL SNDS
HUNTLEY TOWNSHIP CON 02(008)	18 423303 5017601 ^L	2001/07 3323	90	SU 0050 SU 0250	005 / 260 008 / 1:0	DO	DERWIN 109 (2 CLAY
HUNTLEY TOWNSHIP CON 02(008)	18 423307 5017600 ^L	1991/05 1558	90 90	UK 0289	025 / 200 002 / 1:0	DO	SHLE LMSN 0260 1525420 (100071) BRWN CLAY SAND DRY 0008 GREY HPAN BLDR
HUNTLEY TOWNSHIP CON 02(008)	18 423307 5017600 ^L	1991/06 1558	90 90	UK 0219	030 / 175 003 / 1:0	DO	1525480 (101330) BRWN CLAY STUS PCKD 0006 GREY GRVL
HUNTLEY TOWNSHIP CON 02(008)	18 423303 5017601 ^L	2001/10 1558	90 90	UK 0025 UK 0045	004 / 025 015 / 1:0	DO	GOLD GREI LMSN MGVL 30284) 0005 GREY SAND GRVL GRVL FCRD ROCK 0024
HUNTLEY TOWNSHIP CON 02(008)	18 423307 5017600 ^L	1992/09 1558	90 90	UK 0243 UK 0049	006 / 200 005 / 1:30	DO	LAMAN 0050 1526582 (60325) BRWN CLAY SNDY STNS 0005 GREY SAND BLDR 0016 GREY LMSN 0250
HUNTLEY TOWNSHIP CON 02(009)	18 422890 5018910 ^L	1998/06 4875	06 06	UK 0164	006 / 007 012 / 3:0	DO	D) BLDR
HUNTLEY TOWNSHIP CON 02(009)	18 4 22911 5018061 ^L	1992/02 5222	90 90	FR 0042 FR 0135 FR 0167	016 / 180 004 / 2:0	DO	
HUNTLEY TOWNSHIP	18 422911 5018061 ^L	1994/05 5222	90 90	FR 0032 FR 0043	005 / 025 050 / 2:0	8	599 (152991 FSND 0003 BRWN CLAY LYRD 0020 LMSN FCRD 0050
HUNTLEY TOWNSHIP CON 02(009)	18 423390 5018396™	1974/08 3658	90 90	FR 0250 FR 0302	027 / 220 008 / 2:0	DO	1514640 () BRWN SAND 0007 GREY LMSN 0245 BLCK LMSN 0305
HUNTLEY TOWNSHIP CON 02(009)	18 422530 5017921 ^W	1983/12 1558	90 90	FR 0185 FR 0209	075 / 170 004 / 1:0	O	1518822 () BRWN CLAY DCKD 0012 GREY CLAY PCKD 0023 GREY SAND PCKD 0060 BRWN SAND PCKD 0071 BRWN SAND BLDR GRVL 0096 GREY GRNT LYRD HARD 0215
HUNTLEY TOWNSHIP CON 02(009)	18 423491 5018329 ^W	1973/11 3504	90	FR 0090	020 / 075 005 / 0:30	DO	0002 LMSN
HUNTLEY TOWNSHIP CON 02(009)	18 422671 5018022 ^W	1952/02	04 04	FR 0065 FR 0158 FR 0176	023 / 085 003 / 1:0	OD	1503063 () PRDR 0052 LMSN 0179

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a as of Fel	WATER ^{5,6} DETAIL	SU 0110 SU 0195 SU 0065	FR 0235	SU 0095	FR 0120	FR 0178	FR 0165	FR 0080	UK 0074 UK 0147 UK 0132	FR 0032 FR 0038	FR 0189 FR 0140	FR 0030 FR 0060 FR 0100 FR 0280	FR 0050 FR 0061 FR 0070 FR 0073	0340 0485	FR 0098
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Well Computer Print Out I	UTM ¹	$18 \ 422911 \ 5018061^{ m L}$	18 422251 5017922™	18 422311 5018132 ^W	18 421891 5018222 ^W	18 421951 5018122 ^W	18 422515 5018528 ^L	18 421930 5018421 ^W	18 422515 5018528 ^L	18 422371 5017907 ^W	18 422515 5018528 ^L	18 422111 5018993 ¹	18 422107 5018994 ^L	18 421921 5018437 ^W	18 421721 5018422 ^W
E	CONCESSION (LOT)	CON 02(009)	HUNTLEY TOWNSHIP CON 02(010)	HUNTLEY TOWNSHIP CON 02(010)	HUNTLEY TOWNSHIP CON 02(010)	HUNTLEY TOWNSHIP CON 02(010)	HONTLEY TOWNSHIP CON 02(010)	HONILEY TOWNSHIP CON 02(010)	HUNTLEY TOWNSHIP CON 02(010)	\sim 1		HUNTLEY TOWNSHIP CON 02(011)	HUNTLEY TOWNSHIP CON 02(011)	HUNTLEY TOWNSHIP CON 02(011)	HUNTLEY TOWNSHIP CON 02(011)

