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## **Boundary Road Distribution Centre**

Stormwater Management Report

#### STORMWATER MANAGEMENT REPORT

# BOUNDARY ROAD DISTRIBUTION CENTRE OTTAWA, ONTARIO

#### Prepared For:

## **Boundary Road Development Inc.**

16766 Transcanadienne, Suite 500 Kirkland, Québec H9H 4M7

Prepared By:

#### **NOVATECH**

Suite 200, 240 Michael Cowpland Drive Ottawa, Ontario K2M 1P6

April 12, 2018

Novatech File: 117217 Report Number: R-2018-034



April 12, 2018

City of Ottawa Planning and Growth Management Department Infrastructure Approvals Division 110 Laurier Avenue West, 4<sup>th</sup> Floor Ottawa, ON K1P 1J1

Attention: Mr. Kevin Hall

Dear Sir:

Re: Proposed Boundary Road Distribution Centre

5371 Boundary Road, Ottawa ON Stormwater Management Report

Novatech File No.: 117217

Please find enclosed the Stormwater Management Report for the proposed Boundary Road Distribution Centre at 5371 Boundary Road. This report is submitted in support of an application for Site Plan Approval.

If you require any additional information, please contact the undersigned.

Yours truly,

**NOVATECH** 

Kallie Auld, P.Eng.

Kallii Huld.

Project Coordinator | Water Resources

cc: Matthew LeBlanc (South Nation Conservation)

Stephen Kapusta (Ministry of Transportation Ontario)

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117217-GP1	General Plan of Services, Rev 5
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117217-GPND	Servicing Notes and Details, Rev 3
117217-ESC	Erosion and Sediment Control Plan, Rev 3
117217-ESND	Erosion and Sediment Control Notes and Details, Rev 3
117217-SWMF1	Stormwater Management Facility – Plan, Rev 4
117217-SWMF2	Stormwater Management Facility – Sections, Rev 4
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117217-PRE	Pre-Development Storm Drainage Area Plan, Rev 1
117217-POST	Post-Development Storm Drainage Area Plan, Rev 1
117217-DR	Ditch Relocation Plan

#### **Enclosed CD**

**PCSWMM Modelling Files** 

Stormwater Management Report including drawings listed above (PDF)

Novatech ii

#### 1.0 INTRODUCTION

Novatech has been retained by Boundary Road Development Inc. to complete the stormwater management design for a new distribution centre near the eastern boundary of the City of Ottawa, located at 5371 Boundary Road. The proposed development consists of a single large distribution warehouse, distribution trucking lot, staff parking facility, and a stormwater management facility. Refer to the enclosed site plan for details. **Figure 1** – Key Plan shows the general site area.

This report addresses the stormwater management approach for the proposed development and is submitted in support of an application for Site Plan Approval. This report should be read in conjunction with the engineering drawings (enclosed).

#### 1.1 Background

The subject property (38.9 ha) is located on the east side of Boundary Road and is bounded by Highway 417 to the north, and predominantly undeveloped land to the east and south. The site is approximately 1.6 km south of Carlsbad Springs.

#### 1.2 Land Use

Under existing conditions, site consists of a mix of heavily forested / tree covered lands, agricultural lands, and vacant property. There is currently a Rogers Communications cell tower located on the site. Existing Conditions are shown on **Figure 2** – Existing Conditions.

#### 1.3 Topography & Drainage Outlets

The site is relatively flat, with an average slope of 0.25% from west to east. Under existing conditions, stormwater runoff flows overland across the subject property into a man-made drainage ditch system. The drainage ditches direct runoff into a culvert crossing under the Highway 417, at the eastern end of the site.

The entire site is within the drainage area of the Regimbald Municipal Drain. The upper end of the municipal drain terminates just upstream of the culvert crossing under Highway 417. The Regimbald Municipal Drain Assessment map can be found in **Appendix A**.

Existing contours and drainage patterns are shown on the Pre-Development Drainage Areas Plan (**Figure 3**).

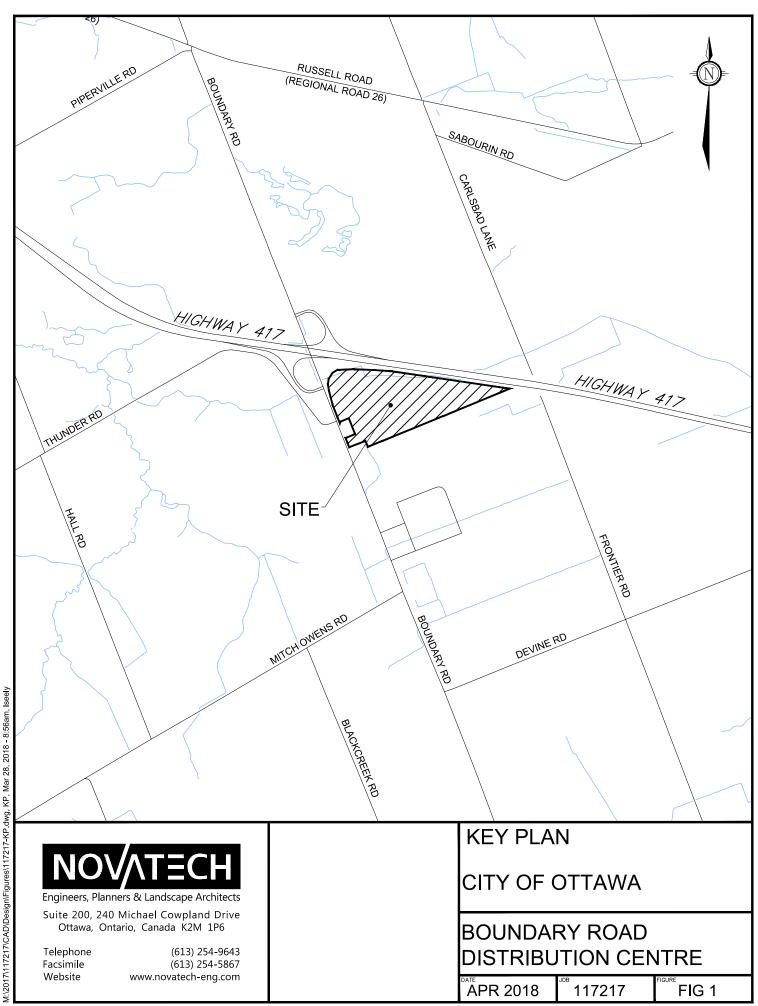
#### 1.4 Subsurface Conditions

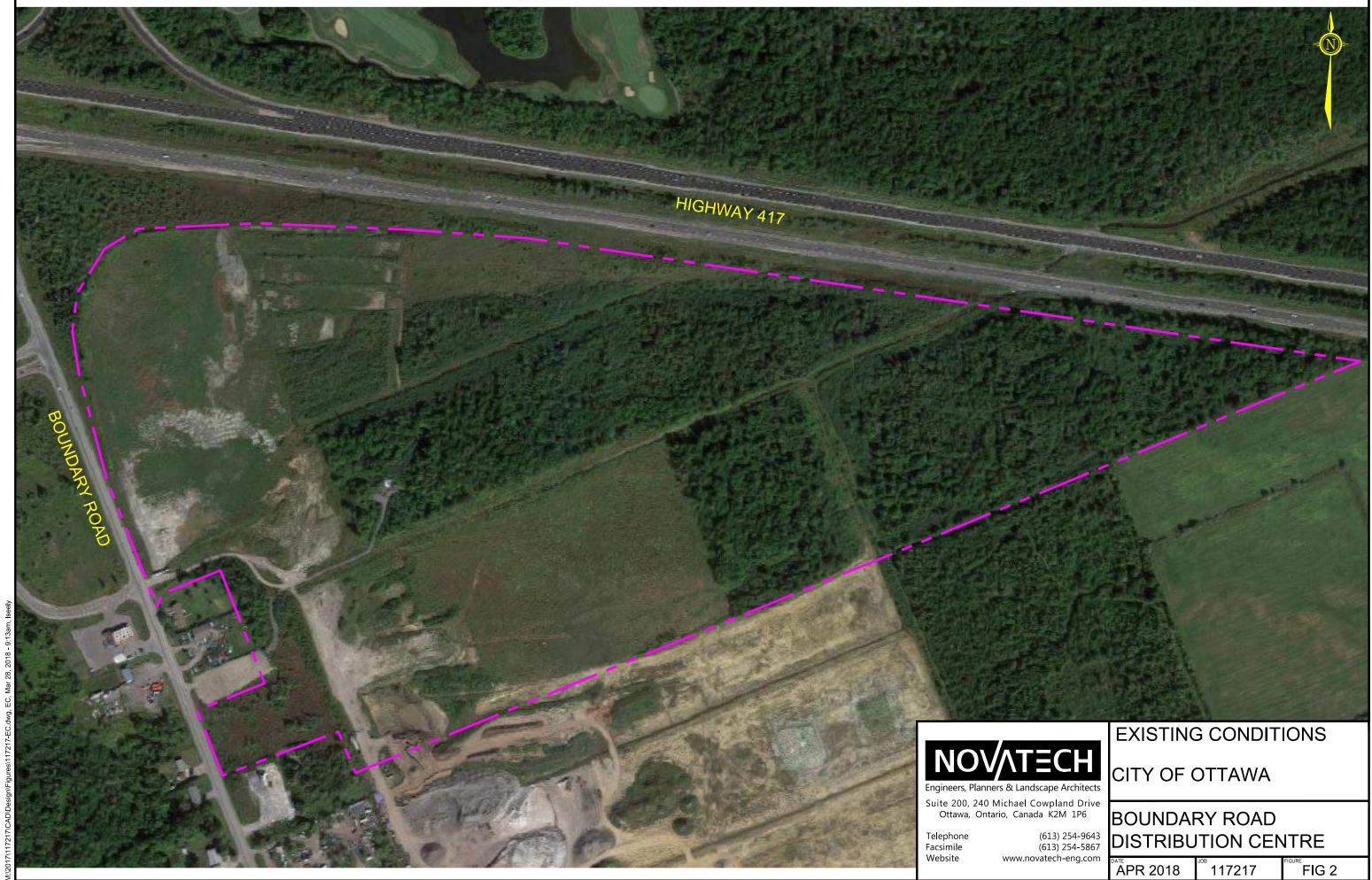
Paterson Group conducted a Preliminary Geotechnical Investigation of the site on July 15, 2014. The investigation consisted of and overall field survey and six (6) test pits dug to a maximum depth of 5.2m below the existing ground surface. In general, the soil consists of imported fill material and topsoil, underlain by silty sand and stiff to soft silty clay. The overall site is underlain by a firm to soft sensitive grey silty clay deposit. Based on the available geological mapping, the overburden thickness is between 25m to 35m.

During the geotechnical investigation, the groundwater levels were noted in each of the test pits. Based on observations during the investigation, groundwater levels range from 0.5m to 2.0m below the ground surface.

Fur further information, please refer to the following report:

 Geotechnical Investigation - Proposed Warehouse Complex - Boundary Road, Ottawa, Ontario (Patterson Group, February 9, 2018, Report Number PG4366-1)





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#### 2.0 STORMWATER MANAGEMENT DESIGN CRITERIA AND OBJECTIVES

The subject site is located within the jurisdiction of the South Nation Conservation Authority (SNCA). As such, the following stormwater management criteria and objectives have been developed through consultation with the SNCA and the City of Ottawa Sewer Design Guidelines.

#### Stormwater Quantity

- Design a storm drainage system (a combination of storm sewers, ditches, and culverts) to convey post-development peak flows from the site to the proposed stormwater management facility;
- The proposed storm drainage system should not have any adverse impact on downstream properties or development;
- No ponding within the asphalt parking for storm events up to and including the 2-year event;
- Road crossing culverts are to be sized for the 5-year event, and to minimize the overflow onto the adjacent parking areas;
- Post-development peak flows are to be controlled to pre-development levels for all storm events, up to and including the 100-year event.

#### Stormwater Quality

- Implement lot level and conveyance Best Management Practices;
- Provide an 'Enhanced' level of stormwater quality control corresponding to a long-term removal rate of 80% Total Suspended Solids (TSS).

#### **Erosion and Sediment Control**

• Minimize the impact on the downstream receiving watercourses by minimizing the potential erosion and volume of sediment entering the watercourses on a temporary basis (during construction) and on a permanent basis.

#### 3.0 PROPOSED DEVELOPMENT

The proposed Boundary Road Distribution Centre is approximately 38.9 ha and is to consist of a single large distribution warehouse, distribution trucking lot, staff parking facility, and a stormwater management facility. The proposed development is shown on the enclosed engineering plans listed below:

- 117217-GR Overall Grading Plan, Rev 4
  - 117217-GR1 Grading Plan, Rev 3
  - o 117217-GR2 Grading Plan, Rev 3
  - o 117217-GR3 Grading Plan, Rev 3
  - 117217-GR4 Grading Plan, Rev 3
  - 117217-GRND Grading Notes and Details, Rev 1
- 117217-GP Overall Plan of Services. Rev 4
  - 117217-GP1 General Plan of Services, Rev 3
  - o 117217-GP2 General Plan of Services, Rev 3
  - o 117217-GP3 General Plan of Services, Rev 3
  - o 117217-GP4 General Plan of Services, Rev 3
  - 117217-GPND Servicing Notes and Details, Rev 1
- 117217-ESC Erosion and Sediment Control Plan, Rev 1
  - 117217-ESND Erosion and Sediment Control Notes and Details, Rev 1
- 117217-SWMF1 Stormwater Management Facility Plan, Rev 3
  - o 117217-SWMF1 Stormwater Management Facility Sections, Rev 2
  - 117217-SWMF1 Stormwater Management Facility Details, Rev 2
- 117217-PRE Pre-Development Storm Drainage Area Plan, Rev 1
- 117217-POST Post-Development Storm Drainage Area Plan, Rev 1
- 117217-DR Ditch Relocation Plan

Runoff from all storm events will be conveyed by a combination of storm sewers (minor system) and a ditch network throughout the property (overland flow path). The proposed SWM facility will be the outlet for both the storm sewers and the ditch network.

#### 3.1 Storm Sewer Design (Minor System)

The proposed storm sewers have been designed using the Rational Method and the PCSWMM modeling software to convey peak flows associated with a 5-year storm event from the roof drains of the proposed warehouse building. Storm sewers have been matched invert-to-invert due to the grade restrictions on-site. Overflows from the storm sewers as a result of surcharging during large (100-yar) storm events are to be directed overland across the parking areas to the adjacent ditch network. The corresponding Storm Drainage Area Plan has been provided in **Appendix D**.

#### 3.2 Ditch Design (Overland Flow Path)

To convey peak flows for all storm events from the parking areas and surrounding grassed areas, a network of ditches throughout the property have been proposed. Starting at the western parking lot, the ditches slope to the north and south, following along the boundary of the parking areas. For the southern portion of the site, the ditch network follows along proposed access roads. The geometry of the ditches varies throughout the site, with bottom widths ranging from 1.0m to 4.0m and depths from 0.30m to 0.45m. The side slopes of the proposed ditches are to be 3:1 (H:V) throughout. Refer to the Grading Plans (117217-GR, GR1-4) for details.

#### 3.3 Stormwater Management Facility

The proposed grading and drainage design includes on-site quantity and quality control. Stormwater runoff from the proposed development will be directed to a wet pond SWM facility in the eastern corner of the site for water quality and quantity control. Outflows from the SWM facility will directed to the culvert crossing under Highway 417.

- Quantity Control: Post-development flows from the subject site will be controlled to predevelopment levels by and pond outlet structure for all storms up to and including the 100-year storm event.
- **Quality Control:** The two forebays and permanent pool have been sized based on the MOECC criteria to provide up to 80% TSS removal.

Additional information on the SWM facility (including design criteria) is provided in **Section 0**.

