# MINTO COMMUNITIES INC. HARMONY STAGE 1 – BLOCK 104 DETAILED NOISE CONTROL STUDY

July 2018

Prepared for:

### MINTO COMMUNITIES INC.

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Prepared by:

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# HARMONY STAGE 1 – BLOCK 104 DETAILED NOISE CONTROL STUDY

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### 1.0 INTRODUCTION

Minto Communities Inc. (Minto) retained the services of J.L. Richards & Associates Limited (JLR) to assess the potential environmental noise impact on the proposed stacked townhome development referred to as Harmony Stage 1 – Block 104, located at 4025 Strandherd Drive in the Barrhaven South Community (BSC) in the City of Ottawa.

This study is prepared to satisfy the Ministry of Environment (MOE) Environmental Noise Guidelines NPC-300 and the City of Ottawa Environmental Noise Control Guidelines (approved by City Council January 2016) and in particular Part 4 Section 3.2 Noise Control Detailed Study Requirements in support of the Site Plan Application.

## 2.0 PROJECT DESCRIPTION

The lands subject of this Study, identified on Figure 1 (refer to attached) as Harmony Stage 1 – Block 104, are bounded by Chakra Street to the north, Chapman Mills Drive to the west, a future transitway to the south, and future residential development to the east. The proposed development has an area of approximately 0.32 ha and consists of two stacked townhome blocks consisting of 12 units each for a total of 24 units on site.

Appendix 'A' includes the overall Harmony Draft Plan of Subdivision. The proposed stacked townhome development Block is referred to as Block 104.

# 3.0 TRANSPORTATION NOISE SOURCE

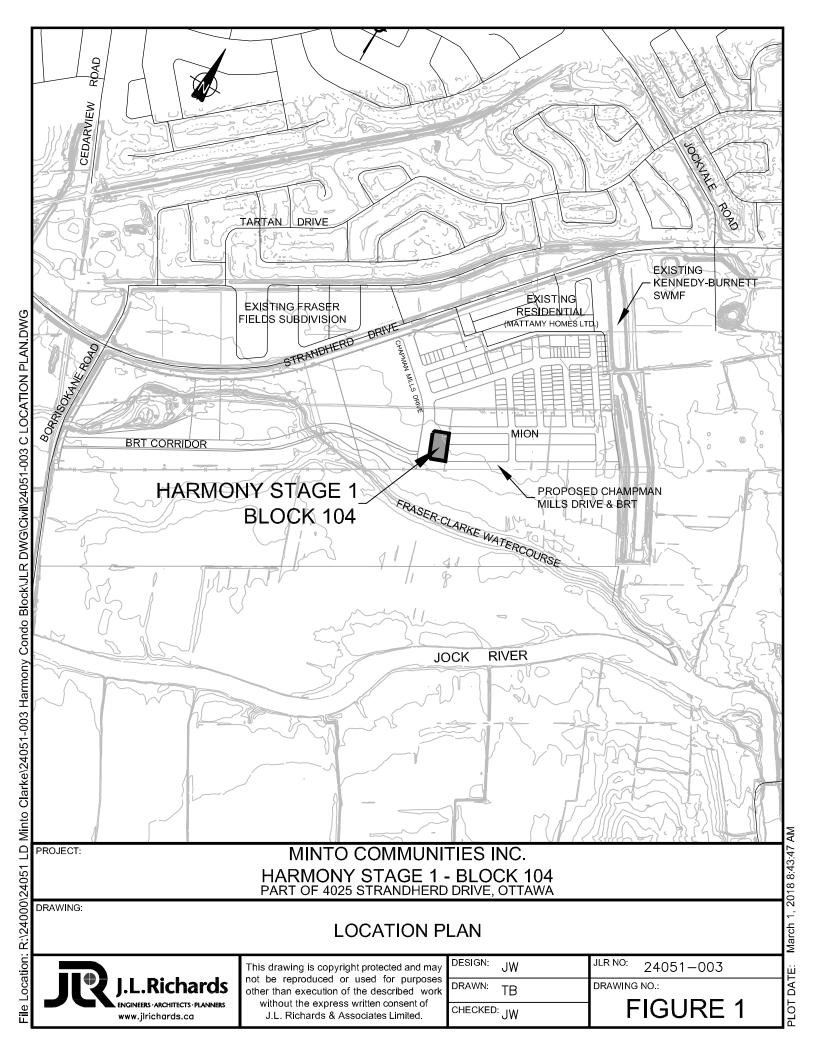
The transportation noise sources for this study include Chapman Mills Drive, and the proposed BRT. Drawing N1 (refer to Appendix 'B') shows the location of the existing and proposed roadways in relation to the proposed development. Strandherd Drive is outside the 100 m range of influence; therefore, it is not considered a noise source for the purposes of this study.

#### 3.1 Transportation Sound Level Criteria

For the purpose of determining the predicted noise levels, and based on the sound level criteria established by the City of Ottawa Environmental Noise Control Guidelines (ENCG), the following will be used as the maximum acceptable sound levels (Leq) for residential development and other land uses, such as nursing homes, schools and daycare centres:

Receiver Location	<u>Criteria</u>	Time Period
Outdoor living area:	55 dBA	Daytime (0700 - 2300 hrs)
Indoor living/dining rooms (inside):	45 dBA	Daytime (0700 - 2300 hrs)
General Office, Reception Area (inside):	50 dBA	Daytime (0700 - 2300 hrs)
Sleeping Quarters (inside):	40 dBA	Nighttime (2300 - 0700 hrs)

Outdoor Living Areas (OLA) are defined as that portion of the outdoor amenity area of a dwelling for the quiet enjoyment of the outdoor environment during the daytime period.



Typically, the point of assessment in an OLA is 3.0 m from the building façade mid-point and 1.5 m above the ground within the designated OLA for each individual unit. OLAs commonly include backyards, balconies (with a minimum depth of 4 m as per NPC-300), common outdoor living areas, and passive recreational areas. For the purpose of this study the amenity space identified on Drawing N1 is considered the only OLA for the Harmony Stage 1 – Block 104. The point of assessment was chosen to be the middle of the amenity space as shown on Drawing N1.

For indoor noise impact, the point of assessment at the Plane of Window (POW) will be the middle of each floor as calculated from the building elevation drawings provided by Minto (refer to Appendix 'C').

## 3.2 Transportation Noise Attenuation Requirements

When the sound levels are equal to or less than the specified criteria, per the City of Ottawa ENCG and/or MOE NPC-300, noise attenuation (control) measures may not be required.

The following tables outline noise attenuation measures to achieve required dBA Leq for surface transportation noise, per the City of Ottawa ENCG.

Table 1: Outdoor Noise Control Measures for Surface Transportation Noise

	Secondary Mitigation Measures			
Primary Mitigation Measure (in order of preference)	Landscape plantings and/or non-acoustic fence to obscure noise source	Warning Clauses		
Distance setback with soft ground				
Insertion of Noise insensitive land uses between the source and receiver receptor	Recommended			
Orientation of buildings to provide sheltered zones in rear yards		Warning Clauses necessary and to include: - Reference to specific noise		
Shared outdoor amenity areas	Paguirod	mitigation measures in the development.		
Earth berms (sound barriers)	Required	- Whether noise is expected to increase in the future.		
Acoustic Barriers (acoustic barriers)		- That there is a need to maintain mitigation.		

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Table 2: Indoor Noise Control Measures for Surface Transportation Noise

	Secondary Mitigation Measures			
Primary Mitigation Measure (in order of preference)	Landscape plantings and/or non-acoustic fence to obscure noise source	Warning Clauses		
Distance setback with soft ground				
Insertion of Noise insensitive land uses between the source and receiver	Recommended	Not necessary		
receptor				
Orientation of buildings to provide sheltered zones or modified interior spaces and amenity areas		Warning Clauses necessary and to include: - Reference to specific noise		
Enhanced construction techniques and construction quality	Required	mitigation measures in the development.		
Earth berms (sound barriers)		- Whether noise is expected		
Indoor isolation – air conditioning and ventilation, enhanced dampening materials (indoor isolation)		to increase in the future.  That there is a need to maintain mitigation.		

The following tables outline the noise level limits per the MOE NPC-300 and City of Ottawa ENCG.

Table 3: Outdoor Living Area (OLA) Noise Limit for Surface Transportation

Time Period	Leq (16 hr) (dBA)	
16 hr, 07:00 am - 23:00	55	

**Table 4: Indoor Noise Limit for Surface Transportation** 

Type of Space	Time Period	Leq (dBA)	
Type of Space	Time Period	Road	Rail
Living/Dining, den areas of residences, hospitals, nursing homes, schools, daycare centres, etc.	07:00-23:00	45	40
Living/Dining, den areas of residences, hospitals, nursing homes, etc. (except schools or daycare centres)	23:00-07:00	45	40
	07:00-23:00	45	40
Sleeping Quarters	23:00-07:00	40	35

In addition to the implementation of noise attenuation features, if required, and depending on the severity of the noise problem, warning clauses may be recommended to advise the prospective purchasers/tenants of affected units of the potential environmental noise. These warning clauses should be included in the Site Plan and Subdivision Agreements, in the Offers of Purchase and Sale, and should be registered on Title. Warning clauses may be included for any development, irrespective of whether it is considered a noise sensitive land use.

Where site measures are required to mitigate noise levels, the City of Ottawa requires that notices be placed on Title informing potential buyers and/or tenants of the site conditions. Sample templates of the notices that could be registered on Title as presented in the City of Ottawa ENCG (Part 4 Appendix 'A').

Detailed wording for clauses should be provided as part of the Detailed Noise Control Study completed in support of the Site Plan Application. Clauses are to be worded to describe the mitigation measures and noise conditions applicable where MOE and City of Ottawa noise criteria are exceeded.

### 3.3 Prediction of Noise Levels (Transportation)

#### 3.3.1 Road Traffic Data

The following traffic data was used to predict noise levels:

**Chapman Mills Drive** Total Traffic Volume (AADT) 12.000 Day/Night Split (%) 92/8 Medium Trucks (%) 7 Heavy Trucks (%) 5 Posted Speed (km/hr) 50 Road Gradient (%) 1 2-Lane Major Road Classification Collector (2-UMCU)

Table 5: Road Traffic Data to Predict Noise Levels

Schedule 'E' and Annex 1 of the City of Ottawa Official Plan (May 2003) were utilized to determine the correct road classification and protected right-of-way. These road classifications were compared to Map 6 of the City of Ottawa Transportation Master Plan (Road Network – Urban). All findings were then compared to Table B1 (Part 4, Appendix 'B') of the City of Ottawa Environmental Noise Control Guidelines in order to determine an appropriate AADT value.

#### 3.3.2 Bus Rapid Transit Corridor Data

Figure 1 shows the location of the Bus Rapid Transit (BRT) Corridor in relation to the proposed residential development. The City has classified this corridor as a Bus Rapid Transit Corridor. The following data was used to predict noise levels:

Table 6: Bus Rapid Transit Corridor Data to Predict Noise Levels

	Bus Rapid Transit Corridor
Total Traffic Volume (AADT)	258
Day/Night Split (%)	74/26
Medium Trucks (%)	100
Heavy Trucks (%)	0
Posted Speed Limit (km/hr)	80
Road Gradient (%)	1

The assumed posted speed limit along the dedicated BRT corridor is 80 km/hr. Appendix 'D' includes a summary of the information provided by the City specific to the Bus Rapid Transit Corridor, including how the AADT value and the day/night split was calculated.

The computer program Stamson is used to predict noise levels associated with the bus rapid transit corridor.

# 3.3.3 Noise Level Calculations (Transportation)

The noise levels for the daytime and nighttime periods were calculated for a number of representative receivers described in Table 7 and shown on Drawing N1, using the MOE Road Traffic Noise Computer program STAMSON, Version 5.03.

Computer printouts are included in Appendix 'E'.

**Table 7: Predicted Noise Levels (Transportation)** 

		Noise Le	vels (dBA)
Receiver No. and File Names	Receiver Description and Location	Daytime	Nighttime
R1 condoR1	Outdoor Living Area of Harmony Stage 1 – Block 104 (Amenity Area) at a distance of 25.5 m from the centreline of Chapman Mills Drive and 54.1 m from the centreline of the BRT.	61.65	n/a
R2a condoR2a	Plane of Window (Lower Unit, 12A) fronting on Chapman Mills Drive & BRT at a distance of 24.6 m from the centreline of Chapman Mills Drive and the BRT.	63.26	56.98
R2b condoR2b	Plane of Window (Upper Unit, 12B) fronting on Chapman Mills Drive and the BRT at a distance of 24.6 m from the centreline of Chapman Mills Drive and the BRT.	63.59	57.76
R3a condor3a	Plane of Window (Lower Unit, 4A) fronting on Chapman Mills Drive at a distance of 19.9 m from the centreline of Chapman Mills Drive and 85.1 m from the centreline of the BRT.	64.20	56.65
R3b condor3b	Plane of Window (Upper Unit, 4B) fronting on Chapman Mills Drive at a distance of 19.9 m from the centreline of Chapman Mills Drive and 85.1 m from the centreline of the BRT.	64.46	57.35

# 3.4 Summary of Findings (Transportation)

A summary of the minimum noise requirements and required Warning Clauses is shown on Table 8. The units will require notices to be registered on Title, advising the occupants of the environmental noise problems and/or of the noise attenuation measures being implemented.

**Table 8: Minimum Required Control Features/Warning Clauses (Transportation)** 

Receiver Location	Noise Attenuation Barrier	Central Air Conditioning	Forced Air Heating	Warning Clauses	Building Components Study
Amenity Area	No	No	No	А	No
Plane of Window (Units 1A, 1B, 2A, 2B, 3A, 3B, 4A, 4B, 5A, 5B, 6A, 6B, 7A, 7B, 8A, 8B, 9A, 9B, 10A, 10B, 11A, 11B, 12A, 12B)	No	No	Yes	В	No

JLR calculated predicted mitigated noise levels using 2.2 m and 2.5 m high noise barriers. Detailed calculations are included in Appendix 'F'. Table 9 summarizes the predicted freefield daytime noise level at receiver R1 and the mitigated noise level resulting from the inclusion of the possible noise attenuation barriers, as shown on Drawing N1. Calculations indicate that a 2.5 m high noise barrier for the Harmony Stage 1 – Block 104 Amenity Area will mitigate noise levels to 54.58 dBA.

Table 9: Noise Attenuation Due to Assessed Barriers

Receiver No. and File Name	Receiver Location	Daytime Noise Level (dBA)	Attenuated Leq 16 hr (dBA) with a 2.2 m High Barrier	Attenuated Leq 16 hr (dBA) with a 2.5 m High Barrier	Receiver Ground Elevation (m)	Barrier Base Elevation + Barrier Height = Top of Barrier (m)
R1 R1BR22 R1BR25	Amenity Area	61.65	55.70	54.58	93.97	93.80 <b>+ 2.5</b> = 96.30

A copy of the grading plan(s) has been included in Appendix 'G'. The grading plan(s) were used to determine the ground elevation for the noise receivers and barrier base.

The intent of the Block 104 Amenity Area is to be a shared inviting open space with landscaping where residents of Block 104 can gather to enjoy the outdoors and feel connected to the neighbourhood. Construction of a noise barrier will always interfere with this goal. However, in this instance, the construction of a noise barrier to achieve a 1.5 dBA noise reduction may be interpreted as an invasive treatment for nominal benefit. Rather than prescriptively recommending that a noise barrier be installed, a short discussion is presented identifying administrative and economic challenges of this solution.

# 1. Administrative Challenges -

Inconsistent Application of Interpretation: The Amenity area is a shared space exclusively for residents of Block 104 but is not a private rear yard and should not be treated as such. By definition, the Amenity Area more closely reflects a City park or school yard, rather than a private rear yard. Parks and school yards are generally not subject to the rigorous noise examination as private rear yards. In this case, the amenity space fits the model of a park/school yard rather than a private rear yard.

Arbitrary Size Limit: The City's Zoning By-Law defines an Amenity Area as "...the total passive or active recreational area provided on a lot for the personal, shared or communal use of the residents of a building or buildings, and includes balconies, patios, rooftop gardens and other similar features, but does not include indoor laundry or locker facilities." By this definition all landscaped/grassed areas, regardless of size are Amenity Areas. Therefore, the only reason the "labelled" Amenity Area requires a noise assessment is due to its size. Each of the 24 units will have a private balcony which are anticipated to be the most used amenity space on the site and will add overall outdoor space for the residents as a private amenity space. From a zoning perspective the Amenity Area does not require any form of noise mitigation, however, strictly due to its size and location the proposed shared amenity area surpasses the area requirements of the Environmental Noise Control Guidelines (ENCG) triggering a noise assessment. The balconies do not require mitigation from transportation noise sources, due to their size.

Amenity Area location is the Result of City Consultation: City staff encouraged Minto, as part of the pre-consultation follow-up email dated January 15, 2018 (included in Appendix 'H'), to "incorporate landscaping and/or increased setbacks in order to minimize the impact of parking along Chapman Mills..." thereby creating an amenity

area adjacent to a noise source. Regardless, Minto tried its best to locate the Amenity Area between the buildings to reduce the exposure angles to the noise source. Minto's decision to respond to City suggestions for Site Plan modifications created an amenity space where none existed before. Given the nominal exceedance of the noise criteria, it is our opinion that cooperation with City staff should not be met with additional administrative requirements.

Barrier will Partition the Site from the Community: Construction of a noise barrier would create a closed off area that would not be enjoyable to use by interfering with the movement and views of the residents and would separate the Amenity Area from the neighbourhood. Furthermore, a noise barrier would negatively contribute to the urban design of the site and neighbourhood, as well as reduce safe access along the pathways and minimize the area available for landscaping.

### 2. Economic Challenges -

Additional Cost to Further Revise the Site Plan: Different building orientations have previously been explored by Minto. After integrating the City's pre-consultation recommendations, the current Site Plan provides the preferred building orientation for all parties. Revising the Site Plan, would cause undue construction delay for Minto as well as exponentially increasing costs associated with Block 104 redesign. It is JLR's opinion that additional costs to review alternative Site Plan arrangements are an excessive attempt to meet a 1.5 dBA noise reduction in the amenity area.

Minor Variance: Minto could apply for a Minor Variance to remove the Amenity Area requirement. This process is predicted to be more affordable than constructing a noise barrier. Removing the Amenity Area is not Minto's preferred approach. Minto would rather keep the Amenity area for the enjoyment of the residents. The City's Minor Variance application fee is \$2,500 and is much less than the noise barrier installation.

Given the above challenges and nominal benefit of trying to achieve at least 60 dBA (a 1.5 dBA noise reduction), it is recommended that the noise barrier be eliminated as a requirement for the site development.

#### 3.5 Summary of Findings (Building Component)

Building Component analysis is not required since the Plane of Window (i.e., see Table 8, R3B) noise levels are below the minimum Building Component threshold of 65 dBA.

Minto provided floor plan and building elevation drawings, for the 'Jasmine', 'Rooibos', 'Matcha' and 'Chai' units. Floor and elevation drawings are included in Appendix 'C'. These units are considered representative units for a typical Minto stacked townhome development. The 'Jasmine' and 'Rooibos' could be expected to represent the end units and the 'Rooibos' and 'Matcha' could be expected to represent the interior units.

A standard wall construction detail with a 38 x 89 mm complete with siding, sheathing, insulation and 12.7 mm gypsum board will provide satisfactory acoustic insulation to achieve indoor noise requirements.

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Minto's standard exterior wall construction is 38 x 148 mm complete with 140 mm fibre insulation, siding, 19 mm sheathing, 12.7 mm gypsum board, and often a brick veneer on the exterior lower level wall.

# 4.0 OPINION OF PROBABLE COSTS (OPC) FOR MITIGATION MEASURES

Based on discussions with Minto, the following table summarizes our opinion of probable costs for the mitigation measures identified in this report.

Item	Cost per Unit	Estimated Quantity	Estimated Sub- Total
Noise Barrier (2.5m High)	\$450/m	31 m	\$13,950
Estima	\$13,950		

**Table 10: Opinion of Probable Costs for Mitigation Measures** 

# 5.0 CONCLUSION AND RECOMMENDATIONS

Predicted noise levels are expected to exceed the City of Ottawa ENCG and MOE criteria for daytime outdoor living areas for the proposed amenity space adjacent to Chapman Mills Drive, and the proposed BRT. To address these exceedances, Minto has revised the site plan to reduce the reliance of noise barriers as the primary noise mitigation tool. Building orientation and increased separation to the transportation noise source have been used to reduce noise levels for residential units in close proximity to a significant transportation noise source. Calculations indicate that a 2.5 m high noise barrier will satisfactorily mitigate noise levels for the amenity area. Although a 2.2 m high barrier will help to mitigate the noise levels, it will not mitigate the noise sufficiently enough to meet the MOE's and City's criteria. Regardless, it is recommended that no noise barrier be constructed so that the residents can enjoy the outdoor Amenity Area with minimal interference due to road/transitway traffic.

