Geotechnical Engineering

Environmental Engineering

Hydrogeology

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Materials Testing

Building Science

Archaeological Services

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Geotechnical Investigation

Proposed Warehouse Expansion
2390 Stevenage Drive
Ottawa, Ontario

Prepared For

Sysco

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July 30, 2018

Report: PG4583-1

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Appendices

1.0 Introduction

Paterson Group (Paterson) was commissioned by Sysco to conduct a geotechnical investigation for the proposed warehouse expansion to be located at 2390 Stevenage Drive, in the City of Ottawa, Ontario (refer to Figure 1 - Key Plan in Appendix 2 of this report).

The objective of the investigation was to:

❏ determine the subsoil and groundwater conditions at this site by means of boreholes.

❏ provide geotechnical recommendations for the design of the proposed development including construction considerations which may affect its design.

The following report has been prepared specifically and solely for the aforementioned project which is described herein. It contains our findings and includes geotechnical recommendations pertaining to the design and construction of the subject development as they are understood at the time of writing this report.

Investigating the presence or potential presence of contamination on the subject property was not part of the scope for this investigation. Therefore, the present report does not address environmental issues.

2.0 Proposed Development

Based on the current conceptual site plan, it is our understanding that the proposed warehouse expansion consists of additional low-rise warehouse structures and office space along with associated loading docks, access lanes, car parking areas and landscaped areas. It is further understood that construction of the proposed warehouse expansion will require demolition of the southern portion of the existing warehouse.

3.0 Method of Investigation

3.1 Field Investigation

The field program for the geotechnical investigation was carried out on July 11, 2018. At that time, a total of 12 boreholes (BH 1 to BH 12) were distributed in a manner to provide general coverage of the proposed development taking into consideration existing site features and underground utilities. The locations of the test holes are shown on Drawing PG4583-1 - Test Hole Location Plan included in Appendix 2.

The boreholes were advanced using either a track-mounted auger drill rig or a truck-mounted auger drill rig, both operated by a two person crew. All fieldwork was conducted under the full-time supervision of Paterson personnel under the direction of a senior engineer. The test hole procedures consisted of augering to the required depths at the selected locations and sampling the overburden.

Sampling and In Situ Testing

Soil samples were recovered using a 50 mm diameter split-spoon sampler or from the auger flights. The split-spoon and auger samples were classified on site and placed in sealed plastic bags. All samples were transported to our laboratory. The depths at which the split-spoon and auger samples were recovered from the boreholes are shown as SS and AU, respectively, on the Soil Profile and Test Data sheets in Appendix 1.

The Standard Penetration Test (SPT) was conducted in conjunction with the recovery of the split-spoon samples. The SPT results are recorded as “N” values on the Soil Profile and Test Data sheets. The “N” value is the number of blows required to drive the split-spoon sampler 300 mm into the soil after a 150 mm initial penetration using a 63.5 kg hammer falling from a height of 760 mm.

Undrained shear strength testing, using a vane apparatus, was carried out at regular intervals of depth in cohesive soils.

The overburden thickness was evaluated by a dynamic cone penetration test (DCPT) at borehole BH 1. The DCPT consists of driving a steel drill rod, equipped with a 50 mm diameter cone at the tip, using a 63.5 kg hammer falling from a height of 760 mm. The number of blows required to drive the cone into the soil is recorded for each 300 mm increment.

The subsurface conditions observed in the test holes were recorded in detail in the field. The soil profiles are logged on the Soil Profile and Test Data sheets in Appendix 1 of this report.

Groundwater

Groundwater monitoring wells were installed in boreholes BH 4, BH 6 and BH 11 and flexible piezometers were installed in the remaining boreholes to permit monitoring of the groundwater levels subsequent to the completion of the sampling program.

Sample Storage

All samples will be stored in the laboratory for a period of one month after issuance of this report. They will then be discarded unless we are otherwise directed.

3.2 Field Survey

The test hole locations were selected by Paterson to provide general coverage of the proposed development taking into consideration the existing site features and underground utilities. The test hole locations and ground surface elevation at each test hole location were surveyed by Paterson. The ground surface elevations at the borehole locations were referenced to a temporary benchmark (TBM), consisting of the top spindle of the fire hydrant located just east of the subject property on Stevenage Drive. A geodetic elevation of 83.60 m was provided for the TBM by Annis O'Sullivan Vollebekk, Ltd. The location of the test holes and ground surface elevation at each test hole location are presented on Drawing PG4583-1 - Test Hole Location Plan in Appendix 2.

3.3 Laboratory Testing

Soil samples were recovered from the boreholes and visually examined in our laboratory to review the field logs.

3.4 Analytical Testing

One (1) soil sample was submitted for analytical testing to assess the corrosion potential for exposed ferrous metals and the potential of sulphate attacks against subsurface concrete structures. The sample was submitted to determine the concentration of sulphate and chloride, the resistivity and the pH of the sample. The results are presented in Appendix 1 and are discussed further in Subsection 6.7.

4.0 Observations

4.1 Surface Conditions

The subject site is bordered to the east and west by adjacent industrial properties, to the south by a residential neighbourhood, and to the north by Stevenage Drive. The site is currently occupied by an existing warehouse facility along with associated paved parking areas and access lanes. The south portion of the property is currently vacant and partially forested. A large berm is located along the south boundary. The developed portion on the northern end of the site is relatively flat and approximately at grade with the adjacent roadway and neighboring properties. The undeveloped portion to the south of the site slopes gradually down towards the south edge of the property.

4.2 Subsurface Profile

Generally, the subsurface profile encountered at the test hole locations consists of a layer of topsoil, asphalt pavement structure and/or fill up to 0.6 m in thickness overlying a very stiff to firm, brown to grey silty clay deposit. At several borehole locations, the silty clay deposit was underlain by a glacial till layer consisting of grey silty clay with gravel, cobbles and boulders.

Practical refusal to augering was encountered at some of the south borehole locations at depths ranging between 5 and 5.3 m below existing ground surface. Practical refusal to DCPT was encountered at BH 1 at a depth of 8.5 m below existing ground surface.

Reference should be made to the Soil Profile and Test Data sheets in Appendix 1 for specific details of the soil profiles encountered at each test hole location.

Based on available geological mapping, bedrock in the area of the subject site consists of shale of the Carlsbad Formation with overburden drift thickness between 10 to 15 m depth.

4.3 Groundwater

Groundwater levels were measured in the boreholes on July 17, 2018, with the exception of boreholes BH 4 and BH 6. The measured groundwater level (GWL) readings are presented in Table 1 below and in the Soil Profile and Test Data sheets in Appendix 1. It is important to note that groundwater readings at the piezometers can be influenced by water perched within the borehole backfill material. Long-term groundwater level can also be estimated based on the observed colour and consistency of the recovered soil samples. Based on the observations of the soil samples, the samples were changing from a brownish to a greyish colour generally between a 3 to 4 m depth. Therefore, it is estimated that the long-term groundwater table can be expected between 3 to 4 m depth.

It should be noted that groundwater levels are subject to seasonal fluctuations. Therefore, the groundwater level could vary at the time of construction.

Table 1 - Measured Groundwater Levels

Test Hole Location	Ground Surface Elevation (m)	Groundwater Level		Date
		Depth (m)	Elevation (m)	
BH 1	82.59	1.30	81.29	July 17, 2018
BH 2	82.78	Blocked	-	July 17, 2018
BH 3	82.21	1.97	80.24	July 17, 2018
BH 5	82.67	Blocked	-	July 17, 2018
BH 7	80.57	3.20	77.37	July 17, 2018
BH 8	81.02	4.17	76.85	July 17, 2018
BH 9	81.89	3.21	78.68	July 17, 2018
BH 10	80.26	Blocked	-	July 17, 2018
BH 11*	80.86	3.70	77.16	July 17, 2018
BH 12	80.24	Blocked	-	July 17, 2018

Note: - * Denotes borehole instrumented with a 51 mm diameter monitoring well.
- It should be noted that the ground surface elevations are referenced to a temporary benchmark (TBM), consisting of the top spindle of the fire hydrant located just east of the subject property on Stevenage Drive. A geodetic elevation of 83.60 m was provided for the TBM by Annis O'Sullivan Vollebekk, Ltd.

5.0 Discussion

5.1 Geotechnical Assessment

From a geotechnical perspective, the subject site is suitable for the proposed warehouse expansion. It is expected that the proposed building will constructed with conventional shallow foundations bearing on the undisturbed, very stiff to stiff silty clay.

Due to the presence of a silty clay deposit, permissible grade raise restrictions are recommended for this area.

The above and other considerations are further discussed in the following sections.

5.2 Site Grading and Preparation

Stripping Depth

Topsoil and deleterious fill, such as those containing organics, should be stripped from under any buildings, paved areas, pipe bedding and other settlement sensitive structures.

Fill Placement

Fill used for grading beneath the building footprints, unless otherwise specified, should consist of clean imported granular fill, such as Ontario Provincial Standard Specifications (OPSS) Granular A or Granular B Type II. The fill should be tested and approved prior to delivery to the site. It should be placed in lifts no greater than 300 mm thick and compacted using suitable compaction equipment for the lift thickness. Fill placed beneath the building area should be compacted to at least 98% of its standard Proctor maximum dry density (SPMDD).

Site excavated soil can be used as general landscaping fill where settlement of the ground surface is of minor concern. These materials should be spread in thin lifts and at least compacted by the tracks of the spreading equipment to minimize voids. If these materials are to be used to build up the subgrade level for areas to be paved, they should be compacted in thin lifts to a minimum density of 95% of their respective SPMDD. Site excavated soils are not suitable for use as backfill against foundation walls due to the frost heave potential of the site excavated soils below settlement sensitive areas, such as concrete sidewalks and exterior concrete entrance areas.

Fill used for grading beneath the base and subbase layers of paved areas should consist, unless otherwise specified, of clean imported granular fill, such as OPSS Granular A, Granular B Type II or select subgrade material. This material should be tested and approved prior to delivery to the site. The fill should be placed in lifts no greater than 300 mm thick and compacted using suitable compaction equipment for the lift thickness. Fill placed beneath the paved areas should be compacted to at least 95% of its SPMDD.

5.3 Foundation Design

Bearing Resistance Values

Strip footings, up to 3 m wide, and pad footings, up to 5 m wide, placed on an undisturbed, very stiff to stiff silty clay bearing surface can be designed using a bearing resistance value at serviceability limit states (SLS) of **150 kPa** and a factored bearing resistance value at ultimate limit states (ULS) of **250 kPa**.