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Well Computer Print Out Data as of February 19

2009 Page: 4 / 10	WELL # (AUDIT#) WE. THS TO WHICH FORMATION	MSN 0130	1503070 () LOAM 0004 GREY LMSN 0105	1510501 () HPAN SHLE 0004 GREY LMSN 0506	1510511 () GREY SHLE 0009 GREY LMSN 0121	1511759 () GREY CLAY GRVL 0011 GREY LMSN 0139	1511921 () BRWN SAND FILL 0003 BRWN SAND STNS	GREI LMSN 182 () 0010 GREY	1514247 () BRWN CLAY SAND PCKD 0006 GREY HPAN BLDR HPAN 0030 GREY LMSN FCRD 0033	GREI LMSN 0002 1516282 () BEWN CSND BLDR 0021 WHIT SNDS CGRD	GREY HPAN GRVL 0010 GREY SHLE GRVL	SAND STNS	281 () 281 () 281 () 1.MSN 0298	SAND 0008	CLAY CLAY GREY PCKD	83 (8 SAND 0015 SILT
© Queen's Printer, 2009	WATER SCREEN USE ⁹ INFO ¹⁰															
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ta as of Febi	WATER ^{5,6} DRTAII		FR 0105 FR 0071	FR 0136 UK 0475	FR 0073 FR 0121	FR 0139	FR 0090 FR 0138	FR 0063 FR 0129	FR 0044 FR 0060	FR 0041	FR 0060	UK 0048 UK 0145	SU 0290 FR 0030	SU 0155 SU 0250	FR 0165	SU 0190 FR 0145
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Well Cor	\mathtt{UTM}^1	18 421766 5018362 ^W	18 421781 5018487 ^W	18 422591 5019102 ^W	18 421851 5018392 ^W	18 421631 5018542 ^M	18 421631 5018548 ^W	18 421671 5018532 ^W	18 421943 5018748 ^W	18 421830 5018321 ^W	18 421731 5018522 ^W	18 421630 5018521 ^W	18 421930 5018521 ^W	18 421630 5018521 ^W	18 422111 5018993 ^L	18 421715 5019458 ^L
		HUNTLEY TOWNSHIP CON 02(011)		HUNTLEY TOWNSHIP CON 02(011)	HUNTLEY TOWNSHIP CON 02(011)	HUNTLEY TOWNSHIP CON 02(011)	HUNTLEY TOWNSHIP CON 02(011)	HUNTLEY TOWNSHIP CON 02(011)	HUNTLEY TOWNSHIP CON 02(011)	HUNTLEY TOWNSHIP CON 02(011)	HUNTLEY TOWNSHIP CON 02(011)	HUNTLEY TOWNSHIP CON 02(011)	HUNTLEY TOWNSHIP CON 02(011)	HUNTLEY TOWNSHIP CON 02(011)	HUNTLEY TOWNSHIP CON 02(011)	HUNTLEY TOWNSHIP CON 02(012)