Standard wall and window construction details that Minto utilize for their residential units, as presented with their elevation drawings, will exceed the minimum requirements to mitigate the exterior noise levels to meet the MOE and City of Ottawa indoor noise criteria.

#### 5.1 Indoor Noise Control Features

#### 5.1.1 Forced Air Heating System

The following Units/Lots shall be fitted with a forced air heating system, with the provision for the future installation of central air conditioning:

- Units 1A, 1B, 2A, 2B, 3A, 3B, 4A, 4B, 5A, 5B, 6A, 6B;
- Units 7A, 7B, 8A, 8B, 9A, 9B, 10A, 10B, 11A, 11B, 12A, 12B.

## 5.2 Warning Clauses

#### 5.2.1 Warning Clause Type A

Clause A is to be registered on Title for the outdoor amenity space of Block 104 (Units 1A, 1B, 2A, 2B, 3A, 3B, 4A, 4B, 5A, 5B, 6A, 6B, 7A, 7B, 8A, 8B, 9A, 9B, 10A, 10B, 11A, 11B, 12A, 12B, inclusive):

"Purchasers/tenants are advised that, sound levels due to increasing road/transitway traffic may, on occasion, interfere with some outdoor activities as the sound levels exceed the sound level limits of the City and the Ministry of the Environment."

### 5.2.2 Warning Clause Type B

Clause B is to be registered on Title for Units 1A, 1B, 2A, 2B, 3A, 3B, 4A, 4B, 5A, 5B, 6A, 6B, 7A, 7B, 8A, 8B, 9A, 9B, 10A, 10B, 11A, 11B, 12A, 12B, inclusive:

"Purchasers/tenants are advised that despite the inclusion of noise control features within the building units, sound levels due to increasing road/transitway traffic may, on occasion, interfere with some activities of the dwelling occupants as the sound levels exceed the sound level limits of the City and the Ministry of the Environment.

To help address the need for sound attenuation this dwelling unit includes:

- single/multi-pane glass windows;
- provision for central air conditioning.

To ensure that provincial sound level limits are not exceeded it is important to maintain these sound attenuation features.

This dwelling unit has also been designed with the provision for adding central air conditioning at the occupant's discretion. Installation of central air conditioning will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the sound level limits of the City and the Ministry of the Environment."

# 5.3 Site Plan Agreement and Notices on Title

It is recommended that the previous recommendations and Warning Clauses are to be included in the Site Plan Agreement and in the Offers of Purchase and Sale and/or lease of the affected units, and be registered on Title.

This report has been prepared for the exclusive use of Minto Communities Inc., for the stated purpose, for the named facility. Its discussions and conclusions are summary in nature and cannot be properly used, interpreted or extended to other purposes without a detailed understanding and discussions with the client as to its mandated purpose, scope and

# HARMONY STAGE 1 – BLOCK 104 DETAILED NOISE CONTROL STUDY

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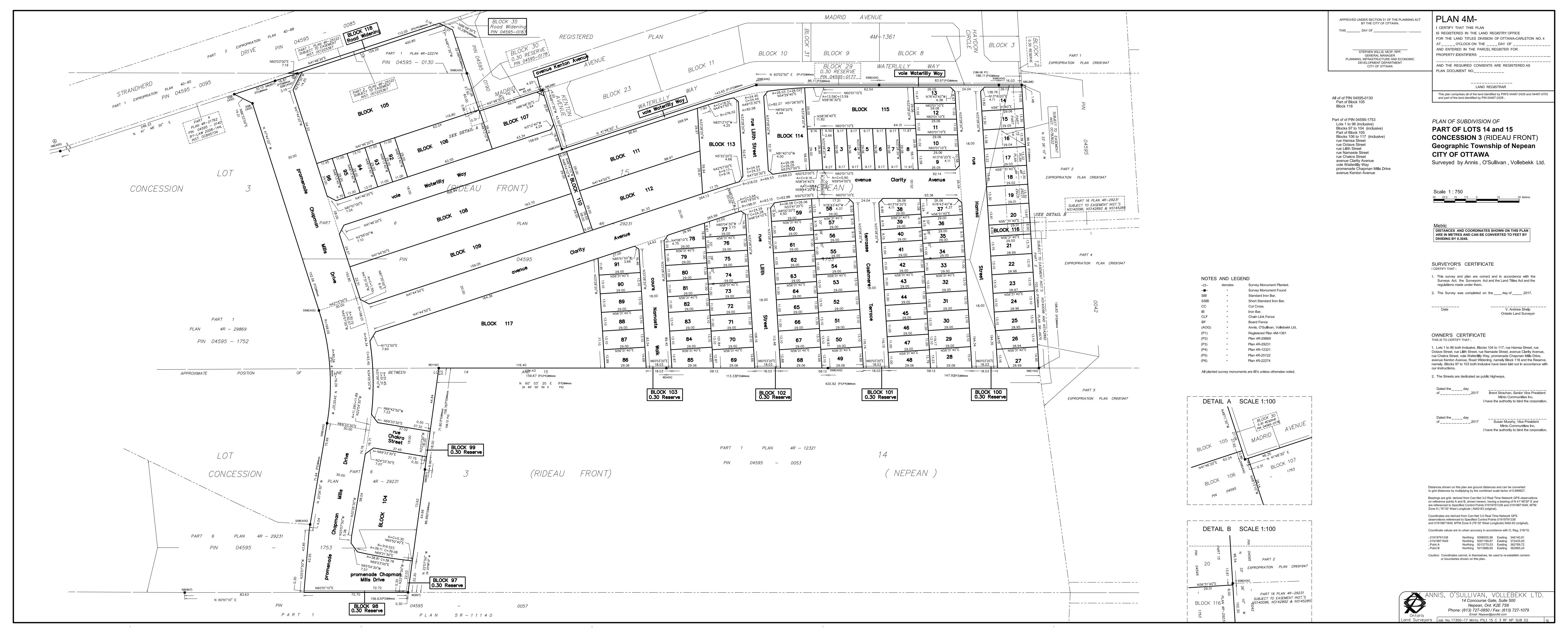
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HARMONY	STAGE 1 – BLOCK 104
DETAIL ED	NOISE CONTROL STUDY