A geotechnical resistance factor of 0.5 was applied to the reported bearing resistance value at ULS.

An undisturbed soil bearing surface consists of a surface from which all topsoil and deleterious materials, such as loose, frozen or disturbed soil, whether in situ or not, have been removed, in the dry, prior to the placement of concrete for footings.

Lateral Support

The bearing medium under footing-supported structures is required to be provided with adequate lateral support with respect to excavations and different foundation levels. Adequate lateral support is provided to a very stiff to stiff silty clay above the groundwater table when a plane extending down and out from the bottom edge of the footing at a minimum of 1.5H:1V passes only through in situ soil of the same or higher capacity as the bearing medium soil.

Settlement and Permissible Grade Raise

Footings placed on a soil bearing surface and designed using the bearing resistance values at SLS given above will be subjected to potential post construction total and differential settlements of 25 and 20 mm, respectively.

Due to the presence of the silty clay deposit at the site, a permissible grade raise restriction of **2 m** is recommended for grading within 6 m of the proposed warehouse expansion and existing structure.

5.4 Design for Earthquakes

The proposed site can be taken as seismic site response **Class C** as defined in the Ontario Building Code 2012 (OBC 2012; Table 4.1.8.4.A) for foundations considered at this site. The soils underlying the subject site are not susceptible to liquefaction.

5.5 Slab on Grade Construction

With the removal of all topsoil and deleterious materials, within the footprint of the proposed building, the native soil or engineered fill surface will be considered to be an acceptable subgrade surface on which to commence backfilling for the floor slab. The upper 200 mm of sub-slab fill should consist of an OPSS Granular A crushed stone. All backfill material within the footprint of the proposed buildings should be placed in maximum 300 mm thick loose lifts and compacted to at least 98% of its SPMDD.

Any soft areas should be removed and backfilled with appropriate backfill material. OPSS Granular B Type II, with a maximum particle size of 50 mm, are recommended for backfilling below the floor slab.

5.6 Pavement Design

Car only parking areas, access lanes and heavy truck parking areas are anticipated at this site. The proposed pavement structures are shown in Tables 2 and 3.

Table 2 - Recommended Pavement Structure - Car Only Parking Areas

Thickness (mm)	Material Description
50	**Wear Course -** HL-3 or Superpave 12.5 Asphaltic Concrete
150	**BASE** - OPSS Granular A Crushed Stone
300	**SUBBASE** - OPSS Granular B Type II
	SUBGRADE - Either fill, in situ soil, or OPSS Granular B Type I or II material placed over in situ soil or fill

Table 3 - Recommended Pavement Structure
Access Lanes and Heavy Truck Parking Areas

Thickness (mm)	Material Description
40	**Wear Course** - Superpave 12.5 Asphaltic Concrete
50	**Binder Course** - Superpave 19.0 Asphaltic Concrete
150	**BASE** - OPSS Granular A Crushed Stone
450	**SUBBASE** - OPSS Granular B Type II
	SUBGRADE - Either fill, in situ soil, or OPSS Granular B Type I or II material placed over in situ soil or fill

Minimum Performance Graded (PG) 58-34 asphalt cement should be used for this project.

If soft spots develop in the subgrade during compaction or due to construction traffic, the affected areas should be excavated and replaced with OPSS Granular B Type II material. The pavement granular base and subbase should be placed in maximum 300 mm thick lifts and compacted to a minimum of 98% of the material's SPMDD using suitable vibratory equipment.

Pavement Structure Drainage

Satisfactory performance of the pavement structure is largely dependent on keeping the contact zone between the subgrade material and the base stone in a dry condition. Failure to provide adequate drainage under conditions of heavy wheel loading can result in the fine subgrade soil being pumped into the voids in the stone subbase, thereby reducing its load carrying capacity.

Due to the impervious nature of the subgrade materials consideration should be given to installing subdrains during the pavement construction as per City of Ottawa standards. The subdrain inverts should be approximately 300 mm below subgrade level. The subgrade surface should be crowned to promote water flow to the drainage lines.

6.0 Design and Construction Precautions

6.1 Foundation Drainage and Backfill

It is recommended that a perimeter foundation drainage system be provided for the proposed structure. The system should consist of a 150 mm diameter perforated corrugated plastic pipe, surrounded on all sides by 150 mm of 19 mm clear crushed stone, placed at the footing level around the exterior perimeter of the structures. The pipe should have a positive outlet, such as a gravity connection to the catch basins or running drainage ditches.

Backfill against the exterior sides of the foundation walls should consist of free-draining non frost susceptible granular materials, such as clean sand or OPSS Granular B Type I granular material. The greater part of the site excavated materials will be frost susceptible and, as such, are not recommended for re-use as backfill against the foundation walls. A drainage geocomposite, such as Miradrain G100N or Delta Drain 6000, connected to the perimeter foundation drainage system is recommended.

Concrete Sidewalks Adjacent to Building

To avoid differential settlements within the proposed sidewalks adjacent to the proposed buildings, it is recommended that the upper 600 mm of backfill placed below the concrete sidewalks adjacent to the building footprint to consist of free draining, non frost susceptible material such as, Granular A or Granular B Type II. The granular material should be placed in maximum 300 mm loose lifts and compacted to 95% of the material's SPMDD using suitable compaction equipment. The subgrade material should be shaped to promote positive drainage towards the building's perimeter drainage pipe.

6.2 Protection of Footings and Slabs Against Frost Action

Perimeter footings of heated structures are required to be insulated against the deleterious effect of frost action. A minimum of 1.5 m thick soil cover (or equivalent) should be provided in this regard.

Exterior unheated footings, such as those for isolated exterior piers and loading docks, are more prone to deleterious movement associated with frost action than the exterior walls of the structure proper and require additional protection, such as soil cover of 2.1 m or a combination of soil cover and foundation insulation. It is recommended that the geotechnical consultant review the proposed frost protection detail for the loading dock footings.

It is understood that a portion of the proposed warehouse expansion will be utilized as freezer space. Given that this will create a permanent freezing condition, it is expected that subslab insulation in conjunction with a slab heating system should be utilized to protect the subslab soils from frost action in this portion of the building. Further details can be provided regarding this issue, if required.

6.3 Excavation Side Slopes

The side slopes of excavations in the soil and fill overburden materials should either be cut back at acceptable slopes or should be retained by shoring systems from the start of the excavation until the structure is backfilled. It is expected that sufficient room will be available for the greater part of the excavation to be undertaken by open-cut methods (i.e. unsupported excavations).

The excavation side slopes above the groundwater level extending to a maximum depth of 3 m should be cut back at 1H:1V or flatter. The flatter slope is required for excavation below groundwater level. Excavations below the groundwater level should be cut back at a maximum slope of 1.5H:1V. The subsoil at this site is considered to be mainly a Type 2 and 3 soil according to the Occupational Health and Safety Act and Regulations for Construction Projects.

Excavated soil should not be stockpiled directly at the top of excavations and heavy equipment should be kept away from the excavation sides.

Slopes in excess of 3 m in height should be periodically inspected by the geotechnical consultant in order to detect if the slopes are exhibiting signs of distress.

It is recommended that a trench box be used at all times to protect personnel working in trenches with steep or vertical sides. It is expected that services will be installed by “cut and cover” methods and excavations will not be left open for extended periods of time.

6.4 Pipe Bedding and Backfill

Bedding and backfill materials should be in accordance with the most recent Material Specifications & Standard Detail Drawings from the Department of Public Works and Services, Infrastructure Services Branch of the City of Ottawa.

The pipe bedding for sewer and water pipes should consist of at least 150 mm of OPSS Granular A material. Where the bedding is located within the firm grey silty clay, the thickness of the bedding material should be increased to a minimum of 300 mm as directed by the geotechnical consultant at the time of construction. The material should be placed in maximum 300 mm thick lifts and compacted to a minimum of 95% of its SPMDD. The bedding material should extend at least to the spring line of the pipe.

The cover material, which should consist of OPSS Granular A, should extend from the spring line of the pipe to at least 300 mm above the obvert of the pipe. The material should be placed in maximum 300 mm thick lifts and compacted to a minimum of 95% of its SPMDD.

It should generally be possible to re-use the moist (not wet) brown silty clay above the cover material if the excavation and filling operations are carried out in dry weather conditions. Wet silty clay materials will be difficult to re-use, as the high water contents make compacting impractical without an extensive drying period.

Where hard surface areas are considered above the trench backfill, the trench backfill material within the frost zone (about 1.8 m below finished grade) should match the soils exposed at the trench walls to minimize differential frost heaving. The trench backfill should be placed in maximum 300 mm thick loose lifts and compacted to a minimum of 95% of the material's SPMDD.

To reduce long-term lowering of the groundwater level at this site, clay seals should be provided in the service trenches. The seals should be at least 1.5 m long (in the trench direction) and should extend from trench wall to trench wall. Generally, the seals should extend from the frost line and fully penetrate the bedding, subbedding and cover material. The barriers should consist of relatively dry and compactable brown silty clay placed in maximum 225 mm thick loose layers and compacted to a minimum of 95% of the material's SPMDD. The clay seals should be placed at the site boundaries and at strategic locations at no more than 60 m intervals in the service trenches.

6.5 Groundwater Control

Groundwater Control for Building Construction

It is anticipated that groundwater infiltration into the excavations should be low to moderate and controllable using open sumps. Pumping from open sumps should be sufficient to control the groundwater influx through the sides of shallow excavations.

The contractor should be prepared to direct water away from all bearing surfaces and subgrades, regardless of the source, to prevent disturbance to the founding medium.

A temporary Ministry of the Environment and Climate Change (MOECC) permit to take water (PTTW) may be required for this project if more than 400,000 L/day of ground and/or surface water is to be pumped during the construction phase. A minimum 4 to 5 months should be allowed for completion of the PTTW application package and issuance of the permit by the MOECC.

For typical ground or surface water volumes, being pumped during the construction phase, between 50,000 to 400,000 L/day, it is required to register on the Environmental Activity and Sector Registry (EASR). A minimum of two to four weeks should be allotted for completion of the EASR registration and the Water Taking and Discharge Plan to be prepared by a Qualified Person as stipulated under O.Reg. 63/16. If a project qualifies for a PTTW based upon anticipated conditions, an EASR will not be allowed as a temporary dewatering measure while awaiting the MOECC review of the PTTW application.