#### 3.4 Drainage Outlets

Under post-development conditions, the SWM facility will outlet to the existing ditch, and through the existing 1350mm culvert crossing under Highway 417.

#### 3.4.1 Ditch Realignment

Under existing conditions, the ditch running north-south, located towards the eastern end of the site (reach "F3"), receives drainage from an adjacent property to the south. To accommodate the proposed stormwater management facility, the ditch has been realigned around the boundary of the SWM facility, and maintain the existing outlet at the 1350mm culvert crossing under the Highway 417.

**Table 3.1** outlines the existing and proposed ditch parameters. Supporting calculations are provided in **Appendix D**, and details of the location of the ditch relocation have been provided on the Ditch Relocation Plan (117217-DR).

Table 3.1: Existing vs. Proposed Ditch Parameters

Parameter	<b>Existing Ditch</b>	Proposed Ditch
Bankfull Depth (m)	1.4	1.3 - 1.5
Bankfull Width (m)	6.0	5.7 - 6.5
Longitudinal Slope (%)	0.10%	0.10%
Side Slopes (H:V)	2:1	2:1
Capacity (m3/s)	2.9	2.7 - 3.8

As shown, the relocated ditch will provide sufficient capacity to convey the runoff from the upstream areas.

#### 4.0 HYDROLOGIC & HYDRAULIC MODELING

The City of Ottawa Sewer Design Guidelines requires hydrologic modelling for all dual drainage systems. The performance of the proposed storm drainage system was evaluated using the PCSWMM hydrologic/ hydraulic model.

#### 4.1 Deign Storms

The hydrologic & hydraulic analysis was completed using the following synthetic design storms and historical storms. The IDF parameters used to generate the design storms were taken from the *Ottawa Sewer Design Guidelines* (October, 2012).

4-Hour Chicago Storms:	12-Hour SCS Type II Storms:
25mm 4-hour Chicago Storm 2-year 4-hour Chicago Storm 5-year 4-hour Chicago Storm 100-year 4-hour Chicago Storm	2-year 12-hour SCS Type II Storm 5-year 12-hour SCS Type II Storm 100-year 12-hour SCS Type II Storm

The proposed drainage system has also been stress tested using a 4-hour Chicago design storm that has a 20% higher intensity and total volume compared to the 100-year event.

#### 4.2 Model Development

The PCSWMM model has been developed to account for both minor and major system flows, including the routing of flows through the storm sewer network (minor system), and overland along the parking lots and through the proposed ditch network throughout the property. The results of the analysis were used to:

- Calculate the storm sewer gradeline for the 100-year storm event:
- Estimate overland flow depths and ponding volumes in the parking areas and ditch network during the 100-year event;
- Size the stormwater management facility; and
- Determine the total major and minor system runoff from the site.

#### 4.2.1 Storm Drainage Areas

The site has been divided into subcatchments for both pre and post-development conditions. Predevelopment drainage areas have been based on the existing conditions, topography, and overland flow paths. Post-development drainage areas have been based on the proposed storm drainage system. The catchment areas are shown on the following drawings:

Pre-Development Storm Drainage Area Plan
 Post-Development Storm Drainage Area Plan
 117217-POST

#### 4.2.2 Subcatchment Model Parameters

Hydrologic modeling parameters for each subcatchment area were developed based on soil type, existing and proposed land use, and topography. Modeling parameters were determined as follows:

• Soil types were identified based on test pit data from the geotechnical investigation (Paterson Group, 2015);

- Land use and ground cover were determined from satellite imagery (Figure 2);
- For pre-development conditions, SCS Curve Numbers (CN) and Initial Abstraction (IA) values were assigned for each subcatchment area based on the soil type and land use;
  - Pre-development conditions were modeled in PCSWMM using the 'Alternative Runoff Method' Nash IUH runoff method;
- For post-development conditions, the percentage of impervious area was determined for each subcatchment based on the proposed road cross-section and proposed land use;
  - Post-development conditions are modeled in PCSWMM using the SWMM5 engine.

An overview of the model parameters is provided in **Table 4.1** and **Table 4.2**. Supporting calculations are provided in **Appendix B**.

**Table 4.1: Pre-Development Model Parameters** 

Area ID	Area (ha)	Weighted CN	Weighted IA	Time to Peak (hrs)	Average Slope (%)
PreA	22.79	56	9	0.50	0.46%
PreB	4.12	71	5	0.35	0.14%
PreC	12.06	55	10	0.28	0.43%

**Table 4.2: Post-Development Model Parameters** 

Area ID	Catchment Area	Runoff Coefficient	Percent Impervious	No Depression	Equivalent Width	Average Slope
	(ha)	(c)	(%)	(%)	(m)	(%)
A-01	3.706	0.59	56%	0%	350	1%
A-02	1.519	0.69	70%	0%	150	1%
A-03	2.220	0.75	78%	0%	230	1%
B-01	2.234	0.51	44%	0%	180	1%
B-02	0.881	0.70	72%	0%	100	1%
B-03	0.793	0.77	82%	0%	85	1%
B-04	2.458	0.80	86%	0%	300	1%
B-05	3.002	0.56	51%	0%	150	1%
B-06	3.827	0.30	14%	0%	300	1%
R-01	1.300	0.90	100%	100%	87	2%
R-02	0.722	0.90	100%	100%	87	2%
R-03	0.720	0.90	100%	100%	87	2%
R-04	0.983	0.90	100%	100%	87	2%
R-05	1.027	0.90	100%	100%	87	2%
R-06	1.300	0.90	100%	100%	87	2%
R-07	0.706	0.90	100%	100%	87	2%
R-08	0.731	0.90	100%	100%	87	2%
R-09	0.978	0.90	100%	100%	87	2%
R-10	1.037	0.90	100%	100%	87	2%
POND	8.828	0.45	36%	0%	250	0%

#### Infiltration

Infiltration losses for all catchment areas were modeled using Horton's infiltration equation, which defines the infiltration capacity of the soil over the duration of a precipitation event using a decay function that ranges from an initial maximum infiltration rate to a minimum rate as the storm progresses. The default values for the City of Ottawa were used for all catchments.

Horton's Equation: Initial infiltration rate:  $f_o = 76.2$  mm/hr  $f(t) = f_c + (f_o - f_c)e^{-k(t)}$  Final infiltration rate:  $f_c = 13.2$  mm/hr Decay Coefficient: k = 4.14/hr

#### Depression Storage

The default values for depression storage in the City of Ottawa were used for all catchments. Residential rooftops were assumed to provide no depression storage.

Depression Storage (pervious areas): 4.67 mm
Depression Storage (impervious areas): 1.57 mm

#### Impervious Values

Impervious (TIMP) values for each subcatchment area were calculated based on the concept plan (Figure 2). The impervious values correspond to the Runoff Coefficients used in the Rational Method calculations using the equation:

$$C = 0.90(\%IMP) + 0.20(1-\%IMP)$$

#### 4.2.3 Roof Drains

Runoff from the roof of the building will be captured by a series of roof drains along the perimeter of the building and conveyed to the proposed storm sewers. The model accounts for the capture rate of the roof drains on a per-catchment basis. Each roof drain has a capture rate of approximately 73 L/s, and the release rate from each of the roof drain outlets in the model has been calculated based on the number of roof drains within each roof catchment area – refer to **Table 4.3**. Flows which exceed the capacity of the roof drain will overflow through scuppers (represented as weirs in the model) and will be directed across the parking area to the proposed ditches.

Table 4.3: Roof Drain Capture Rates (L/s)

Catchment ID	Number of Roof Drains	Allowable Release Rate (L/s)
R-01	5	365
R-02	2	146
R-03	3	219
R-04	4	292
R-05	3	219
R-06	5	365
R-07	2	146
R-08	3	219
R-09	4	292
R-10	3	219

#### 4.3 Model Results

The results of the analysis are summarized as follows. Supporting calculations have been provided in **Appendix B** and **C**, and PCSWMM model files have been provided on the enclosed CD at the back of this report.

#### 4.3.1 Peak Flows

Pre- vs. Post-development peak flows are outlined in **Table 4.4**. The proposed SWM facility provides sufficient storage to attenuate post-development peak flows to pre-development levels for all storms up to and including the 100-year event.

Table 4.4: Pre- vs. Post-Development Peak Flows (L/s)

Storm Distribution->		4	hr Chicaç	12hr SCS				
Return Period->	25mm	2yr	5yr	100yr	100yr+ 20%	2yr	2yr 5yr	
Pre-Development	64	162	347	1133	1637	234	457	1316
Post-Development	15	93	286	1089	1399	127	338	1127

For all storm events, the post-development peak flow is below the pre-development levels. As such, pond outflows should not have a noticeable impact on the downstream watercourse or MTO culvert.

As noted in **Section 3.4**, the outlet for the site is a 1350mm culvert which crosses Highway 417. The culvert has an approximate slope of 0.10%, which gives it a maximum capacity of approximately 1,760 L/s. Outflow from the pond for all storms up to and including the 100-year event will not exceed the available capacity of the MTO culvert. At most, the culvert will be flowing 83% full during the 100-year+20% storm event.

#### 4.3.2 Storm Sewers (Minor System)

The storm sewers have been sized to convey the 5-year peak flows from the roof drains for the proposed warehouse facility. As this is a private site and the proposed warehouse facility is to consist of slab-on-grade construction, there is no requirement to maintain a 0.30m buffer between the 100-year HGL and the USF elevation. HGL elevations during the 100-year events (both Chicago and SCS Type II) are outlined in **Table 4.5**:

Table 4.5: 100-yeah HGL Elevations in Manholes

	МН	T/G	HGL EI	evation	T/G Cle	earance
Manhole ID	Invert Elevation	Elevation	Chicago 100yr 4hr	SCS 100yr 12hr	Chicago 100yr 4hr	SCS 100yr 12hr
	(m)	(m)	(m)	(m)	(m)	(m)
STM101	74.85	76.42	75.54	75.41	0.88	1.01
STM103	74.76	76.42	75.46	75.36	0.96	1.06
STM105	74.67	76.35	75.29	75.28	1.06	1.07
STM107	74.55	76.42	75.27	75.28	1.15	1.14
STM109	74.42	76.42	75.27	75.27	1.15	1.15
STM111	74.85	76.41	75.55	75.42	0.86	0.99
STM113	74.76	76.38	75.47	75.37	0.91	1.01
STM115	74.67	76.41	75.30	75.28	1.11	1.13
STM117	74.55	76.30	75.27	75.27	1.03	1.03
STM119	74.42	76.17	75.27	75.27	0.90	0.90

#### 4.3.3 Ditch Network (Overland Flow Path)

The ditch network throughout the site has been designed to store and convey runoff from the parking and grassed areas surrounding the warehouse facility. As described in the above section, flows which overflow from the roof drains through the scuppers will be directed across the parking areas and into the ditch system. During larger storm events, the ditches will overflow into the outer edges of the parking areas. The flow depth over the parking lot will be less than 0.30 m and will not encroach on the building perimeter.

Ditches vary in size from a triangular ditch with a depth of 0.30m, and trapezoidal ditches with depths ranging from 0.20 m to 0.45 m deep, bottom widths of 1.0 m to 4.0 m, all with side slopes of 3:1 (H:V). Refer to the Grading Plans for further details (117217-GR, GR1-4)

#### 5.0 STORMWATER MANAGEMENT FACILITY

The proposed SWM facility has been sized to provide water quality and quantity control for a total tributary drainage area of 38.9 ha. The design of the SWM facility is shown on the following drawings (**Appendix D**):

- Stormwater Management Facility Plan 117217-SWMF1
- Stormwater Management Facility Sections 117217-SWMF2
- Stormwater Management Facility Details 117217-SWMF3

Supporting calculations for the stormwater management facility are provided in **Appendix C**.

#### 5.1 Design Criteria

The proposed SWM facility has been designed to meet the following criteria:

- Provide an Enhanced level of water quality control (80% long-term TSS removal):
- Provide quantity control storage to limit post-development peak flows to pre-development levels;
- The SWM facility will have side slopes of 3:1 (H:V) or shallower;
- The forebays have been sized to provide sufficient storage for 10 years of sediment accumulation;
- A sediment management area has been provided within the SWM block to allow for storage and drying of material removed during maintenance/ cleanout;
- Guardrails conforming to City standards will be installed at the inlet and outlet structures
  of the SWM facility;
- Infiltration tests are to be performed on the native material during constriction to determine whether a liner will be required.

#### 5.2 Pathways/ SWM Facility Access

Access to the inlet and outlet structures and the sediment storage area will be provided by pathways. The pathways will provide access from the north and south parking lots to both inlet structures, forebays, and the outlet structure. Details of the pathway are shown on **117217-SWMF3**.

#### 5.3 Pond Inlet Structures

The inlets to the SWM facility will consist of 864mm x 1346mm storm sewers outletting to each of the north and south forebays via a concrete headwall. The ditch network to the north and south of the warehouse facility will also outlet directly to the north and south forebays. For both inlets, riprap will be placed around the inlet slightly above the normal water level to prevent erosion as per City of Ottawa specifications/ standards. For further details, refer to Drawing 117217-SWMF3.

#### 5.4 Sediment Forebays & Permanent Pool

The sediment forebays have been sized in accordance with the MOE SWM Planning and Design Manual (March 2003). The forebays will both be approximately 40m long and 15m wide. A submerged riprap berm set at 0.30m below the normal water level will separate the forebay from the main cell of the pond. The forebay berm will be constructed from 300mm riprap, with side slopes of 2:1 and a top width of 2.0 m.

The upstream drainage area to the SWM Facility (38.9 ha) has an average imperviousness of 62%. For an *Enhanced* level of protection (80% long-term TSS removal), the required permanent pool volume is approximately 6200 m³. The proposed SWM facility will have a permanent pool volume of approximately 7700 m³.

Annual sediment loading to the SWM facility from the upstream drainage area has been estimated at approximately 53 m<sup>3</sup>/yr to the north forebay and 50 m<sup>3</sup>/yr to the south forebay (see pond design calculations in **Appendix C**). If the SWM facility provides a long-term TSS removal rate of 80%, then sediment accumulation can be estimated at  $0.80 \times 53 = 42.4 \text{ m}^3/\text{yr}$  for the north forebay and at  $0.80 \times 50 = 40 \text{ m}^3/\text{yr}$  for the south forebay.

Each forebay has been designed to allow for a minimum of 10 years of sediment accumulation. At a sediment loading rate of 425 m³/yr, this corresponds to a sediment volume of 402 m³ over a period of 10 years. The north forebay provides a storage volume of approximately 755 m³ at a depth of 1.5 m, and has a total volume of approximately 656 m³ at the top of the submerged berm between the forebay and the main cell, at a depth of 1.2 m. The south forebay provides a storage volume of approximately 785 m³ at a depth of 1.5 m, and has a total volume of approximately 689 m³ at the top of the submerged berm between the forebay and the main cell, at a depth of 1.2 m.

#### 5.5 SWM Facility Outlet Structure

Outflows from the SWM facility will be directed to an extension of an existing ditch, and then through the 1350mm culvert crossing under Highway 417. Details of the outlet structures are provided on Drawing 117217-SWMF3. Supporting calculations have been provided in Appendix C.

#### 5.5.1 Extended Detention

Extended detention will be provided for the first 1,600 m³ of active storage to allow for settling of suspended sediment in the pond. Extended detention outflows will be conveyed to the outlet structure via a 250mm reverse slope pipe with an invert of 73.35 m at the bottom of the SWM facility permanent pool, sloping upwards at 12% to an invert of 74.85 m (normal water level) at the connection to the outlet structure. The extended detention volume will be released over a period of 24 hours through a 165mm slide-in orifice plate installed at the upstream end of the 250mm pipe outletting to the proposed ditch from the outlet structure.