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CONCESSION (LOT)	\mathtt{UTM}^1	DATE 2 CNTR 3	CASING DIA 4	WATER ^{5,6}	STAT LVL/PUMP LVL ⁷ RATE ⁸ /TIME HR:MIN		SCREEN INFO ¹⁰	WELL # (AUDIT#) WELL
HUNTLEY TOWNSHIP CON 02(012)	18 421715 5019458 ^L	1988/08 5222	90	FR 0163	/ 075 025 / 2:0	ă		읍
								0050 CLAY
HUNTLEY TOWNSHIP CON 02(012)	18 421096 5018982 ^W	2005/11	40 35	FR 0026	021 / 021	95	0026	CGVL 0165 1536029 (Z28740) A035191
HUNTLEY TOWNSHID	2000	#/ 00			\		02	- 14 2
CON 02(014)	5020378 ^L	1994/09 1558	90 90	UK 0133	035 / 071 005 / 7:0	DO		326 (147747) CLAY 0008 GREY CLAY 0130
12	18 420925	1987/00	000		-			SAND WBRG 0146 GREY LMSN 0298 GREY LMSN 0330
CON 02(014)	5020379 ^L	3644	90 90	FR 0158	030 / 150 006 / 1:0	DO		CLAY
HUNTLEY TOWNSHIP	18 420926	1988/04	90 90	FR 0151	1	5	1310	0165
CON 02 (014)	5020378 ²	5222			060 / 2:0	3	03	1523230 (32730) BRWN LOAM PCKD 0001 BLUE CLAY PCKD
								SAND 0140
1-	18 420926	1985/09	06	PD 0140				BLCK LMSN
CON 02(014)	5020378^{L}	5222)		018 / 050 050 / 2:0	00		000
HUNTLEY TOWNSHIP	18 420926	1985/10	90 90	FR 0140	038 / 140	8	0.4	PCKD 0145
CON 02(014)	5020378^{L}	5222		FR 0170	` `	3	0140	1520195 () GREY CLAY STKY 0130 GREY SAND CGRD
	18 422291	1961/03	04 04	TPD 0000	7 110			EY LMSN SOFT 0175
CON 03 (009)	5017602 ^w	4824			005 / 020	DQ		1503122 () RED MSND 0038 2DEV IMSN 0003
HUNTLEY TOWNSHIP	18 422360	07/100			-			NOW THE
CON 03 (009)	5017601 ^W	3658	90	FR 0076	006 / 020 030 / 2:0	DO		0008 GREY
HUNTLEY TOWNSHIP	18 421807	1972/10	90 90	FR 0124	025 / 075	ОО		1512118 ()
CON CO (CIT)	.9178716	1558			_			GREY GRVL SAND 0015 GREY LMSN 0125
HONTLEY TOWNSHIP CON 03 (010)	$18 \ 421493 \ 5017616^{\mathrm{L}}$	1988/10 3644	90 90	FR 0115	018 / 110	ОО		27144)
HINTLEY TOWNSHID	000	1000			·			GREY CLAY 0023 GREY CLAY GRVL 0035 GREY LMSN 0143
CON 03 (010)	18421489 5017618^{L}	2001/06 4875	90	UK 0148	006 / 012 012 / 1:0	DO		1532014 (221765) GREY LMSN SHLE 0151
HUNTLEY TOWNSHIP	18 421493	1988/11	20 20	100	-			
CON 03 (010)	5017616 ^L	3644		/ TTO % 4	015 / 080 009 / 1:0	00		1523096 (27167) GREY GRVL 0018 GREY LMSN 0123
HUNTLEY TOWNSHIP CON 03(010)	18 422018 5017602W	2006/12	90	9900		NO		7040818 (Z55593) A043542
HINDLEY TOWNSHIP	700	6111		0073	<u> </u>			SAND GRVL 0052 GREY LMSN 0080
CON 03 (010)	18 421493 5017616^{L}	1985/06 3142	90 90	FR 0063	012 / 025 040 / 4:0	ОО		25 () SAND SILT PCKD LOOS 0027 GREY
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rinter, 2009 Page: 6 / 10	WELL # (AUDIT#) WE:	E E	LMSN 0063 1536296 (Z39257) A035418 BRWN LOAM STNS PCKD 0004 BRWN SNDS 0023 GREY SNDS STNS 0044 GREY LMSN	0123 1536342 (Z39913) A023024 SAND CLAY GRVL 0042 GREY QTZ LMSN 0080	108220) 0002 GREY SAND 0044 REI	GREY LMSN 108219) 0002 GREY GREY LMSN	LMSN 0298 1524267 (39039) BRWN SAND GRVL LOOS 0016 GREY SILT CLAY WBRG 0036 GREY LMSN MUCK HARD			GREY LMSN 197 (27143) SAND 0009 0035 GREY	1518464 () BLCK LOAM LOOS 0002 RED SAND PCKD 0010 REPEX CLAY SAND LOOS 0038 GREY		94 () SAND GRVL 0009 GREY HPAN	263 () 263 () 264 () 265 () 269 () 26	508 () 508 () 5AND STNS 0029 GREY
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ata as of February 19 2010	STAT LVL/PUMP LVL 7 RATE 8 /TIME HR:MIN	004 / 040 020 / 1:0		010 / 063 015 / 1:0	006 / 147 004 / 1:0	006 / 297 002 / 1:0	008 / 055 010 / 2:0	004 / 030 015 / 2:0	012 / 021 040 / 2:0	015 / 040 020 / 1:0	028 / 030 030 / 2:0	004 / 015 040 / 4:0	010 / 020 020 / 1:0	020 / 050 020 / 2:0	010 / 016 020 / 0:30
ta as of Feb	WATER ^{5,6} DRTAII,	FR 0057	0118	0073	FR 0123	FR 0160	FR 0060	FR 0028 FR 0046	FR 0055	FR 0055	FR 0068	FR 0069	FR 0037	SU 0118	UK 0071
it Out Dai	CASING DIA 4	90 90	90	90	90 90	90 90	90 90	90 90	90 90	90 90	90 90	90 90	90	90 90	90 90
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Well Computer Print Out D	UIM	18 421493 5017616 ¹	18 421624 5018051 ^W	18 421901 5017612 ^W	18 421493 5017616 ^L	18 421493 5017616 ^L	18 421493 5017616 ^L	18 421493 5017616 ^L	18 421230 5017621 ^W	18 421493 5017616 ^L	18 421230 5017721 ^W	18 421530 5018021"	18 421306 5017777 ^W	18 420930 5017821 ^W	18 421419 5018710 ^W
			HUNTLEY TOWNSHIP CON 03(010)	HUNTLEY TOWNSHIP CON 03(010)	HUNTLEY TOWNSHIP CON 03(010)	HUNTLEY TOWNSHIP CON 03(010)	HUNTLEY TOWNSHIP CON 03(010)	HUNTLEY TOWNSHIP CON 03(010)	HUNTLEY TOWNSHIP CON 03(010)	HUNTLEY TOWNSHIP CON 03(010)	HUNTLEY TOWNSHIP CON 03(010)	HUNTLEY TOWNSHIP CON 03(010)	HUNTLEY TOWNSHIP CON 03(010)	HUNTLEY TOWNSHIP CON 03(011)	HUNTLEY TOWNSHIP CON 03(011)