6.6 Winter Construction

Precautions must be taken if winter construction is considered for this project.

The subsoil conditions at this site consist of frost susceptible materials. In the presence of water and freezing conditions, ice could form within the soil mass. Heaving and settlement upon thawing could occur.

In the event of construction during below zero temperatures, the founding stratum should be protected from freezing temperatures by the use of straw, propane heaters and tarpaulins or other suitable means. In this regard, the base of the excavations should be insulated from sub-zero temperatures immediately upon exposure and until such time as heat is adequately supplied to the building and the footings are protected with sufficient soil cover to prevent freezing at founding level.

Trench excavations and pavement construction are also difficult activities to complete during freezing conditions without introducing frost in the subgrade or in the excavation walls and bottoms. Precautions should be taken if such activities are to be carried out during freezing conditions. Additional information could be provided, if required.

6.7 Corrosion Potential and Sulphate

The results of analytical testing show that the sulphate content is less than 0.1%. This result is indicative that Type 10 Portland cement (normal cement) would be appropriate for this site. The chloride content and the pH of the sample indicate that they are not significant factors in creating a corrosive environment for exposed ferrous metals at this site, whereas the resistivity is indicative of a moderate to aggressive corrosive environment.

6.8 Tree Planting Restrictions

Given that the proposed warehouse expansion will be a slab-on-grade structure, the underside of footing is expected at a maximum depth of 1.5 m. As such, the silty clay which extends 3 to 3.5 m below design footing level should be considered low to medium sensitivity and should not be considered a sensitive marine clay.

Based on the above discussion, shrubs and other small plantings are permitted within 4.5 m of the perimeter foundations walls. Trees may be placed at distances greater than 4.5 m from the foundation walls.

It is documented in the literature, and is our experience, that fast-growing trees located near buildings founded on cohesive soils which shrink on drying can result in long-term differential settlements of the structures. Tree varieties that have the most pronounced effect on foundations are seen to consist of poplars, willows and some maples (i.e. Manitoba Maples) and should not be considered in the landscaping design.

7.0 Recommendations

It is a requirement for the foundation design data provided herein to be applicable that the following material testing and observation program be performed by the geotechnical consultant.

- ☐ Review the grading plan from a geotechnical perspective, once available.
- ☐ Observation of all bearing surfaces prior to the placement of concrete.
- ☐ Sampling and testing of the concrete and fill materials used.
- ☐ Periodic observation of the condition of unsupported excavation side slopes in excess of 3 m in height, if applicable.
- ☐ Observation of all subgrades prior to backfilling.
- ☐ Field density tests to determine the level of compaction achieved.
- ☐ Sampling and testing of the bituminous concrete including mix design reviews.

A report confirming that these works have been conducted in general accordance with our recommendations could be issued upon the completion of a satisfactory inspection program by the geotechnical consultant.

8.0 Statement of Limitations

The recommendations made in this report are in accordance with our present understanding of the project. We request that we be permitted to review the grading plan once available and to review our recommendations when the drawings and specifications are complete.

A geotechnical investigation of this nature is a limited sampling of a site. The recommendations are based on information gathered at the specific test locations and can only be extrapolated to an undefined limited area around the test locations. The extent of the limited area depends on the soil, bedrock and groundwater conditions, as well the history of the site reflecting natural, construction, and other activities. Should any conditions at the site be encountered which differ from those at the test locations, we request notification immediately in order to permit reassessment of our recommendations.

The present report applies only to the project described in this document. Use of this report for purposes other than those described herein or by person(s) other than Sysco or their agent(s) is not authorized without review by Paterson Group for the applicability of our recommendations to the altered use of the report.

Paterson Group Inc.

Colin Belcourt

Colin Belcourt, P.Eng.

LICENSED PROFESSIONAL ENGINEER
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Report Distribution:

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APPENDIX 1

SOIL PROFILE & TEST DATA SHEETS

SYMBOLS AND TERMS

ANALYTICAL TESTING RESULTS

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SOIL PROFILE AND TEST DATA

Geotechnical Investigation
Prop. Warehouse Expansion - 2390 Stevenage Drive
Ottawa, Ontario

DATUM TBM - Top spindle of fire hydrant located just east of subject site. Geodetic elevation = 83.60m.

REMARKS

BORINGS BY CME 55 Power Auger

DATE July 11, 2018

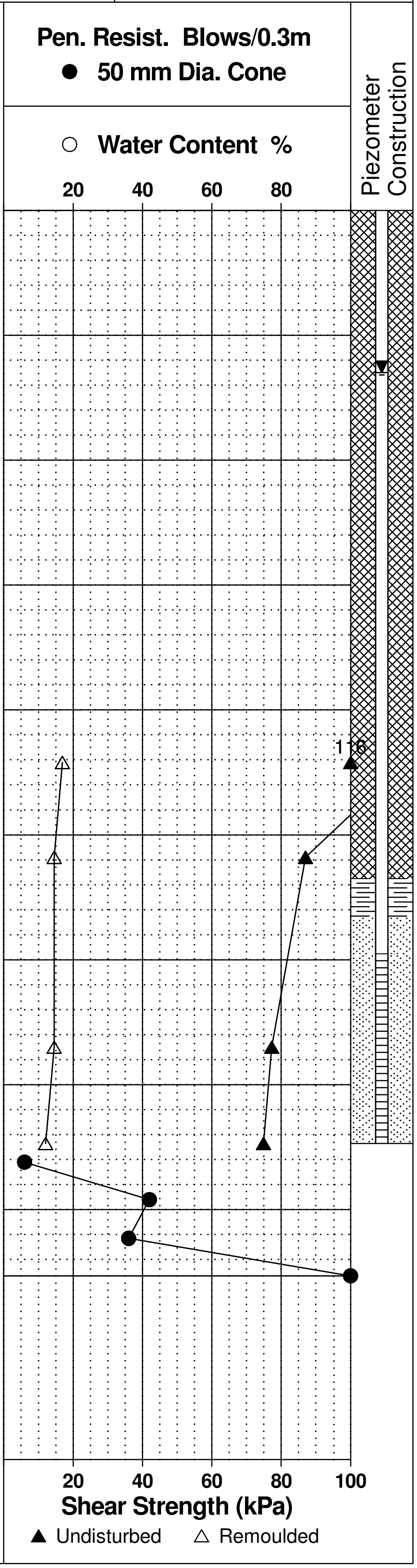
FILE NO. PG4583

HOLE NO. BH 1

SOIL DESCRIPTION	Depth (m)
GROUND SURFACE	
Asphaltic concrete	0.10
FILL: Brown silty sand with gravel	0.43
Very stiff to stiff, brown **SILTY CLAY** - grey by 3.0m depth	7.47
Dynamic Cone Penetration Test commenced at 7.47m depth	8.53
End of Borehole Practical DCPT refusal at 8.53m depth (GWL @ 1.30m - July 16, 2018)	

SAMPLE TYPE	NUMBER	% RECOVERY	N VALUE or RQD
AU	1		
SS	2	58	7
SS	3	83	8
SS	4	96	4
SS	5	100	2
SS	6	96	1

DEPTH (m)	ELEV. (m)
0	82.59
1	81.59
2	80.59
3	79.59
4	78.59
5	77.59
6	76.59
7	75.59
8	74.59



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154 Colonnade Road South, Ottawa, Ontario K2E 7J5

SOIL PROFILE AND TEST DATA

Geotechnical Investigation
Prop. Warehouse Expansion - 2390 Stevenage Drive
Ottawa, Ontario

DATUM TBM - Top spindle of fire hydrant located just east of subject site. Geodetic elevation = 83.60m.

REMARKS

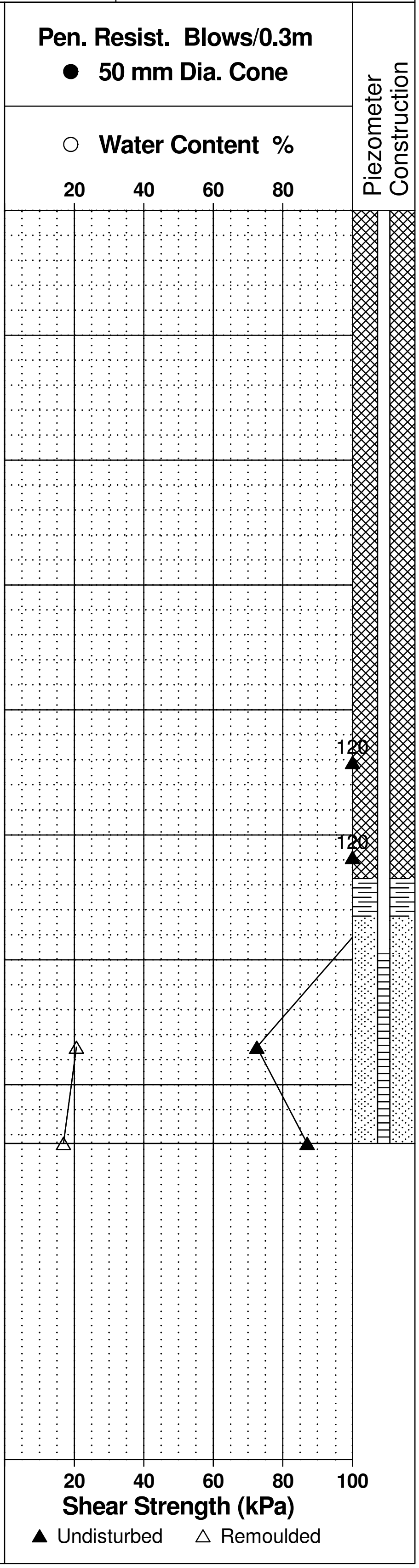
BORINGS BY CME 55 Power Auger

DATE July 11, 2018

FILE NO. PG4583

HOLE NO. BH 2

SOIL DESCRIPTION	STRATA PLOT	SAMPLE				DEPTH (m)	ELEV. (m)
		TYPE	NUMBER	% RECOVERY	N VALUE or RQD		
GROUND SURFACE						0	82.78
FILL: Crushed stone		AU	1				
0.63							
		SS	2	33	11	1	81.78
		SS	3	88	10		
						2	80.78
Very stiff to stiff, brown **SILTY CLAY**		SS	4	92	7		
- grey by 3.0m depth						3	79.78
		SS	5		3		
						4	78.78
						5	77.78
		SS	6	96	1		
						6	76.78
						7	75.78
7.47							
End of Borehole (Piezometer blocked at 1.21m depth - July 16, 2018)							



patersongroup Consulting Engineers

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

SOIL PROFILE AND TEST DATA

Geotechnical Investigation
Prop. Warehouse Expansion - 2390 Stevenage Drive
Ottawa, Ontario

DATUM TBM - Top spindle of fire hydrant located just east of subject site. Geodetic elevation = 83.60m.

