



September 20, 2018

City of Ottawa  
Development Review - Urban Services Branch  
Planning and Growth Management Department  
110 Laurier Avenue West, 4th Floor  
Ottawa, ON, K1P 1J1

Attention: Mélanie Gervais, Planner

**Re Riverside South Elementary School, Ottawa-Carleton District School Board  
925 Ralph Hennessy Avenue, Ottawa  
Site Servicing Report**

Dear Mélanie:

We provide the following Site Servicing Report in accordance with the City of Ottawa Site Plan Control Application requirements for the Conseil des écoles catholiques du Centre-Est proposed Riverside South Elementary School at 925 Ralph Hennessy Avenue, Ottawa. The purpose of the report is to confirm that existing municipal and site services, including water, storm, and sanitary, can support the demand from the proposed new building.

#### Reference documents

- Site Servicing Plan – C1, Grading and Drainage, Erosion and Sediment Control Plan – C2 by Jp2g Consultants Inc., September 20, 2018.
- Stormwater Management Report by Jp2g Consultants Inc., September 20, 2018.
- Topographical Survey by Annis, O'Sullivan, Vollebakk Ltd., April 11, 2018, Job No. 18720-18.
- Riverside South Development Corporation Phase 13 Site Servicing and Stormwater Management Report, September 20, 2017

#### Background

The proposed elementary school is to be located on an existing vacant property, at the intersection of Ralph Hennessy Avenue and Mount Nebo Way, in the Riverside South subdivision phase 13, east of Spratt Road and south of Earl Armstrong Road in Ottawa, Ontario. The total site area is approximately 2.003 ha. The proposed site development includes a new school building, a bus lay-by, a car lay-by, asphalt parking, hard surface walkways and play areas, landscaped areas, a sports field, an area for portables and a future expansion of the building.

#### Servicing

##### **1.1 Storm Sewer and Stormwater Management**

Uncontrolled site storm drainage for the sidewalk and boulevard areas west and north of the proposed school will be collected by the existing curb inlet catch basins along Ralph Hennessy Way and Mount Nebo Way.

Controlled site storm drainage for the roof, asphalt parking, hard surface walkways and play areas, landscaped areas, sports field, area for portables and future expansion of the building will be collected to the existing 1650 mm diameter municipal storm sewer flowing west on Mount Nebo Way with an existing 600 mm diameter storm sewer stub teeing in from the subject property, via the new 1200 mm diameter storm manhole MHST-01 with a new 525 mm diameter storm sewer service inlet connection. The site currently has an existing ditch inlet connected to the 1650 mm diameter storm sewer on Mount Nebo Way. The ditch inlet and associated pipe will be removed up to the property line and abandoned to accommodate the new development.

Stormwater quantity control will be achieved using flow restrictors for the parking area and school yard. Stormwater management calculations are included in the Stormwater Management Report prepared by Jp2g, dated June 29, 2018.

## 1.2 Sanitary Sewer

There is an existing 450 mm diameter sanitary sewer flowing north along Ralph Hennessy Way with an existing 200 mm diameter sanitary sewer stub teeing in from the subject property. As indicated in the Stantec Consulting Report, dated June 30, 2017, wastewater generated in Riverside South Subdivision Phase 13 will be conveyed to the existing 450 mm diameter sanitary sewer on Ralph Hennessy way and 525 mm diameter sanitary sewer on Portico Way, then northerly to the existing Rideau River crossing, and ultimately to the existing West River Collector.

A proposed 1200 mm diameter sanitary manhole MHSA-01, connected to the existing 200 mm sanitary sewer service outlet with a new 200 mm diameter sanitary sewer service inlet approximately 2.0m deep, will service the proposed building. The sanitary sewer will outlet the building at a slope of 1.0% and connect to the proposed 1200 mm diameter sanitary sewer manhole MHSA-01 which ultimately connects to existing municipal sanitary sewer as per City of Ottawa Standard Detail S11.1.