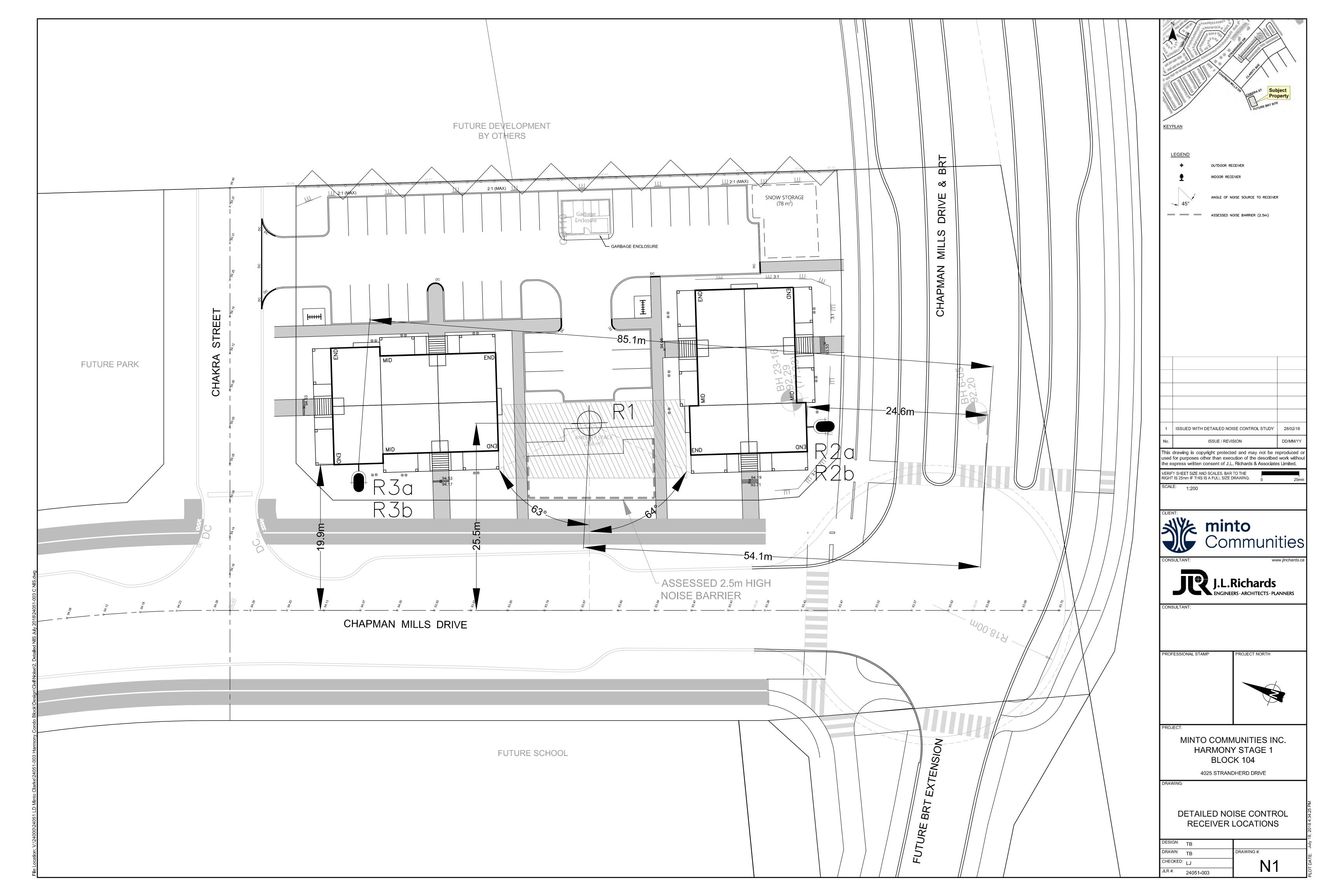
# **Appendix A**

Draft Plan of Subdivision



# **Appendix B**

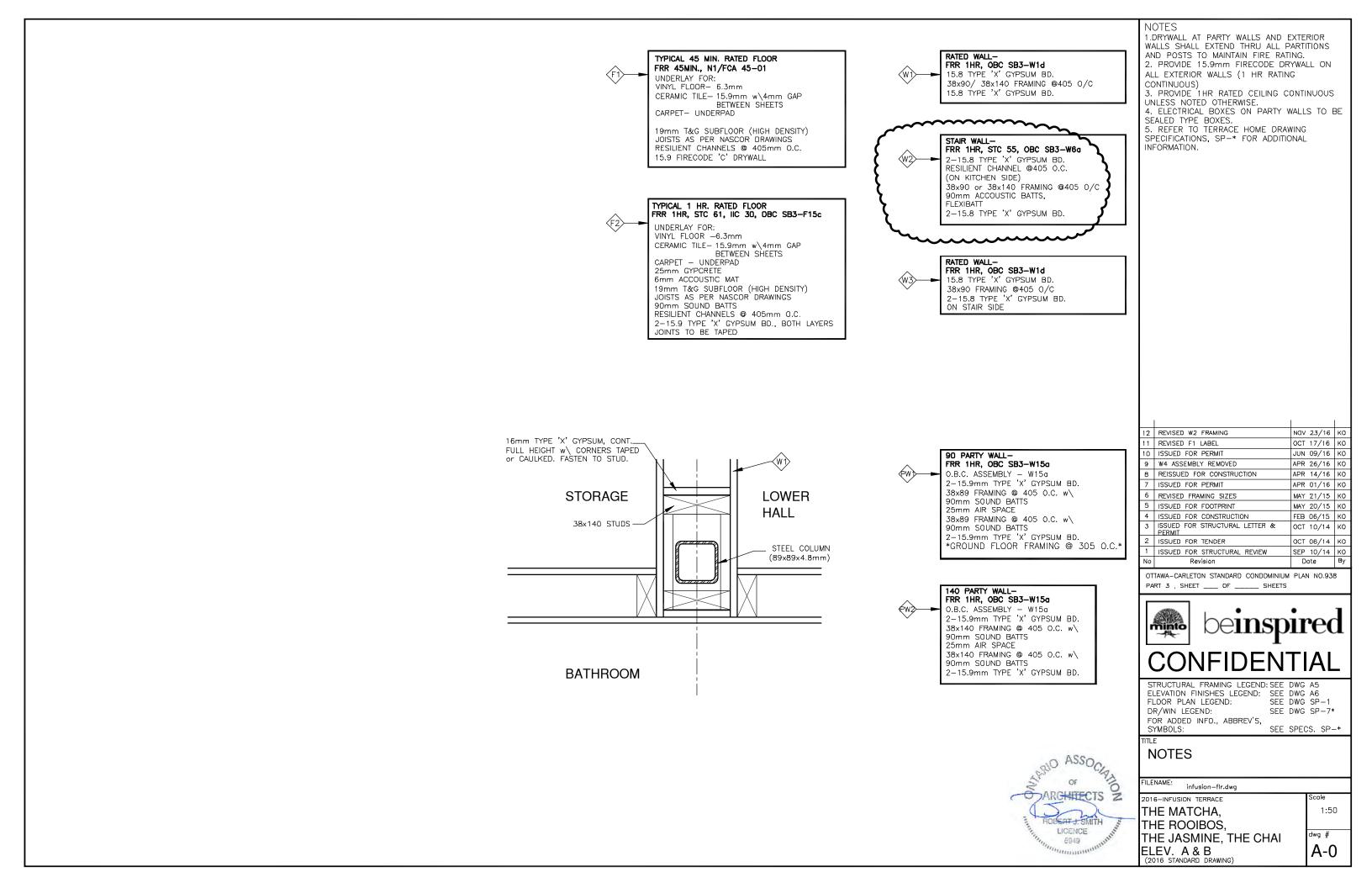
Noise Receiver Locations – Drawing N1

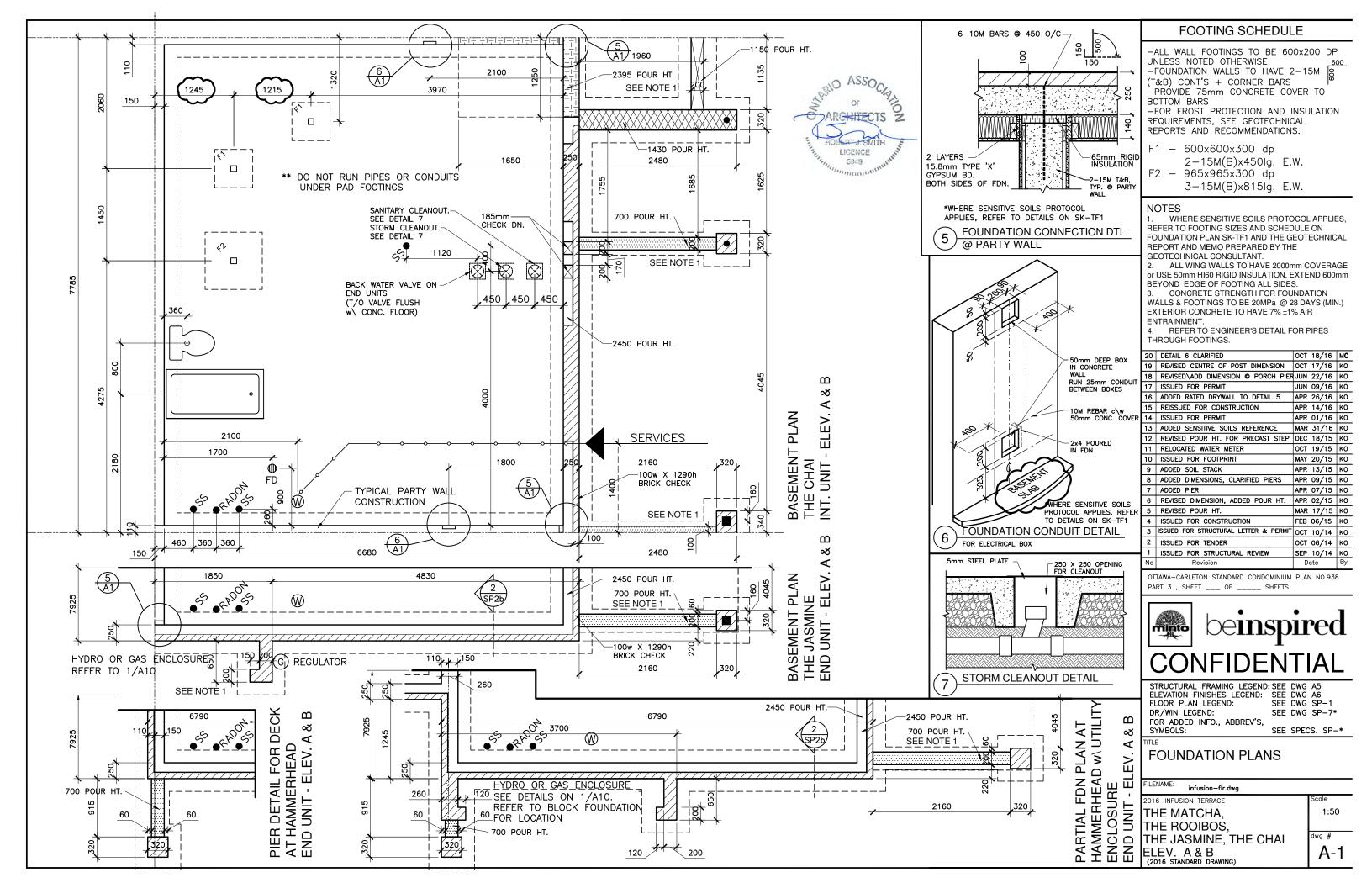


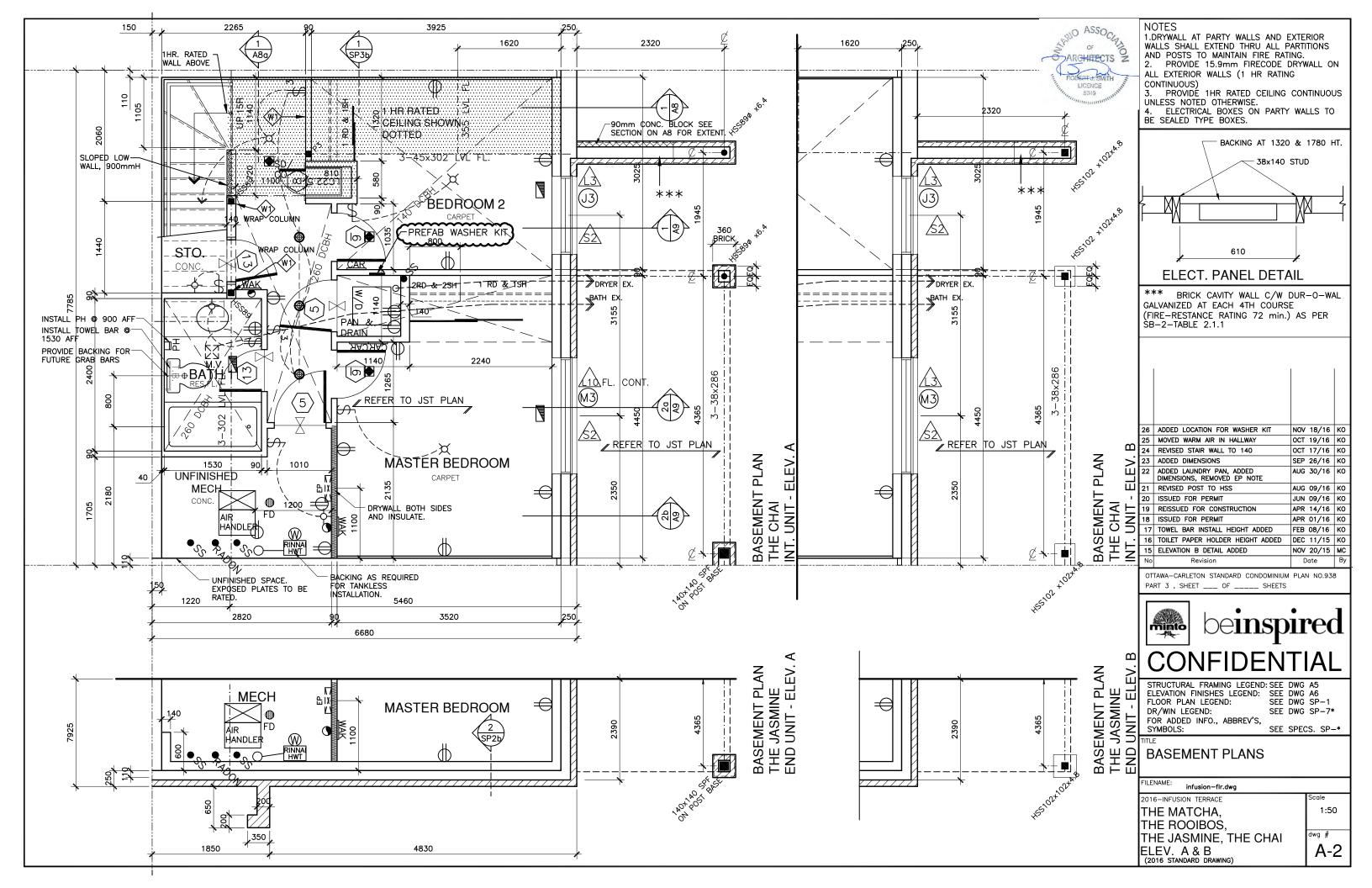
# **Appendix C**

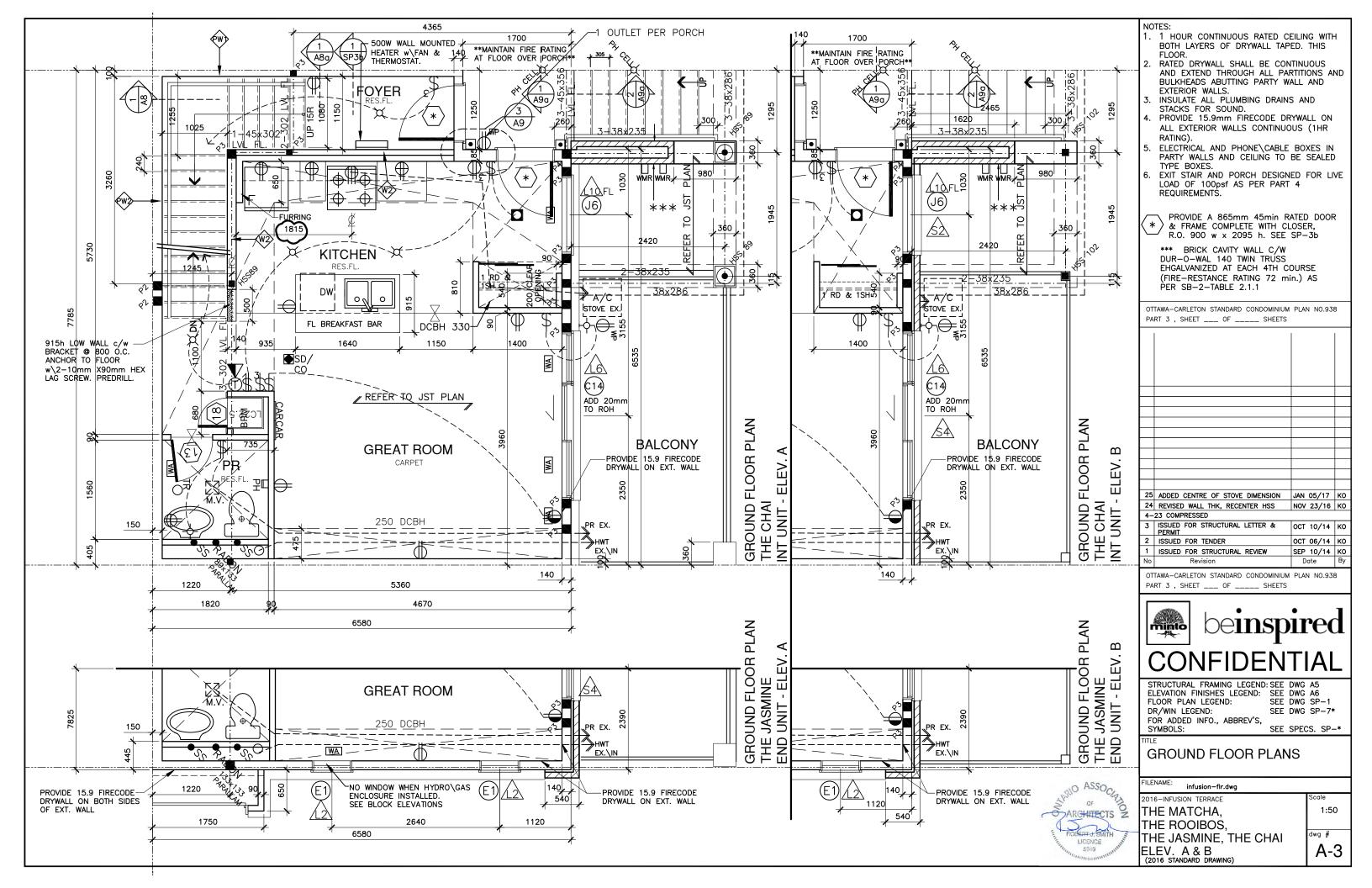
Building Elevation Drawings 2016 Infusion Terrace

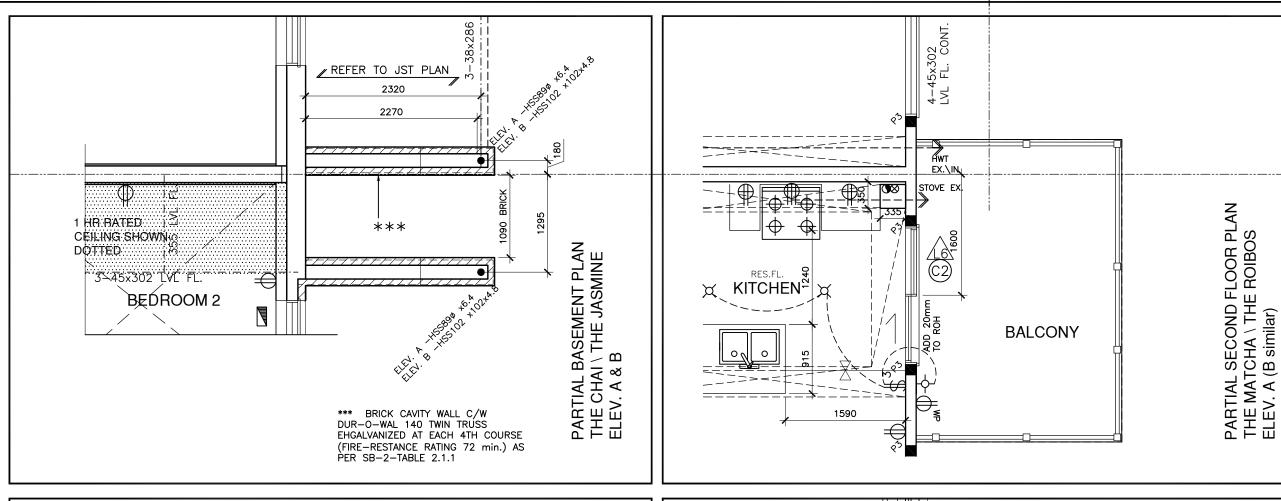
- The Matcha
- The Rooibos
- The Jasmine
- The Chai











FOUNDATION PLAINTHE JASMINE

ECHAI\THE V. A & B

PARTIAL I THE CHA ELEV. A 8

1800

2100

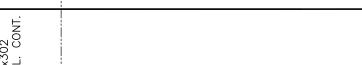
1650

2480

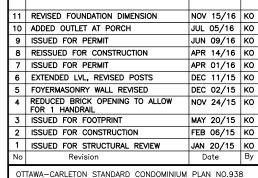
1960

SEE NOTE 1

-1470 POUR HT.



- 1 HOUR CONTINUOUS RATED CEILING WITH BOTH LAYERS OF DRYWALL TAPED. THIS
  - RATED DRYWALL SHALL BE CONTINUOUS AND EXTEND THROUGH ALL PARTITIONS AND BULKHEADS ABUTTING PARTY WALL AND
- EXTERIOR WALLS.
  INSULATE ALL PLUMBING DRAINS AND STAKCS FOR SOUND.
- PROVIDE 15.9mm FIRECODE DRYWALL ON ALL EXTERIOR WALLS CONTINUOUS (1HR RATING).
- ELECTRICAL AND PHONE\CABLE BOXES IN PARTY WALLS AND CEILING TO BE SEALED TYPE BOXES.
- EXIT STAIR AND PORCH DESIGNED FOR LIVE LOAD OF 100psf AS PER PART 4 REQUIREMENTS.
- PROVIDE A 865mm 45min RATED DOOR & FRAME COMPLETE WITH CLOSER, R.O. 900 w x 2095 h. SEE SP-3b
- \*\*\* BRICK CAVITY WALL C/W DUR-O-WAL 140 TWIN TRUSS EHGALVANIZED AT EACH 4TH COURSE (FIRE-RESTANCE RATING 72 min.) AS PER SB-2-TABLE 2.1.1



PART 3 , SHEET \_\_\_ OF \_\_\_\_ SHEETS



STRUCTURAL FRAMING LEGEND: SEE DWG A5 ELEVATION FINISHES LEGEND: SEE DWG A6 FLOOR PLAN LEGEND: SEE DWG SP-1 SEE DWG SP-7\*

DR/WIN LEGEND: FOR ADDED INFO., ABBREV'S,

SEE SPECS. SP-\*

# PARTIAL FLOOR PLANS FOR SINGLE WIDE FOYER

infusion-flr.dwg

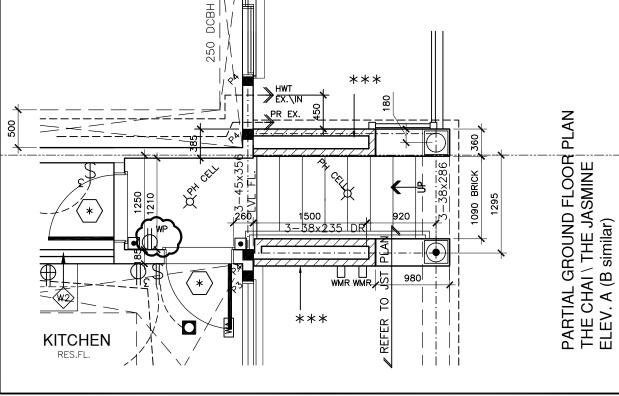
2016-INFUSION TERRACE

ELEV. A & B (2016 STANDARD DRAWING)

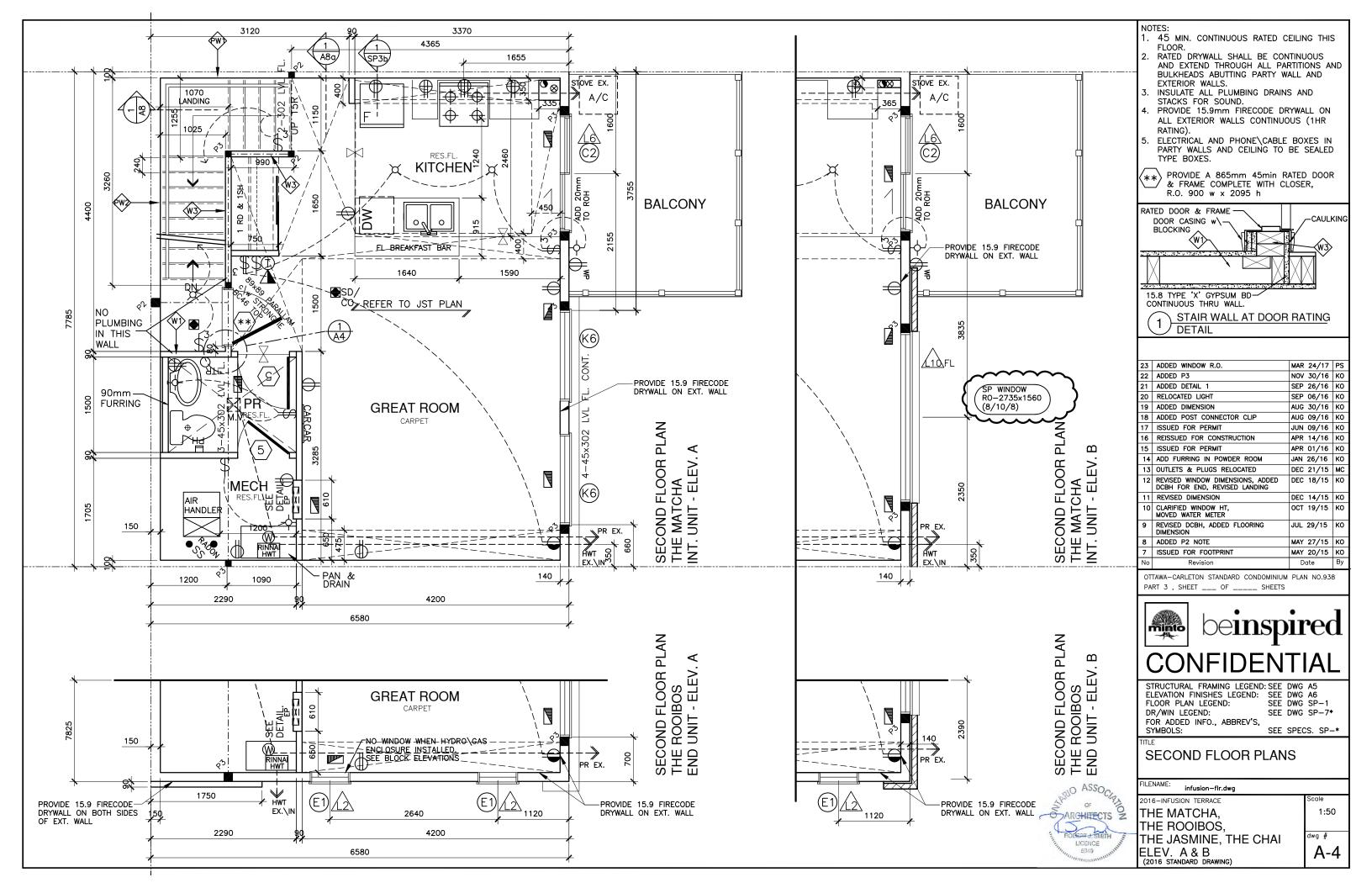
THE MATCHA. THE ROOIBOS, THE JASMINE, THE CHAI