REMARKS

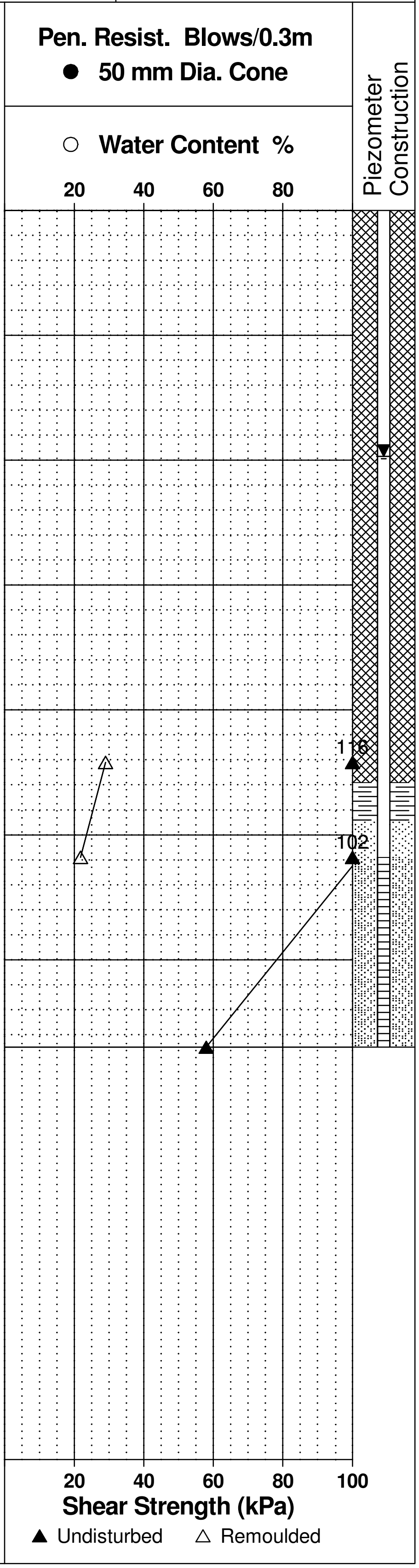
BORINGS BY CME 55 Power Auger

DATE July 11, 2018

FILE NO. PG4583

HOLE NO. BH 3

SOIL DESCRIPTION	SAMPLE TYPE	NUMBER	% RECOVERY	N VALUE or RQD	DEPTH (m)	ELEV. (m)
GROUND SURFACE					0	82.21
FILL: Crushed stone	AU	1				
0.51						
	SS	2	54	16	1	81.21
	SS	3	75	15		
					2	80.21
Very stiff to stiff, brown **SILTY CLAY**	SS	4	83	8		
- grey by 3.0m depth					3	79.21
	SS	5	92	4		
					4	78.21
					5	77.21
	SS	6	100	3		
					6	76.21
6.70						
End of Borehole						
(GWL @ 1.97m - July 16, 2018)						



SOIL PROFILE AND TEST DATA

Geotechnical Investigation
Prop. Warehouse Expansion - 2390 Stevenage Drive
Ottawa, Ontario

DATUM TBM - Top spindle of fire hydrant located just east of subject site. Geodetic elevation = 83.60m.

REMARKS

BORINGS BY CME 55 Power Auger

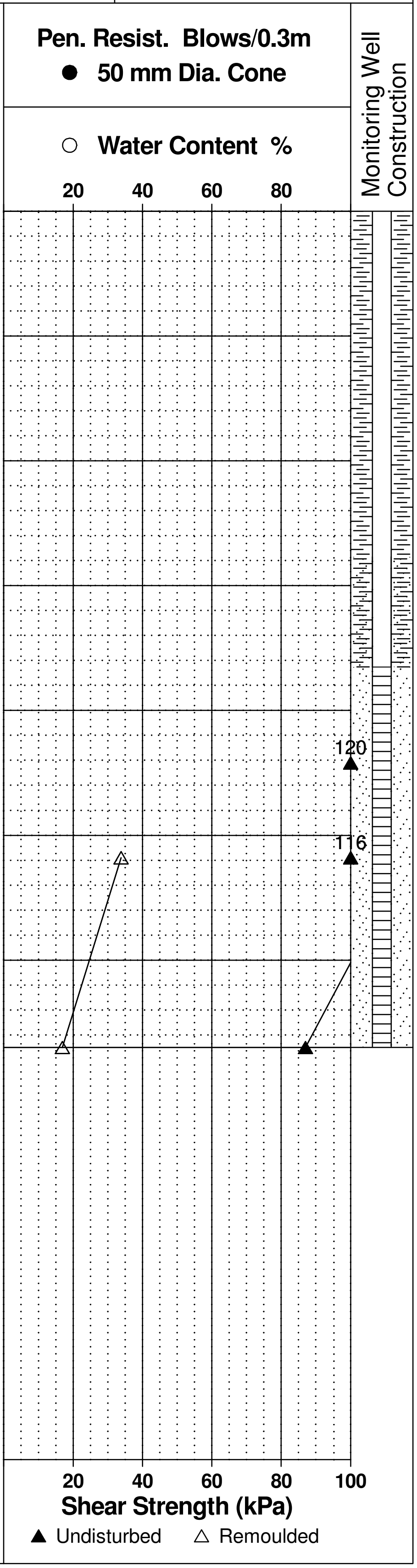
DATE July 11, 2018

FILE NO. PG4583

HOLE NO. BH 4

SOIL DESCRIPTION	STRATA PLOT	SAMPLE TYPE	SAMPLE NUMBER	SAMPLE % RECOVERY	SAMPLE N VALUE or RQD
GROUND SURFACE					
FILL: Crushed stone with silt and sand 0.60	▨	AU	1		
Very stiff, brown **SILTY CLAY,** trace gravel 1.45	▨	SS	2	42	6
Very stiff to stiff, brown **SILTY CLAY** - grey by 3.0m depth	▨	SS	3	96	10
	▨	SS	4	92	8
	▨	SS	5	96	5
6.70	▨	SS	6	0	1
End of Borehole					

DEPTH (m)	ELEV. (m)
0	82.62
1	81.62
2	80.62
3	79.62
4	78.62
5	77.62
6	76.62



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154 Colonnade Road South, Ottawa, Ontario K2E 7J5

SOIL PROFILE AND TEST DATA

Geotechnical Investigation
Prop. Warehouse Expansion - 2390 Stevenage Drive
Ottawa, Ontario

DATUM TBM - Top spindle of fire hydrant located just east of subject site. Geodetic elevation = 83.60m.

REMARKS

BORINGS BY CME 55 Power Auger

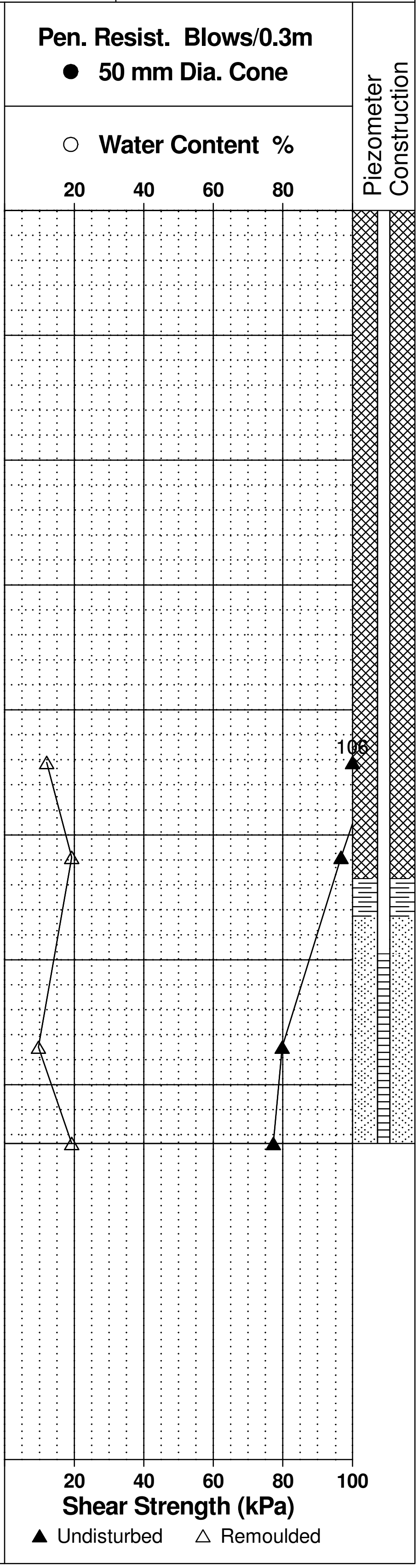
DATE July 11, 2018

FILE NO. PG4583

HOLE NO. BH 5

SOIL DESCRIPTION	TYPE	NUMBER	% RECOVERY	N VALUE or RQD
GROUND SURFACE				
FILL: Brown silty sand, some gravel 0.18	AU	1		
	SS	2	54	9
	SS	3	88	9
Very stiff to stiff, brown **SILTY CLAY**	SS	4	83	6
- grey by 3.0m depth	SS	5	96	3
	SS	6	100	W
7.47				
End of Borehole (Piezometer blocked at 3.33m depth - July 16, 2018)				

DEPTH (m)	ELEV. (m)
0	82.67
1	81.67
2	80.67
3	79.67
4	78.67
5	77.67
6	76.67
7	75.67



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SOIL PROFILE AND TEST DATA

Geotechnical Investigation
Prop. Warehouse Expansion - 2390 Stevenage Drive
Ottawa, Ontario

DATUM TBM - Top spindle of fire hydrant located just east of subject site. Geodetic elevation = 83.60m.