#### 5.5.2 Quantity Control & Overflow Spillway

Flows that exceed the extended detention storage will outlet through a 4.15 m wide by 0.28 m tall concrete weir located to the north-east of the extended detention outlet structure. This outlet structure will control peak flows for all storm events, up to and including the 100-year storm event. As the outlet for the SWM facility consists of a large weir spilling into a ditch, a separate overflow spillway has not been proposed. During extreme storm events (100-year+20%) flow depth over the crest of the weir will be 0.36 m, or 0.08 m above the 100-year water level and the top of the weir structure.

#### 5.6 Stage-Storage-Discharge Table

The stage-storage curve for the proposed SWM facility is provided in **Table 5.1**. Supporting calculations are provided in **Appendix C**.

**Table 5.1: Stage-Storage-Discharge Table** 

			Vol	ume		Outflow	
Stage	Elevation (m)	Area (m)	Stage (m3)	Total (m3)	Orifice (L/s)	Weir (L/s)	Total (L/s)
Pond Bottom	73.35	4526	0	0	0		
	74.00	5108	1249	3129	0	0	0
	74.50	5571	1364	5799	0	0	0
Permanent Pool	74.85	8146	795	8259	0	0	0
Extended Detention	75.00	27946	2707	10966	15	0	15
2-year	75.07	28113	1962	12928	22	141	163
5-year	75.13	28256	1691	14620	26	358	384
100-year	75.28	28592	4264	18883	35	1131	1166
Top of Pond	75.58	29740	8750	27633	47	3373	3420

#### 6.0 EROSION AND SEDIMENT CONTROL

#### 6.1 Temporary Measures

The following erosion and sediment control measures will be implemented during construction and are as follows:

- Silt fences are to be installed along the perimeter of the site;
- Straw bales are to be installed in ditches and swales until construction is completed and until vegetation is established;

It is proposed that the SWM facility be used as a temporary sediment control pond during construction. The construction of the temporary sediment pond would include the following:

- Excavate and shape the ultimate pond footprint, including the sediment forebays;
- Construct temporary drainage ditches to convey storm runoff to the pond;
- Construct temporary berms to isolate the areas near the ultimate inlets and outlets;
- Install silt curtains in the forebays to provide additional sediment control during construction;
- Construct the outlet to the 1350mm culvert crossing Highway 417;
- Once the ultimate stormwater management facility has been approved, construct the ultimate inlets and remove the berm protecting the ultimate outlet.

Details and specific locations will be specified during the detailed design stage. The temporary erosion and sediment control measures are to be implemented prior to construction and are to remain in place throughout construction and should be inspected regularly.

#### **6.2** Permanent Measures

Permanent erosion and sediment control measures are to include the following:

- Swales and ditches are to be constructed at minimum grade, where possible;
- Swales and ditches are to be vegetated to provide permanent erosion and sediment control.

The proposed temporary erosion and sediment control measures shall be implemented prior to construction, shall remain in place throughout each phase of construction and shall be inspected regularly. No control measure shall be permanently removed without prior authorization from the Engineer.

#### 7.0 CONCLUSIONS AND RECOMMENDATIONS

- The proposed development will consist of a single large distribution warehouse, distribution trucking lot, staff parking facility, and associated amenity spaces.
- The proposed development will be graded to direct stormwater runoff towards a proposed water quality and quantity wet pond which will ultimately discharge to an existing culvert crossing Highway 417.
- On-site stormwater quantity control will be provided by a wet pond equipped with a controlled outlet structure and an approximate pond volume of 21,706 m³, including the permanent pool, which will be required in order to maintain pre-development flow rates for all storms up to and including the 1:100 year event prior to being discharged to the Highway 417 culvert.
- An Enhanced level of stormwater quality control corresponding to a long-term removal rate of 80% Total Suspended Solids (TSS) will be provided by the proposed wet pond.
- Erosion and sediment controls will be provided both during construction and on a permanent basis.

#### **NOVATECH**

#### Prepared By:



Kallie Auld, P. Eng.
Project Coordinator | Water Resources

#### **Reviewed By:**



Michael Petepiece, P.Eng.

Project Manager | Water Resources

#### **Reviewed By:**

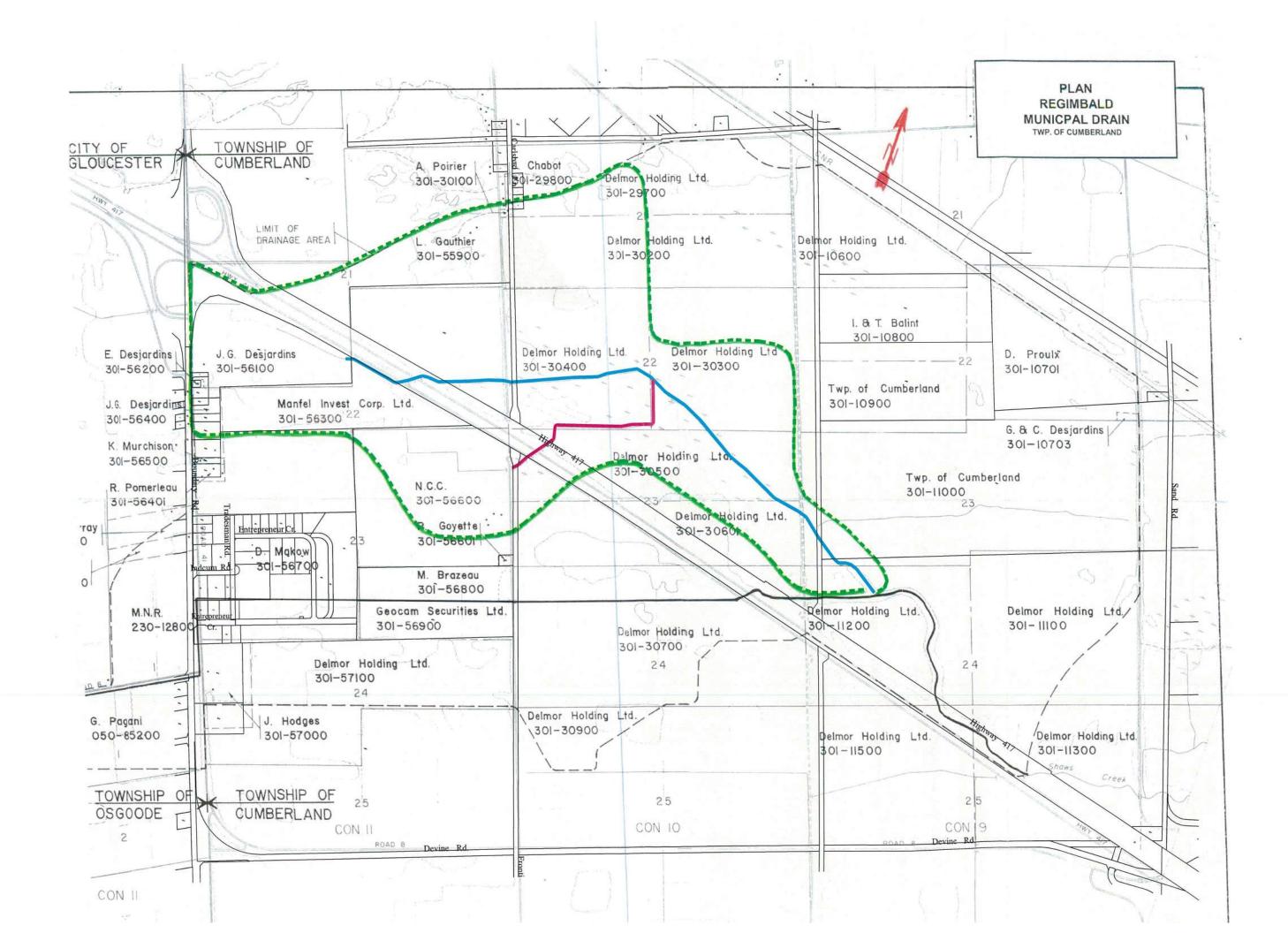


J. Lee Sheets, C.E.T.

Director | Land Development & Public Sector

## **APPENDIX A**

Regimbald Municipal Drain Assessment



## **APPENDIX B**

SWM Modeling Calculations & Files

## 5371 Boundary Road Distribution Centre Pre-Development Model Parameters



#### **Time to Peak Calculations**

(Uplands Overland Flow Method)

### **Existing Conditions**

			Overland	l Flow					Concentrate	d Overland Flo	w				Overall		
Area	Longth	Elevation	Elevation	Slope	Velocity	Travel	Length	Elevation	Elevation	Slope	Velocity	Travel	Time of	Time to	Time to	Time to	Average
ID	Length	U/S	D/S	Slope	Velocity	Time	Lengui	U/S	D/S	Slope	velocity	Time	Concentration	Peak	Peak	Peak	Slope
	(m)	(m)	(m)	(%)	(m/s)	(min)	(m)	(m)	(m)	(%)	(m/s)	(min)	(min)	(min)	(min)	(hrs)	(%)
PreA	100	77.98	76.58	1.4%	0.10	16.67	335	76.58	76.00	0.2%	0.2	27.92	45	30	30	0.50	0.46%
PreB	100	77.23	76.65	0.6%	0.10	16.67	263	76.50	76.57	0.0%	0.3	14.61	31	21	21	0.35	0.14%
PreC	100	76.39	76.02	0.4%	0.25	6.67	219	76.02	75.0	0.5%	0.2	18.25	25	17	17	0.28	0.43%

### **Weighted Curve Number Calculations**

Soil type 'B'

Area ID	Land Use 1	Area	CN	Land Use 2	Area	CN	Weighted CN
PreA	Open Space (good)	65%	61	Forest (good)	30%	55	56
PreB	Open Space (fair)	90%	69	Gravel	10%	85	71
PreC	Forest	100%	55	-	0%	0	55

### Weighted IA Calculations

Area ID	Land Use 1	Area	IA	Land Use 2	Area	IA	Weighted IA
PreA	Open Field (fair)	70%	8	Forest (good)	30%	10	9
PreB	Open Space (fair)	90%	8	Gravel/ Road	10%	85	5
PreC	Forest	100%	10	-	0%	0	10

# **5371 Boundary Road Distribution Centre Post-Development Model Parameters**



Area ID	Catchment Area	Runoff Coefficient	Percent Impervious	No Depression	Equivalent Width	Average Slope
	(ha)	(c)	(%)	(%)	(m)	(%)
A-01	3.71	0.59	56%	0%	350	1%
A-02	1.52	0.69	70%	0%	150	1%
A-03	2.22	0.75	78%	0%	230	1%
B-01	2.23	0.51	44%	0%	180	1%
B-02	0.88	0.70	72%	0%	100	1%
B-03	0.79	0.77	82%	0%	85	1%
B-04	2.46	0.80	86%	0%	300	1%
B-05	3.00	0.56	51%	0%	150	1%
B-06	3.83	0.30	14%	0%	300	1%
R-01	1.30	0.90	100%	100%	87	2%
R-02	0.72	0.90	100%	100%	87	2%
R-03	0.72	0.90	100%	100%	87	2%
R-04	0.98	0.90	100%	100%	87	2%
R-05	1.03	0.90	100%	100%	87	2%
R-06	1.30	0.90	100%	100%	87	2%
R-07	0.71	0.90	100%	100%	87	2%
R-08	0.73	0.90	100%	100%	87	2%
R-09	0.98	0.90	100%	100%	87	2%
R-10	1.04	0.90	100%	100%	87	2%
POND	8.83	0.45	36%	0%	250	0.1%

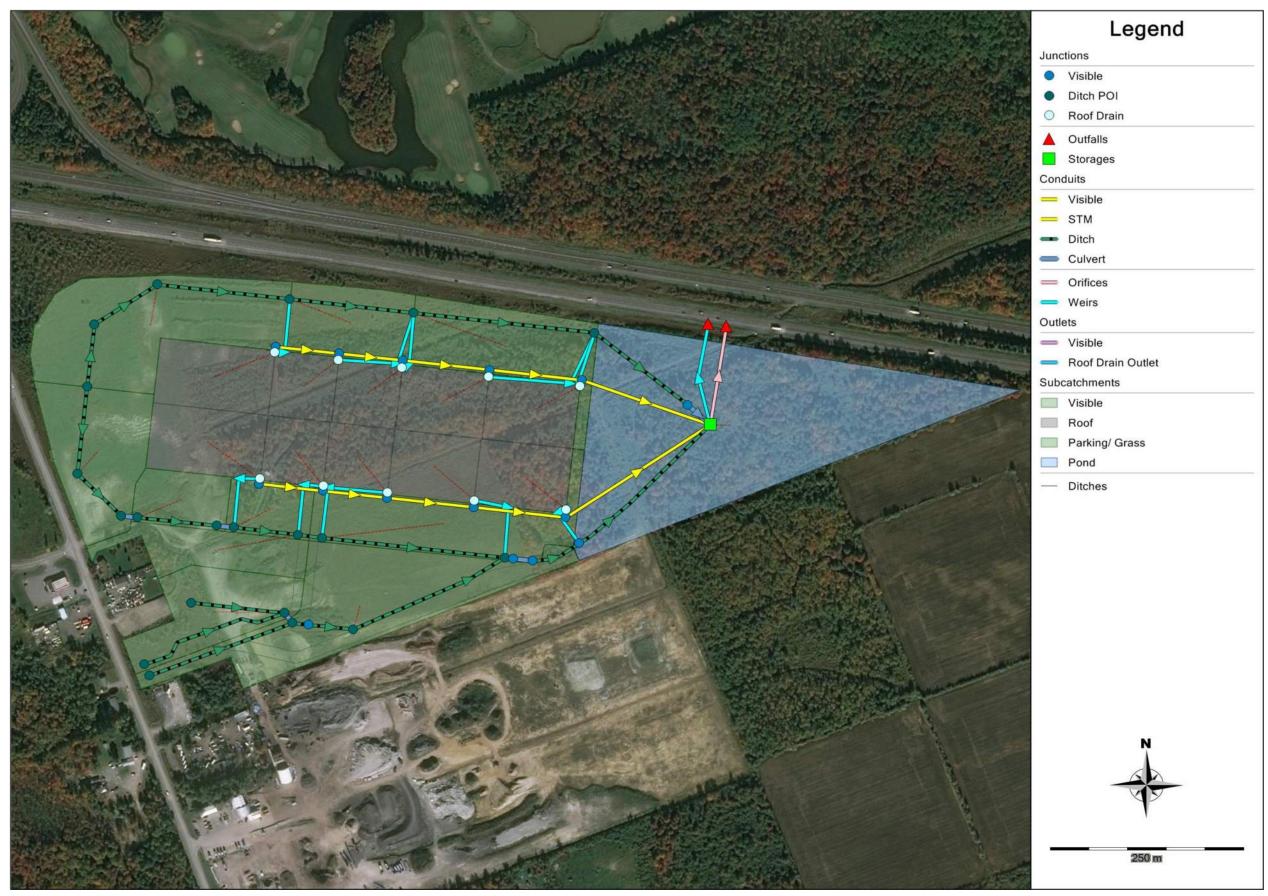
TOTAL: 38.97





# 5371 Boundary Road Distribution Centre Post-Development Model Schematic





## 5371 Boundary Road Distribution Centre Design Storm Time Series Data 4-hour Chicago Design Storms



C25mr	m-4.stm	C2-	4.stm	C5	4.stm
Duration	Intensity	Duration	Intensity	Duration	Intensity
min	mm/hr	min	mm/hr	min	mm/hr
0:00	0	0:00	0	0:00	0
0:10	1.34	0:10	1.98	0:10	2.49
0:20	1.49	0:20	2.23	0:20	2.77
0:30	1.69	0:30	2.58	0:30	3.14
0:40	1.96	0:40	3.06	0:40	3.62
0:50	2.33	0:50	3.81	0:50	4.31
1:00	2.91	1:00	5.1	1:00	5.37
1:10	3.91	1:10	7.91	1:10	7.19
1:20	6.1	1:20	19.04	1:20	11.14
1:30	14.53	1:30	76.81	1:30	26.25
1:40	58.72	1:40	23.64	1:40	104.19
1:50	17.11	1:50	11.91	1:50	30.86
2:00	8.32	2:00	7.98	2:00	15.15
2:10	5.5	2:10	6.03	2:10	10.07
2:20	4.13	2:20	4.87	2:20	7.58
2:30	3.32	2:30	4.1	2:30	6.11
2:40	2.79	2:40	3.55	2:40	5.14
2:50	2.41	2:50	3.14	2:50	4.45
3:00	2.12	3:00	2.82	3:00	3.93
3:10	1.9	3:10	2.57	3:10	3.53
3:20	1.73	3:20	2.35	3:20	3.21
3:30	1.58	3:30	2.18	3:30	2.94
3:40	1.46	3:40	2.03	3:40	2.72
3:50	1.36	3:50	1.9	3:50	2.53
4:00	1.27	4:00	1.79	4:00	2.37