Based on the City of Ottawa Sewer Design Guidelines, the peak sanitary flow for the site was calculated to be 2.3 l/s (Refer to Appendix A - Sanitary Sewer Design Sheet). This is in accordance with the sanitary flows accounted for in the Riverside South Development Corporation Phase 13 Site Servicing and Stormwater Management Report Sanitary Sewer Design Sheet, Phase 8 Stub 5 (Ralph Hennessy Avenue), Area ID Number I23AA with a total flow of 2.3 l/s, included Appendix A. The proposed 200mm diameter sanitary service will have a full flow capacity of 32.8 l/s, which will be sufficient to handle the proposed development sanitary flows.

## 1.3 Water

There is an existing 300 mm diameter watermain located on the east side of Ralph Hennessy Way, with an existing 200 mm diameter watermain service teeing in complete with an existing service valve box up to the property line of the subject property. A proposed 200mm diameter watermain will service the proposed school, and connect to the municipal watermain, in the right-of-way. The water meter will be located inside the school's mechanical room and a remote water meter will be installed along the building exterior.

The water demand for the proposed school was calculated based on Table 4.2 from the City of Ottawa Design Guidelines for Water Distribution. The calculations are based on the following criteria:

- Average daily demand for schools = 70 l/student/day
- School day = 8 hours
- Maximum school occupancy = 490 persons (staff and students)

Average Daily Demand:  $\frac{70 \text{ l/student/day} \times 490 \text{ students}}{8 \text{ hrs/day} \times 3600 \text{ s/hr}} = 1.19 \text{ l/s}$

Maximum Daily Demand:  $1.19 \text{ l/s} \times 1.5 = 1.79 \text{ l/s}$

Maximum Hour Demand:  $1.19 \text{ l/s} \times 1.8 = 2.14 \text{ l/s}$

There is an existing fire hydrant on Ralph Hennessy Avenue located along the front of the school building which will provide fire protection to the site. The proposed building will be equipped with sprinklers and a siamese connection located at the front of the building at the southeast entrance within 20 metres of the municipal fire hydrant. Based on the Fire Underwriters Survey Method, the fire flow demand for the proposed school was calculated to be:

Fire Flow Demand: 116.7 l/s (Refer to Appendix B – Fire Flow Calculations).

The above water demand requirements were provided to the City of Ottawa for the hydraulic analysis of the boundary conditions at the proposed school location. The following Boundary Conditions, included in Appendix B, were returned:

Max. HGL = 147.8 m (head) / 78.9 psi (pressure)  
PKHR = 145.6 m (head) / 75.8 psi (pressure)  
MXDY+Fire = 143.9 m (head) / 73.4 psi (pressure)

According to the City of Ottawa Design Guidelines, the installation of a pressure reducing valve will be required inside the building.

---

End of Site Servicing Report

Please contact the undersigned should you require any clarification.

Yours truly,

**Jp2g Consultants Inc.**  
ENGINEERS • PLANNERS • PROJECT MANAGERS



Roxanne Tubb, P.Eng.  
Civil Engineer

## **Appendix A - Sanitary Sewer Design Sheet**

Appendix A - Sanitary Sewer Design Sheet

A.1.1 - Peak Flow Design Based on Site Area

Definitions

Manning's Coefficient (n) = 0.013

Manning's Formula

$Q = A \cdot R^{2/3} S^{1/2} / n$  (l/s), where

A = Areas in Hectares (ha)

R = Hydraulic Radius (m)

S = Slope

Design Parameters\*

1) Average Daily Flow = 350 L/p/day

2) Commercial/Institutional Flow = 50,000 L/ha/day

3) Maximum Residential Peak Factor = 4

4) Commercial/Institutional Peak Factor = 1.50

5) Extraneous Flow = 0.28L/s/ha

6) Minimum Velocity = 0.76 m/s

Designed PH

Checked RT

Dwg. Reference C1

Jp2g project No 18-1015A

Location		Residential Flow**							Institutional Flow			Infiltration Flow		Total Flow	Sewer Data						
From	To	Area (ha)	Units	Population	Cumulative		Peak Factor	Peak Flow (l/s)	Area (ha)		Peak Flow (l/s)	Area (ha)		Inf. Flow (l/s)	Total Flow (l/s)	Length (m)	Dia. (mm)	Slope (%)	Capacity (full) (l/s)	Velocity (full) (m/s)	Utilization (%)
					Area	Population			Individual	Cumulative		Individual	Cumulative								
School	MHSA-01	0.00	0	0	0.00	0	4.00	0.00	2.003	2.003	1.74	2.003	2.003	0.56	2.30	8.3	200	1.0	32.8	1.0	7.0
MHSA-01	Ex. 450mm San. Sewer	0.00	0	0	0.00	0	4.00	0.00	0.000	2.003	1.74	0.000	2.003	0.56	2.30	13.2	200	1.0	32.8	1.0	7.0