© Queen's Printer, 2009 Page: 7 / 10	WATER SCREEN WELL # (AUDIT#) WELL TAG # USE ⁹ INFO ¹⁰ DEPTHS TO WHICH FORMATIONS EXTEND ^{5,11}	1510221 () LOAM MSND 0	1503127 () GRVL 0010 LMSN 0081) 1503126 () SHLE 0012 GREY LMSN 0108) 1503125 () CLAY 0006 LMSN 0127	r 1503124 () CLAY LOAM 0007 GREY LMSN 0101	F 1503123 () CLAY LOAM 0012 GREY LMSN 0124	D 1524588 (84306) D BRWN LOAM PCKD 0001 BRWN CLAY SNDY PCKD 0003 GREY LMSN HARD 0200	0025 1524591 (84305) 03 BRWN FSND 0010 BRWN MSND SILT CLAY 0040	0030 15245 03 BRWN 0005 MSND BRWN		DO 1513273 () YLLW SAND 0020 HPAN 0032 GREY LMSN 0260	IN BRWN GRVL SAND PCKD 0003 BRWN SAND PCKD 0018 GREY SAND PCKD 0012 GREY CLAY LOOS 0042 GREY SAND GRVL STNS 0047 BLCK LMSN 0188	128 () LOAM 0036	1516828 () DO BRWN CLAY BLDR 0021 GREY HPAN BLDR PCKD 0035 GREY LMSN SOFT 0145	S89 () CLAY PCKD 0015 GREY 0057 GREY SAND CMTD
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as of Feb	WATER ^{5,6} DETAIL	FR 0060	FR 0080	FR 0108 FR 0071	FR 0125	FR 0100	FR 0122	FR 0085 FR 0190	FR 0025	FR 0030	FR 0075	SU 0256	SU 0080 SU 0187	FR 0094	FR 0145	FR 0083 FR 0185
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outer Print	DATE 2 CNTR 3	1969/05 4847	1966/03 4824	1964/09 4806	1962/05 4825	1961/09 4833	1959/12 4833	5222	5222	5222	1983/09 3644	1973/04 1836	1972/12 1558	1960/09 4833	1978/11	1981/11 4006
Well Com	UTM^1	18 421581 5018292 ^W	18 421691 5018272"	18 421631 5018442 ^W	18 421431 5018662 ^W	18 421741 5018272 ^W	18 421371 5018322 ^W	18 420854 5018003 ^L	18 420949 5017761 ^L	18 421532 5018171 ^L	$18 421089$ $5018090^{\rm L}$	18 421227 5018949 ^W	18 421126 5018996 ^W	18 421151 5018922 ^W	18 420831 5019422™	18 420930 5019321 ^W
	TOWNSHIP CONCESSION (LOT)	HUNTLEY TOWNSHIP CON 03(011)	HUNTLEY TOWNSHIP CON 03(011)	HUNTLEY TOWNSHIP CON 03(011)	HUNTLEY TOWNSHIP CON 03(011)	HUNTLEY TOWNSHIP CON 03(011)	HUNTLEY TOWNSHIP CON 03(011)		HUNTLEY TOWNSHIP CON 03 (011)	HUNTLEY TOWNSHIP CON 03(011)	HUNTLEY TOWNSHIP CON 03(011)	HUNTLEY TOWNSHIP CON 03(012)	HUNTLEY TOWNSHIP CON 03(012)	HUNTLEY TOWNSHIP CON 03(012)	HUNTLEY TOWNSHIP CON 03(013)	HUNTLEY TOWNSHIP CON 03(013)