REMARKS

BORINGS BY CME 55 Power Auger

DATE July 11, 2018

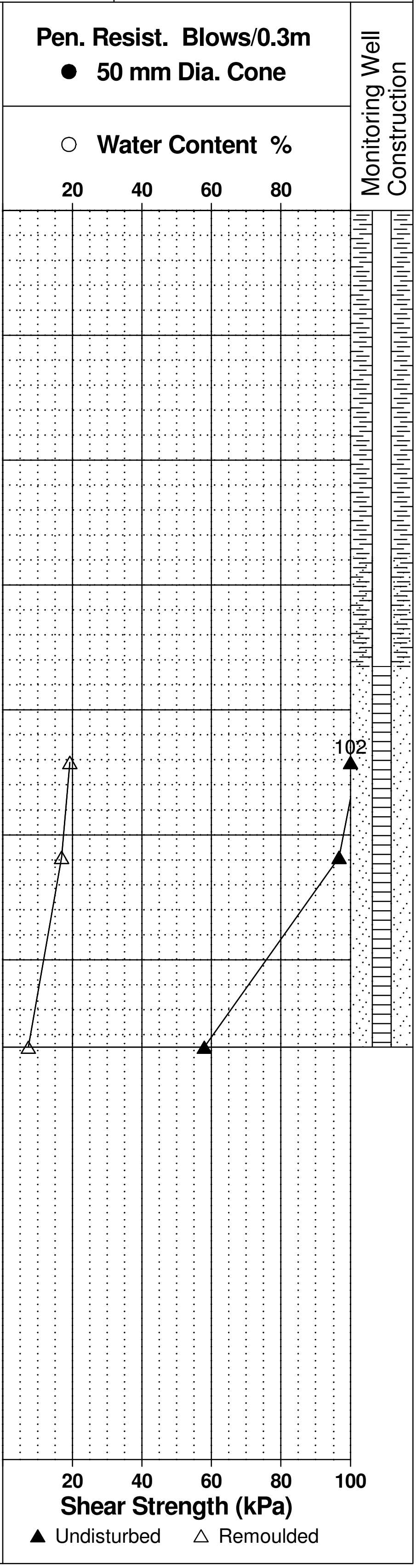
FILE NO. PG4583

HOLE NO. BH 6

SOIL DESCRIPTION	DEPTH (m)
GROUND SURFACE	
FILL: Crushed stone	0.59
Very stiff to stiff, brown **SILTY CLAY** - grey by 3.0m depth	6.70
End of Borehole	

SAMPLE TYPE	NUMBER	% RECOVERY	N VALUE or RQD
AU	1		
SS	2	33	5
SS	3	54	3
SS	4	83	4
SS	5	96	2
SS	6	100	W

DEPTH (m)	ELEV. (m)
0	82.68
1	81.68
2	80.68
3	79.68
4	78.68
5	77.68
6	76.68



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154 Colonnade Road South, Ottawa, Ontario K2E 7J5

SOIL PROFILE AND TEST DATA

Geotechnical Investigation
Prop. Warehouse Expansion - 2390 Stevenage Drive
Ottawa, Ontario

DATUM TBM - Top spindle of fire hydrant located just east of subject site. Geodetic elevation = 83.60m.

REMARKS

BORINGS BY CME 55 Power Auger

DATE July 11, 2018

FILE NO. PG4583

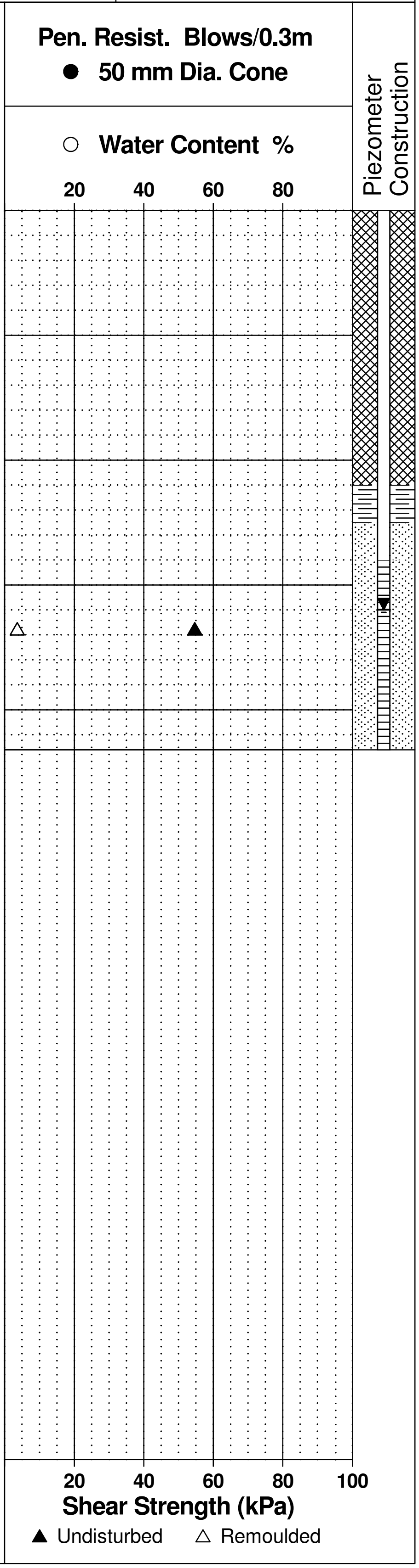
HOLE NO. BH 7

SOIL DESCRIPTION	TYPE	NUMBER	% RECOVERY	N VALUE or RQD	DEPTH (m)	ELEV. (m)
GROUND SURFACE					0	80.57
TOPSOIL 0.30	AU	1				
Very stiff to stiff, brown **SILTY CLAY**	SS	2	17	15	1	79.57
	SS	3	100	9	2	78.57
	SS	4	100	4		
- grey by 3.0m depth 3.81					3	77.57
GLACIAL TILL: Grey silty clay, some gravel, cobbles, boulders, trace sand 4.32	SS	5	64	50+	4	76.57

End of Borehole

Practical refusal to augering at 4.32m depth

(GWL @ 3.20m - July 16, 2018)



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SOIL PROFILE AND TEST DATA

Geotechnical Investigation
Prop. Warehouse Expansion - 2390 Stevenage Drive
Ottawa, Ontario

DATUM TBM - Top spindle of fire hydrant located just east of subject site. Geodetic elevation = 83.60m.

REMARKS

BORINGS BY CME 55 Power Auger

DATE July 11, 2018

FILE NO. PG4583

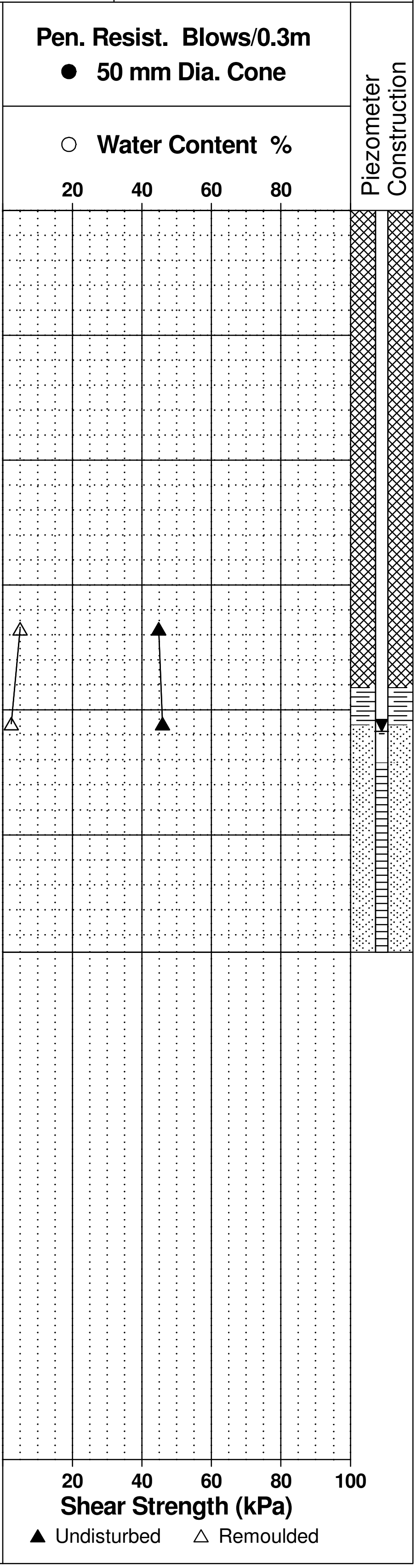
HOLE NO. BH 8

SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	SAMPLE % RECOVERY	SAMPLE N VALUE or RQD	DEPTH (m)	ELEV. (m)
GROUND SURFACE					0	81.02
TOPSOIL 0.33	AU	1				
Very stiff to stiff, brown **SILTY CLAY**	SS	2	100	17	1	80.02
	SS	3	100	10	2	79.02
	SS	4	100	4	3	78.02
- firm and grey by 3.0m depth 4.57					4	77.02
GLACIAL TILL: Dense, grey silty sand with gravel, cobbles, boulders, some clay 5.33	SS	5	79	42	5	76.02
Inferred weathered **BEDROCK** 5.94	SS	6	55	50+		

End of Borehole

Practical refusal to augering at 5.94m depth

(GWL @ 4.17m - July 16, 2018)



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SOIL PROFILE AND TEST DATA

Geotechnical Investigation
Prop. Warehouse Expansion - 2390 Stevenage Drive
Ottawa, Ontario

DATUM TBM - Top spindle of fire hydrant located just east of subject site. Geodetic elevation = 83.60m.