A.1.2 - Peak Flow Design Based on Design Population

Design Parameters\*

1) Average Daily Sewage Flow for day school with cafeteria or gym and showers = 70 L/person/day

2) Institutional Peak Factor = 1.50

Type of Establishment	Population	Average Daily Flow** (l/s)	Infiltration Flow		Total Flow (l/s)	Sewer Data						
			Individual	Cumulative		Length (m)	Dia. (mm)	Slope (%)	Capacity (full) (l/s)	Velocity (full) (m/s)	Utilization (%)	
School	490	1.79	2.003	2.003	0.56	2.35	8.3	200	1.0	32.8	1.5	7.2

\* City of Ottawa Sewer Design Guidelines, Section 4 - Sanitary Sewer Systems

\*\*Residential flow data from Half Moon Bay Subdivision, Phase 1, 2, 3, 5, 6, sanitary sewer calculation sheets by DSEL, dated August 2010.

\*\*\*Calculated based on an 8-hour school day.



SUBDIVISION:  
**Riverside South Development Corporation - Phase 13**  
 DATE: April 6, 2017  
 REVISION: 1  
 DESIGNED BY: WAJ  
 CHECKED BY: AMP

**SANITARY SEWER DESIGN SHEET**  
 (City of Ottawa)

FILE NUMBER: 1604-01260

DESIGN PARAMETERS		External Areas	
MAX PEAK FACTOR (RES.)=	4.0	AVG. DAILY FLOW / PERSON	350 L/p/day
MIN PEAK FACTOR (RES.)=	2.0	COMMERCIAL	50,000 L/ha/day
PEAKING FACTOR (INDUSTRIAL):	2.4	INDUSTRIAL (HEAVY)	55,000 L/ha/day
PEAKING FACTOR (COMM., INST.):	1.5	INDUSTRIAL (LIGHT)	35,000 L/ha/day
PERSONS / SINGLE UNIT	3.2	INSTITUTIONAL	50,000 L/ha/day
PERSONS / TOWNHOME	2.4	INFILTRATION	0.28 L/s/ha
PERSONS / APARTMENT	1.9		
		MINIMUM VELOCITY	0.60 m/s
		MAXIMUM VELOCITY	3.00 m/s
		MANNINGS n	0.013
		BEDDING CLASS	B
		MINIMUM COVER	2.50 m
		Low Density	22 unit/ha*
		Medium Density	38 unit/ha*
		High Density	60 unit/ha
		* As per the RSCISSU, populations for low and medium density residential are based on 70% of the total area	