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	UTM	DATE 2 CNTR 3	CASING DIA 4	WATER ^{5,6} DETAIL	STAT LVL/PUMP LVL 7 RATE $^8/$ TIME HR:MIN	WATER USE ⁹	SCREEN INFO ¹⁰	WELL # (AUDIT#) WELL TAG # DEPTHS TO WHICH FORMATIONS EXTEND 5,11
HUNTLEY TOWNSHIP 01(011)	18 423127 5019896 ^L	1993/08 3749	90	FR 0094 FR 0083	016 / 074 030 / 1:0	DO		1527433 (137653) BRWN SAND STNS GRVL 0024 GREY SILT CLAY 0032 GREY GRVL 0036 BLCK GRNT COPT 0.06
HUNTLEY TOWNSHIP 01(011)	$18 \ 423127$ 5019896^{L}	1993/08 3749	90	FR 0115 FR 0122 FR 0064	018 / 094 025 / 1:0	AC DO		1527432 (137654) BRWN SAND STNS GRVL 0027 GREY SILT GRVL 0034 GREY GRVL HPAN 0049 BLCK GRNT SOFT 0130
HUNTLEY TOWNSHIP 02 (008)	18 423307 5017600 ^L	1987/06 5222	90 90	FR 0047 FR 0036	003 / 020 100 / 2:0	00		187 (13919) SAND CLAY PCKD 0003 HARD 0006 GREY LMSN GRVL LMSN LOOS 0012
HUNTLEY TOWNSHIP 02(008)	18 422866 5017546 ^w	2006/11 1119						347 (Z55508)
	18 423270 5018146 ^W	2008/06 1558	90		. \	DO		7112979 (277369) A051522 BRWN HPAN BLDR PCKD 0012 GREY GRVL STNS WBRG 0016 GREY LMSN MGRD 0200
HONTLEY TOWNSHIP 02(008)	18 423399 5018274™	2008/04	90	UK 0366 UK 0458	017 / 208 012 / 4:0	DO		LMSN
HUNTLEY TOWNSHIP 02(009)	$18 ext{ 422911} \\ 5018061^{L}$	1992/07 3323	90	FR 0115	017 / 060 020 / 1:0	OQ		1526956 (126336) BRWN SAND 0007 WHIT LMSN 0045 RED GRNT 0120
HUNTLEY TOWNSHIP 02(011)	18 421726 5018881 ^L	1988/11 3142	90 90	UK 0158 FR 0090	015 / 140 007 / 1:30	OG		1523034 (44875) BRWN SAND BLDR PCKD 0019 GREY LMSN HARD 0090 GREY LMSN SHLE PORS 0160
HUNTLEY TOWNSHIP 03 (006)	18 421648 5017568™	2009/05 1558	90	UK 0150 UK 0251 UK 0269	006 / 052 008 / 1:0	DO		095287) A076853 SNDY 0012 GREY SAND LMSN LYRD 0273
HUNTLEY TOWNSHIP 03 (010)	18 421493 5017616 ^L	1988/10 1558	90 90	FR 0145 FR 0170	030 / 100 006 / 1:0	OO		1523014 (38358) BRWN LOAM SNDY 0005 BRWN SAND WBRG 0012 GREY SAND 0030 GREY CLAY STNS 0042 GREY LMSN 0175
HUNTLEY TOWNSHIP 03 (010)	18 421418 5017799™	2008/12 1558	90	0269	018 / 142 005 / 2:0	OG .		7119248 (Z84466) A076810 BRWN LOAM FILL 0005 BRWN SAND LOOS 0009 GREY SAND WBRG 0015 BRWN CLAY PCKD 0027 GREY CLAY GRVL BLDR 0044 GREY LMSN MGRD 0273
HUNTLEY TOWNSHIP 03(010)	18 421805 5017734 ^W	2009/08 1119	90 90	0076 0080	013 / 040 020 / 1:0	DO		7131310 (Z102574) A082479 SAND GRVL BLDR 0028 GREY LMSN 0090
HUNTLEY TOWNSHIP 03 (010)	18 421567 5017859 ^W	2009/10 1119						7132598 (Z102713) A089342
HUNTLEY TOWNSHIP 03 (010)	18 421755 5018048 ^W	2009/10 1558						7139851 (Z101735) A076883