## 5371 Boundary Road Distribution Centre Design Storm Time Series Data 4-hour Chicago Design Storms



0.400		0.400.4	2001
	)-4.stm		-20%.stm
Duration	Intensity	Duration	Intensity
min	mm/hr	min	mm/hr
0:00	0	0:00	0
0:10	4.07	0:10	4.88
0:20	4.54	0:20	5.45
0:30	5.14	0:40	7.14
0:40	5.95	0:50	8.51
0:50	7.09	1:00	10.62
1:00	8.85	1:10	14.28
1:10	11.9	1:20	22.25
1:20	18.54	1:30	53.03
1:30	44.19	1:40	214.27
1:40	178.56	1:50	62.45
1:50	52.04	2:00	30.37
2:00	25.31	2:10	20.08
2:10	16.73	2:20	15.07
2:20	12.56	2:30	12.11
2:30	10.09	2:40	10.16
2:40	8.47	2:50	8.78
2:50	7.32	3:00	7.75
3:00	6.46	3:10	6.95
3:10	5.79	3:20	6.3
3:20	5.25	3:30	5.78
3:30	4.82	3:40	5.34
3:40	4.45	3:50	4.97
3:50	4.14	4:00	4.66
4:00	3.88		

## 5371 Boundary Road Distribution Centre Design Storm Time Series Data SCS Design Storms



S2-1	2.stm	S5-1	2.stm	S100-	·12.stm
Duration	Intensity	Duration	Intensity	Duration	Intensity
min	mm/hr	min	mm/hr	min	mm/hr
0:00	0.00	0:00	0	0:00	0
0:30	1.27	0:30	1.69	0:30	2.82
1:00	0.59	1:00	0.79	1:00	1.31
1:30	1.10	1:30	1.46	1:30	2.44
2:00	1.10	2:00	1.46	2:00	2.44
2:30	1.44	2:30	1.91	2:30	3.19
3:00	1.27	3:00	1.69	3:00	2.82
3:30	1.69	3:30	2.25	3:30	3.76
4:00	1.69	4:00	2.25	4:00	3.76
4:30	2.29	4:30	3.03	4:30	5.07
5:00	2.88	5:00	3.82	5:00	6.39
5:30	4.57	5:30	6.07	5:30	10.14
6:00	36.24	6:00	48.08	6:00	80.38
6:30	9.23	6:30	12.25	6:30	20.47
7:00	4.06	7:00	5.39	7:00	9.01
7:30	2.71	7:30	3.59	7:30	6.01
8:00	2.37	8:00	3.15	8:00	5.26
8:30	1.86	8:30	2.47	8:30	4.13
9:00	1.95	9:00	2.58	9:00	4.32
9:30	1.27	9:30	1.69	9:30	2.82
10:00	1.02	10:00	1.35	10:00	2.25
10:30	1.44	10:30	1.91	10:30	3.19
11:00	0.93	11:00	1.24	11:00	2.07
11:30	0.85	11:30	1.12	11:30	1.88
12:00	0.85	12:00	1.12	12:00	1.88

## 5371 Boundary Road Distribution Centre Design Storm Time Series Data SCS Design Storms



S2-2	4.stm	S5-24	4.stm	S100	)-24.stm
Duration	Intensity	Duration	Intensity	Duration	n Intensity
min	mm/hr	min	mm/hr	min	mm/hr
0:00	0	0:00	0	0:00	0
1:00	0.72	1:00	0.44	1:00	0.6
2:00	0.34	2:00	0.44	2:00	0.75
3:00	0.63	3:00	0.81	3:00	1.39
4:00	0.63	4:00	0.81	4:00	1.39
5:00	0.81	5:00	1.06	5:00	1.81
6:00	0.72	6:00	0.94	6:00	1.6
7:00	0.96	7:00	1.25	7:00	2.13
8:00	0.96	8:00	1.25	8:00	2.13
9:00	1.3	9:00	1.68	9:00	2.88
10:00	1.63	10:00	2.12	10:00	3.63
11:00	2.59	11:00	3.37	11:00	5.76
12:00	20.55	12:00	26.71	12:00	45.69
13:00	5.23	13:00	6.8	13:00	11.64
14:00	2.3	14:00	2.99	14:00	5.12
15:00	1.54	15:00	2	15:00	3.42
16:00	1.34	16:00	1.75	16:00	2.99
17:00	1.06	17:00	1.37	17:00	2.35
18:00	1.11	18:00	1.44	18:00	2.46
19:00	0.72	19:00	0.94	19:00	1.6
20:00	0.58	20:00	0.75	20:00	1.28
21:00	0.81	21:00	1.06	21:00	1.81
22:00	0.53	22:00	0.68	22:00	1.17
23:00	0.48	23:00	0.63	23:00	1.07
0:00	0.48	0:00	0.63	0:00	1.07

## 5371 Boundary Road Distribution Centre Ditch Relocation Manning's Calculations - 1.3m deep

Location: Boundary Road Distribution Centre

**Description:** New Ditch - Relocation

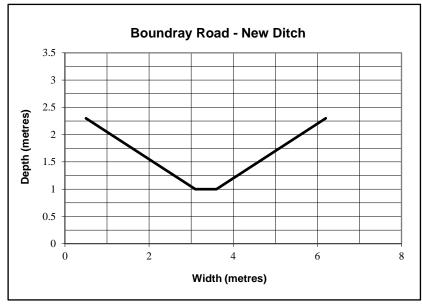
**Dimensions:** Bottom width = 0.50 m

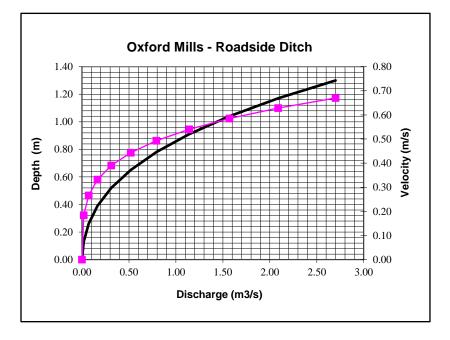
Right Side slopes = 2.0 :1 Left Side slopes = 2.0 :1

Slope = 0.10% Mannings n = 0.035 Average depth = 1.30 m

Depth	Area	Hydraulic Radius	Velocity	Flow
(m)	(m2)	(m)	(m/s)	(m3/s)
0.00	0.00	0.00	0.00	0.00
0.13	0.10	0.09	0.18	0.02
0.26	0.27	0.16	0.27	0.07
0.39	0.50	0.22	0.33	0.17
0.52	0.80	0.28	0.39	0.31
0.65	1.17	0.34	0.44	0.52
0.78	1.61	0.40	0.49	0.79
0.91	2.11	0.46	0.54	1.14
1.04	2.68	0.52	0.59	1.57
1.17	3.32	0.58	0.63	2.09
1.30	4.03	0.64	0.67	2.70







## 5371 Boundary Road Distribution Centre Ditch Relocation Manning's Calculations - 1.5m deep

Location: Boundary Road Distribution Centre

**Description:** New Ditch - Relocation

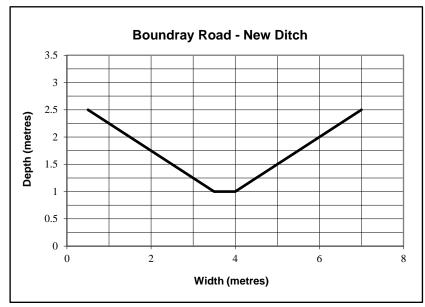
**Dimensions:** Bottom width = 0.50 m

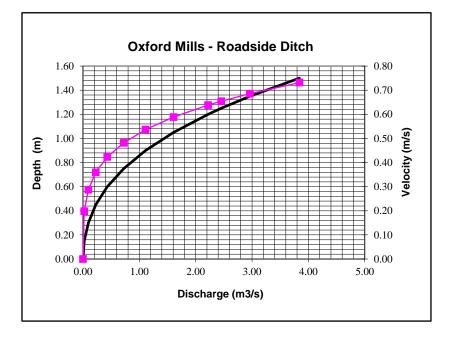
Right Side slopes = 2.0 :1 Left Side slopes = 2.0 :1

Slope = 0.10% Mannings n = 0.035 Average depth = 1.50 m

Depth	Area	Hydraulic	Velocity	Flow
(m)	(m2)	Radius (m)	(m/s)	(m3/s)
0.00	0.00	0.00	0.00	0.00
0.15	0.12	0.10	0.20	0.02
0.30	0.33	0.18	0.29	0.09
0.45	0.63	0.25	0.36	0.23
0.60	1.02	0.32	0.42	0.43
0.75	1.50	0.39	0.48	0.72
0.90	2.07	0.46	0.54	1.11
1.05	2.73	0.53	0.59	1.61
1.20	3.48	0.59	0.64	2.22
1.25	3.75	0.62	0.65	2.45
1.35	4.32	0.66	0.69	2.96
1.50	5.25	0.73	0.73	3.84







## **APPENDIX C**

SWM Facility Supporting Calculations

# **5371 Boundary Road Distribution Centre SWM Facility Design**



#### **Required Storage Volumes (Quality)**

Drainage Area	38.9	ha					
% Impervious:	62%						
Enhanced protection (80% TSS removal):							
Treatment Volume	199	m3/ha					
Extended Detention Storage:	40 1,558 1600 41.1	m3/ha required m3 required m3 provided m3/ha provided					
Perm Pool:	159 6191 7700	m3/ha required m3 required m3 provided					
•	197.7	m3/ha provided					
Extended Detention:	37.04 92.59	L/s average L/s max (2.5 x avg)					
(% impervious was calculated as the average imperviousness for the drainage areas tributary to the SWM facility)							



#### Required Forebay Length and width North Forebay:

#### Parameters:

Length to width ratio of forebay, r =5.0:1

0.093 m<sup>3</sup>/s (24hr ext. det) Peak outflow rate during 25 mm storm, Target particle size = 150 mm

Settling velocity,  $V_s =$ 0.0003 m/s

#### Forebay Settling Length, Dist

$$Dist \, \Box \sqrt{\frac{rQ_P}{V_S}}$$
= 39 m

#### Check Dispersion Length, Dist<sub>2</sub>

Desired velocity in forebay,  $V_f =$ 0.15 m/s

 $0.540 \text{ m}^3/\text{s}$ Inlet flow rate,  $Q_{5yr} =$ Depth in forebay, d =

 $= 19 \, \text{m}$ 

Therefore, the settling length of 39 m governs the design.

1.5 m

Required Length	= 39 m
Provided Length	= 40 m

#### Minimum Forebay width:

Length of Forebay, L = 39 m

5.0:1 Minimum width. W = W = 7.9 m

**Required Width** = 7.9 m**Provided Width** = 15.0 m

### Required Forebay Length and width South Forebay:

#### Parameters:

Length to width ratio of forebay, r =5.0:1

Peak outflow rate during 25 mm storm 0.093 m<sup>3</sup>/s (24hr ext. det)

Target particle size = 150 mm

Settling velocity,  $V_s =$ 0.0003 m/s

#### Forebay Settling Length, Dist

$$Dist \Box \sqrt{\frac{rQ_F}{V_S}}$$
= 39 m

#### Check Dispersion Length, Dist<sub>2</sub>

Desired velocity in forebay,  $V_f =$ 

Inlet flow rate,  $Q_{5\gamma r} =$ 

 $0.558 \text{ m}^3/\text{s}$ 1.5 m

0.15 m/s

$$Dist_2 \square \frac{8Q}{dV_f}$$

Depth in forebay, *d* =

 $= 20 \, \text{m}$ 

Therefore, the settling length of 39 m governs the design.

Required Length	= 39 m
Provided Length	= 40 m

#### Minimum Forebay width:

Length of Forebay, L =

39 m

Minimum width. W = W =

5.0:1 7.9 m

**Required Width** = 7.9 m**Provided Width** = 15.0 m



#### **SWM Facility - Outlet Calculations**

Orifice

C 0.62
Dia 165.00 mm
Area 0.0214 m²
Invert 74.85 m
C/L 74.93 m

37.04

For Elevation = 075.28 m

Q orifice =  $C x A x (2 x g x H)^{(1/2)}$ 

Q orifice =  $1000 \text{ L/m}^3 \text{ x } 0.62 \text{ x}$   $0.0214 \text{ m}^2 \text{ x } (2 \text{ x } 9.81 \text{ x } (75.28 \text{ m } -74.93 \text{ m }))$  (1/2)

Q orifice = 34.62 L/s

#### **Suppressed Rectangular Weir**

 $Q(m^3/s) = C \times L \times H^{(3/2)}$ 

Weir Coefficeint	1.84
Bottom Width (m)	4.2
Bottom of Weir Elevation (m)	75.00

Water Level Elevation	Flow Rate Ove	r Weir
(m)	(m³/s)	(L/s)
75.00	0.000	0
75.07	0.141	141
75.13	0.358	358
75.28	1.131	1131
75.58	3.373	3373

PREPARED BY: NOVATECH

28/03/2018



#### **Sediment Loading Estimate - North**

Table 6.3 - MOE SWM Planning & Design Manual

Table 6.3 - MOE SWM Flatifility & Design Marida			
Catchment Imperviousness	Annual Loading (kg/ha)	Wet Density (kg/m³)	Annual Loading (m³/ha)
	50	1,230	0.05
35%	770	1,230	0.6
55%	2,300	1,230	1.9
70%	3,495	1,230	2.8
85%	4,680	1,230	3.8

Catchment Area:	14.94 ha
% Impervious:	81%
Annual Sediment Loading:	4,371 kg/ha/yr
	3.55 m <sup>3</sup> /ha/yr
	53.1 m³/yr

Sediment Removal Efficiency:	80%
	42.48 m <sup>3</sup> /yr

Sediment Accumulation:	
10yrs	425 m³

Approx. Forebay Volume:	755	m <sup>3</sup>
@ depth:	1.20	m

(Depth to top of Forebay Berm)

655.6

#### City of Ottawa-average precipitation and TSS data

Drainage Area:	14.9	ha
Runoff Coefficient:	0.77	
Estimate Influent TSS Level (max):		mg/L
(Long-term average):		mg/L
Sediment Density:	1,230	kg/m³
Total Annual Precipitation:	907	mm
Total Annual Rain (Ice Free Period):	686	mm
Total Annual Runoff:	103,933	m³
Runoff during Ice-free period:	78,609	m³
Max Annual TSS Loading:	25,983	٠ .
(total precipitation)	21.1	m³/yr
Max Annual TSS Loading:	19,652	•
(precipitation during ice-free period)	16.0	m³/yr
Average Annual TSS Loading:	15,590	ka
-	•	•
(total precipitation)	12.7	m³/yr
Average Annual TSS Loading:	11,791	kg
(precipitation during ice-free period)		m³/yr
J. S.		,