LOCATION	AREA ID NUMBER	FROM M.H.	TO M.H.	RESIDENTIAL AREA AND POPULATION						COMMERCIAL		INDUSTRIAL (L)		INDUSTRIAL (H)		INSTITUTIONAL		GREEN / UNUSED		C+I+I	INFILTRATION			TOTAL FLOW (L/s)	PIPE										
				AREA (ha)	SINGLE	UNITS TOWN	APT.	POP.	CUMULATIVE AREA (ha)	POP.	PEAK FACT.	PEAK FLOW (L/s)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)		ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)		PEAK FLOW (L/s)	TOTAL AREA (ha)	ACCU. AREA (ha)	INFILT. FLOW (L/s)	LENGTH (m)	DIA (mm)	MATERIAL	CLASS	SLOPE (%)	CAP. (FULL) (L/s)	CAP. V PEAK FLOW (%)
<b>Phase 8 Stub 7 (Portico Way)</b>																																			
External 3D, 3E, 4A, R80B (External), R80A																																			
	R79A	80	79	107.75	1169	373	1062	6652	107.75	6652	3.13	84.3	0.00	0.00	0.00	0.00	11.72	11.72	39.97	39.97	10.2	159.44	159.44	44.6	139.1	63.4	525	PVC	SDR 35	0.19	196.7	70.71%	0.88	0.84	
	R78A	79	78	0.11	0	0	0	0	107.86	6652	3.13	84.3	0.00	0.00	0.00	0.00	0.00	11.72	0.00	39.97	10.2	0.11	159.55	44.7	139.1	41.1	525	PVC	SDR 35	0.19	195.1	71.33%	0.87	0.83	
	R77AA	78	77	0.11	0	0	0	0	107.97	6652	3.13	84.3	0.00	0.00	0.00	0.00	0.00	11.72	0.00	39.97	10.2	0.11	159.66	44.7	139.2	41.1	525	PVC	SDR 35	0.19	200.1	69.53%	0.90	0.84	
	R77AA	77A	77	7.75	0	0	0	0	7.75	0	4.00	0.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0	7.75	7.75	2.2	2.2	13.0	200	PVC	SDR 35	1.00	33.4	6.49%	1.05	0.49		
	R77B, R77A	77	76	0.48	0	0	0	0	116.20	6652	3.13	84.3	0.00	0.00	0.00	0.00	0.00	11.72	0.00	39.97	10.2	0.48	167.89	47.0	141.5	110.6	525	PVC	SDR 35	0.19	195.7	72.30%	0.88	0.84	
	R76A	76	75	0.07	0	0	0	0	116.27	6652	3.13	84.3	0.00	0.00	0.00	0.00	0.00	11.72	0.00	39.97	10.2	0.07	167.96	47.0	141.5	26.4	525	PVC	SDR 35	0.19	197.2	71.77%	0.88	0.84	
	R75A	75	74	0.19	0	0	0	0	116.46	6652	3.13	84.3	0.00	0.00	0.00	0.00	0.00	11.72	0.00	39.97	10.2	0.19	168.15	47.1	141.5	71.3	525	PVC	SDR 35	0.19	195.1	72.56%	0.87	0.83	
	R74A	74	73	0.08	0	0	0	0	116.54	6652	3.13	84.3	0.00	0.00	0.00	0.00	0.00	11.72	0.00	39.97	10.2	0.08	168.23	47.1	141.6	32.3	525	PVC	SDR 35	0.19	195.4	72.47%	0.87	0.84	
	R73AA	73A	73	6.00	0	0	0	684	6.00	684	3.90	10.8	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0	6.00	6.00	1.7	12.5	13.0	200	PVC	SDR 35	1.00	33.4	37.34%	1.05	0.83		
	R73A	73	60E	0.20	0	0	0	0	122.74	7336	3.09	91.7	0.00	0.00	0.00	0.00	0.00	11.72	0.00	39.97	10.2	0.20	174.43	48.8	150.7	78.2	525	PVC	SDR 35	0.19	195.9	76.95%	0.88	0.85	
<b>Phase 8 Stub 6 (Pathfinder Way)</b>																																			
	R41A	41	40	0.45	4	0	0	13	0.45	13	4.00	0.2	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0	0.45	0.45	0.1	0.3	77.1	200	PVC	SDR 35	0.65	27.1	1.23%	0.85	0.24		
	R40A	40	39	0.34	4	0	0	13	0.78	26	4.00	0.4	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0	0.34	0.78	0.2	0.6	76.4	200	PVC	SDR 35	0.32	18.9	3.36%	0.60	0.23		
	R39A	39	38	0.13	1	0	0	3	0.91	29	4.00	0.5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0	0.13	0.91	0.3	0.7	11.4	200	PVC	SDR 35	0.32	18.9	3.82%	0.60	0.24		
	R38A	38	37	0.52	9	0	0	29	1.44	58	4.00	0.9	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0	0.52	1.44	0.4	1.3	77.0	200	PVC	SDR 35	0.32	18.9	7.06%	0.60	0.29		