REMARKS

BORINGS BY CME 55 Power Auger

DATE July 11, 2018

FILE NO. PG4583

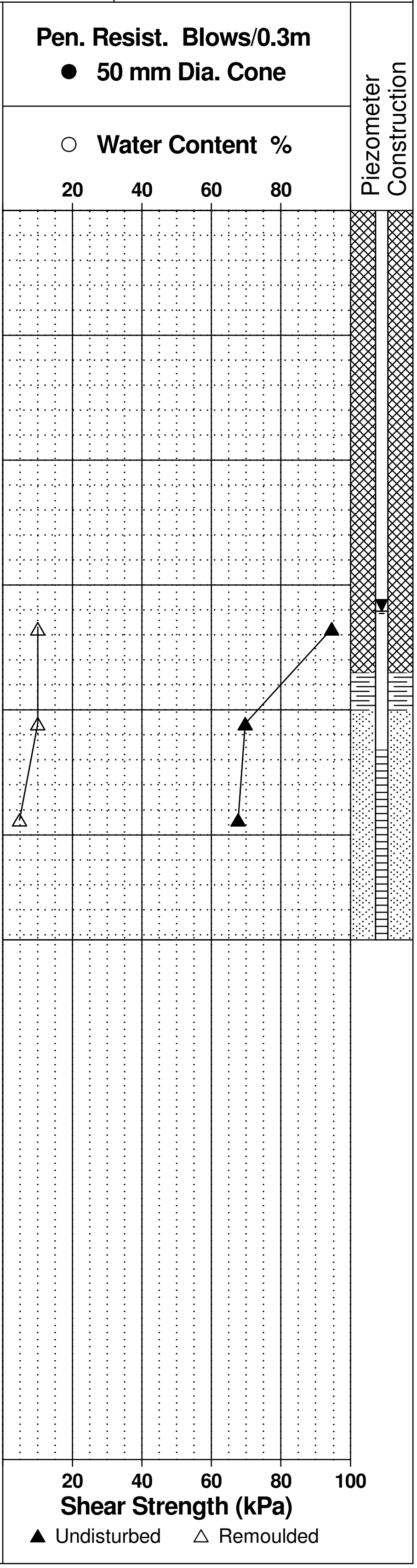
HOLE NO. BH 9

SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	% RECOVERY	N VALUE or RQD
GROUND SURFACE				
TOPSOIL (to 0.36)	AU	1		
Very stiff to stiff, brown **SILTY CLAY**	SS	2	92	17
	SS	3	100	12
	SS	4	100	5
- grey by 3.8m depth (to 5.33)				
GLACIAL TILL: Brown silty clay with gravel, cobbles, boulders, some sand (to 5.84)	SS	5	59	21
End of Borehole				

Practical refusal to augering at 5.84m depth

(GWL @ 3.21m - July 16, 2018)

DEPTH (m)	ELEV. (m)
0	81.89
1	80.89
2	79.89
3	78.89
4	77.89
5	76.89



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SOIL PROFILE AND TEST DATA

Geotechnical Investigation
Prop. Warehouse Expansion - 2390 Stevenage Drive
Ottawa, Ontario

DATUM TBM - Top spindle of fire hydrant located just east of subject site. Geodetic elevation = 83.60m.

REMARKS

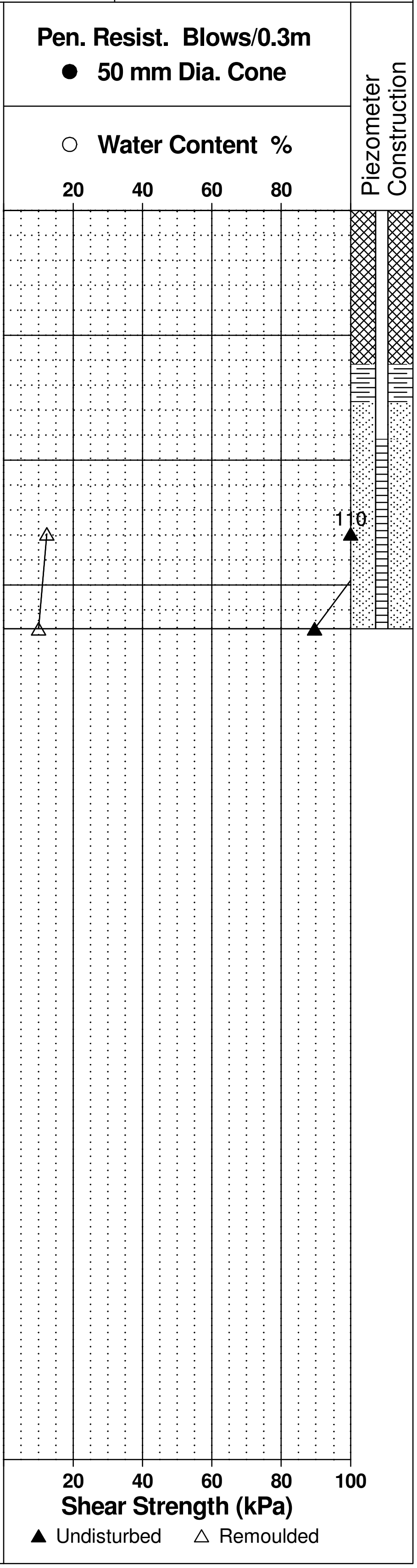
BORINGS BY CME 55 Power Auger

DATE July 11, 2018

FILE NO. PG4583

HOLE NO. BH10

SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	% RECOVERY	N VALUE or RQD	DEPTH (m)	ELEV. (m)
GROUND SURFACE					0	80.26
TOPSOIL 0.25	AU	1				
Very stiff to stiff, brown **SILTY CLAY**	SS	2	83	10	1	79.26
	SS	3	100	6	2	78.26
					3	77.26
3.35 End of Borehole (Piezometer blocked at 1.29m depth - July 16, 2018)						



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SOIL PROFILE AND TEST DATA

Geotechnical Investigation
Prop. Warehouse Expansion - 2390 Stevenage Drive
Ottawa, Ontario

DATUM TBM - Top spindle of fire hydrant located just east of subject site. Geodetic elevation = 83.60m.

REMARKS

BORINGS BY CME 55 Power Auger

DATE July 11, 2018

FILE NO. **PG4583**

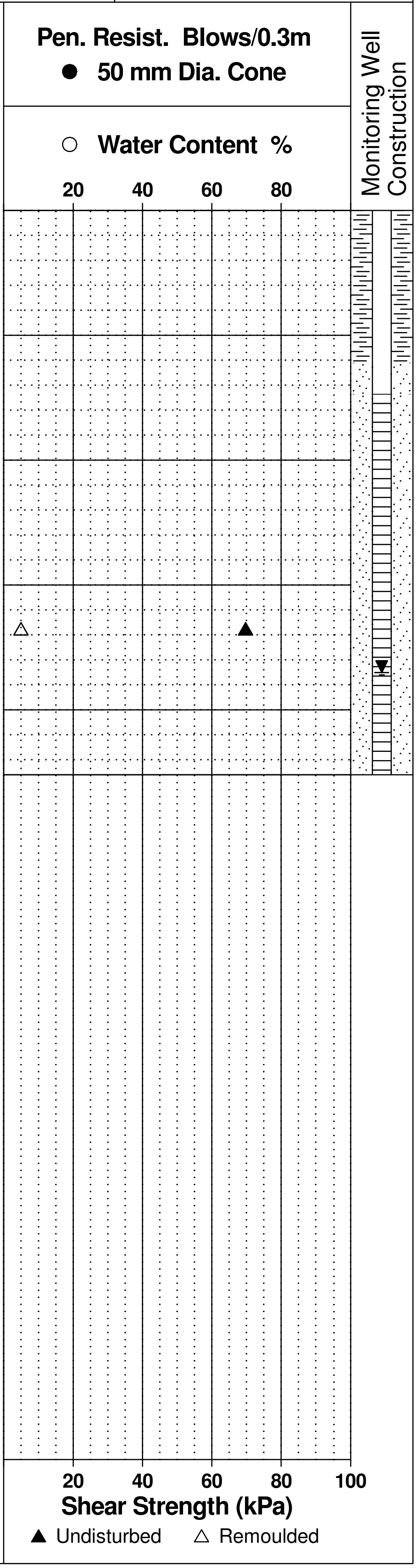
HOLE NO. **BH11**

SOIL DESCRIPTION	STRATA PLOT	SAMPLE TYPE	SAMPLE NUMBER	SAMPLE % RECOVERY	SAMPLE N VALUE or RQD	DEPTH (m)	ELEV. (m)
GROUND SURFACE						0	80.86
TOPSOIL 0.28		AU	1				
Very stiff to stiff, brown **SILTY CLAY** - grey by 2.3m depth		SS	2	83	12	1	79.86
		SS	3	100	9	2	78.86
		SS	4	100	4	3	77.86
3.81							
GLACIAL TILL: Grey silty clay with gravel, cobbles, boulders, trace sand		SS	5	100	50+	4	76.86
4.52							

End of Borehole

Practical refusal to augering at 4.52m depth

(GWL @ 3.70m - July 16, 2018)



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154 Colonnade Road South, Ottawa, Ontario K2E 7J5

SOIL PROFILE AND TEST DATA

Geotechnical Investigation
Prop. Warehouse Expansion - 2390 Stevenage Drive
Ottawa, Ontario

DATUM TBM - Top spindle of fire hydrant located just east of subject site. Geodetic elevation = 83.60m.

REMARKS

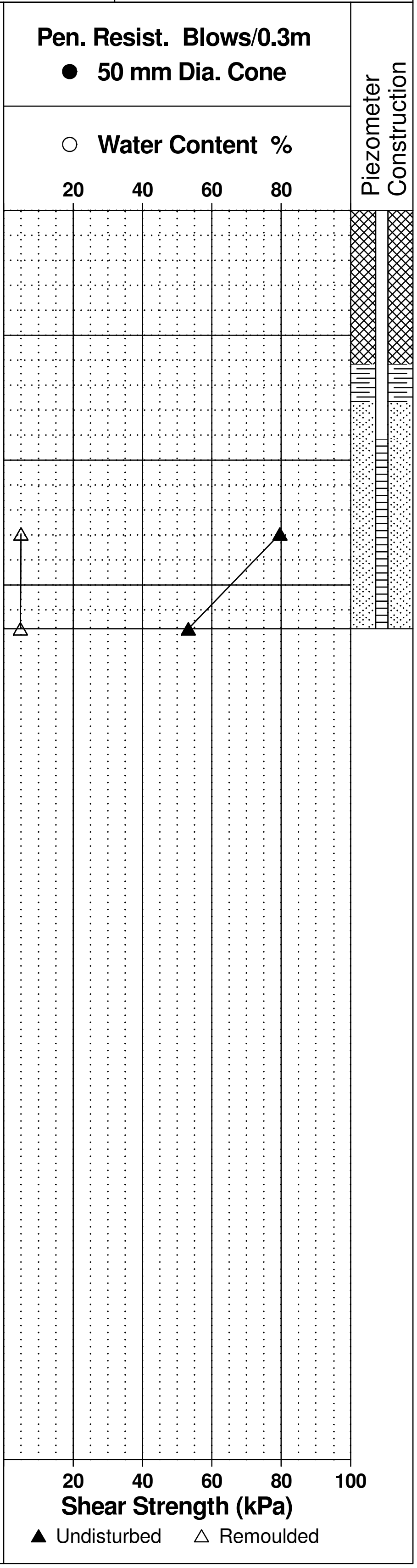
BORINGS BY CME 55 Power Auger

DATE July 11, 2018

FILE NO. PG4583

HOLE NO. BH12

SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	SAMPLE % RECOVERY	SAMPLE N VALUE or RQD	DEPTH (m)	ELEV. (m)
GROUND SURFACE					0	80.24
TOPSOIL 0.25	AU	1				
Very stiff to stiff, brown **SILTY CLAY**	SS	2		13	1	79.24
	SS	3		6	2	78.24
3.35					3	77.24
End of Borehole (Piezometer blocked at 1.73m - July 17, 2018)						



SYMBOLS AND TERMS

SOIL DESCRIPTION

Behavioural properties, such as structure and strength, take precedence over particle gradation in describing soils. Terminology describing soil structure are as follows:

Desiccated	-	having visible signs of weathering by oxidation of clay minerals, shrinkage cracks, etc.
Fissured	-	having cracks, and hence a blocky structure.
Varved	-	composed of regular alternating layers of silt and clay.
Stratified	-	composed of alternating layers of different soil types, e.g. silt and sand or silt and clay.
Well-Graded	-	Having wide range in grain sizes and substantial amounts of all intermediate particle sizes (see Grain Size Distribution).
Uniformly-Graded	-	Predominantly of one grain size (see Grain Size Distribution).