r; 2009 Page: 9 / 10	WELL # (AUDIT#) WELL TAG # DEPTHS TO WHICH FORMATIONS EXTEND ^{5,11}	7112989 (277368) A051521 BRWN LOAM SNDY FILL 0005 STNS BRWN LOAM SNDY 0013 BRWN CLAY PCKD HARD 0023 GREY CLAY SNDY STNS 0040 GREY LMEN PKCT, LYDD 0272 MCBD	7123248 (Z095326) A076799 BRWN LOAM ROCK FCRD 0004 BRWN CLAY PCKD 0014 BRWN SAND WBRG 0022 GREY TIM, PORD 0032 GREY IMEN MASH 0140	1	7035379 (Z51855) A046053 BRWN LOAM LOOS 0004 BRWN SAND SILT 0012 GREY CLAY SILT WBRG 0012	7051249 (Z60314) A065666 BRWN SAND LOAM BLDR 0012 GREY HPAN BLDR PCKD 0040 GREY SAND CLAY 0050 GREY LMSN LYRD 0273	1534651 (Z04926) A004780 SAND FILL 0004 GREY GRNT QTZ 0180	7049976 (Z50987) A017504
© Queen's Printer, 2009	${ m SCREEN}$				0005			
© Quee	WATER USE ⁹	00	OD	OO		OG	<u>8</u>	
ata as of February 19 2010	STAT LVL/PUMP LVL 7 RATE $^8/$ TIME HR:MIN	017 / 102 007 / 1:30	012 / 015 012 / 2:0	016 / 042 012 / 1:0		022 / 126 008 / 6:0	004 / 005 / 1:0	
a as of Fet	WATER ^{5,6} DETAIL	UK 0260 UK 0273	0140	0169		UK 0266	UK 0170	
t Out Dat	CASING DIA 4	90	90	90	02		90	
Well Computer Print Out D	DATE 2 CNTR 3	2008/05 1558	2009/03 1558	2009/06 1558	2006/07 72 4 1	2007/08 1558	2004/05 1119	2007/05 6907
Well Con	UTM1	18 421477 5017754™	18 421668 5017988 ^W	18 421558 5017784 ^W	18 420944 5019366 ^W	18 423437 5018559 ^W	18 423744 5020314 ^W	18 421372 5018928"
	TOWNSHIP CONCESSION (LOT)	HUNTLEY TOWNSHIP 03 (010)	HUNTLEY TOWNSHIP 03(010)	HUNTLEY TOWNSHIP 03(010)	HUNTLEY TOWNSHIP ()	MARCH TOWNSHIP CON 01(008)	MARCH TOWNSHIP CON 01(011)	OTTAWA CITY 02 (012)

Notes:

- UTM in Zone, Easting, Northing and Datum is NAD83; L: UTM estimated from Centroid of Lot; W: UTM not from Lot Centroid UTM in Zone,
 - Date Work Completed