	R37A	37	36	0.93	17	0	0	54	2.37	112	4.00	1.8	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0	0.93	2.37	0.7	2.5	120.0	200	PVC	SDR 35	0.32	18.9	13.10%	0.60	0.34		
	R36A	36	35	0.05	0	0	0	0	2.42	112	4.00	1.8	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0	0.05	2.42	0.7	2.5	33.8	200	PVC	SDR 35	0.32	18.9	13.18%	0.60	0.34		
	G72A, R72A	72	47	0.46	6	0	0	19	0.46	19	4.00	0.3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0	2.18	2.18	0.6	0.9	100.1	200	PVC	SDR 35	0.65	27.0	3.42%	0.85	0.34		
	R58A	58	51	0.36	0	9	0	22	0.36	22	4.00	0.4	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0	0.36	0.36	0.1	0.5	68.2	200	PVC	SDR 35	0.65	26.9	1.68%	0.85	0.26		
	R57A	57	53	0.36	0	10	0	24	0.36	24	4.00	0.4	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0	0.36	0.36	0.1	0.5	71.6	200	PVC	SDR 35	0.32	18.9	2.59%	0.60	0.22		
	R67A	67	66	0.34	0	9	0	22	0.34	22	4.00	0.4	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0	0.34	0.34	0.1	0.4	61.4	200	PVC	SDR 35	0.65	27.0	1.65%	0.85	0.26		
	R66B (External), R66A	66	56	0.22	0	5	0	12	0.56	34	4.00	0.5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0	1.52	1.86	0.5	1.1	49.3	200	PVC	SDR 35	0.32	18.9	5.63%	0.60	0.27		
	R56A	56	55	0.32	0	8	0	19	0.88	53	4.00	0.9	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0	0.32	2.18	0.6	1.5	61.5	200	PVC	SDR 35	0.32	18.9	7.75%	0.60	0.30		
	R55A	55	54	0.07	0	1	0	2	0.95	55	4.00	0.9	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0	0.07	2.25	0.6	1.5	10.0	200	PVC	SDR 35	0.32	18.9	8.06%	0.60	0.30		
	R54A	54	53	0.39	0	10	0	24	1.34	79	4.00	1.3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0	0.39	2.64	0.7	2.0	82.1	200	PVC	SDR 35	0.32	18.9	10.69%	0.60	0.33		
	R53A	53	52	0.66	0	21	0	50	2.37	154	4.00	2.5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0	0.66	3.67	1.0	3.5	78.8	200	PVC	SDR 35	0.32	18.9	18.58%	0.60	0.38		
	R52A	52	51	0.12	0	4	0	10	2.48	163	4.00	2.6	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0	0.12	3.78	1.1	3.7	18.0	200	PVC	SDR 35	0.32	18.9	19.58%	0.60	0.39		
	R51A	51	50	0.45	0	11	0	26	3.29	211	4.00	3.4	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0	0.45	4.59	1.3	4.7	81.9	200	PVC	SDR 35	0.32	18.9	24.89%	0.60	0.41		
	R60A	60	59	0.37	4	6	0	27	0.37	27	4.00	0.4	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0	0.37	0.37	0.1	0.5	41.8	200	PVC	SDR 35	0.32	18.9	2.88%	0.60	0.22		
	R59A	59	50	0.89	9	15	0	65	1.27	92	4.00	1.5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0	0.89	1.27	0.4	1.8	114.6	200	PVC	SDR 35	0.32	18.9	9.76%	0.60	0.31		
	R50A	50	49	0.07	0	0	0	0	4.63	303	4.00	4.9	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0	0.07	5.93	1.7	6.6	49.0	200	PVC	SDR 35	0.32	18.9	34.75%	0.60	0.46		
	R65A	65	64	0.50	0	11	0	26	0.50	26	4.00	0.4	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0	0.50	0.50	0.1	0.6	77.2	200	PVC	SDR 35	0.32	18.9	3.00%	0.60	0.23		
	R64A	64	63	0.58	0	16	0	38	1.08	65	4.00	1.1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0	0.58	1.08	0.3	1.4	58.5	200	PVC	SDR 35	0.32	18.9	7.15%	0.60	0.29		
	R63A	63	62	0.56	5	3	0																												