14.8 m³/yr
,
6.7 m³/yr

Sediment Accumulation:	
10yrs	148 m³



#### **Sediment Loading Estimate - South**

Table 6.3 - MOE SWM Planning & Design Manual

Table 6.5 - MOE SWM Flamming & Design Manual						
Catchment Imperviousness	Annual Loading   Wet Density		Annual Loading (m³/ha)			
	50	1,230	0.05			
35%	770	1,230	0.6			
55%	2,300	1,230	1.9			
70%	3,495	1,230	2.8			
85%	4,680	1,230	3.8			

Catchment Area:	20.68 ha
% Impervious:	64%
Annual Sediment Loading:	2,989 kg/ha/yr
	2.43 m³/ha/yr
	50.2 m³/yr

Sediment Removal Efficiency:	80%
	40.20 m <sup>3</sup> /yr

Sediment Accumulation:	
10yrs	402 m <sup>3</sup>

Approx. Forebay Volume:	785	m <sup>3</sup>
@ depth:	1.20	m

(Depth to top of Forebay Berm)

689.4

#### City of Ottawa-average precipitation and TSS data

Drainage Area:	20.7 ha
Runoff Coefficient:	0.65
Estimate Influent TSS Level (max): (Long-term average): Sediment Density:	250 mg/L 150 mg/L 1,230 kg/m³
Total Annual Precipitation:	907 mm
Total Annual Rain (Ice Free Period):	686 mm
Total Annual Runoff:	121,544 m³
Runoff during Ice-free period:	91,928 m³
Max Annual TSS Loading:	30,386 kg
(total precipitation)	24.7 m³/yr
Max Annual TSS Loading:	22,982 kg
(precipitation during ice-free period)	18.7 m³/yr
Average Annual TSS Loading: (total precipitation)	18,232 kg 14.8 m³/yr
Average Annual TSS Loading:	13,789 kg
(precipitation during ice-free period)	11.2 m³/yr

Target 70% TSS Removal:	
Max:	17.3 m³/yr
Min:	7.8 m³/yr

Sediment Accumulation:	
10yrs	173 m <sup>3</sup>

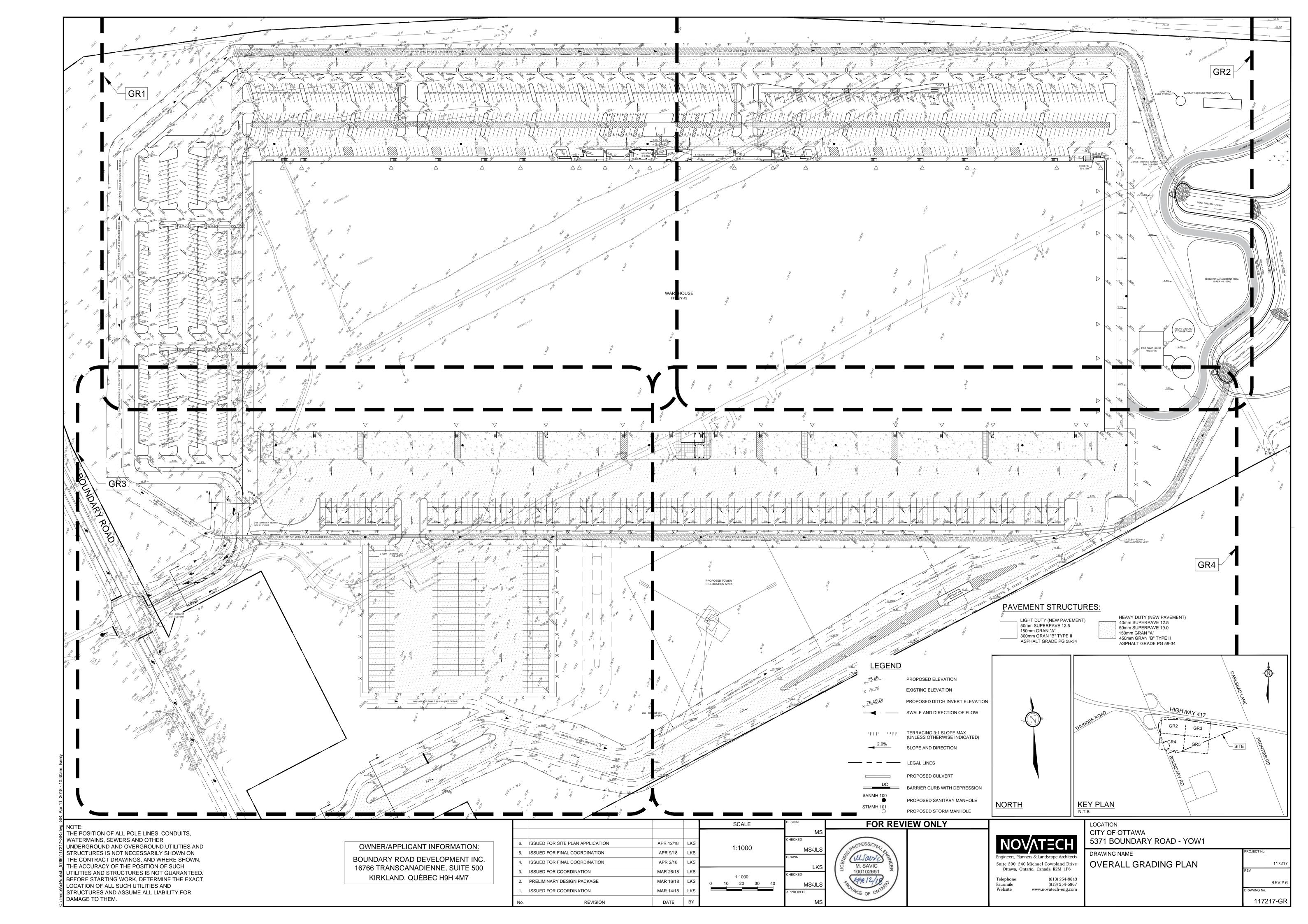


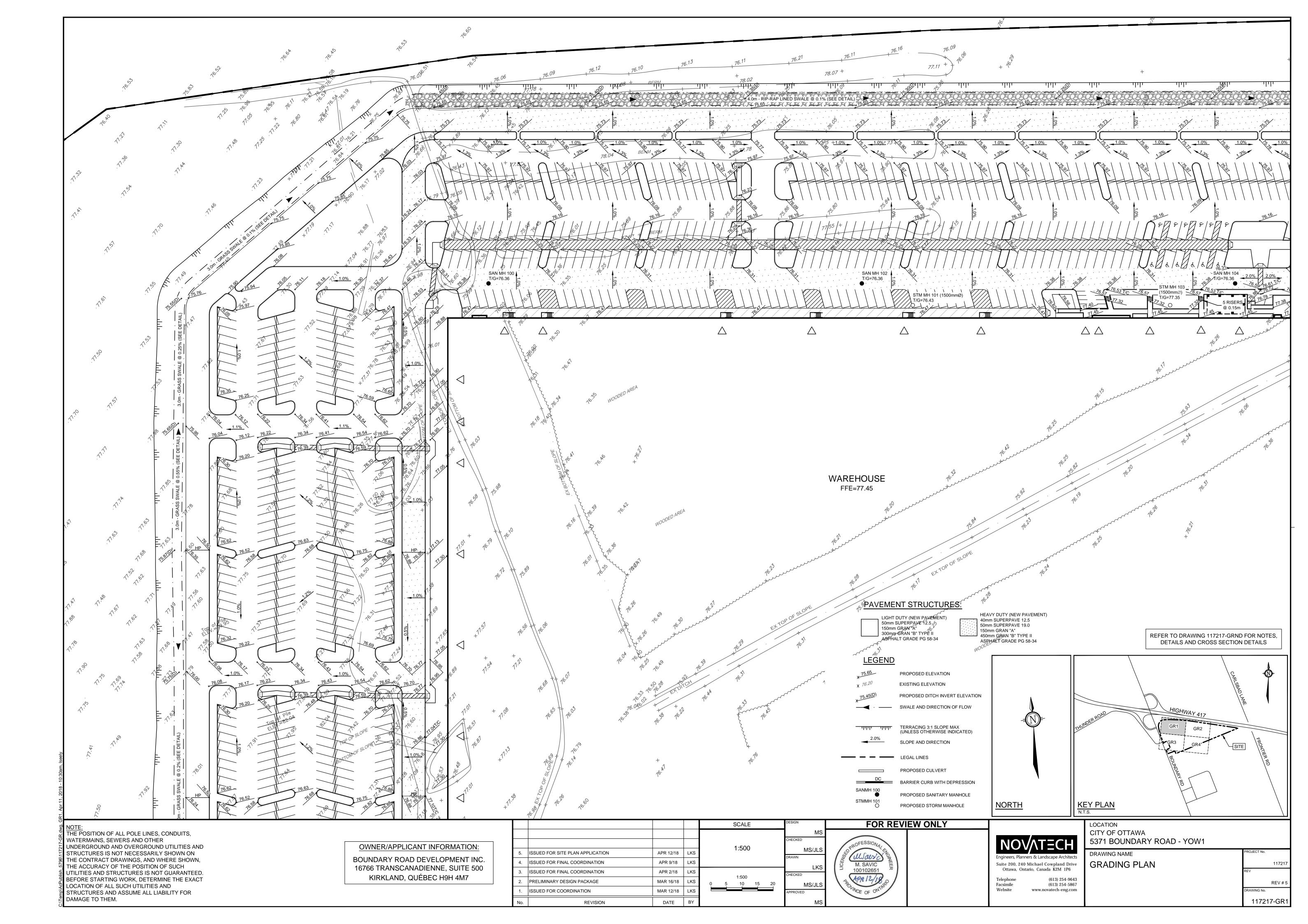
## SWM Facility - Stage-Storage

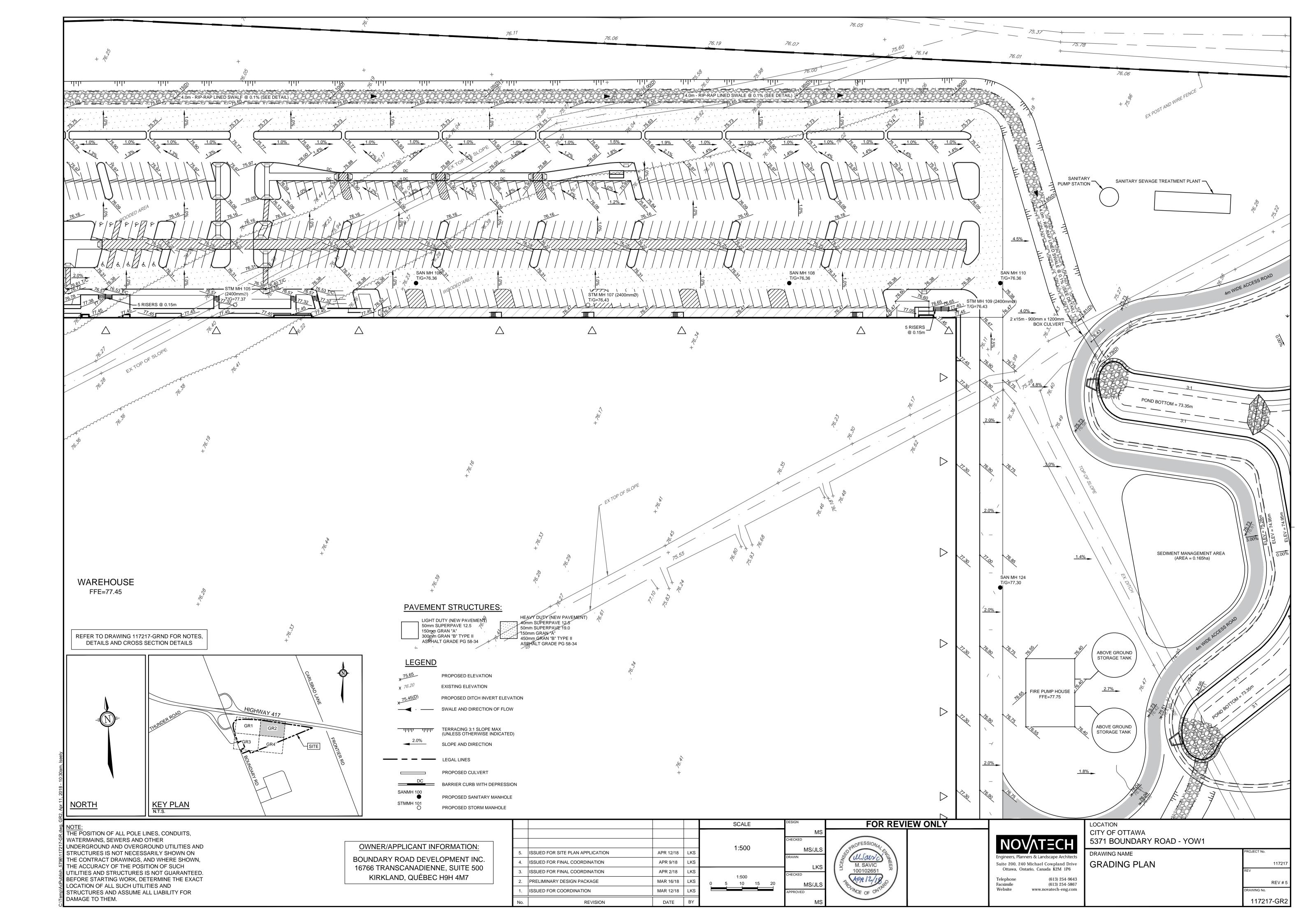
Elevatio			Vol	ıme	Outflow		
Stage	(m)	Area (m)	Stage (m3)	Total (m3)	Orifice (L/s)	Weir (L/s)	Total (L/s)
Pond Bottom	73.35	4526	0	0	0		
	74.00	5108	1249	3129	0	0	0
	74.50	5571	1364	5799	0	0	0
Permanent Pool	74.85	8146	795	8259	0	0	0
Extended Detention	75.00	27946	2707	10966	15	0	15
2-year	75.07	28113	1962	12928	22	141	163
5-year	75.13	28256	1691	14620	26	358	384
100-year	75.28	28592	4264	18883	35	1131	1166
Top of Pond	75.58	29740	8750	27633	47	3373	3420