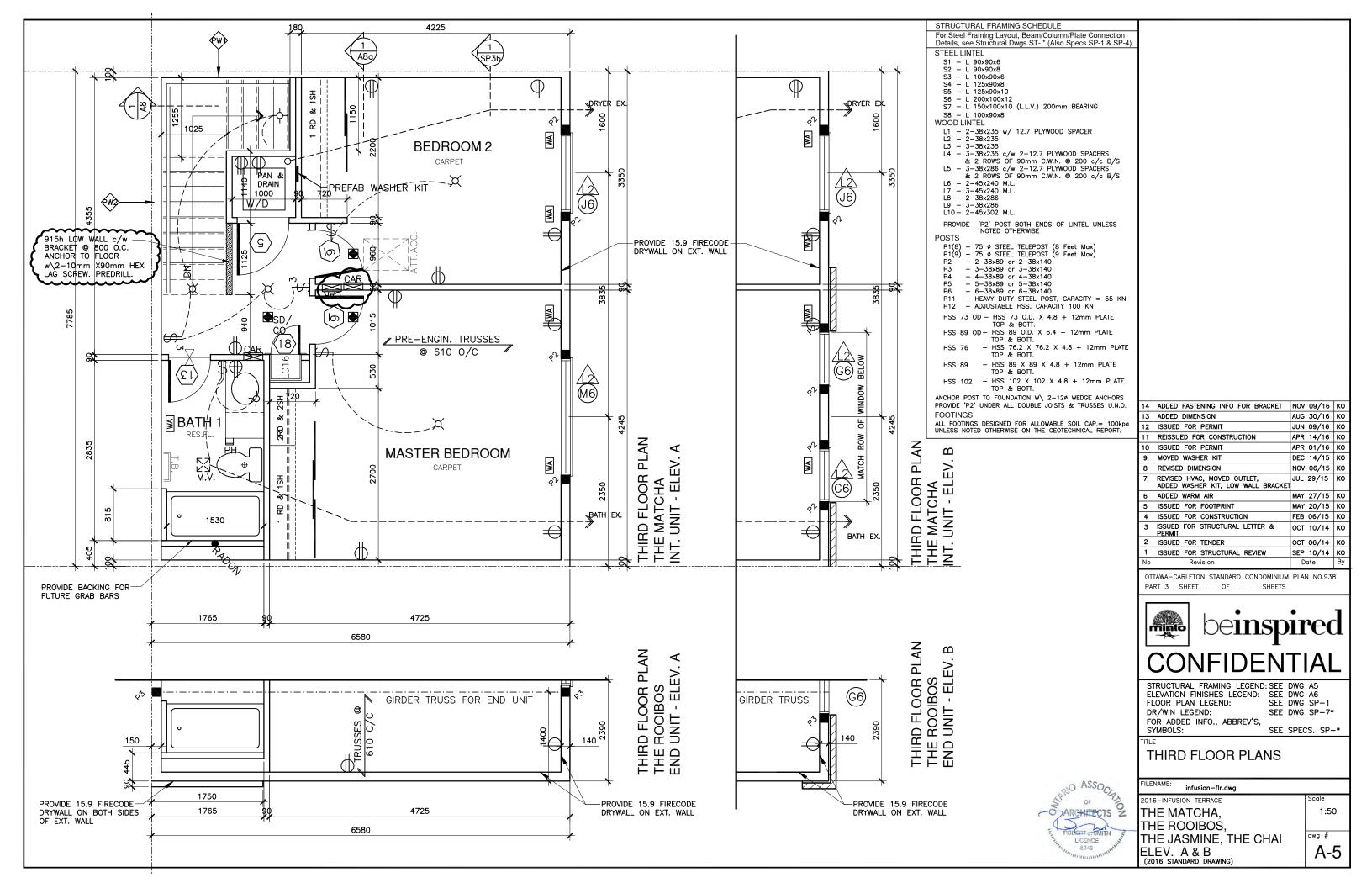
lwg # A-3a

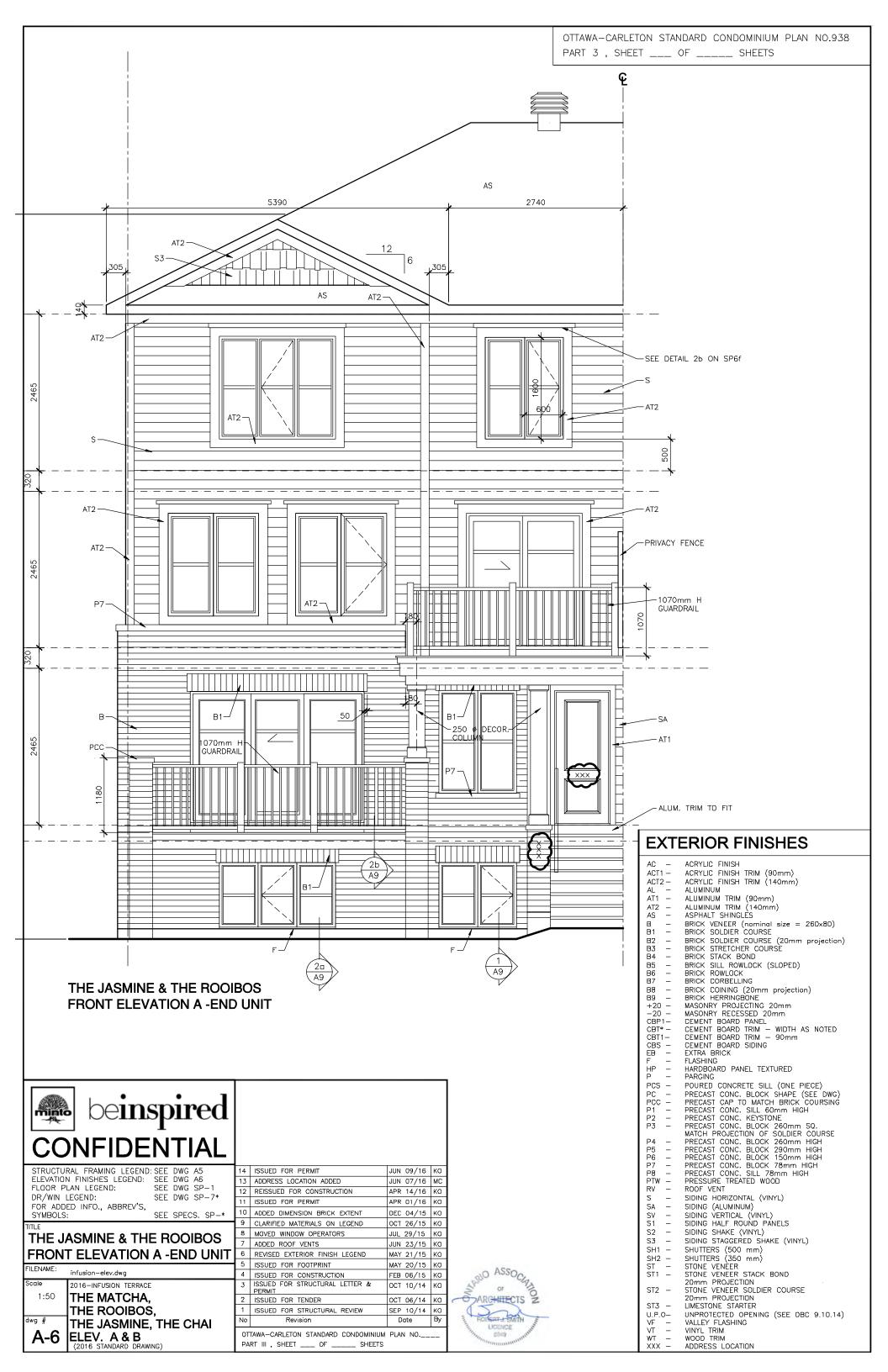
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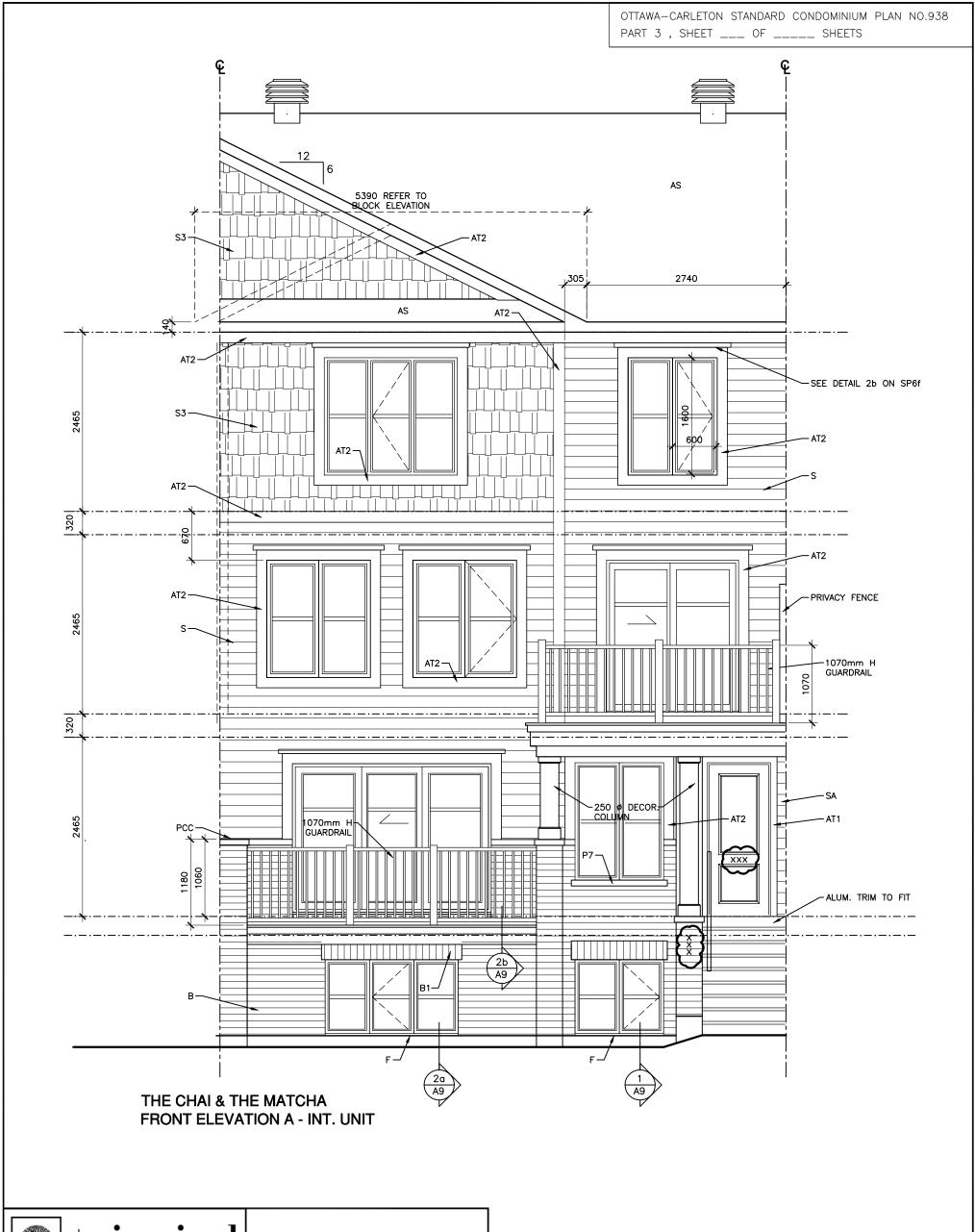


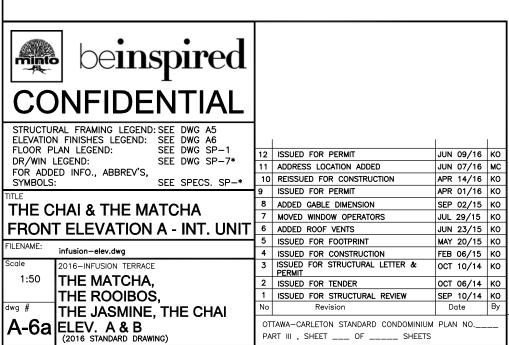
ARGHITECTS Z



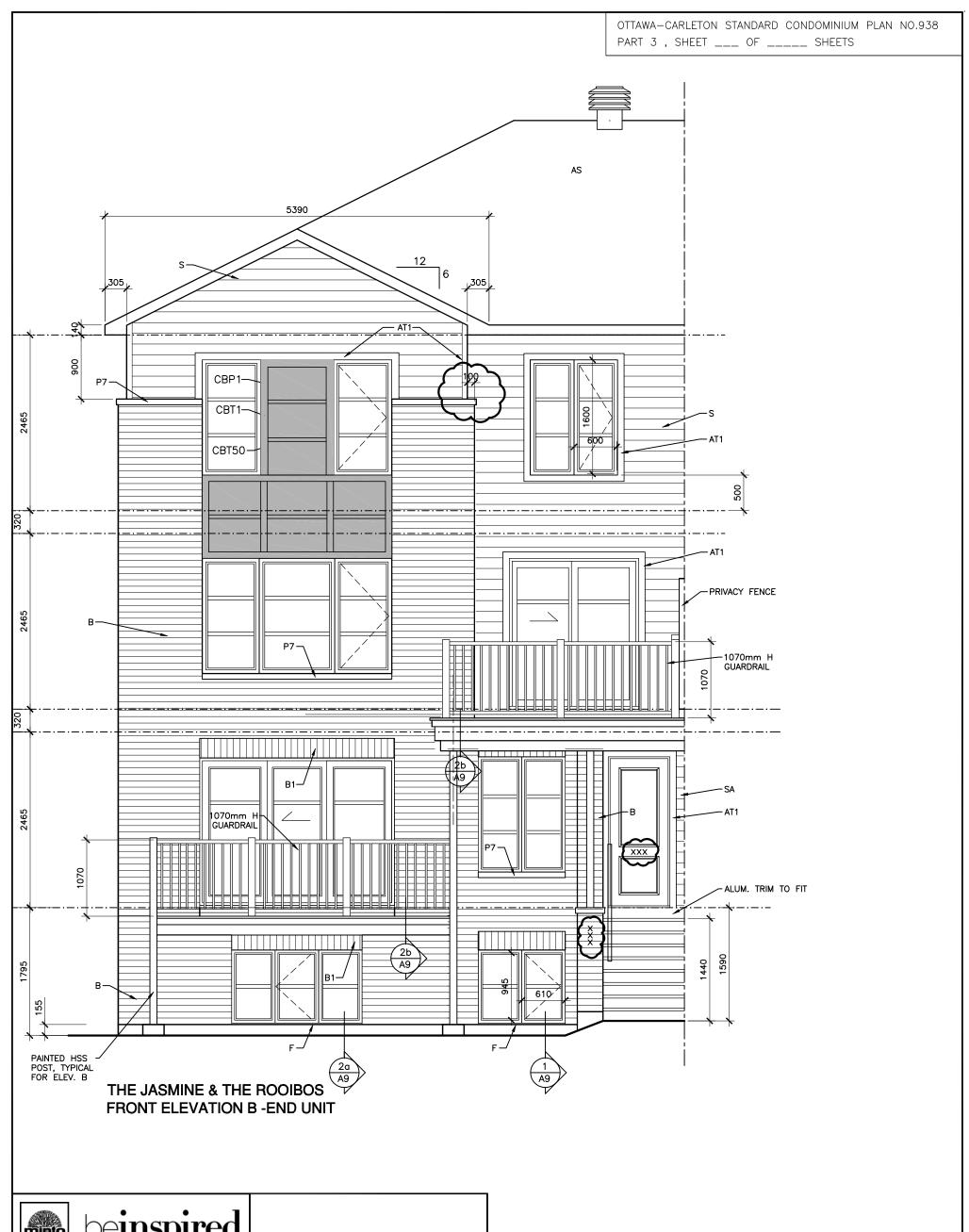


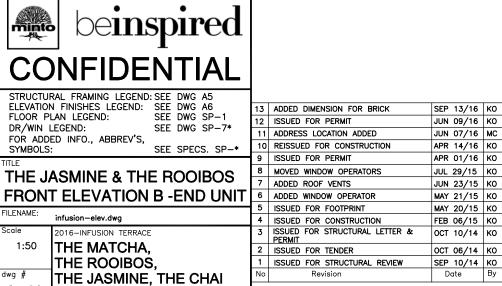












A-6b ELEV. A&B

(2016 STANDARD DRAWING)

OTTAWA-CARLETON STANDARD CONDOMINIUM PLAN NO.

\_ SHEETS

PART III , SHEET \_\_\_ OF \_

ARCHITECTS Z

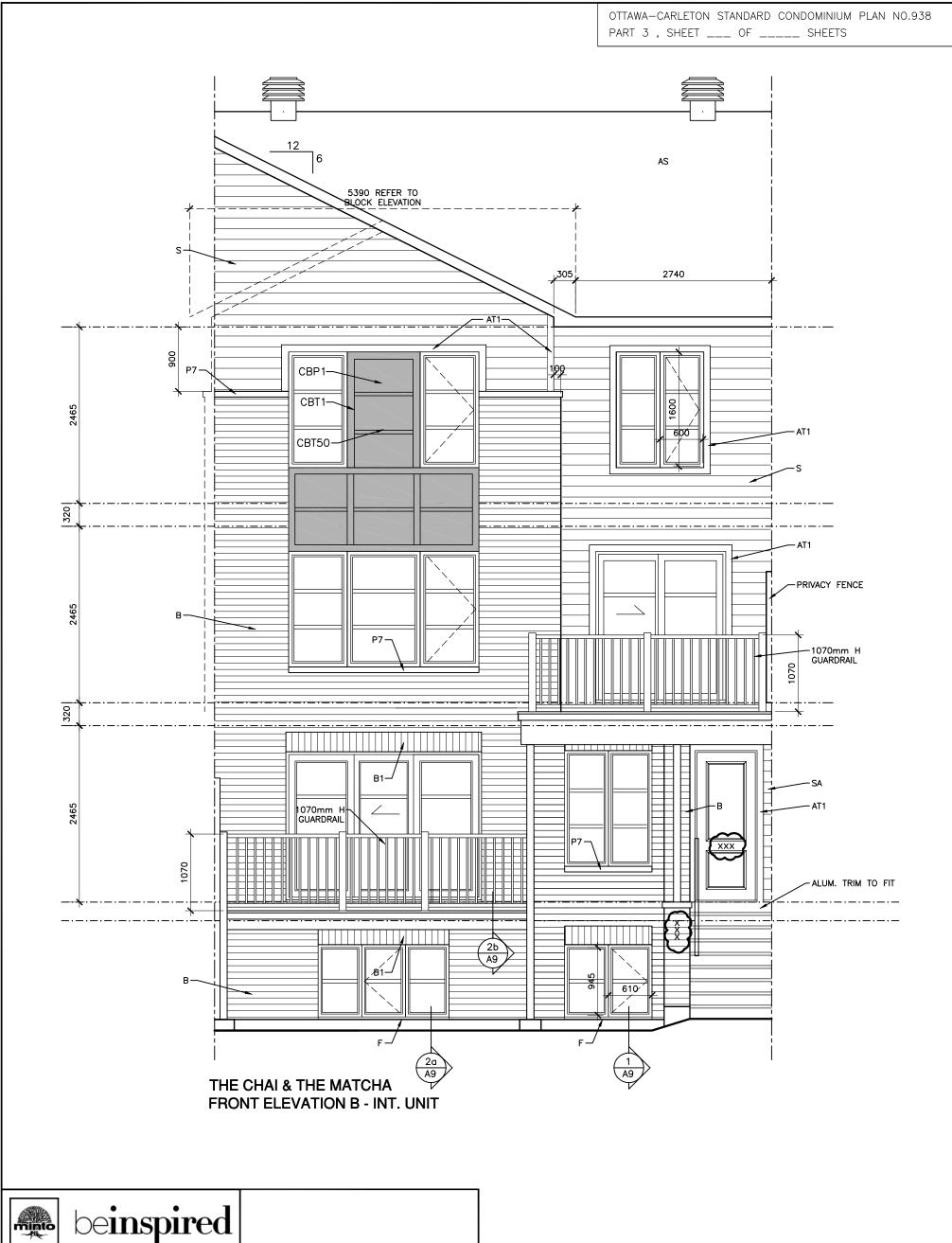
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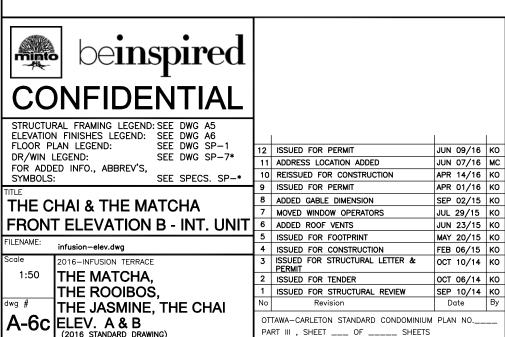
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LICENCE

5949

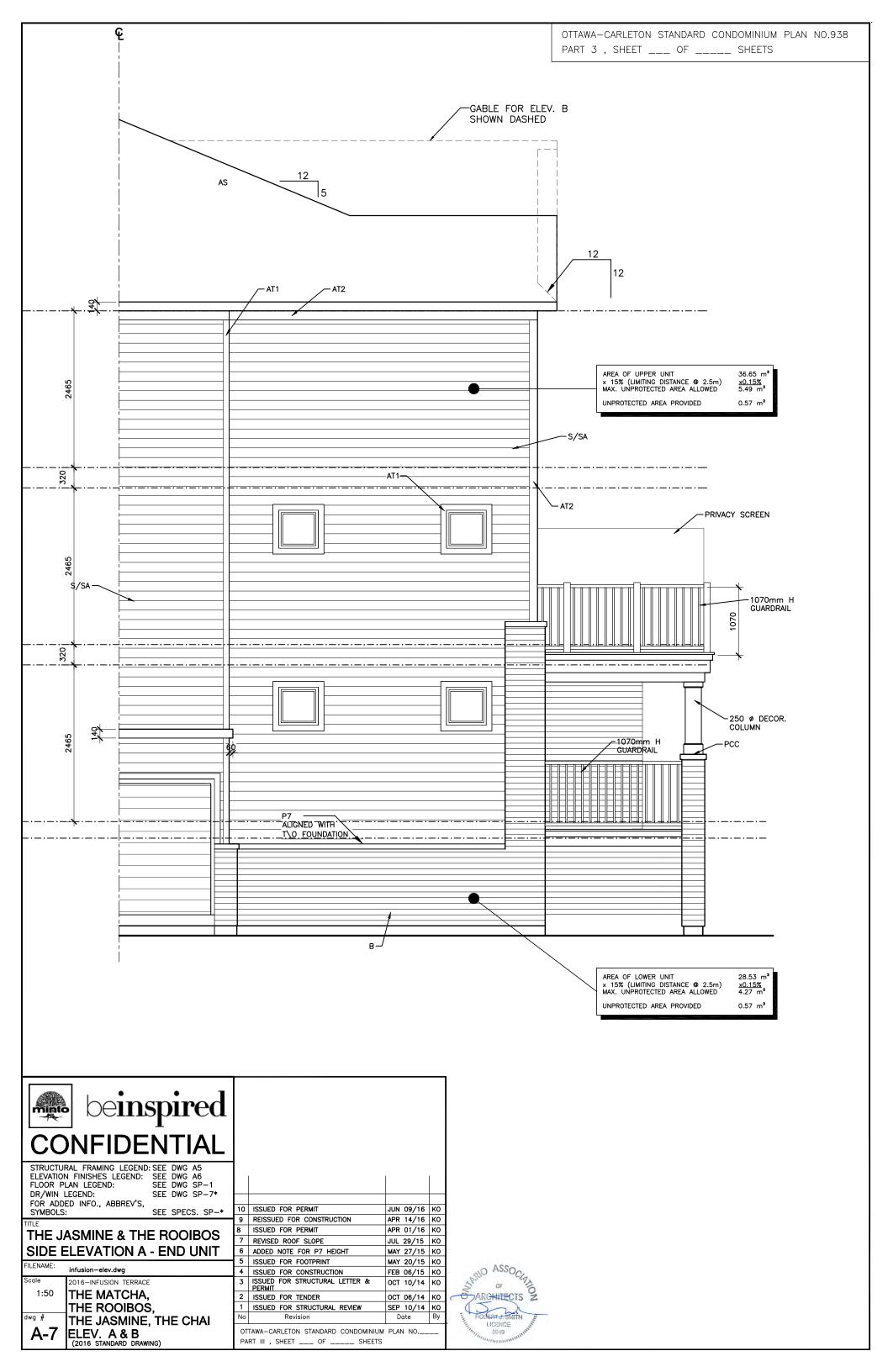
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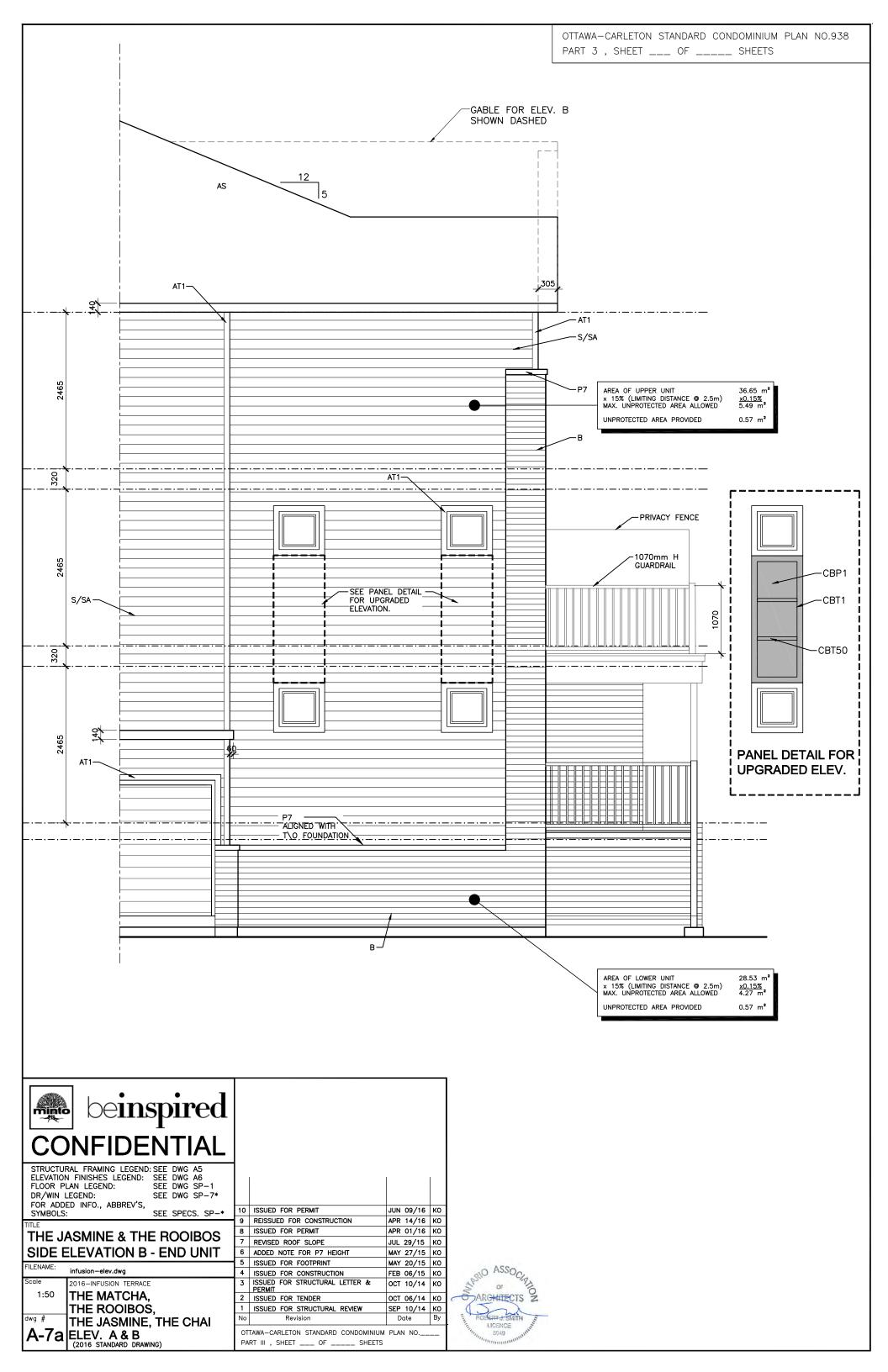