SUBDIVISION:  
**Riverside South Development Corporation - Phase 13**  
 DATE: April 6, 2017  
 REVISION: 1  
 DESIGNED BY: WAJ  
 CHECKED BY: AMP

**SANITARY SEWER DESIGN SHEET**  
 (City of Ottawa)

FILE NUMBER: 1604-01260

DESIGN PARAMETERS		External Areas	
MAX PEAK FACTOR (RES.)=	4.0	Low Density	22 uni/ha*
MIN PEAK FACTOR (RES.)=	2.0	Medium Density	38 uni/ha*
PEAKING FACTOR (INDUSTRIAL):	2.4	High Density	60 uni/ha*
PEAKING FACTOR (COMM., INST.):	1.5	* As per the RSCISSU, populations for low and medium density residential are based on 70% of the total area	
PERSONS / SINGLE UNIT	3.2		
PERSONS / TOWNHOME	2.4		
PERSONS / APARTMENT	1.9		
AVG. DAILY FLOW / PERSON	350 L/p/day	MINIMUM VELOCITY	0.60 m/s
COMMERCIAL	50,000 L/ha/day	MAXIMUM VELOCITY	3.00 m/s
INDUSTRIAL (HEAVY)	55,000 L/ha/day	MANNINGS n	0.013
INDUSTRIAL (LIGHT)	35,000 L/ha/day	BEDDING CLASS	B
INSTITUTIONAL	50,000 L/ha/day	MINIMUM COVER	2.50 m
INFILTRATION	0.28 L/s/ha		