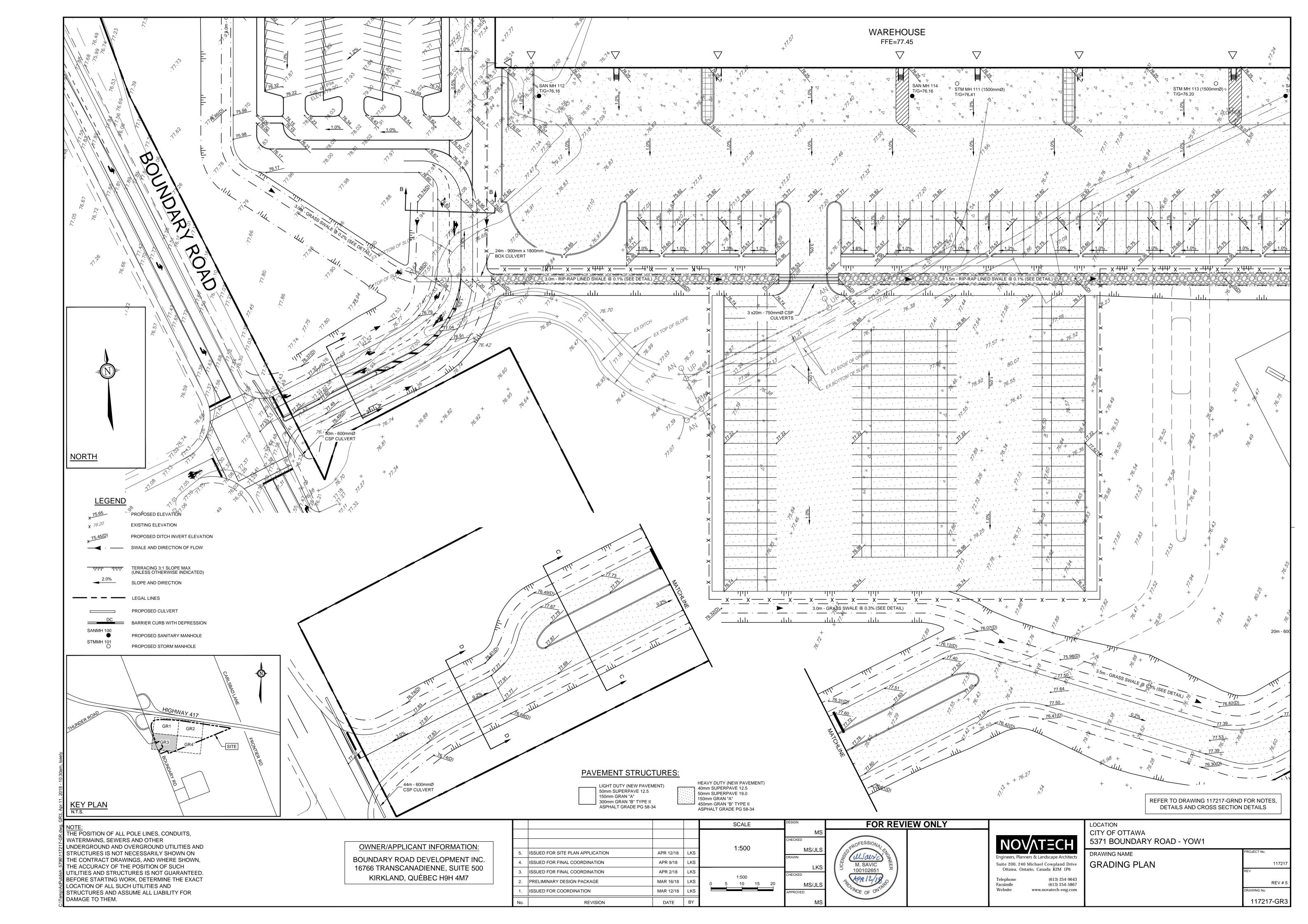
# **APPENDIX D**

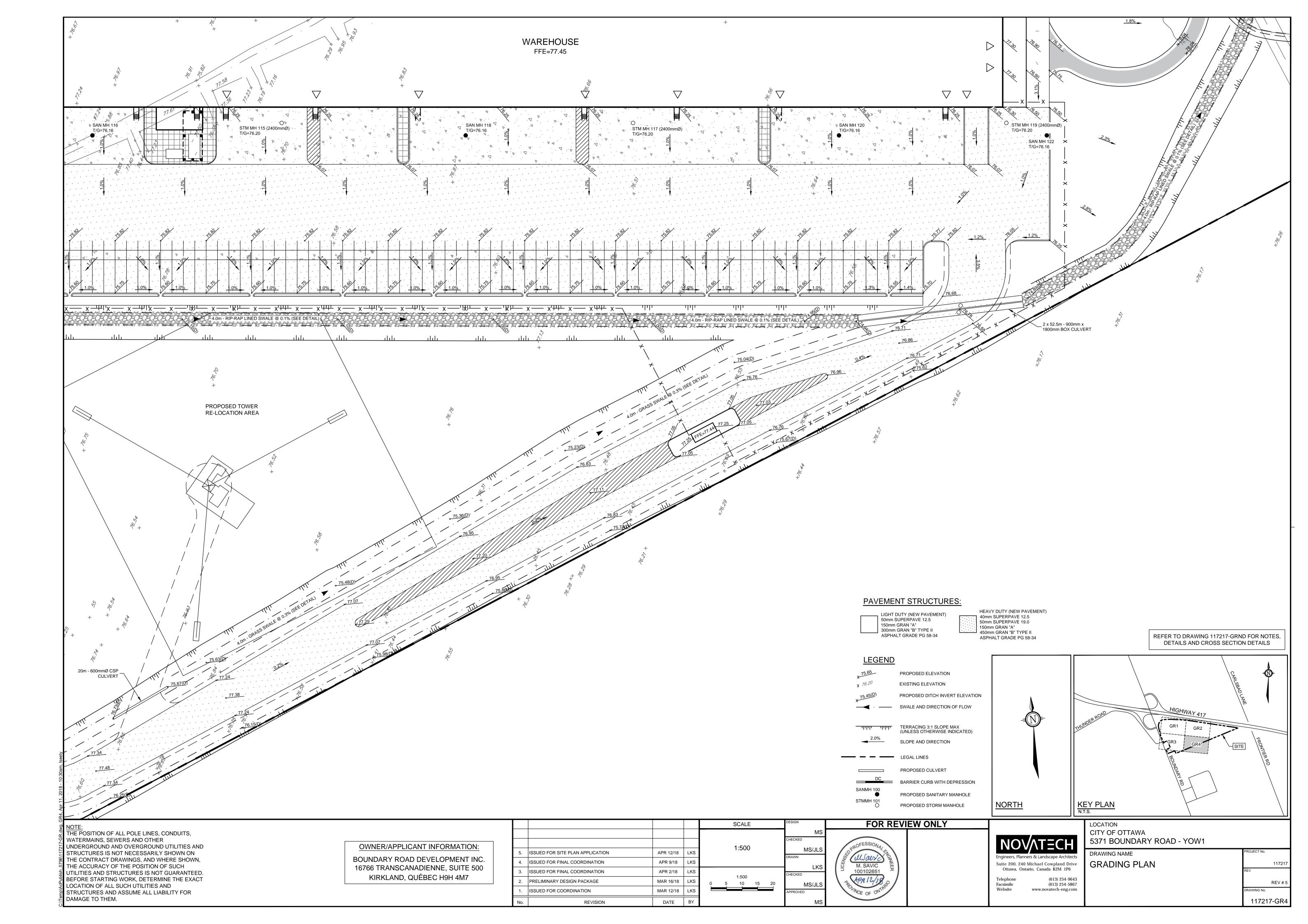
Drawings











## **GENERAL NOTES:**

- 1. COORDINATE AND SCHEDULE ALL WORK WITH OTHER TRADES AND CONTRACTORS.
- 2. DETERMINE THE EXACT LOCATION, SIZE, MATERIAL AND ELEVATION OF ALL EXISTING UTILITIES PRIOR TO COMMENCING CONSTRUCTION. PROTECT AND ASSUME RESPONSIBILITY FOR ALL EXISTING UTILITIES WHETHER OR NOT SHOWN ON THIS
- 3. OBTAIN ALL NECESSARY PERMITS AND APPROVALS FROM THE CITY OF OTTAWA BEFORE COMMENCING CONSTRUCTION.
- 4. BEFORE COMMENCING CONSTRUCTION OBTAIN AND PROVIDE PROOF OF COMPREHENSIVE, ALL RISK AND OPERATIONAL LIABILITY INSURANCE FOR \$2,000,000.00. INSURANCE POLICY TO NAME OWNERS, ENGINEERS AND ARCHITECTS AS
- 5. RESTORE ALL DISTURBED AREAS ON-SITE AND OFF-SITE, INCLUDING TRENCHES AND SURFACES ON PUBLIC ROAD ALLOWANCES TO EXISTING CONDITIONS OR BETTER TO THE SATISFACTION OF MUNICIPAL AUTHORITIES.
- 6. REMOVE FROM SITE ALL EXCESS EXCAVATED MATERIAL, ORGANIC MATERIAL AND DEBRIS UNLESS OTHERWISE INSTRUCTED BY ENGINEER. EXCAVATE AND REMOVE FROM SITE ANY CONTAMINATED MATERIAL. ALL CONTAMINATED MATERIAL SHALL BE DISPOSED OF AT A LICENSED LANDFILL FACILITY.
- 7. ALL ELEVATIONS ARE GEODETIC.
- 8. REFER TO GEOTECHNICAL INVESTIGATION REPORT NO. PG4366-1 (DATED FEBRUARY 9, 2018) PREPARED BY PATERSON GROUP INC. FOR SUBSURFACE CONDITIONS, CONSTRUCTION RECOMMENDATIONS AND GEOTECHNICAL INSPECTION REQUIREMENTS. THE GEOTECHNICAL CONSULTANT IS TO REVIEW ON-SITE CONDITIONS AFTER EXCAVATION PRIOR TO PLACEMENT OF THE GRANULAR MATERIAL.
- 9. REFER TO ARCHITECT'S AND LANDSCAPE ARCHITECT'S DRAWINGS FOR BUILDING AND HARD SURFACE AREAS AND
- 10. REFER TO THE STORMWATER MANAGEMENT REPORT (R-2018-034) PREPARED BY NOVATECH.
- 11. SAW CUT AND KEYGRIND ASPHALT AT ALL ROAD CUTS AND ASPHALT TIE IN POINTS AS PER CITY OF OTTAWA STANDARDS (R10 AND R25).

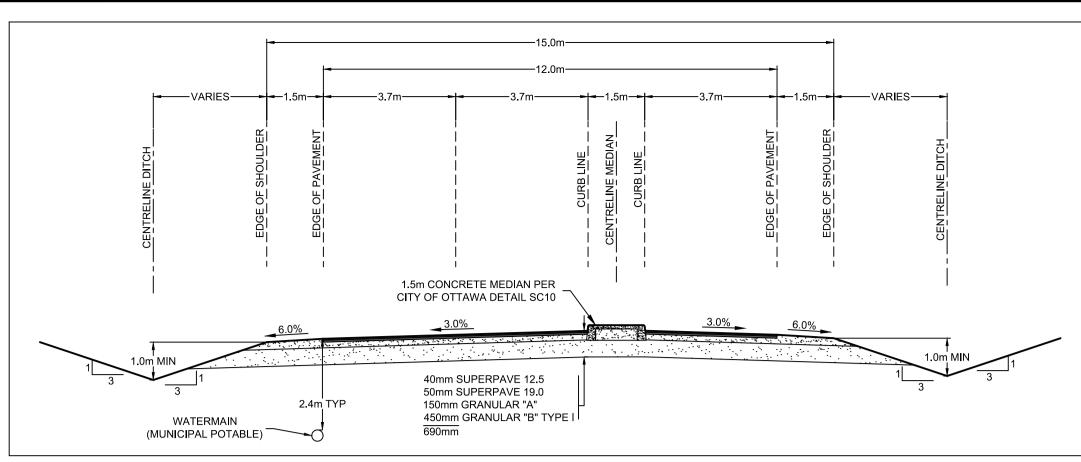
## **GRADING NOTES:**

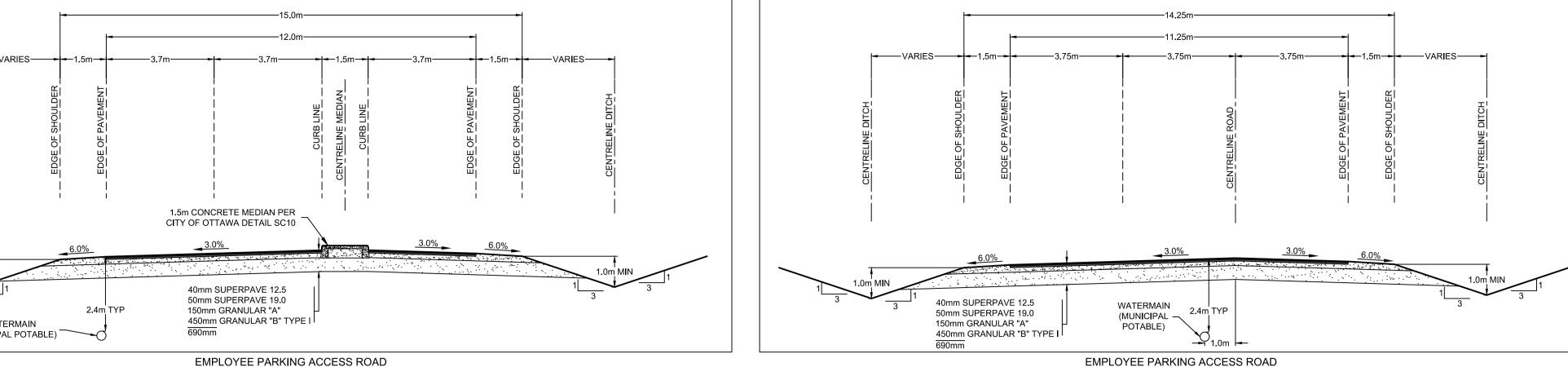
- 1. ALL TOPSOIL, ORGANIC OR DELETERIOUS MATERIAL MUST BE ENTIRELY REMOVED FROM BENEATH THE PROPOSED BUILDING AND PAVED AREAS.
- 2. EXPOSED SUBGRADES IN PROPOSED PAVED AREAS SHOULD BE PROOF ROLLED WITH A LARGE STEEL DRUM ROLLER AND ANY SOFT AREAS EVIDENT FROM THE PROOF ROLLING SHOULD BE SUBEXCAVATED AND REPLACED WITH SUITABLE MATERIAL THAT IS FROST COMPATIBLE WITH THE EXISTING SOILS.
- 3. THE PAVEMENT GRANULAR BASE AND SUBBASE SHOULD BE PLACED IN MAXIMUM 300mm THICK LIFTS AND COMPACTED TO A MINIMUM OF 98% OF THE MATERIAL'S STANDARD PROCTOR MAXIMUM DRY DENSITY VALUE.
- 4. GRADE AND/OR FILL BEHIND PROPOSED CURB AND BETWEEN BUILDINGS AND CURBS, WHERE REQUIRED TO PROVIDE POSITIVE DRAINAGE.
- 5. MINIMUM OF 2% GRADE FOR ALL GRASS AREAS UNLESS OTHERWISE NOTED.
- 6. ALL GRADES BY CURBS ARE EDGE OF PAVEMENT GRADES UNLESS OTHERWISE INDICATED.
- 7. REFER TO LANDSCAPE PLAN FOR PLANTING AND OTHER LANDSCAPE FEATURE DETAILS.
- 8. CONTRACTOR TO PROVIDE THE CONSULTANT WITH A GRADING PLAN INDICATING THE AS-BUILT ELEVATION OF EVERY DESIGN GRADE SHOWN ON THIS PLAN.