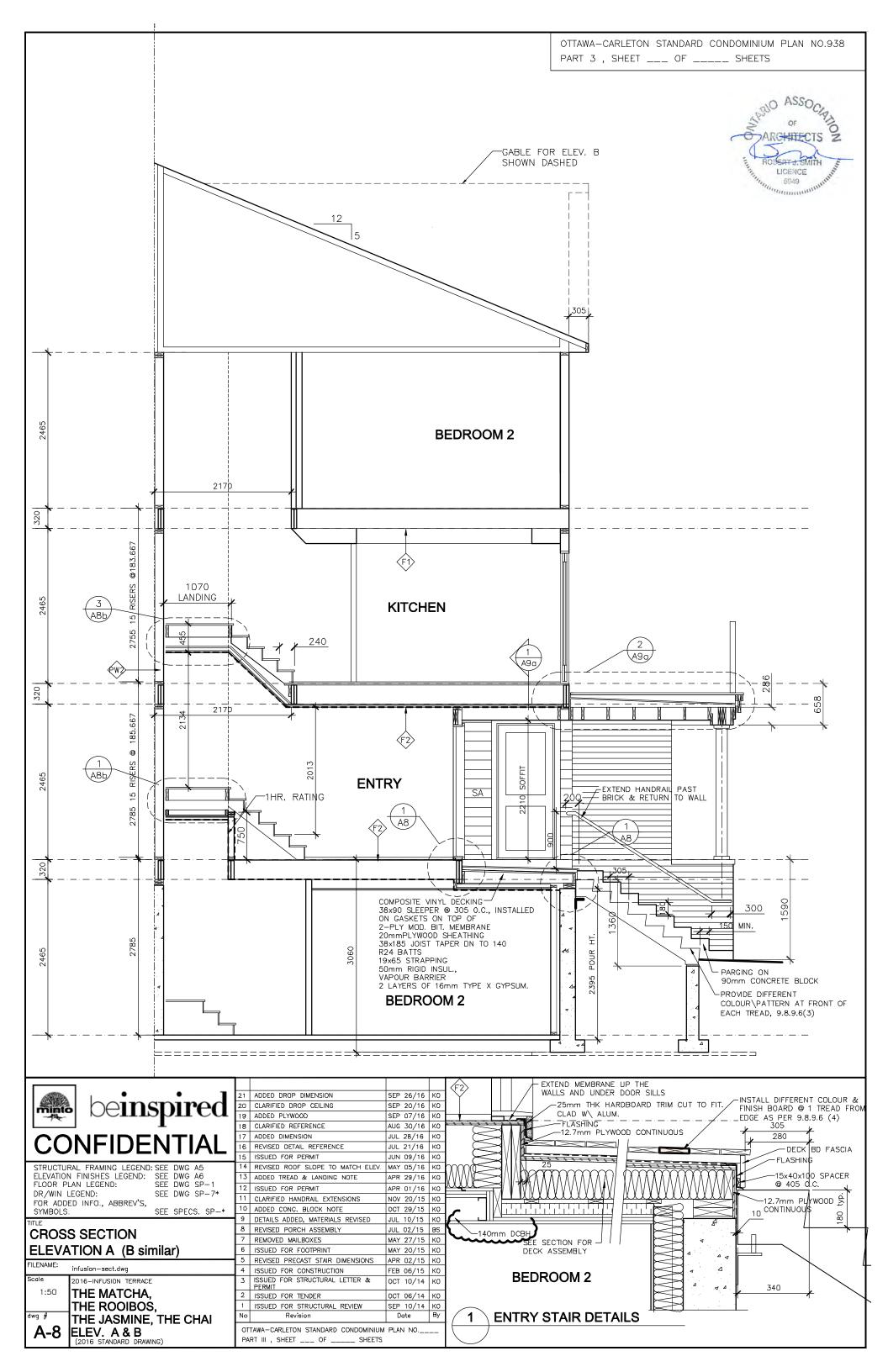


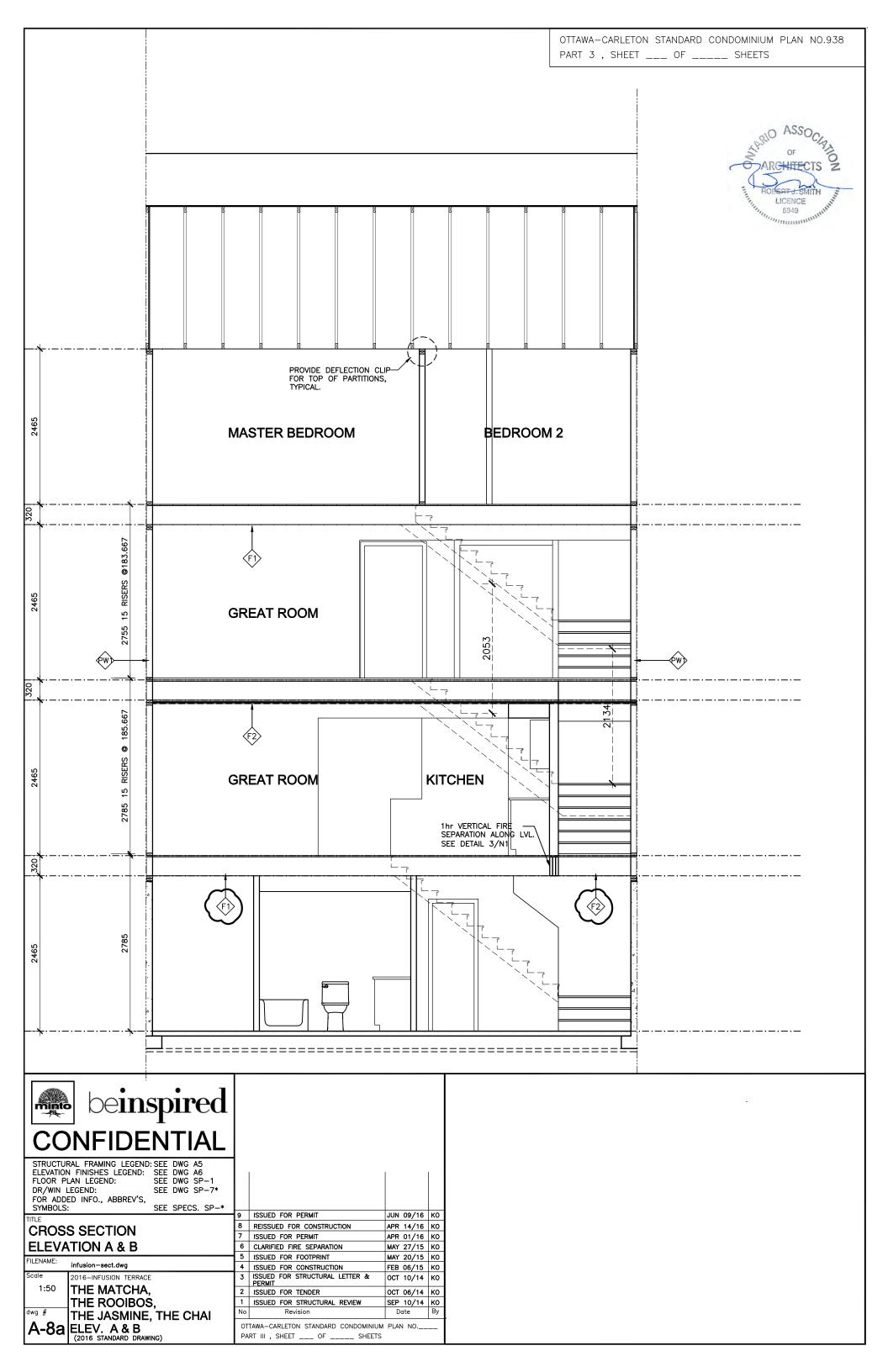
(2016 STANDARD DRAWING)