LOCATION	RESIDENTIAL AREA AND POPULATION										COMMERCIAL		INDUSTRIAL (L)		INDUSTRIAL (H)		INSTITUTIONAL		GREEN / UNUSED		C+I+I	INFILTRATION			TOTAL FLOW (L/s)	PIPE										
	AREA ID NUMBER	FROM M.H.	TO M.H.	AREA (ha)	SINGLE	UNITS TOWN	APT.	POP.	CUMULATIVE AREA (ha)	POP.	PEAK FACT.	PEAK FLOW (L/s)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)		AREA (ha)	ACCU. AREA (ha)	PEAK FLOW (L/s)		TOTAL AREA (ha)	ACCU. AREA (ha)	INFILT. FLOW (L/s)	LENGTH (m)	DIA (mm)	MATERIAL	CLASS	SLOPE (%)	CAP. (FULL) (L/s)	CAP. V PEAK FLOW (%)	VEL. (FULL) (m/s)
R70A	70	69	0.20	2	0	0	6	1.08	48	4.00	0.8	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.20	1.08	0.3	1.1	8.6	200	PVC	SDR 35	0.32	18.9	5.72%	0.60	0.27
R69A	69	68	0.24	3	0	0	10	1.32	58	4.00	0.9	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.24	1.32	0.4	1.3	43.7	200	PVC	SDR 35	0.32	18.9	6.89%	0.60	0.29	
R68A	68	47	0.17	2	0	0	6	1.49	64	4.00	1.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.17	1.49	0.4	1.5	36.8	200	PVC	SDR 35	0.32	18.9	7.68%	0.60	0.30	
R47A	47	46	0.04	0	0	0	0	10.12	554	3.95	8.9	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.04	13.13	3.7	12.5	23.4	200	PVC	SDR 35	0.32	19.0	66.21%	0.60	0.55	
R46A	46	45	0.10	0	0	0	0	10.22	554	3.95	8.9	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.10	13.23	3.7	12.6	62.1	200	PVC	SDR 35	0.32	18.9	66.44%	0.60	0.55	
R45B, R45A	45	44	0.37	4	0	0	13	10.59	567	3.95	9.1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.37	13.60	3.8	12.9	36.5	200	PVC	SDR 35	0.40	21.1	60.90%	0.67	0.60	
R44A	44	43	0.23	4	0	0	13	10.81	580	3.94	9.3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.23	13.83	3.9	13.1	23.4	250	PVC	SDR 35	0.25	30.2	43.52%	0.61	0.50	
R43A	43	42	0.63	12	0	0	38	11.44	618	3.92	9.8	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.63	14.45	4.0	13.9	78.1	250	PVC	SDR 35	0.25	30.3	45.78%	0.61	0.51	
R42A	42	35	0.20	3	0	0	10	11.64	628	3.92	10.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.20	14.65	4.1	14.1	27.7	250	PVC	SDR 35	0.25	30.3	46.44%	0.61	0.51	
R35A	35	34	0.21	3	0	0	10	14.27	750	3.88	11.8	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.21	17.28	4.8	16.6	24.6	250	PVC	SDR 35	0.25	30.3	54.79%	0.61	0.54	
R34A	34	33	0.36	8	0	0	26	14.63	775	3.87	12.1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.36	17.64	4.9	17.1	40.6	250	PVC	SDR 35	0.26	30.7	55.65%	0.62	0.55	
<b>Phase 8 Stub 1 (Taurus Place)</b>																																				
R4A	4	3	0.35	6	0	0	19	0.35	19	4.00	0.3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.35	0.35	0.1	0.4	90.4	200	PVC	SDR 35	0.65	27.0	1.51%	0.85	0.26	
R3AA	3A	3	2.21	0	0	0	252	2.21	252	4.00	4.1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.21	2.21	0.6	4.7	8.3	200	PVC	SDR 35	1.00	33.5	14.05%	1.05	0.61	
R3A	3	2	0.10	2	0	0	6	2.65	278	4.00	4.5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.10	2.65	0.7	5.2	13.9	200	PVC	SDR 35	0.65	27.0	19.44%	0.85	0.54	
	2	1	0.00	0	0	0	0	2.65	278	4.00	4.5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.65	0.7	5.2	2.2	200	PVC	SDR 35	0.34	19.4	26.99%	0.61	0.43	
<b>Phase 8 Stub 2 (Serenade Crescent)</b>																																				
R4B	4	6	0.44	10	0	0	32	0.44	32	4.00	0.5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.44	0.44	0.1	0.6	67.6	200	PVC	SDR 35	0.35	19.7	3.26%	0.62	0.23	
R10A	10	9	1.00	19	0	0	61	1.00	61	4.00	1.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	1.00	0.3	1.3	120.0	200	PVC	SDR 35	0.60	25.9	4.89%	0.81	0.35	
R9A	9	8	0.15	2	0	0	6	1.15	67	4.00	1.1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.15	1.15	0.3	1.4	12.4	200	PVC	SDR 35	0.40	21.1	6.67%	0.67	0.31	
R8A	8	7	0.61	12	0	0	38	1.76	106	4.00	1.7	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.61	1.76	0.5	2.2	79.4	200	PVC	SDR 35	0.40	21.1	10.42%	0.67	0.36	
R7A	7	6	0.56	10	0	0	32	2.32	138	4.00	2.2	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.56	2.32	0.6	2.9	62.0	200	PVC	SDR 35	0.40	21.1	13.61%	0.67	0.39	
	6	5	0.00	0	0	0	0	2.76	170	4.00	2.7	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.76	0.8	3.5	11.6	200	PVC	SDR 35	0.34	19.4	18.13%	0.61	0.38	
<b>Phase 8 Stub 3 (Dreamcatcher Place)</b>																																				
R32A	32	31	0.60	8	0	0	26	0.60	26	4.00	0.4	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.60	0.60	0.2	0.6	59.5	200	PVC	SDR 35	0.65	27.0	2.16%	0.85	0.29	
R31B	31	15	0.43	6	0	0	19	1.02	45	4.00	0.7	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.43	1.02	0.3	1.0	63.7	200	PVC	SDR 35	0.40	21.1	4.79%	0.67	0.28	
R15A	15	14	0.17	2	0	0	6	1.19	51	4.00	0.8	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.17	1.19	0.3	1.2	17.1	200	PVC	SDR 35	0.40	21.2	5.48%	0.67	0.29	
R14A	14	13	0.17	2	0	0	6	1.36	58	4.00	0.9	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.17	1.36	0.4	1.3	30.8	200	PVC	SDR 35	0.40	21.1	6.21%	0.67	0.31	
R13A	13	12	0.48	7	0	0	22	1.83	80	4.00	1.3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.48	1.83	0.5	1.8	61.5	200	PVC	SDR 35	0.40	21.1	8.57%	0.66	0.34	
G19AA	19A	19	0.00	0	0	0	0	0.00	0	4.00	0.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.55	0.55	0.0	0.2	11.0	150	PVC	DR 28	1.00	15.3	1.01%	0.86	0.23	
R19A	19	18	0.39	3	0	0	10	0.39	10	4.00	0.2	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.39	0.94	0.3	0.4	45.0	200	PVC	SDR 35	0.65	27.0	1.56%	0.85	0.26	
R18A	18	17	0.21	2	0	0	6	0.61	16	4.00	0.3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.21	1.16	0.3	0.6	12.7	200	PVC	SDR 35	0.65	27.0	2.16%	0.85	0.29	
R17A	17	12	0.38	6	0	0	19	0.99	35	4.00	0.6	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.38	1.54	0.4	1.0	75.0	200	PVC	SDR 35	0.40	21.1	4.73%	0.67	0.28	
R12A	12	11	0.07	1	0	0	3	2.89	118	4.00	1.9	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.07	3.44	1.0	2.9	13.9	200	PVC	SDR 35	0.34	19.5	14.80%	0.61	0.36	
<b>Phase 8 Stub 4 (Serenade Crescent)</b>																																				
R10B	10	30	0.72	13	0																															