The standard terminology to describe the strength of cohesionless soils is the relative density, usually inferred from the results of the Standard Penetration Test (SPT) ‘N’ value. The SPT N value is the number of blows of a 63.5 kg hammer, falling 760 mm, required to drive a 51 mm O.D. split spoon sampler 300 mm into the soil after an initial penetration of 150 mm.

Relative Density	‘N’ Value	Relative Density %
Very Loose	<4	<15
Loose	4-10	15-35
Compact	10-30	35-65
Dense	30-50	65-85
Very Dense	>50	>85

The standard terminology to describe the strength of cohesive soils is the consistency, which is based on the undisturbed undrained shear strength as measured by the in situ or laboratory vane tests, penetrometer tests, unconfined compression tests, or occasionally by Standard Penetration Tests.

Consistency	Undrained Shear Strength (kPa)	‘N’ Value
Very Soft	<12	<2
Soft	12-25	2-4
Firm	25-50	4-8
Stiff	50-100	8-15
Very Stiff	100-200	15-30
Hard	>200	>30

SOIL DESCRIPTION (continued)

Cohesive soils can also be classified according to their "sensitivity". The sensitivity is the ratio between the undisturbed undrained shear strength and the remoulded undrained shear strength of the soil.

Terminology used for describing soil strata based upon texture, or the proportion of individual particle sizes present is provided on the Textural Soil Classification Chart at the end of this information package.

ROCK DESCRIPTION

The structural description of the bedrock mass is based on the Rock Quality Designation (RQD).

The RQD classification is based on a modified core recovery percentage in which all pieces of sound core over 100 mm long are counted as recovery. The smaller pieces are considered to be a result of closely-spaced discontinuities (resulting from shearing, jointing, faulting, or weathering) in the rock mass and are not counted. RQD is ideally determined from NXL size core. However, it can be used on smaller core sizes, such as BX, if the bulk of the fractures caused by drilling stresses (called "mechanical breaks") are easily distinguishable from the normal in situ fractures.

RQD %	**ROCK QUALITY**
90-100	Excellent, intact, very sound
75-90	Good, massive, moderately jointed or sound
50-75	Fair, blocky and seamy, fractured
25-50	Poor, shattered and very seamy or blocky, severely fractured
0-25	Very poor, crushed, very severely fractured

SAMPLE TYPES

SS	-	Split spoon sample (obtained in conjunction with the performing of the Standard Penetration Test (SPT))
TW	-	Thin wall tube or Shelby tube
PS	-	Piston sample
AU	-	Auger sample or bulk sample
WS	-	Wash sample
RC	-	Rock core sample (Core bit size AXT, BXL, etc.). Rock core samples are obtained with the use of standard diamond drilling bits.

SYMBOLS AND TERMS (continued)

GRAIN SIZE DISTRIBUTION

MC% - Natural moisture content or water content of sample, %
LL - Liquid Limit, % (water content above which soil behaves as a liquid)
PL - Plastic limit, % (water content above which soil behaves plastically)
PI - Plasticity index, % (difference between LL and PL)

Dxx - Grain size which xx% of the soil, by weight, is of finer grain sizes
These grain size descriptions are not used below 0.075 mm grain size
D10 - Grain size at which 10% of the soil is finer (effective grain size)
D60 - Grain size at which 60% of the soil is finer

Cc - Concavity coefficient = $(D30)^2 / (D10 \times D60)$
Cu - Uniformity coefficient = D60 / D10

Cc and Cu are used to assess the grading of sands and gravels:
Well-graded gravels have: $1 < Cc < 3$ and $Cu > 4$
Well-graded sands have: $1 < Cc < 3$ and $Cu > 6$
Sands and gravels not meeting the above requirements are poorly-graded or uniformly-graded.
Cc and Cu are not applicable for the description of soils with more than 10% silt and clay (more than 10% finer than 0.075 mm or the #200 sieve)

CONSOLIDATION TEST

p'_o - Present effective overburden pressure at sample depth
p'_c - Preconsolidation pressure of (maximum past pressure on) sample
Ccr - Recompression index (in effect at pressures below p'_c)
Cc - Compression index (in effect at pressures above p'_c)

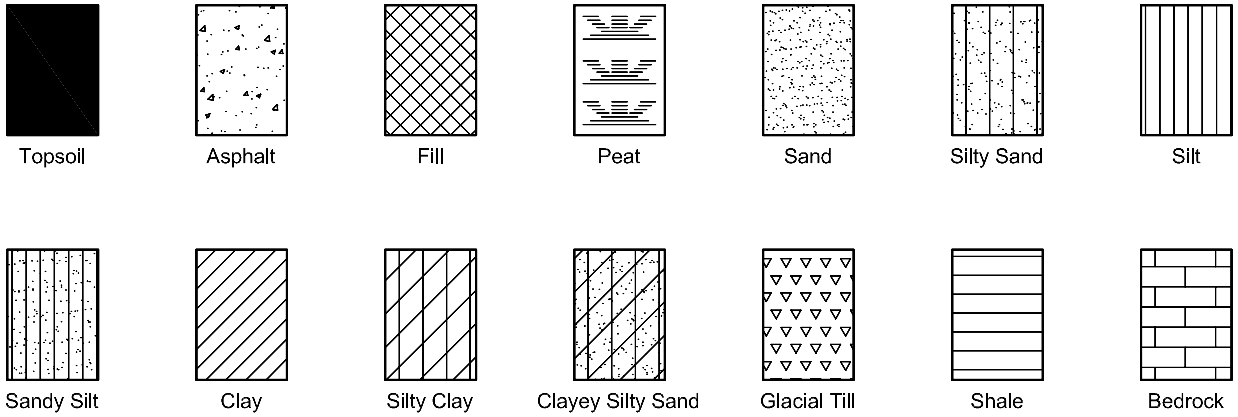
OC Ratio Overconsolidaton ratio = p'_c / p'_o
Void Ratio Initial sample void ratio = volume of voids / volume of solids
Wo - Initial water content (at start of consolidation test)

PERMEABILITY TEST

k - Coefficient of permeability or hydraulic conductivity is a measure of the ability of water to flow through the sample. The value of k is measured at a specified unit weight for (remoulded) cohesionless soil samples, because its value will vary with the unit weight or density of the sample during the test.

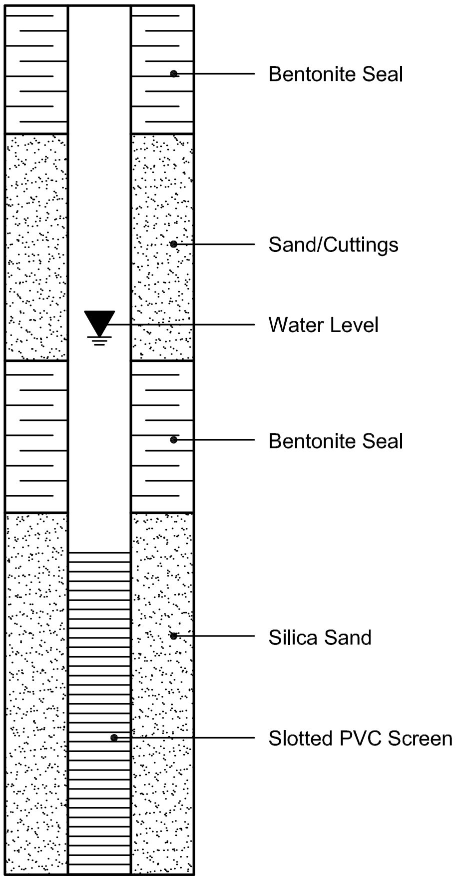
SYMBOLS AND TERMS (continued)