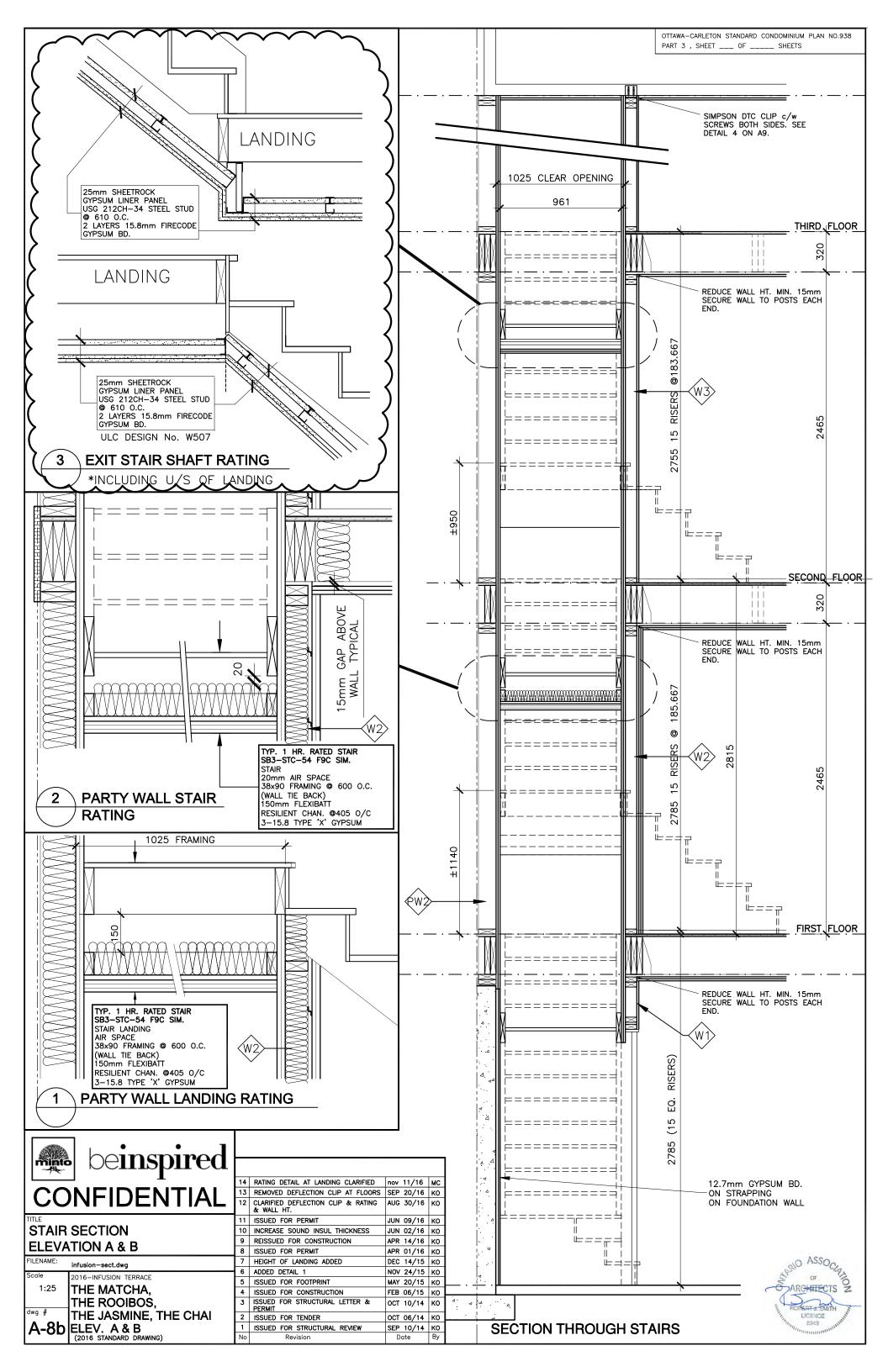


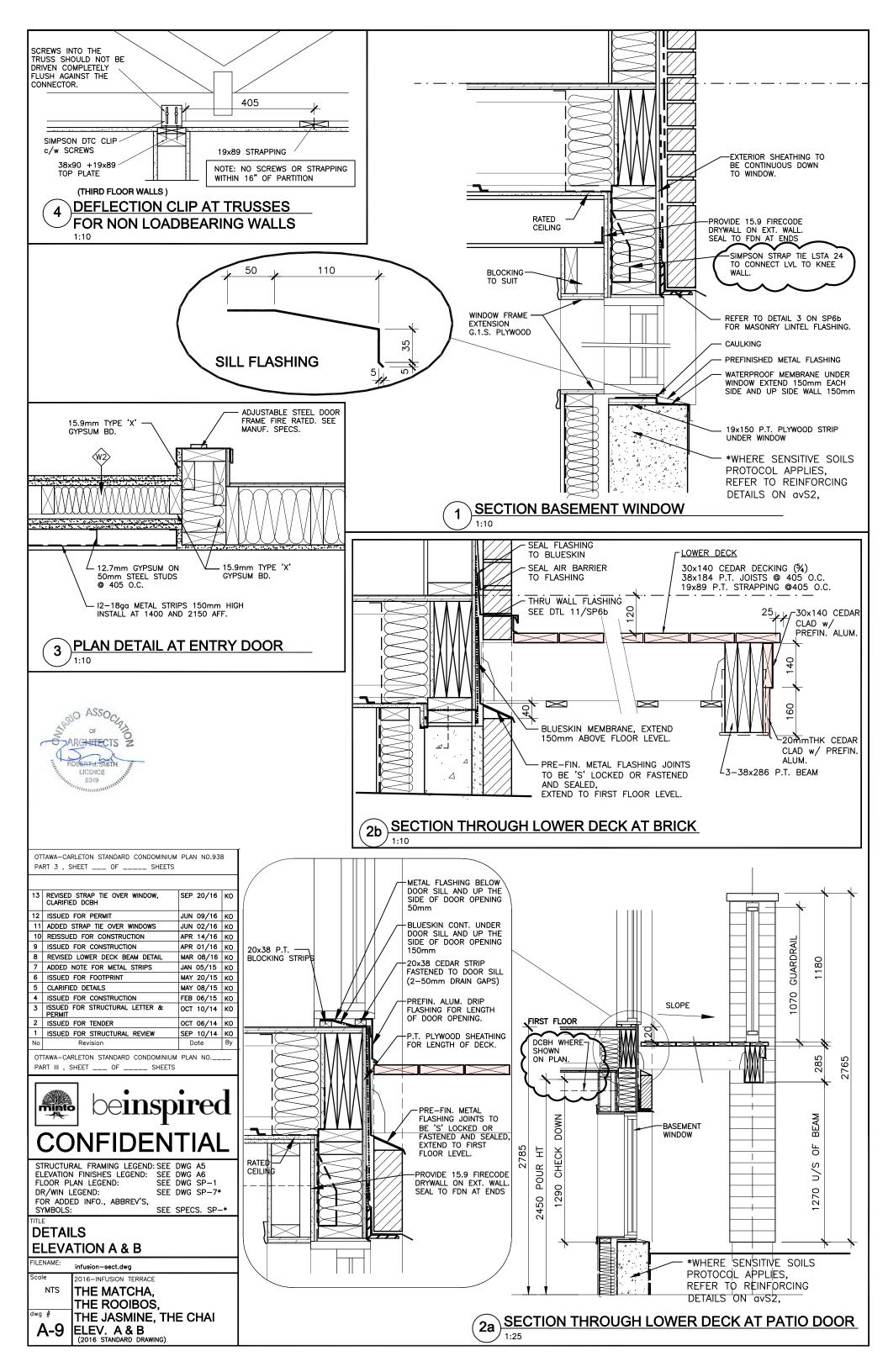


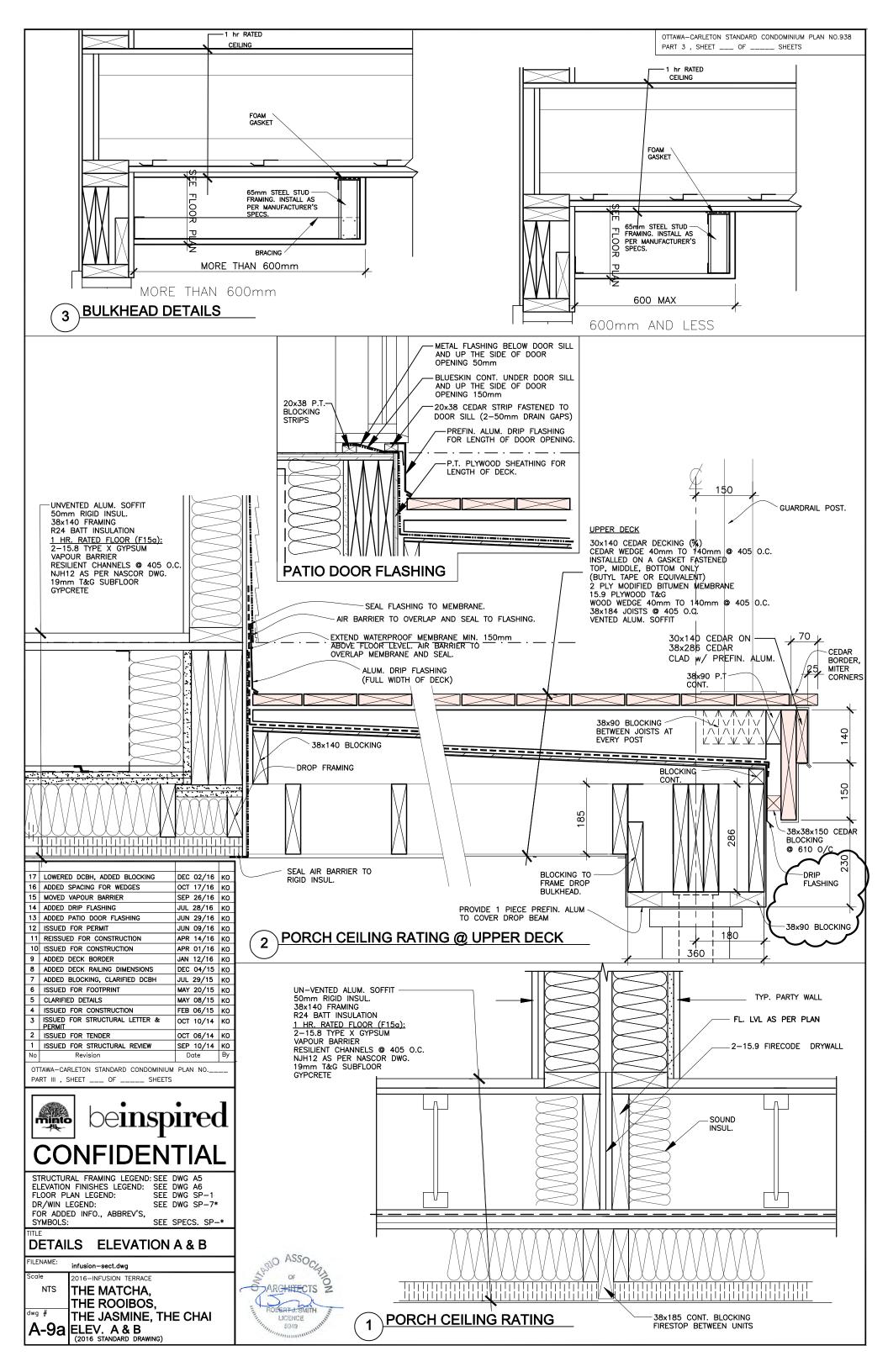


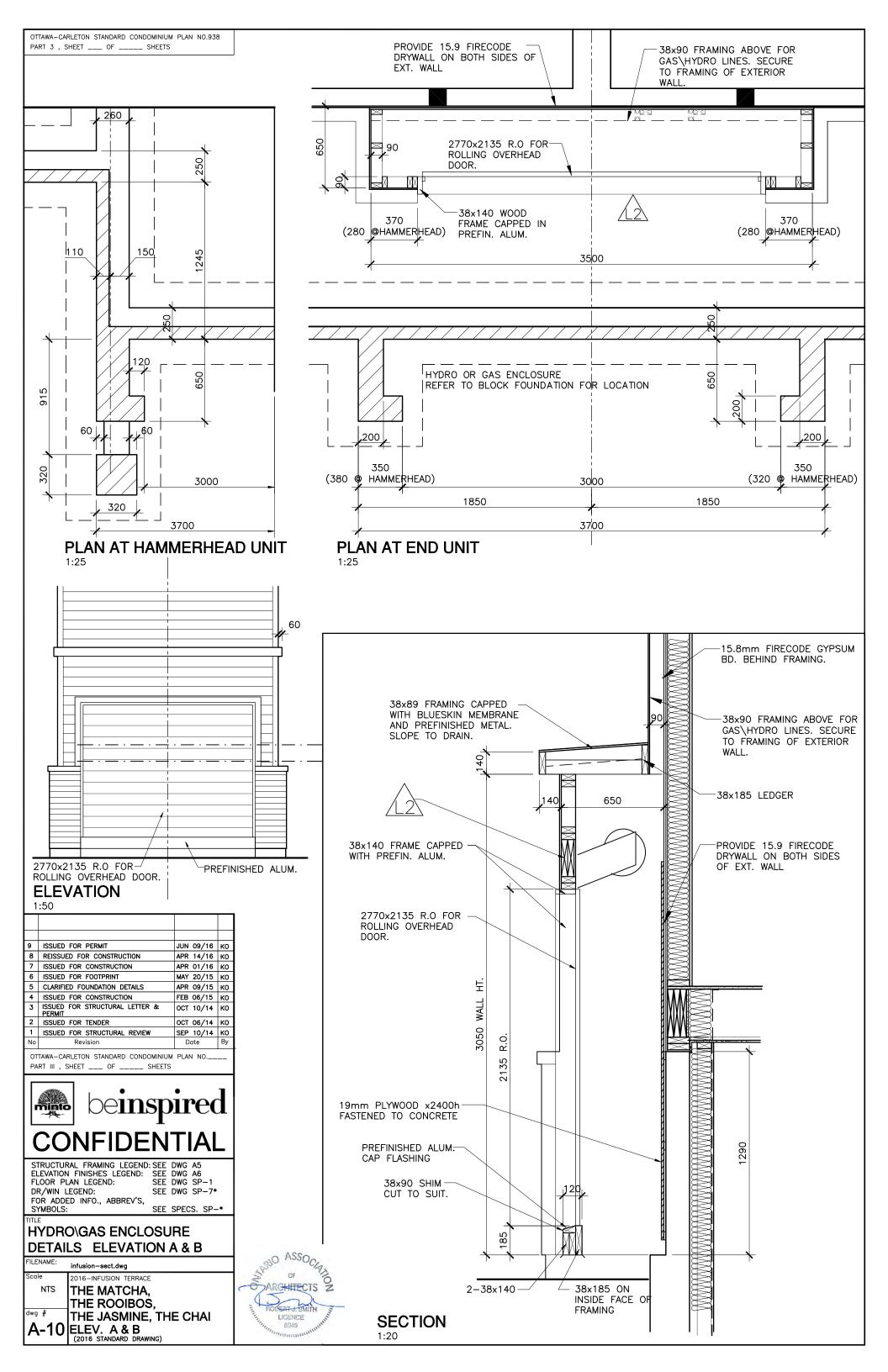


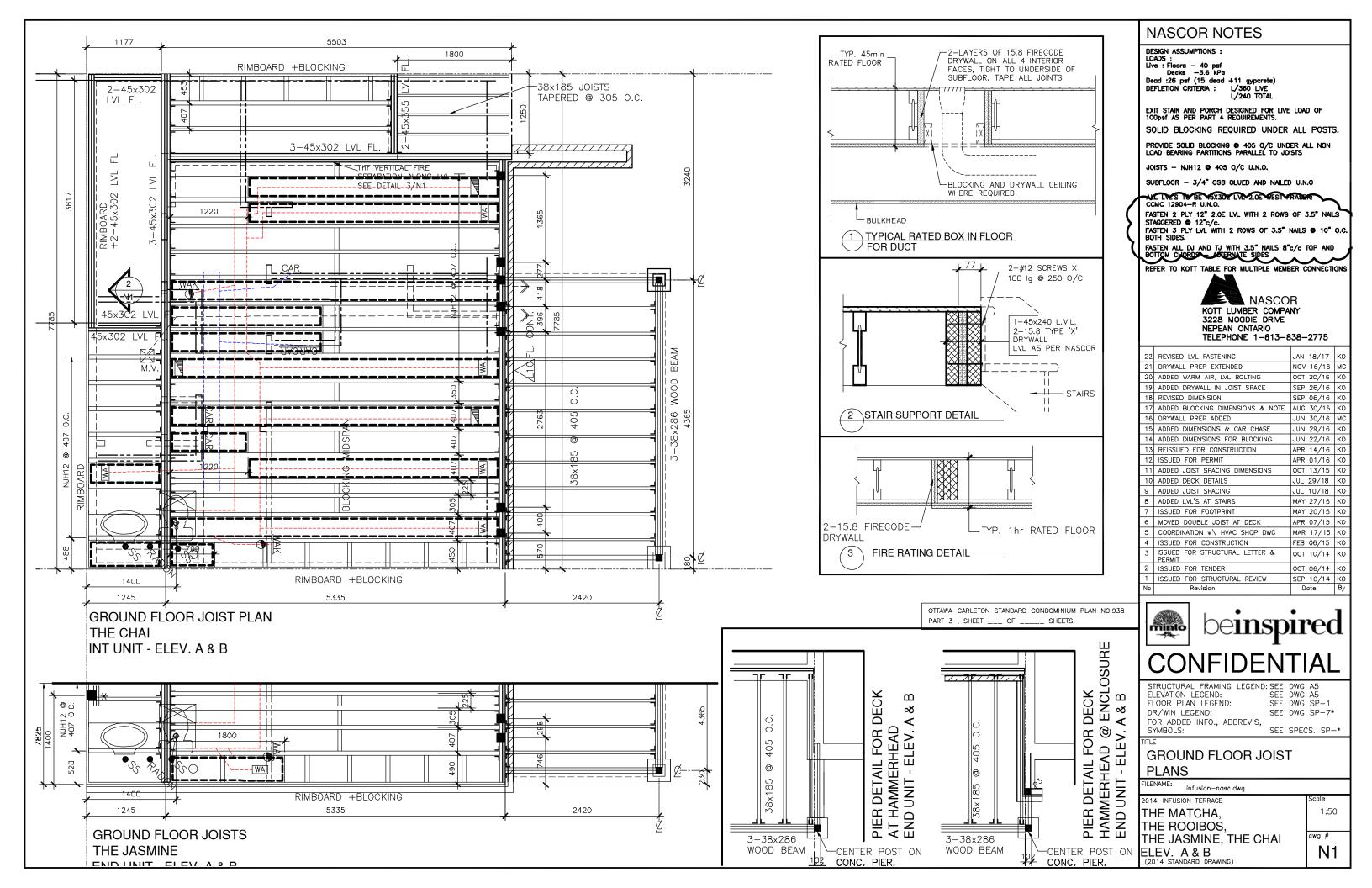


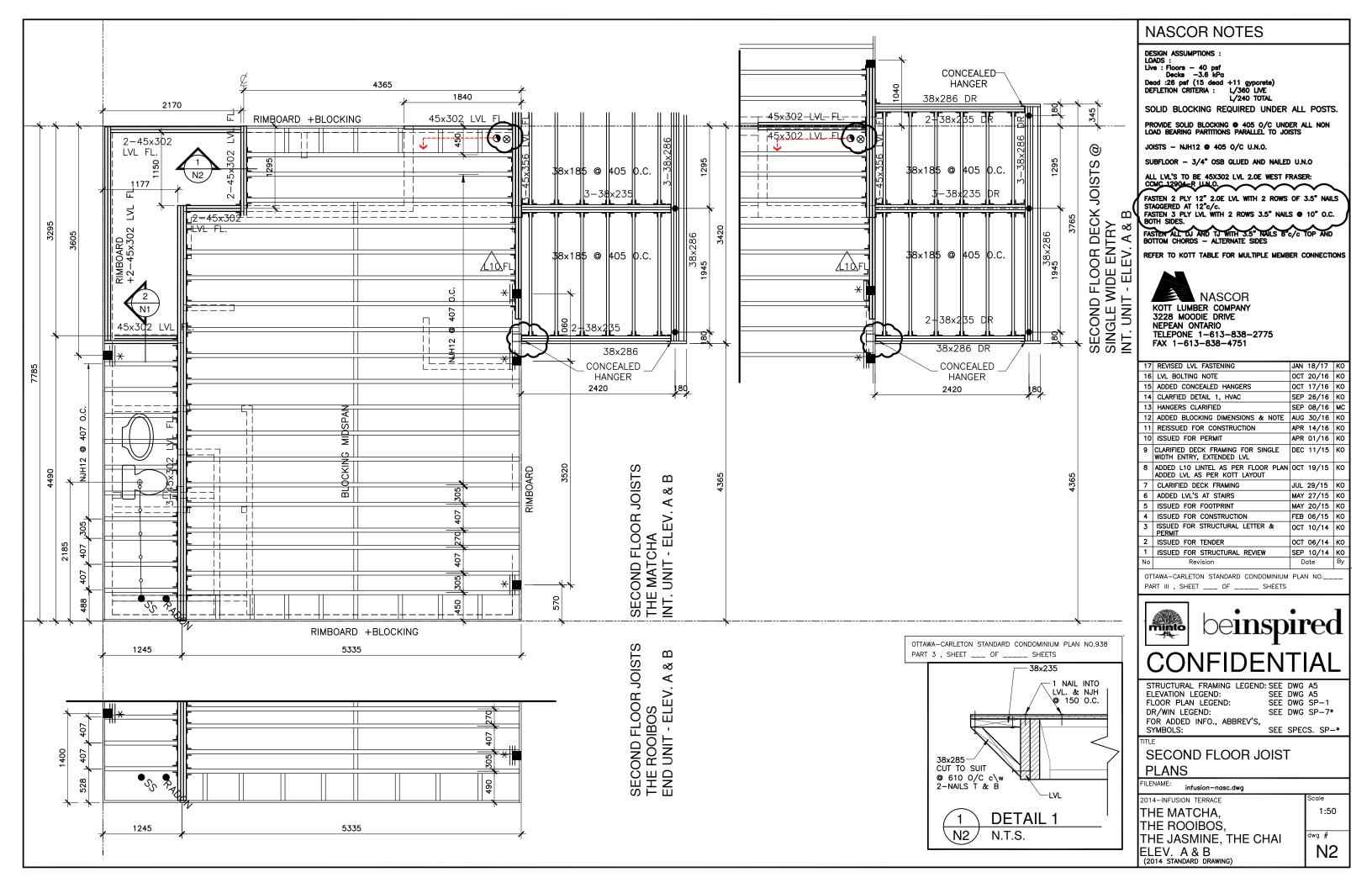


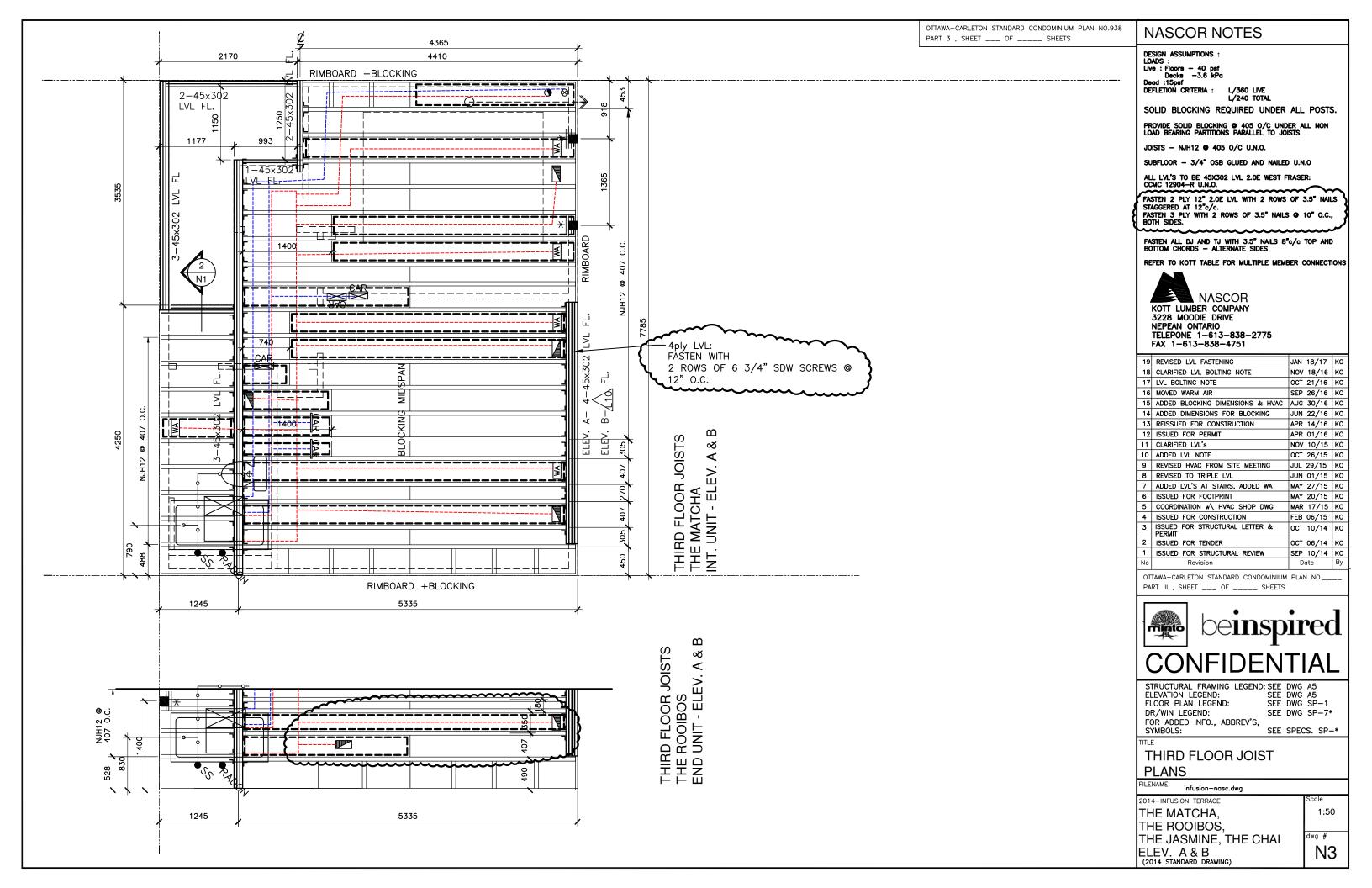












# **Appendix D**

City of Ottawa Bus Rapid Transit Corridor Data

# Appendix 'D' – Rapid Transit Corridor Data to Predict Noise Levels

### Calculation for Total Traffic Volume (AADT) and Day/Night Split

The following information was provided by Colin Simpson in an email dated September 23, 2011:

"5 minute headways should be assumed in each direction using 60' articulated buses with 30 minute headways between 2am and 5am for the night-time Leq dBA calculations."

This information was utilized in the following calculation:

Daytime: 16 hrs = 192 buses

Nighttime: 8 hrs = 5x12 = 60 buses plus 3 x 2 = 66 buses

Total = 192 + 66 = 258 buses Therefore, 74% 26% split

#### Speed Limit

In an email dated September 28, 2011, Colin Simpson indicated that a speed limit of 80 km/hr for the bus rapid transit corridor should be assumed.

#### Medium/Heavy Truck Percentages

A medium/heavy truck ratio of 90/10 was utilized as STAMSON does not permit an input of 100% medium truck traffic.

From: Kate Whitfield
To: Colin Simpson
Date: 12/16/2013 3:14 PM

Subject: RE: Data for Bus Rapid Transit Corridor - Riverside South Phase 13

Thank you for this.

Phase 13 is actually tucked closer to the future bus rapid transitway and not up against Earl Armstrong so we are probably only in the position to apply one scenario. This information is helpful though as we move forward.

Regards,

Kate

>>> "Simpson, Colin" <Colin.Simpson@ottawa.ca> 12/16/2013 1:56 PM >>>

Hi Kate, sorry for my delay in getting back to you.

Yes, the data inputs I gave you back in 2011 associated with the rapid transit corridor near River Road and Earl Armstrong are still valid. This corridor hasn't changed in the 2013 TMP compared to the 2008 TMP: http://ottawa.ca/sites/ottawa.ca/files/tmpmap1\_rapid\_transit.pdf

What has changed is a new "affordable" rapid transit plan which calls for interim Transit Priority buses on Earl Armstrong as shown in the following link:

http://ottawa.ca/sites/ottawa.ca/files/tmpmap2\_rapid\_ttpn.pdf

For your purposes, you should consider both scenarios. The inputs for the ultimate rapid transit corridor that I gave you last time and also and the interim plan to have a high frequency of buses on Earl Armstrong. For the interim plan, you could just model Earl Armstrong to have a higher than normal heavy vehicle composition to account for the buses. I recall the default STAMSON model to include 5% heavy vehicles. You may want to up than to 7% or something justifiable to account for the buses. Earl Armstrong will likely become a truck route after it is extended to Bank Street with its new bridge over the Rideau River anyway. The "affordable" plan is what is expected to be in place in the year 2031 while there is no time frame for the full network concept accept that it is likely beyond 2031 which is why it would be good to consider both scenarios for noise purposes.

You can give me a call if you want to discuss further. Regards, - cs

#### Colin Simpson, MCIP RPP

Senior Project Manager, Transportation - Strategic Planning Unit Planning and Growth Management Department City of Ottawa, 110 Laurier Ave West, 4th Floor, K1P 1J1

Fax: (613) 580-2578

Tel: (613) 580-2424 ext. 27881

colin.simpson@ottawa.ca

From: Kate Whitfield [mailto:KWhitfield@jlrichards.ca]

Sent: December 10, 2013 1:33 PM

To: Simpson, Colin

Subject: Data for Bus Rapid Transit Corridor - Riverside South Phase 13

Good afternoon,

In Sept 2011, you helped me with some data associated with the rapid transit corridor near Riverside South Phase 9 (i.e., in the River Road / Earl Armstrong area) for a noise study. You indicated "5 minute headways should be assumed in each direction using 60' articulated buses with 30 min headways between 2am and 5am for the night-time Leq dBA calculations." You also said that we should assume a speed limit of 80 km/hr for the bus rapid transit corridor. We are now working on a noise study for Phase 13. Can you please confirm whether or not this data is still correct?

Regards,

Kate

Kate Whitfield, MCIP, RPP, P. Eng., LEED-AP Planner/ Civil Engineer J.L. Richards & Associates Limited 864 Lady Ellen Place, Ottawa, ON K1Z 5M2 Tel: 613-728-3571 Fax: 613-728-6012 From: "Simpson, Colin" < Colin.Simpson@ottawa.ca>

To: Kate Whitfield <KWhitfield@JLRICHARDS.CA>, "Blaszynski, Ed" <Ed.Blaszyns...

CC: Jonathan Parraga < JParraga@JLRICHARDS.CA>

**Date:** 9/28/2011 9:18 AM **Subject:** RE: RSDC Phase 9

You should assume 80 km/hr.