# PAVEMENT STRUCTURES:

LIGHT DUTY (NEW PAVEMENT) 50mm SUPERPAVE 12.5 150mm GRAN "A" 300mm GRAN "B" TYPE II ASPHALT GRADE PG 58-34

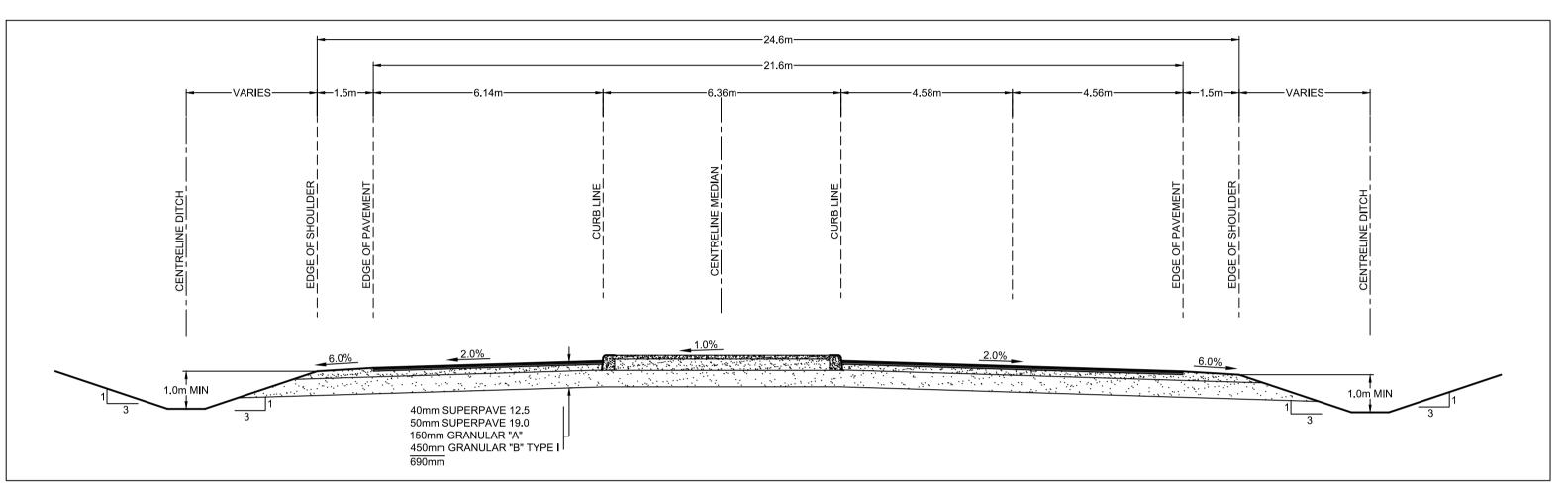
HEAVY DUTY (NEW PAVEMENT) 40mm SUPERPAVE 12.5 50mm SUPERPAVE 19.0 150mm GRAN "A" 450mm GRAN "B" TYPE II ASPHALT GRADE PG 58-34

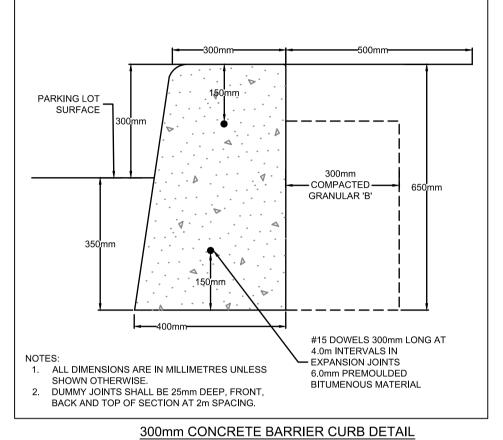




**EMPLOYEE PARKING ACCESS ROAD** (HEAVY DUTY) CROSS-SECTION A-A

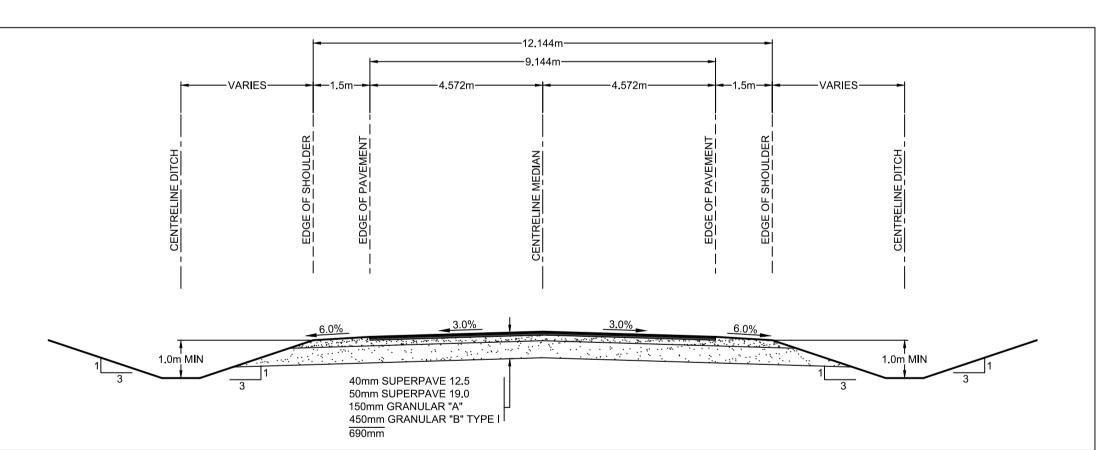
(HEAVY DUTY) CROSS-SECTION B-B



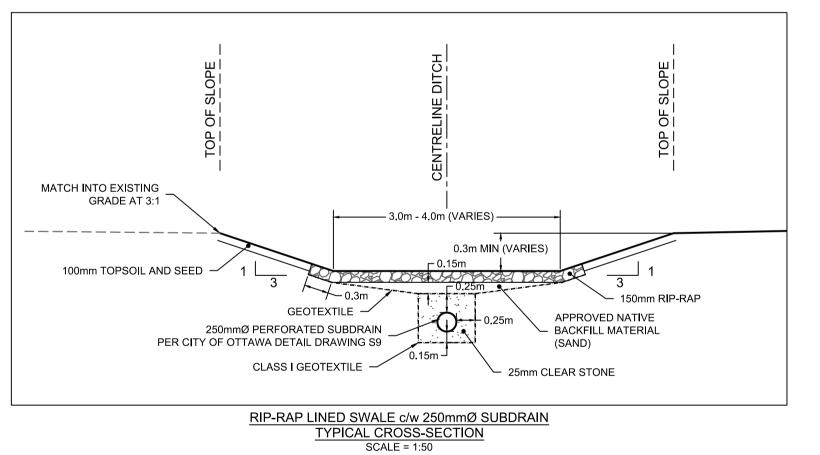


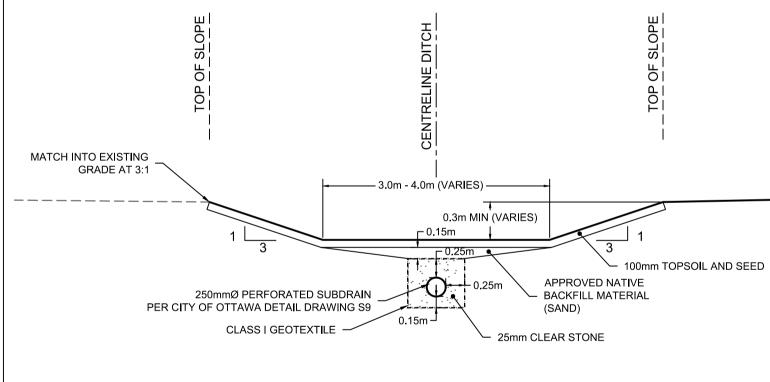
SCALE = N.T.S.

#### TRUCK PARKING ACCESS ROAD (HEAVY DUTY) CROSS-SECTION C-C

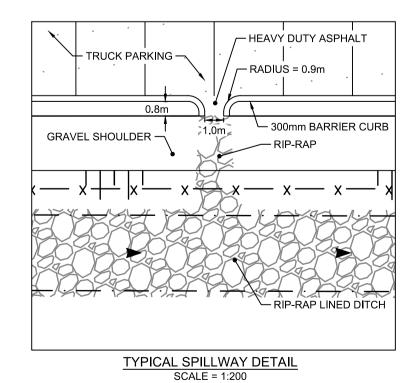


TRUCK PARKING ACCESS ROAD (HEAVY DUTY) CROSS-SECTION D-D





GRASS SWALE c/w 250mmØ SUBDRAIN
TYPICAL CROSS-SECTION
SCALE = 1:50

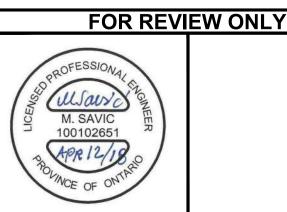


THE POSITION OF ALL POLE LINES, CONDUITS, WATERMAINS, SEWERS AND OTHER UNDERGROUND AND OVERGROUND UTILITIES AND STRUCTURES IS NOT NECESSARILY SHOWN ON THE CONTRACT DRAWINGS, AND WHERE SHOWN, THE ACCURACY OF THE POSITION OF SUCH UTILITIES AND STRUCTURES IS NOT GUARANTEED. BEFORE STARTING WORK, DETERMINE THE EXACT LOCATION OF ALL SUCH UTILITIES AND STRUCTURES AND ASSUME ALL LIABILITY FOR

DAMAGE TO THEM.

OWNER/APPLICANT INFORMATION: BOUNDARY ROAD DEVELOPMENT INC. 16766 TRANSCANADIENNE, SUITE 500 KIRKLAND, QUÉBEC H9H 4M7

				SCALE	N	
					MS	
				CHECK	KED	
				AS SHOWN	MS/JLS	
				DRAWN	N	
3.	ISSUED FOR SITE PLAN APPLICATION	APR 12/18	LKS		LKS	
	ISSUED FOR FINAL COORDINATION	APR 9/18	LKS	CHECK	KED	
					MS/JLS	
1.	ISSUED FOR FINAL COORDINATION	APR 2/18	LKS	APPRO	OVED	
No.	REVISION	DATE	BY		MS	



Suite 200, 240 Michael Cowpland Drive Ottawa, Ontario, Canada K2M 1P6 (613) 254-9643

Facsimile

Website

(613) 254-5867

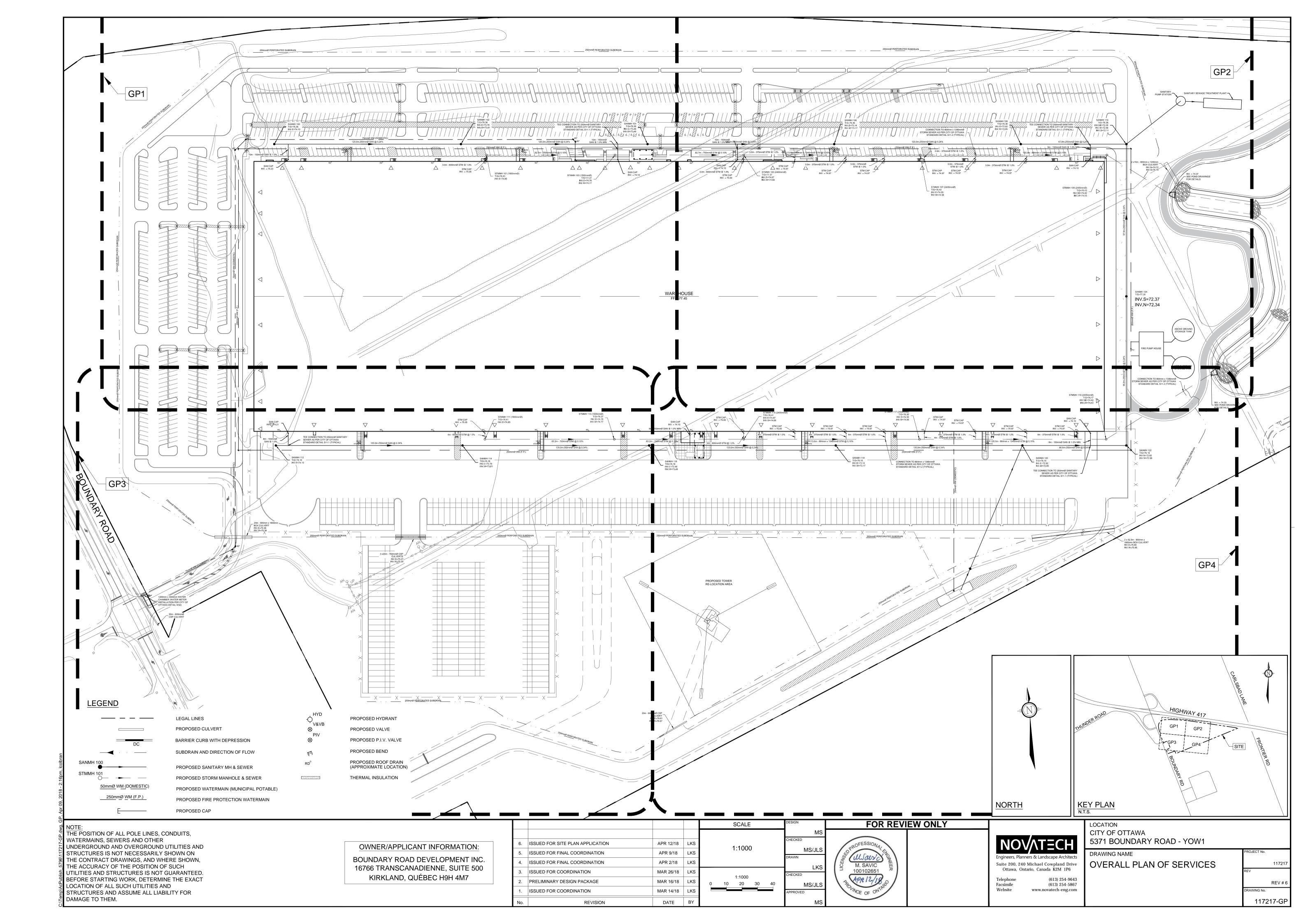
www.novatech-eng.com

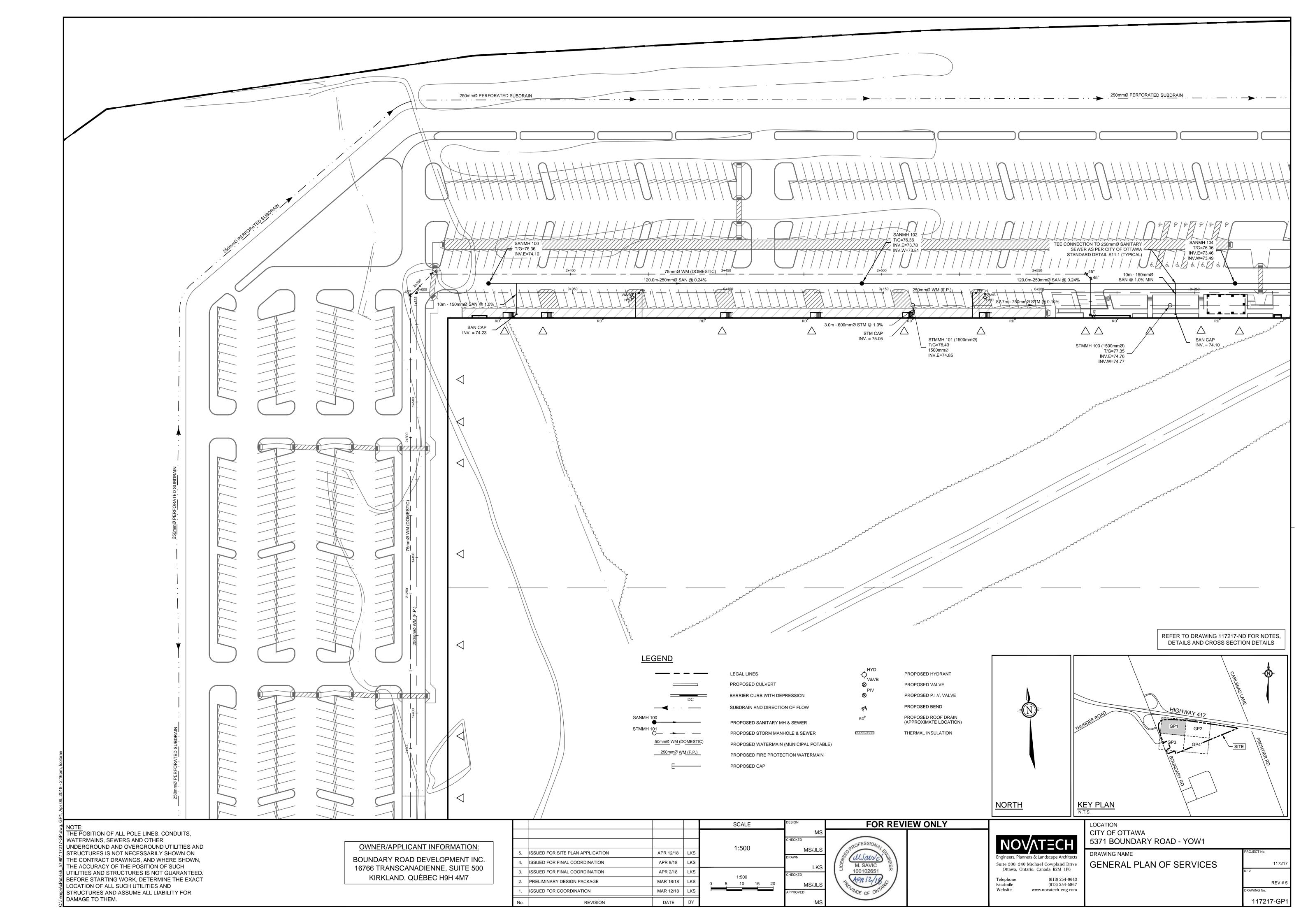
CITY OF OTTAWA 5371 BOUNDARY ROAD - YOW1