 - Well Contractor Licence Number
 - U 4 4 10 0
- Casing diameter in inches Unit of Depth in Feet See Table 4 for Meaning of Code

- 7. STAT LVD: Static Water Level in Feet; PUMP LVL: Water Level After Pumping in Feet
 8. Pump Test Rate in GPM, Pump Test Duration in Hour: Minutes
 9. See Table 3 for Meaning of Code
 10. Screen Depth and Length in feet
 11. See Table 1 and 2 for Meaning of Code

				and out the Party Constitutes		And promotion of the second		200000000000000000000000000000000000000	3REY									
	Description		Y GREY	BLUE BLUE	YLLW YELLOW	N BROWN	RED	BLCK BLACK	Y BLUE-GREY									
		HW	GREY	BITOES	Z Z	BRWIN		BILC	BLGY	essely (quantifyrm a same an	inganatina anakari		-	usyessensoonssans	angazzoonico	поравновнеен	ecoposion memory	
	Describition	SOFT	SOAPSTONE	STICKY	STONES	STONEY	THICK	NIHL	TITT	UNKNOWN TYPE	VERY	WATER- BEARING	WOOD		enumina no rous (como como como como como como como com	оздабда бана компандення в переметру политира в политир	ANIMA VINNA KANA KANA KANA KANA KANA KANA KANA	A CONTRACTOR OF THE PARTY OF TH
	8	SOFT	SPST	STKY	STNS	STNY	THIK	THIN	TILL	UNKN	VERY	WBRG	WDFR	WTHD		Control of Statement Control o	The state of the s	***************************************
	Description	POROUS	PREVIOUSLY	PREV.	QUARTZITE	QUICKSAND	QUARTZ	ROCK	SAND	SHALE	SHALY	SHARP	SCHIST	SILT	SLATE	SILTY	SANDSTONE	THE PERSON OF TH
		PORS	PRDG	PRDR	QRTZ	QSND	QTZ	ROCK	SAND	SHILE	SHLY	SHRP	SHST	SILT	SLITE	SLTY	SUNS	CATINE
and Descriptive terms	Description	IRON	LIMY	LIMESTONE	TOPSOIL	LOOSE	LIGHT- COLOURED	LAYERED	MARL	MEDIUM- GRAINED	MEDIUM GRAVEL	MARBLE	MEDIUM SAND	MUCK	OVERBURDEN	PACKED	PEAT	TENTRUC REIGH
i		IRFM	ГІМУ	LMSN	LOAM	LOOS	LTCL	LYRD	MARL	MGRD	MGVL	MRBL	MSMD	MUCK	OBDN	PCKD	PEAT	DOM
L. Core Material	Description	FRACTURED	FINE-GRAINED	FINE GRAVEL	FILL	FELDSPAR	FLINT	FOSILIFEROUS	FINE SAND	GNEISS	GRANITE	GREENSTONE	GRAVEL	GREYWACKE	GRAVELLY	GYPSUM	HARD	UADODAN
		FCRD	FGRD	FGVL	FILL	FLDS	FLNT	FOSS	FSND	GNIS	GRNT	GRSN	GRVL	GRWK	GVLY	GYPS	HARD	HDAN
	Description	BOULDERS	BASALT	COARSE- GRAINED	COARSE	CHERT	CLAY	CLEAN	CLAYEY	CEMENTED	CONGLOMERATE	CRYSTALLINE	COARSE SAND	DARK- COLOURED	DOLOMITE	DENSE	DIRTY	NBV
		BLDR	BSLT	CGRD	CGVL	CHRT	CLAY	CEN	CLYY	CMIED	CONG	CRYS	CSND	DKCL	DLMT	DNSE	DRTY	אמט

	Other	Test Hole	Dewatering	Monitoring		SECURIORA AND AND AND AND AND AND AND AND AND AN	AMERICAN STREET, STREE		
	8	H	DE	Q	ACCRECATE ON COUNTY OF				
The Park	Domestic	Livestock	Irrigation	Industrial	Commercial	Municipal	Public Public	Cooling And	Not Used
	8	S.	IR	N	8	Ø	Sd	Ş	R

į			Description
æ	Fresh	88	Gas
SAS	Salty	IR	Iron
SG	Sulphur		CONTROL OF STREET, CONTROL OF ST
Z	Mineral		

Unknown

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