## **Appendix B - Fire Flow Calculations**



## Appendix C - Fire Flow Demand Requirements (Fire Underwriters Survey (FUS Guidelines))

Riverside South Elementary School, 925 Ralph Hennessy Avenue, Ottawa, ON



### Appendix C - Water Demand

#### C.1.1 - Fire Flow Demand Requirements

##### Design Parameters\*

Estimated Fire Flow Formula:  $F = 220 \cdot C \cdot A^{1/2}$  (L/min)

F = Required fire flow (L/min)

C = Coefficient related to the type of construction

C<sub>1.5</sub> = 1.5 for wood frame construction

C<sub>1.0</sub> = 1.0 for ordinary construction

C<sub>0.8</sub> = 0.8 for non-combustible construction

C<sub>0.6</sub> = 0.6 for fire-resistive construction

A = Total floor area in square metres

Adjustments to the calculated fire flow are based on: reduction for low fire hazard occupancy (school), reduction for automatic sprinkler protection, and an increase for exposures for residences within 45 metres on two sides of the school. The table below summarizes the adjustments made to the basic fire flow.

Exposure Adjustment Calculation		
Separation Distance		32.0
Length*Height factor of exposed wall	=42m*2 storeys	84.0
Construction of exposed wall	Wood frame or non-combustible	5%

Building Construction	Floor Area***	C	Adjustments (increases or decreases)							Final Adjusted Fire Flow	Final Adjusted Fire Flow
			1	2		3		4			
			Fire Flow (F)	Occupancy		Sprinkler**		Exposure***			
non-combustible construction	(m <sup>2</sup> )		(L/min)	%	Adjusted Fire Flow(s) (L/min)	%	Adjusted Fire Flow(s) (L/min)	%	Adjusted Fire Flow(s) (L/min)	(L/min)	(L/s)
	4,257.0	0.8	11,000.0	0.0	11,000.0	30%	3,300.0	5%	550.0	7,000.0	116.7

\*Water Supply for Public Protection (Fire Underwriters Survey, 1999).

\*\*The building is partially sprinklered, but not monitored.

\*\*\*Including all stories

#### C.1.2 - Existing Water Boundary Conditions

##### Water Demands

Average Daily Demand:	1.00 l/s
Maximum Daily Demand:	1.50 l/s
Maximum Hour Demand:	1.80 l/s
Fire Flow Demand:	116.67 l/s
Maximum Daily + Fire Flow Demand:	118.17 l/s

##### Design Parameters

Pipe Diameter:	200 mm
Pipe Material:	PVC
Pipe Length	58.0 m
Finished Floor Elevation:	93.75
Pavement (R.O.W.) Elevation:	93.30

##### Boundary Conditions

Max. HGL:	147.8 m
Min HGL:	145.6 m
Max. Day + Fire:	143.9 m

##### Boundary Condition Check

Check water pressure at municipal connection:

Min. HGL - Pavement elevation = 52.30 m