STRATA PLOT

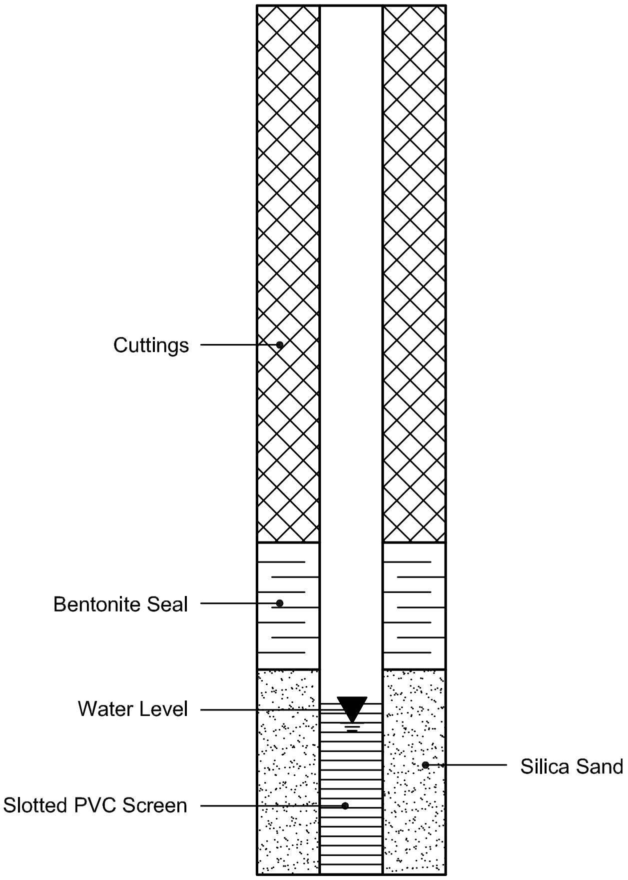


MONITORING WELL AND PIEZOMETER CONSTRUCTION

MONITORING WELL CONSTRUCTION



PIEZOMETER CONSTRUCTION



Certificate of Analysis

Client: Paterson Group Consulting Engineers

Client PO: 24635

Report Date: 19-Jul-2018

Order Date: 12-Jul-2018

Project Description: PG4583

	Client ID:	BH4-SS3	-	-	-
	Sample Date:	07/11/2018 09:00	-	-	-
	Sample ID:	1828523-01	-	-	-
	MDL/Units	Soil	-	-	-
Physical Characteristics					
% Solids	0.1 % by Wt.	70.3	-	-	-
General Inorganics					
pH	0.05 pH Units	7.53	-	-	-
Resistivity	0.10 Ohm.m	22.2	-	-	-
Anions					
Chloride	5 ug/g dry	153	-	-	-
Sulphate	5 ug/g dry	146	-	-	-

APPENDIX 2

FIGURE 1 - KEY PLAN

DRAWING PG4583-1 - TEST HOLE LOCATION PLAN

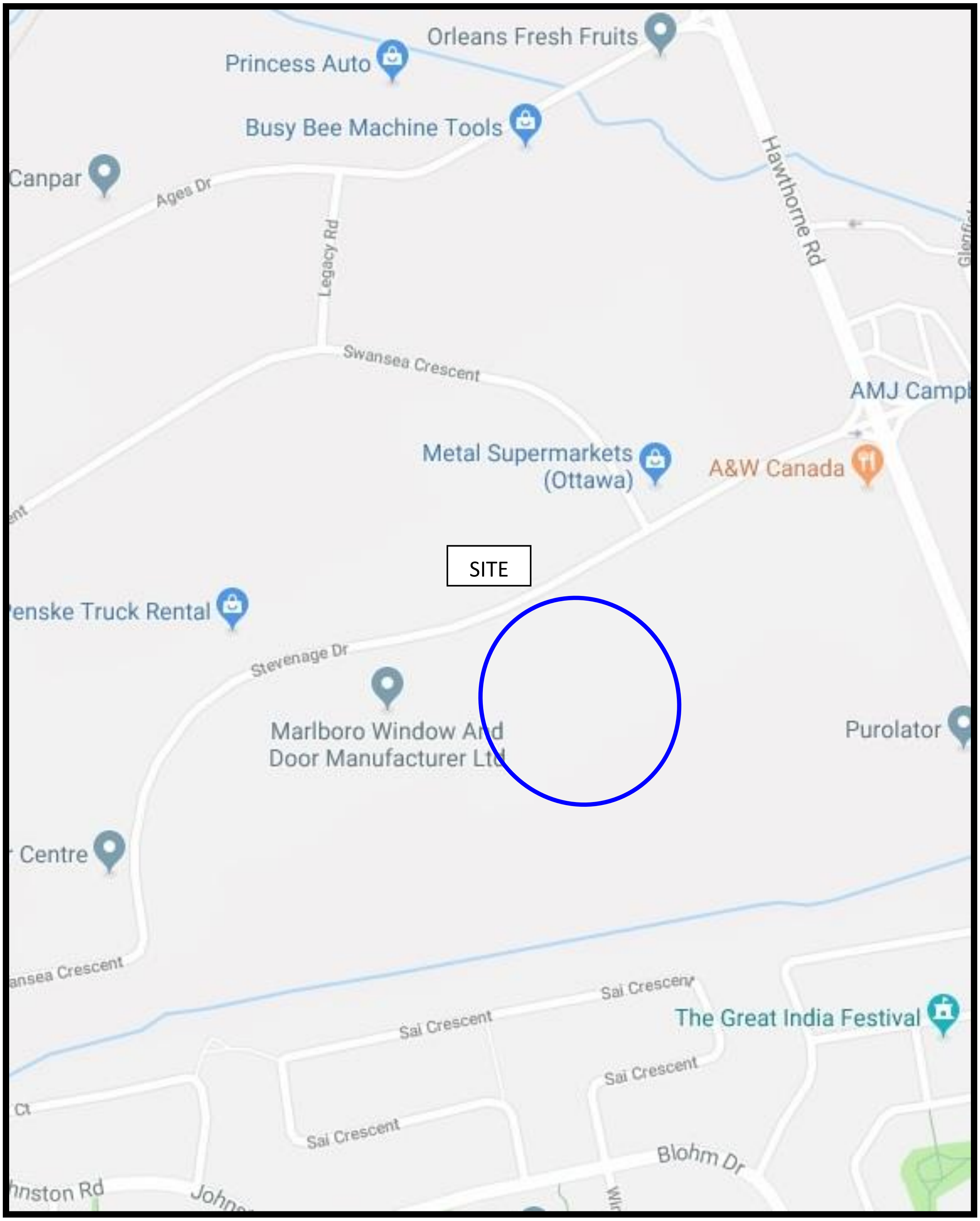
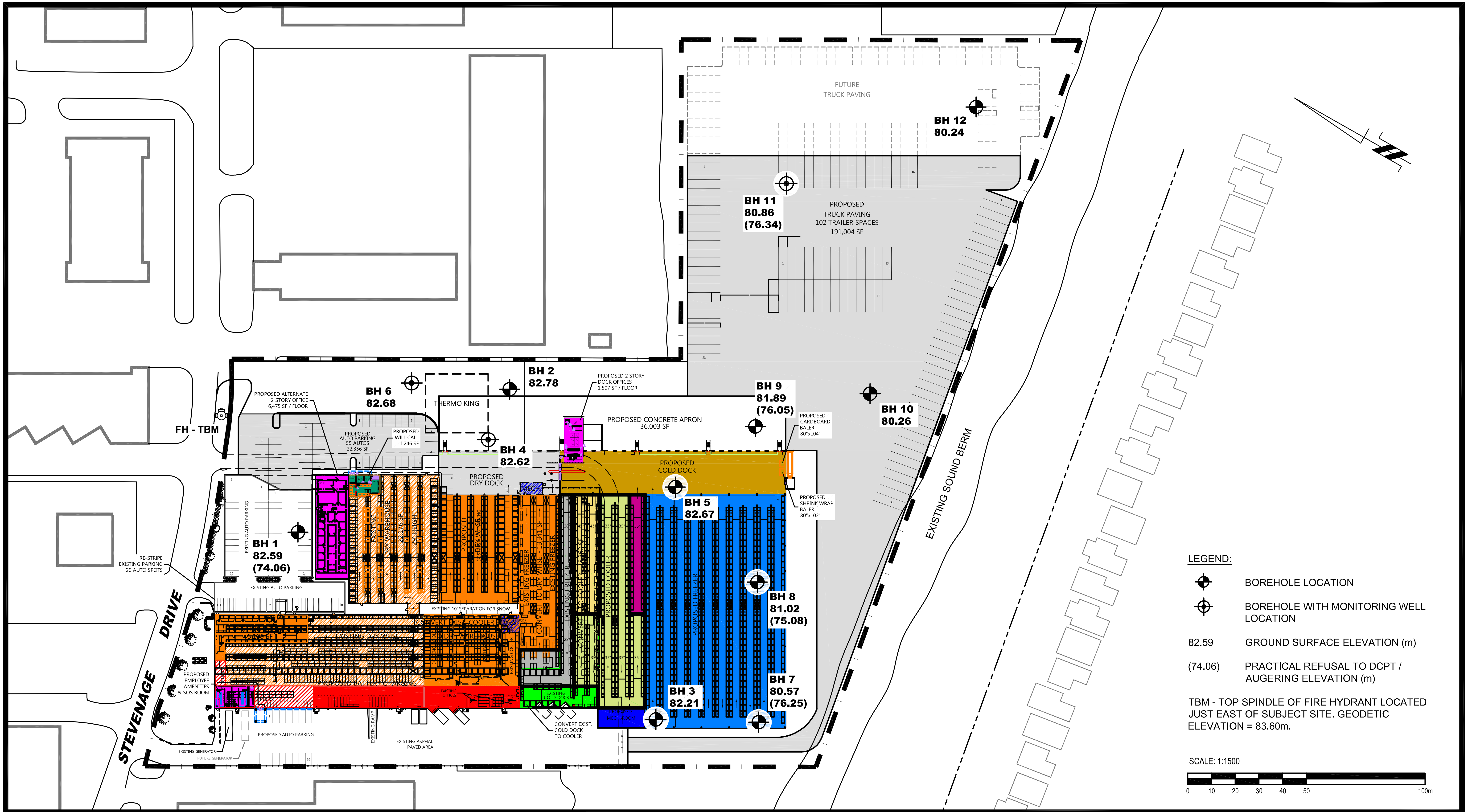


FIGURE 1

KEY PLAN

patersongroup



LEGEND:

⌖	BOREHOLE LOCATION
⌖	BOREHOLE WITH MONITORING WELL LOCATION
82.59	GROUND SURFACE ELEVATION (m)
(74.06)	PRACTICAL REFUSAL TO DCPT / AUGERING ELEVATION (m)

TBM - TOP SPINDLE OF FIRE HYDRANT LOCATED JUST EAST OF SUBJECT SITE. GEODETIC ELEVATION = 83.60m.

patersongroup
consulting engineers

154 Colonnade Road South
Ottawa, Ontario K2E 7J5
Tel: (613) 226-7381 Fax: (613) 226-6344

NO.	REVISIONS	DATE	INITIAL
0			

SYSCO
GEOTECHNICAL INVESTIGATION
PROPOSED WAREHOUSE EXPANSION - 2390 STEVENAGE DRIVE
OTTAWA, ONTARIO

Title:
TEST HOLE LOCATION PLAN

Scale: 1:1500	Date: 07/2018
Drawn by: MPG	Report No.: PG4583-1
Checked by: CB	Dwg. No.: PG4583-1
Approved by: DJG	Revision No.: 0

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