----Original Message----

From: Kate Whitfield [mailto:KWhitfield@JLRICHARDS.CA]

Sent: September 28, 2011 9:09 AM To: Simpson, Colin; Blaszynski, Ed

Cc: Jonathan Parraga

Subject: RE: RSDC Phase 9

Great.

Any chance that you know the speed limit for the buses in the BRT?

Regards,

Kate

>>> "Simpson, Colin" <Colin.Simpson@ottawa.ca> 9/26/2011 4:14 PM >>> Yes, these assumptions look good and are consistent with Table 1.7 of the ENCG. Regards, - cs

----Original Message-----

From: Kate Whitfield [mailto:KWhitfield@JLRICHARDS.CA]

Sent: September 26, 2011 9:50 AM To: Simpson, Colin; Blaszynski, Ed

Cc: Jonathan Parraga Subject: RE: RSDC Phase 9

Colin,

Thank you for sending us the BRT assumptions.

We have put together a table with the roadway assumptions for Riverside South Phase 9 (i.e., AADT and speed limit) based on the Official Plan and the Dillon Transportation Impact Study. Could you please review the assumptions and let me know if they are acceptable?

Regards,

Kate

Kate Whitfield, MCIP, RPP, P. Eng., LEED-AP Planner/ Civil Engineer J.L. Richards & Associates Limited 864 Lady Ellen Place, Ottawa, ON K1Z 5M2 Tel: 613-728-3571 Fax: 613-728-6012 www.jlrichards.ca

>>> Jonathan Parraga 9/26/2011 9:35 AM >>> Ed,

#### Thank you.

Jonathan Párraga, P.Eng. Senior Civil Engineer J.L. Richards & Associates Limited 864 Lady Ellen Place, Ottawa, ON K1Z 5M2 Tel: 613-728-3571 Fax: 613-728-6012 www.jlrichards.ca ( http://www.jlrichards.ca/ )

>>>

From: "Blaszynski, Ed" <Ed.Blaszynski@ottawa.ca> To:Jonathan Parraga

<JParraga@JLRICHARDS.CA>
Date: 9/26/2011 9:31 AM
Subject: RE: RSDC Phase 9

Jonathan,

See attached assumptions. If you required any further information, contact Colin Simpson.

Ed Blaszynski

Project Manager, Transportation Development Review (Suburban Services) Planning and Growth Management Department City of Ottawa

tel: 613-580-2424, ext. 27598

fax: 613- 560-6006

e-mail: Ed.Blaszynski@ottawa.ca

From:Jonathan Parraga [mailto:JParraga@JLRICHARDS.CA]

Sent: September 22, 2011 9:52 AM

To: Blaszynski, Ed

Cc: Kate Whitfield; Lee Jablonski; Mary Jarvis

Subject: RSDC Phase 9

Ed,

We are looking to set up a design meeting with the City to confirm assumptions/variables for the Noise study for the RSDC Phase 9 development. Would you be available next Wednesday (Sept. 28) in the am ?

Regards,

Jonathan Párraga, P.Eng.

Senior Civil Engineer

J.L. Richards & Associates Limited 864 Lady Ellen Place, Ottawa, ON K1Z 5M2 Tel: 613-728-3571 Fax: 613-728-6012 www.jlrichards.ca ( http://www.jlrichards.ca/ )

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To: <u>Thomas Blais</u>

Subject: RE: Minto Clarke Lands Draft Plan Feasibility Study Traffic Data assumptions

**Date:** February 25, 2016 11:31:29 AM

Attachments: image004.png

City of Ottawa ENCG - January 2016.pdf

Hi Tom,

No problem. I know we're working on getting them on the external website, but the document needs to go through accessibility and translation services first; this can be a long process.

Please see the attached. If you have any questions, please let me know.

Jim

### James (Jim) Hall, P.Eng.

Project Manager Infrastructure Approvals

Development Review (Suburban Services)

Gestionnaire de project, Approbation des demandes d'infrastructure

Examen des demandes d'aménagement (Services suburbains)



City of Ottawa | Ville d'Ottawa

**6**13.580.2424 ext./poste 27508

ottawa.ca/planning / ottawa.ca/urbanisme

**From:** Thomas Blais [mailto:tblais@jlrichards.ca] **Sent:** Thursday, February 25, 2016 11:28 AM

To: Hall, James

Subject: RE: Minto Clarke Lands Draft Plan Feasibility Study Traffic Data assumptions

Hi James.

Can you please send me a pdf copy of the approved January 2016 environmental noise control guidelines.

Thanks

Tom

#### Thomas Blais, A.Sc.T.

Geographic Information Systems Technologist

J.L. Richards & Associates Limited 864 Lady Ellen Place, Ottawa, ON K1Z 5M2 Tel: 613-728-3571 Fax: 613-728-6012





From: Carter, Riley [mailto:Riley.Carter@ottawa.ca]

**Sent:** February 25, 2016 8:00 AM

**To:** Thomas Blais

Cc: Lee Jablonski; Hilary MacKay

Subject: RE: Minto Clarke Lands Draft Plan Feasibility Study Traffic Data assumptions

Hi Tom,

I asked James Hall to review the assumptions since he will be doing the review of the study. He confirmed the below information is correct and added the use of the R/T Custom data input can be used for the buses, thus allowing 100% medium truck (actually, there is a template for buses), and that the newly approved guidelines (January 2016) must be followed.

If you need any additional information while preparing this noise study please contact James.

Thanks,

Riley

From: Thomas Blais [mailto:tblais@jlrichards.ca]

**Sent:** Monday, February 22, 2016 9:39 AM

To: Carter, Riley

Cc: Lee Jablonski; Hilary MacKay

Subject: Minto Clarke Lands Draft Plan Feasibility Study Traffic Data assumptions

Hi Riley,

Per our conversation on Friday, here are the traffic and transit data assumptions that we have compiled for the Minto Clark Lands feasibility study. Can you please review and confirm that they are acceptable.

	Strandherd Drive	Chapman Mills Drive
Right-of-Way Width	44.5m	40m (including transit way)
Road Class	4 Lane Urban Divided Arterial	2 Lane Major Collector
Total Traffic Volume (AADT)	35,000	12,000
Day/Night Split (%)	92/8	92/8
Medium Trucks (%)	7	7
Heavy Trucks (%)	5	5
Posted Speed (km/hr)	70	50
Road Gradient (%)	1	1

	Bus Rapid Transit Corridor
Total Traffic Volume (AADT)	258
Day/Night Split (%)	74/26
Medium Trucks (%)	90
Heavy Trucks (%)	10
Posted Speed (km/hr)	80

Road Gradient (%)

1

### Calculation for Total BRT Volume (AADT) and Day/Night Split

\_

The following information was provided by Colin Simpson in an email dated September 23, 2011:

"5 minute headways should be assumed in each direction using 60' articulated buses with 30 minute headways between 2am and 5am for the night-time Leq dBA calculations."

This information was utilized in the following calculation:

Daytime: 16 hrs = 192 buses

Nighttime:  $8 \text{ hrs} = 5 \times 12 = 60 \text{ buses plus } 3 \times 2 = 66 \text{ buses}$ 

Total = 192 + 66 = 258 buses

Therefore, 74% 26% split

### **Speed Limit**

In an email dated September 28, 2011, Colin Simpson indicated that a speed limit of 80 km/hr for the bus rapid transit corridor should be assumed.

# Medium/Heavy Truck Percentages

A medium/heavy truck ratio of 90/10 was utilized as STAMSON does not permit an input of 100% medium truck traffic.

Thanks

Tom

#### Thomas Blais, A.Sc.T.

Geographic Information Systems Technologist

J.L. Richards & Associates Limited 864 Lady Ellen Place, Ottawa, ON K1Z 5M2 Tel: 613-728-3571 Fax: 613-728-6012





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# **Appendix E**

Transportation Noise Source Predictions

 Detailed Predicted Noise Level Calculations

# STAMSON 5.0 NORMAL REPORT Date: 17-07-2018 15:56:35 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r1.te Time Period: Day/Night 16/8 hours

Description: Harmony Block 104 ola r1

Road data, segment # 1: CMD (day/night)

\_\_\_\_\_

Car traffic volume: 9715/845 veh/TimePeriod \* Medium truck volume: 773/67 veh/TimePeriod \* Heavy truck volume: 552/48 veh/TimePeriod \*

Posted speed limit: 50 km/h Road gradient : 1 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 12000 Percentage of Annual Growth : 0.00 Number of Years of Growth : 0.00 Medium Truck % of Total Volume : 7.00 Heavy Truck % of Total Volume : 5.00 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: CMD (day/night)

-----

Angle1 Angle2 : -64.00 deg 63.00 deg

Wood depth : 0 (No woods.)

No of house rows : 0 / 0

Surface : 1 (Absorptive ground surface)

Receiver source distance: 25.50 / 25.50 m

Receiver height : 1.50 / 4.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

Results segment # 1: CMD (day)

\_\_\_\_\_

Source height = 1.50 m

ROAD (0.00 + 61.54 + 0.00) = 61.54 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

\_\_\_\_\_

-64 63 0.66 67.51 0.00 -3.83 -2.15 0.00 0.00 0.00 61.54

Segment Leg: 61.54 dBA

Total Leg All Segments: 61.54 dBA

Results segment # 1: CMD (night)

-----

Source height = 1.50 m

ROAD (0.00 + 54.22 + 0.00) = 54.22 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

\_\_\_\_\_

-64 63 0.57 59.91 0.00 -3.62 -2.07 0.00 0.00 0.00 54.22

Segment Leq: 54.22 dBA

Total Leq All Segments: 54.22 dBA

RT/Custom data, segment # 1: brt (day/night)

\_\_\_\_\_

1 - Bus:

Traffic volume : 192/66 veh/TimePeriod

Speed: 80 km/h

Data for Segment # 1: brt (day/night)

Angle1 Angle2 : 0.00 deg 90.00 deg

Wood depth : 0 (No woods.)

No of house rows : 0 / 0

Surface : 1 (Absorptive ground surface)

Receiver source distance: 54.10 / 54.10 m Receiver height : 1.50 / 4.50 m
Topography : 1 (Flat/ge
Reference angle : 0.00

(Flat/gentle slope; no barrier)

Results segment # 1: brt (day)

-----

Source height = 0.50 m

RT/Custom (0.00 + 45.72 + 0.00) = 45.72 dBA

Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

-----

0 90 0.66 59.44 -9.25 -4.47 0.00 0.00 0.00 45.72

\_\_\_\_\_

Segment Leg: 45.72 dBA

Total Leq All Segments: 45.72 dBA

Results segment # 1: brt (night)

-----

Source height = 0.50 m

RT/Custom (0.00 + 44.53 + 0.00) = 44.53 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

-----

0 90 0.60 57.81 -8.91 -4.37 0.00 0.00 0.00 44.53

\_\_\_\_\_

Segment Leq: 44.53 dBA

Total Leq All Segments: 44.53 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 61.65

(NIGHT): 54.66

# STAMSON 5.0 NORMAL REPORT Date: 14-02-2018 11:23:22 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

<u>Filename: condor2a.te Time Period: Day/Night 16/8 hours</u> <u>Description: Harmony Condo Block ila R2a lower condo</u>

Road data, segment # 1: CMD (day/night)

-----

Car traffic volume: 9715/845 veh/TimePeriod \* Medium truck volume: 773/67 veh/TimePeriod \* Heavy truck volume: 552/48 veh/TimePeriod \*

Posted speed limit : 50 km/h Road gradient : 1 %

Road pavement : 1 (Typical asphalt or concrete)

24 hr Traffic Volume (AADT or SADT): 12000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: CMD (day/night)

-----

Angle1 Angle2 : -90.00 deg 90.00 deg Wood depth : 0 (No woods.)

<sup>\*</sup> Refers to calculated road volumes based on the following input:

No of house rows : 0 / 0 Surface : 1 (Absorptive ground surface)

Receiver source distance: 24.60 / 24.60 m

Receiver height : 2.90 / 0.68 m

Topography : 1 (Flat/gentle slope; no barrier)

Reference angle : 0.00

Results segment # 1: CMD (day)

\_\_\_\_\_

Source height = 1.50 m

ROAD (0.00 + 62.65 + 0.00) = 62.65 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

-90 90 0.62 67.51 0.00 -3.48 -1.39 0.00 0.00 0.00 62.65 \_\_\_\_\_

Segment Leq: 62.65 dBA

Total Leq All Segments: 62.65 dBA

Results segment # 1: CMD (night)

\_\_\_\_\_

Source height = 1.50 m

ROAD (0.00 + 54.89 + 0.00) = 54.89 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

\_\_\_\_\_

-90 90 0.66 59.91 0.00 -3.57 -1.46 0.00 0.00 0.00 54.89

\_\_\_\_\_

Segment Leq: 54.89 dBA

Total Leq All Segments: 54.89 dBA

RT/Custom data, segment # 1: brt (day/night)

\_\_\_\_\_

1 - Bus:

Traffic volume : 192/66 veh/TimePeriod

Speed: 80 km/h

Data for Segment # 1: brt (day/night)

-----

Angle1 Angle2 : -90.00 deg 90.00 deg Wood depth : 0 (No woods.)

No of house rows : 0 / 0

Surface : 1 (Absorptive ground surface)

Receiver source distance: 24.60 / 24.60 m

Receiver height : 2.90 / 0.68 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

Results segment # 1: brt (day)

.....

Source height = 0.50 m

RT/Custom (0.00 + 54.46 + 0.00) = 54.46 dBAAngle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

-90 90 0.65 59.44 -3.54 -1.44 0.00 0.00 0.00 54.46

Segment Leq: 54.46 dBA

Total Leg All Segments: 54.46 dBA

Results segment # 1: brt (night)

\_\_\_\_\_

Source height = 0.50 m

RT/Custom (0.00 + 52.79 + 0.00) = 52.79 dBAAngle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

-90 90 0.66 57.81 -3.57 -1.46 0.00 0.00 0.00 52.79

Segment Leg: 52.79 dBA

Total Leq All Segments: 52.79 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 63.26

(NIGHT): 56.98

#### MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: condor2b.te Time Period: Day/Night 16/8 hours Description: Harmony Condo Block ila R2b upper condo

Road data, segment # 1: CMD (day/night)

-----

Car traffic volume: 9715/845 veh/TimePeriod \* Medium truck volume: 773/67 veh/TimePeriod \* Heavy truck volume: 552/48 veh/TimePeriod \*

Posted speed limit: 50 km/h Road gradient : 1 %

Road pavement : 1 (Typical asphalt or concrete)

24 hr Traffic Volume (AADT or SADT): 12000 Percentage of Annual Growth : 0.00 Number of Years of Growth : 0.00 Medium Truck % of Total Volume : 7.00 Heavy Truck % of Total Volume : 5.00 Day (16 hrs) % of Total Volume : 92.00

#### Data for Segment # 1: CMD (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg

Wood depth : 0 (No woods.)

No of house rows : 0 / 0

Surface : 1 (Absorptive ground surface)

Receiver source distance: 24.60 / 24.60 m Receiver height : 5.70 / 8.50 m

Topography : 1 (Flat/gentle slope; no barrier)

Reference angle : 0.00

Results segment # 1: CMD (day)

-----

Source height = 1.50 m

ROAD (0.00 + 62.98 + 0.00) = 62.98 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

-90 90 0.53 67.51 0.00 -3.30 -1.24 0.00 0.00 0.00 62.98

.....

Segment Leq: 62.98 dBA

Total Leq All Segments: 62.98 dBA

<sup>\*</sup> Refers to calculated road volumes based on the following input:

Results segment # 1: CMD (night)

-----

Source height = 1.50 m

ROAD (0.00 + 55.72 + 0.00) = 55.72 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

-----

-90 90 0.45 59.91 0.00 -3.12 -1.08 0.00 0.00 0.00 55.72

\_\_\_\_\_

Segment Leq: 55.72 dBA

Total Leq All Segments: 55.72 dBA

RT/Custom data, segment # 1: brt (day/night)

\_\_\_\_\_

1 - Bus:

Traffic volume : 192/66 veh/TimePeriod

Speed: 80 km/h

Data for Segment # 1: brt (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg

Wood depth : 0 (No woods.)

No of house rows : 0 / 0

Surface : 1 (Absorptive ground surface)

Receiver source distance: 24.60 / 24.60 m Receiver height : 5.70 / 8.50 m

Topography : 1 (Flat/gentle slope; no barrier)

Reference angle : 0.00

Results segment # 1: brt (day)

Source height = 0.50 m

RT/Custom (0.00 + 54.78 + 0.00) = 54.78 dBA

Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

-----

-90 90 0.56 59.44 -3.36 -1.29 0.00 0.00 0.00 54.78

\_\_\_\_\_

Segment Leq: 54.78 dBA

Total Leg All Segments: 54.78 dBA

Results segment # 1: brt (night)

-----

Source height = 0.50 m

RT/Custom (0.00 + 53.49 + 0.00) = 53.49 dBA Angle1 Angle2 Alpha RefLeg D.Adj F.Adj W.Adj H.Adj B.Adj SubLeg

------

-90 90 0.48 57.81 -3.18 -1.14 0.00 0.00 0.00 53.49

-----

Segment Leg: 53.49 dBA

Total Leq All Segments: 53.49 dBA

TOTAL Leg FROM ALL SOURCES (DAY): 63.59

(NIGHT): 57.76

# STAMSON 5.0 NORMAL REPORT Date: 14-02-2018 11:50:22 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

<u>Filename: condor3a.te Time Period: Day/Night 16/8 hours</u> <u>Description: Harmony Condo Block ila R3a lower condo</u>

Road data, segment # 1: CMD (day/night)

-----

Car traffic volume: 9715/845 veh/TimePeriod \* Medium truck volume: 773/67 veh/TimePeriod \* Heavy truck volume: 552/48 veh/TimePeriod \*

Posted speed limit: 50 km/h Road gradient: 1 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 12000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: CMD (day/night)

\_\_\_\_\_

Angle1 Angle2 : -90.00 deg 90.00 deg Wood depth : 0 (No woods.)

No of house rows : 0 / 0 Surface : 1 (Absorptive ground surface)

Receiver source distance: 19.90 / 19.90 m Receiver height : 2.90 / 0.68 m

Topography : 1 (Flat/gentle slope; no barrier)

Reference angle : 0.00

Results segment # 1: CMD (day)

\_\_\_\_\_

Source height = 1.50 m

ROAD (0.00 + 64.14 + 0.00) = 64.14 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

-90 90 0.62 67.51 0.00 -1.99 -1.39 0.00 0.00 0.00 64.14

\_\_\_\_\_

Segment Leq: 64.14 dBA

Total Leq All Segments: 64.14 dBA

Results segment # 1: CMD (night)

\_\_\_\_\_

Source height = 1.50 m

ROAD (0.00 + 56.42 + 0.00) = 56.42 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

\_\_\_\_\_

-90 90 0.66 59.91 0.00 -2.04 -1.46 0.00 0.00 0.00 56.42 \_\_\_\_\_

Segment Leq: 56.42 dBA

Total Leq All Segments: 56.42 dBA

RT/Custom data, segment # 1: brt (day/night)

\_\_\_\_\_

1 - Bus:

Traffic volume : 192/66 veh/TimePeriod

Speed: 80 km/h

Data for Segment # 1: brt (day/night)

-----

Angle1 Angle2 : -90.00 deg 90.00 deg Wood depth : 0 (No woods.)

No of house rows : 0 / 0

Surface : 1 (Absorptive ground surface)

Receiver source distance: 85.10 / 85.10 m

Receiver height : 2.90 / 0.68 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

Results segment # 1: brt (day)

.....

Source height = 0.50 m

RT/Custom (0.00 + 45.58 + 0.00) = 45.58 dBAAngle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

-90 90 0.65 59.44 -12.42 -1.44 0.00 0.00 0.00 45.58

Segment Leq: 45.58 dBA

Total Leg All Segments: 45.58 dBA

Results segment # 1: brt (night)

\_\_\_\_\_

Source height = 0.50 m

RT/Custom (0.00 + 43.84 + 0.00) = 43.84 dBAAngle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

-90 90 0.66 57.81 -12.51 -1.46 0.00 0.00 0.00 43.84

.....

Segment Leg: 43.84 dBA

Total Leq All Segments: 43.84 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 64.20

(NIGHT): 56.65

#### MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: condor3b.te Time Period: Day/Night 16/8 hours Description: Harmony Condo Block ila R3b upper condo

Road data, segment # 1: CMD (day/night)

-----

Car traffic volume: 9715/845 veh/TimePeriod \* Medium truck volume: 773/67 veh/TimePeriod \* Heavy truck volume: 552/48 veh/TimePeriod \*

Posted speed limit: 50 km/h Road gradient : 1 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 12000 Percentage of Annual Growth : 0.00 Number of Years of Growth : 0.00 Medium Truck % of Total Volume : 7.00 Heavy Truck % of Total Volume : 5.00 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: CMD (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg

Wood depth : 0 (No woods.)

No of house rows : 0 / 0

Surface : 1 (Absorptive ground surface)

Receiver source distance: 19.90 / 19.90 m Receiver height : 5.70 / 8.50 m

Topography : 1 (Flat/gentle slope; no barrier)

Reference angle : 0.00

Results segment # 1: CMD (day)

-----

Source height = 1.50 m

ROAD (0.00 + 64.39 + 0.00) = 64.39 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

-90 90 0.53 67.51 0.00 -1.88 -1.24 0.00 0.00 0.00 64.39

\_\_\_\_\_\_

Segment Leq: 64.39 dBA

Total Leq All Segments: 64.39 dBA

Results segment # 1: CMD (night)

-----

Source height = 1.50 m

ROAD (0.00 + 57.05 + 0.00) = 57.05 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

\_\_\_\_\_

-90 90 0.45 59.91 0.00 -1.78 -1.08 0.00 0.00 0.00 57.05

\_\_\_\_\_

Segment Leq: 57.05 dBA

Total Leq All Segments: 57.05 dBA

RT/Custom data, segment # 1: brt (day/night)

\_\_\_\_\_

1 - Bus:

Traffic volume : 192/66 veh/TimePeriod

Speed: 80 km/h

Data for Segment # 1: brt (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg

Wood depth : 0 (No woods.)

No of house rows : 0 / 0

Surface : 1 (Absorptive ground surface)

Receiver source distance: 85.10 / 85.10 m

Receiver height : 5.70 / 8.50 m

Topography : 1 (Flat/gentle slope; no barrier)

Reference angle : 0.00

Results segment # 1: brt (day)

Source height = 0.50 m

RT/Custom (0.00 + 46.35 + 0.00) = 46.35 dBA

Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

-----

-90 90 0.56 59.44 -11.79 -1.29 0.00 0.00 0.00 46.35

\_\_\_\_\_

Segment Leq: 46.35 dBA

Total Leg All Segments: 46.35 dBA

Results segment # 1: brt (night)

-----

Source height = 0.50 m

RT/Custom (0.00 + 45.52 + 0.00) = 45.52 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

-----

-90 90 0.48 57.81 -11.16 -1.14 0.00 0.00 0.00 45.52

-----

Segment Leq: 45.52 dBA

Total Leq All Segments: 45.52 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 64.46 (NIGHT): 57.35

# **Appendix F**

Transportation Noise Source Predictions

Detailed Predicted Mitigated
 Noise Level Calculations

# STAMSON 5.0 NORMAL REPORT Date: 18-07-2018 08:57:47 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r1 22.te Time Period: Day/Night 16/8 hours Description: Harmony Block 104 ola R1 with 2.2m barrier

Road data, segment # 1: CMD (day/night)

\_\_\_\_\_

Car traffic volume: 9715/845 veh/TimePeriod \* Medium truck volume: 773/67 veh/TimePeriod \* Heavy truck volume: 552/48 veh/TimePeriod \*

Posted speed limit: 50 km/h Road gradient : 1 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 12000 Percentage of Annual Growth : 0.00 Number of Years of Growth : 0.00 Medium Truck % of Total Volume : 7.00 Heavy Truck % of Total Volume : 5.00 Day (16 hrs) % of Total Volume : 92.00

#### Data for Segment # 1: CMD (day/night)

-----

Angle1 Angle2 : -64.00 deg 63.00 deg

Wood depth : 0 (No woods.)

No of house rows : 0 / 0

Surface : 1 (Absorptive ground surface)

Receiver source distance: 25.50 / 25.50 m Receiver height : 1.50 / 4.50 m

Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -64.00 deg Angle2 : 63.00 deg
Barrier height : 2.20 m

Barrier receiver distance: 10.16 / 10.16 m

Source elevation : 93.67 m Receiver elevation : 93.94 m Barrier elevation : 93.80 m Reference angle : 0.00

Results segment # 1: CMD (day)

-----

Source height = 1.50 m

Barrier height for grazing incidence

\_\_\_\_\_

Source ! Receiver ! Barrier ! Elevation of

Height (m)! Height (m)! Barrier Top (m)

1.50! 1.50! 1.53! 95.33

ROAD (0.00 + 55.58 + 0.00) = 55.58 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

-64 63 0.53 67.51 0.00 -3.52 -2.03 0.00 0.00 -6.38 55.58

-----

Segment Leq: 55.58 dBA

Total Leq All Segments: 55.58 dBA

Results segment # 1: CMD (night)

-----

Source height = 1.50 m

Barrier height for grazing incidence

-----

Source ! Receiver ! Barrier ! Elevation of

Height (m)! Height (m)! Barrier Top (m)

1.50 ! 4.50 ! 3.34 ! 97.14

ROAD (0.00 + 54.22 + 0.00) = 54.22 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

-64 63 0.44 59.91 0.00 -3.31 -1.95 0.00 0.00 -0.19 54.46\*

 $\hbox{-64} \quad \ \ \, 63 \ \ \, 0.57 \ \, 59.91 \quad 0.00 \ \ \, -3.62 \ \ \, -2.07 \quad 0.00 \quad 0.00 \quad 0.00 \quad 54.22$ 

-----

Segment Leq: 54.22 dBA

Total Leq All Segments: 54.22 dBA

RT/Custom data, segment # 1: brt (day/night)

-----

1 - Bus:

Traffic volume : 192/66 veh/TimePeriod

Speed: 80 km/h

Data for Segment # 1: brt (day/night)

-----

Angle1 Angle2 : 0.00 deg 90.00 deg Wood depth : 0 (No woods.)

<sup>\*</sup> Bright Zone!

No of house rows : 0 / 0 Surface : 1 (Absorptive ground surface)

Receiver source distance: 54.10 / 54.10 m Receiver height : 1.50 / 4.50 m

Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : 0.00 deg Angle2 : 90.00 deg
Barrier height : 2.20 m

Barrier receiver distance: 10.16 / 10.16 m

Source elevation : 93.14 m Receiver elevation : 93.94 m Barrier elevation : 93.78 m Reference angle : 0.00

#### Results segment # 1: brt (day)

\_\_\_\_\_

Source height = 0.50 m

# Barrier height for grazing incidence

\_\_\_\_\_

Source ! Receiver ! Barrier ! Elevation of Height (m)! Height (m)! Barrier Top (m) -----

0.50! 1.50! 1.32! 95.10

RT/Custom (0.00 + 40.14 + 0.00) = 40.14 dBA

Angle1 Angle2 Alpha RefLeg D.Adj F.Adj W.Adj H.Adj B.Adj SubLeg 

0 90 0.56 59.44 -8.68 -4.29 0.00 0.00 -6.32 40.14 \_\_\_\_\_

Segment Leq: 40.14 dBA

Total Leg All Segments: 40.14 dBA

Results segment # 1: brt (night)

\_\_\_\_\_

Source height = 0.50 m

#### Barrier height for grazing incidence

\_\_\_\_\_

Source ! Receiver ! Barrier ! Elevation of Height (m)! Height (m)! Barrier Top (m)

-----+-----0.50! 4.50! 3.76! 97.54

RT/Custom (0.00 + 44.53 + 0.00) = 44.53 dBAAngle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

0 90 0.47 57.81 -8.18 -4.13 0.00 0.00 -0.62 44.88\*

0 90 0.60 57.81 -8.91 -4.37 0.00 0.00 0.00 44.53

\* Bright Zone!

Segment Leg: 44.53 dBA

Total Leq All Segments: 44.53 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 55.70

(NIGHT): 54.66

#### NORMAL REPORT Date: 18-07-2018 08:58:54 STAMSON 5.0 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r1 25.te Time Period: Day/Night 16/8 hours Description: Harmony Block 104 ola R1 with 2.5m barrier

Road data, segment # 1: CMD (day/night)

\_\_\_\_\_

Car traffic volume: 9715/845 veh/TimePeriod \* Medium truck volume: 773/67 veh/TimePeriod \* Heavy truck volume: 552/48 veh/TimePeriod \*

Posted speed limit: 50 km/h Road gradient : 1 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 12000 Percentage of Annual Growth : 0.00 Number of Years of Growth : 0.00 Medium Truck % of Total Volume : 7.00 Heavy Truck % of Total Volume : 5.00 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: CMD (day/night)

\_\_\_\_\_

Angle1 Angle2 : -64.00 deg 63.00 deg Wood depth : 0 (No woods.)

No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)

Receiver source distance: 25.50 / 25.50 m Receiver height : 1.50 / 4.50 m

Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -64.00 deg Angle2 : 63.00 deg

Barrier height : 2.50 m

Barrier receiver distance: 10.16 / 10.16 m

Source elevation : 93.67 m Receiver elevation : 93.94 m Barrier elevation : 93.80 m Reference angle : 0.00

Results segment # 1: CMD (day)

-----

Source height = 1.50 m

Barrier height for grazing incidence

-----

ROAD (0.00 + 54.44 + 0.00) = 54.44 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

------

-64 63 0.51 67.51 0.00 -3.48 -2.01 0.00 0.00 -7.58 54.44

Segment Leq: 54.44 dBA

Total Leq All Segments: 54.44 dBA

Results segment # 1: CMD (night)

-----

Source height = 1.50 m

Barrier height for grazing incidence

\_\_\_\_\_

ROAD (0.00 + 54.22 + 0.00) = 54.22 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

-----

-64 63 0.42 59.91 0.00 -3.27 -1.93 0.00 0.00 -1.92 52.79\* -64 63 0.57 59.91 0.00 -3.62 -2.07 0.00 0.00 0.00 54.22

-----

<sup>\*</sup> Bright Zone!

Segment Leq: 54.22 dBA

Total Leg All Segments: 54.22 dBA

#### RT/Custom data, segment # 1: brt (day/night)

-----

1 - Bus:

Traffic volume : 192/66 veh/TimePeriod

Speed: 80 km/h

#### Data for Segment # 1: brt (day/night)

-----

Angle1 Angle2 : 0.00 deg 90.00 deg

Wood depth : 0 (No woods.)

No of house rows : 0 / 0

Surface : 1 (Absorptive ground surface)

Receiver source distance: 54.10 / 54.10 m Receiver height : 1.50 / 4.50 m

Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : 0.00 deg Angle2 : 90.00 deg
Barrier height : 2.50 m

Barrier receiver distance: 10.16 / 10.16 m

Source elevation : 93.14 m Receiver elevation : 93.94 m Barrier elevation : 93.78 m Reference angle : 0.00

#### Results segment # 1: brt (day)

Source height = 0.50 m

#### Barrier height for grazing incidence

-----

Source ! Receiver ! Barrier ! Elevation of

Height (m)! Height (m)! Barrier Top (m)

-----0.50! 1.50! 1.32! 95.10

RT/Custom (0.00 + 39.47 + 0.00) = 39.47 dBA

Angle1 Angle2 Alpha RefLeg D.Adj F.Adj W.Adj H.Adj B.Adj SubLeg

0 90 0.54 59.44 -8.58 -4.26 0.00 0.00 -7.13 39.47

Segment Leg: 39.47 dBA

Total Leg All Segments: 39.47 dBA

Results segment # 1: brt (night)

-----

Source height = 0.50 m

Barrier height for grazing incidence

-----

Source ! Receiver ! Barrier ! Elevation of Height (m) ! Height (m) ! Barrier Top (m)

0.50 ! 4.50 ! 3.76 ! 97.54

RT/Custom (0.00 + 44.53 + 0.00) = 44.53 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

0 90 0.45 57.81 -8.08 -4.09 0.00 0.00 -1.03 44.61\*

0 90 0.60 57.81 -8.91 -4.37 0.00 0.00 0.00 44.53

\_\_\_\_\_

Segment Leq: 44.53 dBA

Total Leq All Segments: 44.53 dBA

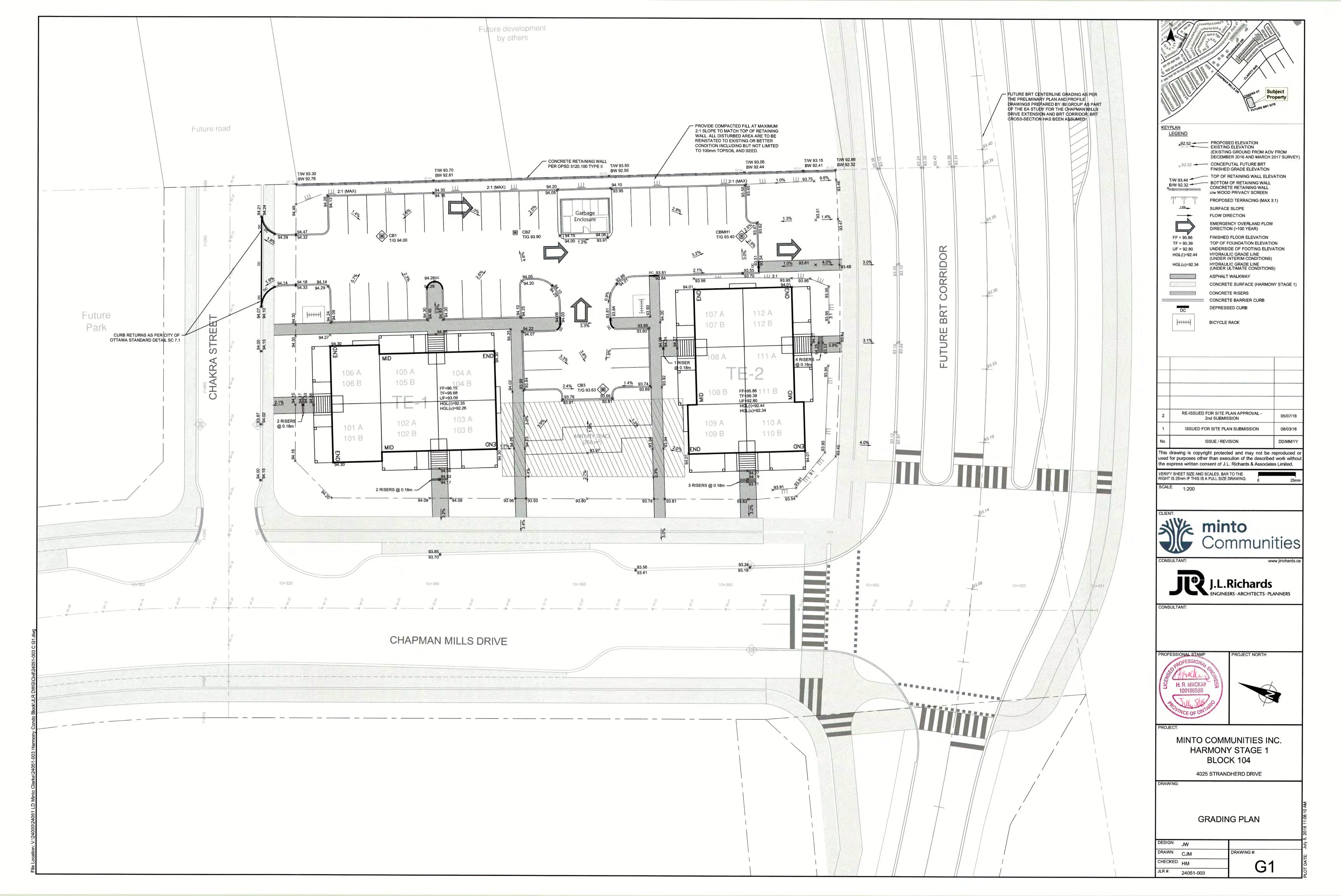
TOTAL Leq FROM ALL SOURCES (DAY): 54.58 (NIGHT): 54.66

<sup>\*</sup> Bright Zone!

HARMONY	STAGE 1 – BLOCK 104
DETAIL ED	NOISE CONTROL STUDY

# Appendix G

Grading Plan (G1)



# **Appendix H**

City of Ottawa Pre-Consultation Correspondence From: Thomas Couper

To: <u>Gregory Winters; Hilary MacKay; Ryan James</u>

Subject: FW: 4025 Strandherd Drive - Preconsultation Followup

**Date:** January 22, 2018 9:21:44 AM

Attachments: Pre-applicationMemo 4025Strandherd18122017.pdf

Studies and plans list.pdf

#### Good Morning All,

I am forwarding on the comments we have received from the City regarding our Harmony Stage 1 Condos. Please let me know if you have any questions. I will be sending out the Site Plan shortly.

Cheers,



?

Land Development Coordinator

Minto Communities - Canada
200-180 Kent St, Ottawa, ON, K1P 0B6
T 613.782.5720 | F 613.782.2416
minto.com

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**From:** Renaud, Jean-Charles [mailto:Jean-Charles.Renaud@ottawa.ca]

**Sent:** Monday, January 15, 2018 12:41 PM **To:** Thomas Couper <TCouper@minto.com>

Cc: Hugo Lalonde < HLalonde@minto.com >; Baggs, Rosanna < Rosanna.Baggs@ottawa.ca >; Sharif,

Sharif <sharif.sharif@ottawa.ca>

Subject: 4025 Strandherd Drive - Preconsultation Followup

Good morning Thomas,

Further to our meeting on December 11, 2017, regarding a proposal to construct a pair of new, 12-

unit apartment buildings, please find below an overview of what was discussed.

#### Official Plan and Zoning

- Official Plan: Designated "General Urban" under <u>Schedule B</u>
- Secondary Plan: Designated "Residential" under <u>Schedule A5</u> of the South Nepean Secondary Plan – <u>Area 8</u>
- Zoning: Residential Fourth Density, Subzone Z (R4Z)

#### **Planning** (JC Renaud)

- The Secondary Plan encourages minimized setbacks to the main street (Chapman Mills) and discourages parking areas next to the main street. Incorporate landscaping and/or increased setbacks in order to minimize the impact of parking along Chapman Mills.
- The Secondary Plan attaches much importance to the main street and its high quality of urban design and presence. This potentially being the first development to be approved on the main street, staff will be looking for it to set the stage for what this main street was intended to be. Enhanced streetscaping, lighting, built form should be sought.
- Please minimize the amount of siding and increase the amount of brick type materials facing both Chapman Mills frontages. Given the site's exposure to these streets, all four building façades should seek this enhancement.
- Be aware of the placement of the amenity area and its requirement for noise walls. Noise walls will be discouraged along Chapman Mills.
- Please relocate the southernmost pathway to be in line with the sidewalk on the east side of the northernmost building. Also include a similar sidewalk on the east side of the southernmost building.
- The following minor variances were mentioned. Please be aware of Bill 73, which may or
  may not affect you. Bell 73 places a two-year freeze on any application for minor variance
  from zoning by-law provisions that have been amended in response to an application by an
  owner, commencing on the passing of the zoning amendment.
  - o Location of garbage enclosure
  - o Parking space No.1 being located in the front yard

#### **Engineering** (Golam Sharif)

The engineering memo is attached.

#### **Transportation / Noise** (Rosanna Baggs)

- A transportation impact assessment screening form was sent to Rosanna Baggs. No triggers were satisfied, therefore no further action is required.
- The access as shown on the plan is too small. Please provide appropriate radii
- TWSIs will be required on the entrance sidewalk on the public ROW.

#### Trees

• Barrhaven falls well below the City's current urban canopy target of 30%. The site plan should be modified to include the planting of medium to large species of trees, in order to address the City's canopy target, to provide shading, and to mitigate the contribution of the development to the urban heat island effect.

#### **Development Applications Required**

- <u>Site Plan Control</u>, Manager Approved, Public Consultation
- Plan of Condominium
- The required plans and studies for the site plan control application are included in the attachment. You can reference the Guide to Preparing Studies and Plans in the link below. <a href="http://ottawa.ca/en/development-application-review-process-0/guide-preparing-studies-and-plans">http://ottawa.ca/en/development-application-review-process-0/guide-preparing-studies-and-plans</a>

I also encourage you to discuss the proposal with the area Councillor Jan Harder and local community associations.

I trust this information is helpful. Please do not hesitate to contact me if you have questions or require clarification.

#### JC

#### Jean-Charles Renaud, MCIP/MICU, RPP/UPC

Planner | *Urbaniste* 

Development Review, South | Examen des projets d'aménagement, Sud

Planning, Infrastructure and Economic Development Department | Services de la planification, de l'infrastructure et du développement économique

City of Ottawa | Ville d'Ottawa

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