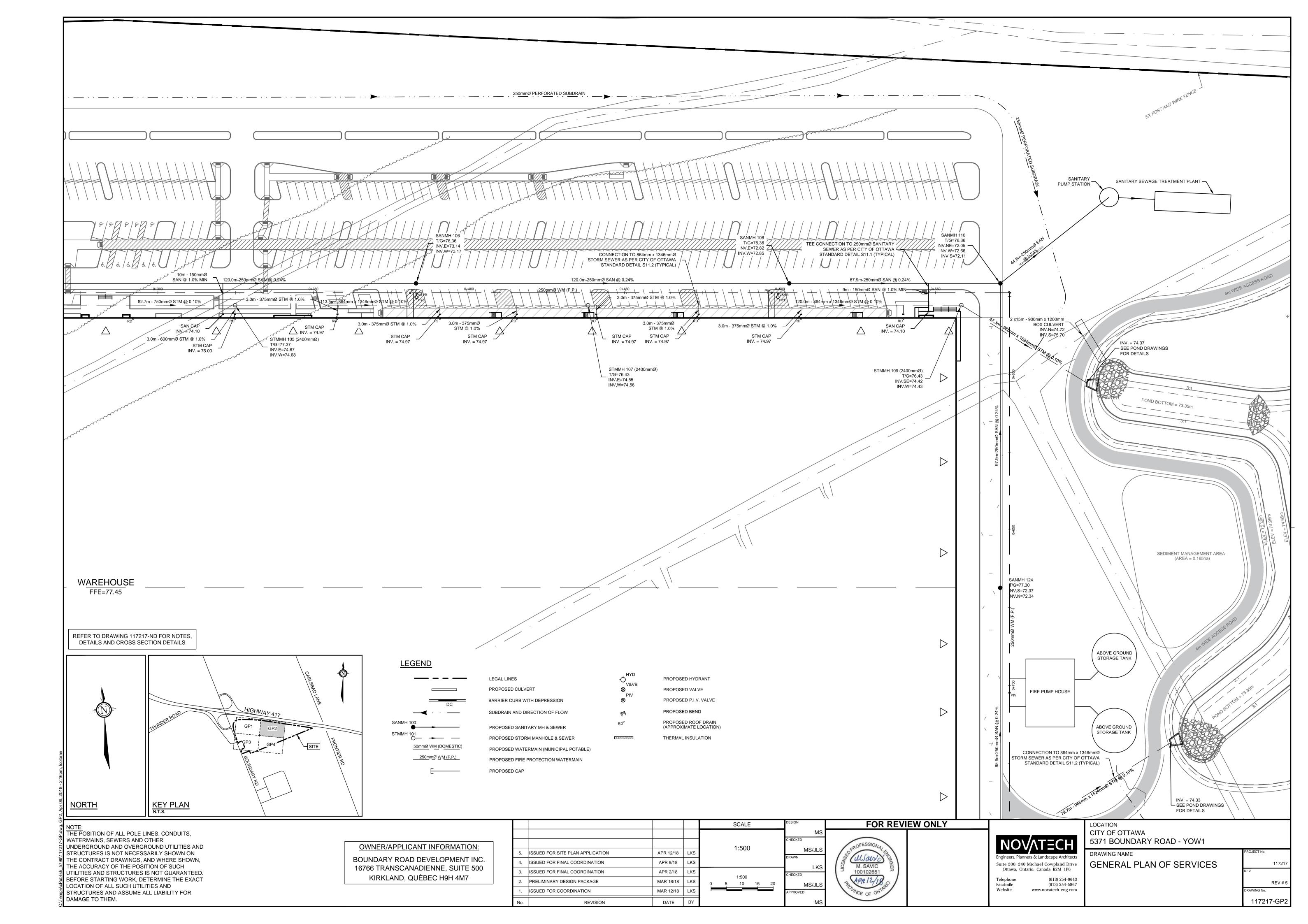
DRAWING NAME **GRADING NOTES AND DETAILS** 

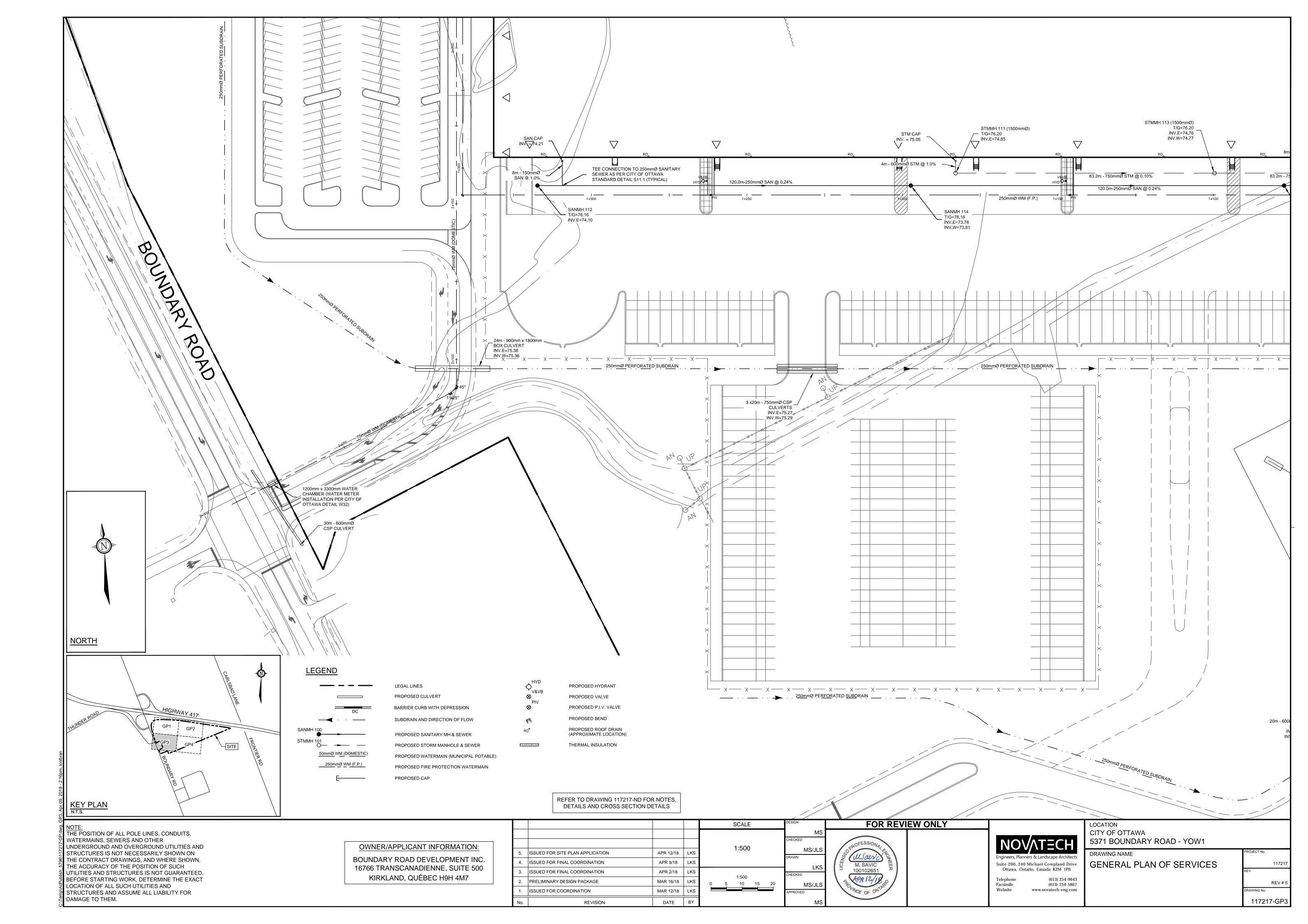
> REV # 3 117217-GRND

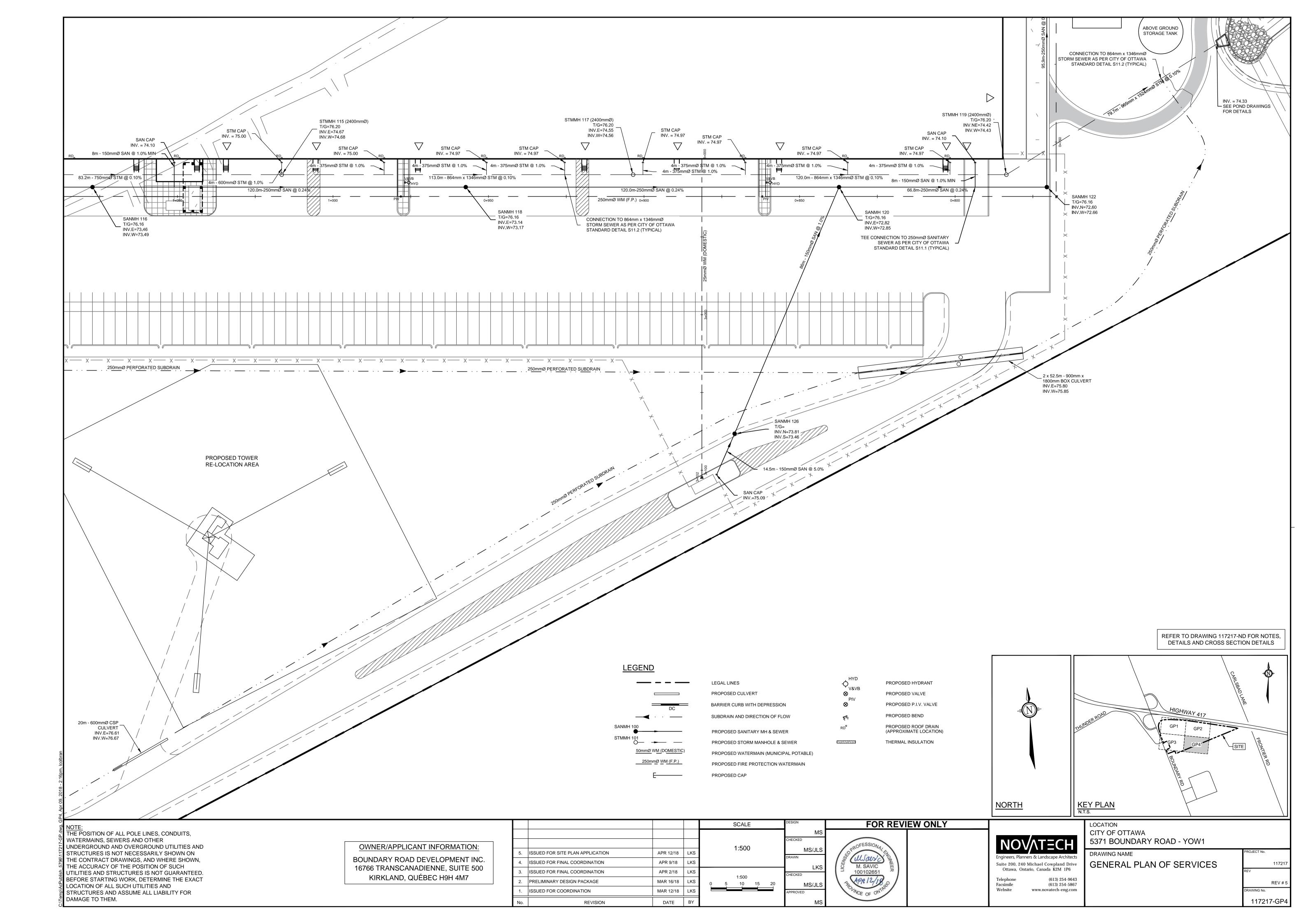
117217











### GENERAL NOTES:

- 1. COORDINATE AND SCHEDULE ALL WORK WITH OTHER TRADES AND CONTRACTORS.
- 2. DETERMINE THE EXACT LOCATION, SIZE, MATERIAL AND ELEVATION OF ALL EXISTING UTILITIES PRIOR TO COMMENCING CONSTRUCTION. PROTECT AND ASSUME RESPONSIBILITY FOR ALL EXISTING UTILITIES WHETHER OR NOT SHOWN ON THIS DRAWING.
- 3. OBTAIN ALL NECESSARY PERMITS AND APPROVALS FROM THE CITY OF OTTAWA BEFORE COMMENCING CONSTRUCTION.
- 4. BEFORE COMMENCING CONSTRUCTION OBTAIN AND PROVIDE PROOF OF COMPREHENSIVE, ALL RISK AND OPERATIONAL LIABILITY INSURANCE FOR \$2,000,000.00. INSURANCE POLICY TO NAME OWNERS, ENGINEERS AND ARCHITECTS AS CO-INSURED.
- 5. RESTORE ALL DISTURBED AREAS ON-SITE AND OFF-SITE, INCLUDING TRENCHES AND SURFACES ON PUBLIC ROAD ALLOWANCES TO EXISTING CONDITIONS OR BETTER TO THE SATISFACTION OF MUNICIPAL AUTHORITIES.
- 6. REMOVE FROM SITE ALL EXCESS EXCAVATED MATERIAL, ORGANIC MATERIAL AND DEBRIS UNLESS OTHERWISE INSTRUCTED BY ENGINEER. EXCAVATE AND REMOVE FROM SITE ANY CONTAMINATED MATERIAL. ALL CONTAMINATED MATERIAL SHALL BE DISPOSED OF AT A LICENSED LANDFILL FACILITY.
- 7. ALL ELEVATIONS ARE GEODETIC.
- 8. REFER TO GEOTECHNICAL INVESTIGATION REPORT NO. PG4366-1 (DATED FEBRUARY 9, 2018) PREPARED BY PATERSON GROUP INC. FOR SUBSURFACE CONDITIONS, CONSTRUCTION RECOMMENDATIONS AND GEOTECHNICAL INSPECTION REQUIREMENTS. THE GEOTECHNICAL CONSULTANT IS TO REVIEW ON-SITE CONDITIONS AFTER EXCAVATION PRIOR TO PLACEMENT OF THE GRANULAR MATERIAL.
- 9. REFER TO ARCHITECT'S AND LANDSCAPE ARCHITECT'S DRAWINGS FOR BUILDING AND HARD SURFACE AREAS AND DIMENSIONS.
- 10. REFER TO THE STORMWATER MANAGEMENT REPORT (R-2018-034) PREPARED BY NOVATECH.
- 11. SAW CUT AND KEYGRIND ASPHALT AT ALL ROAD CUTS AND ASPHALT TIE IN POINTS AS PER CITY OF OTTAWA STANDARDS

## SEWER NOTES:

- 1. SUPPLY AND CONSTRUCT ALL SEWERS AND APPURTENANCES IN ACCORDANCE WITH THE MOST CURRENT CITY OF OTTAWA STANDARDS AND SPECIFICATIONS.
- O OPERIORIONO

SPEC. No.	REFERENCE
701.010	OPSD
701.011	OPSD
701.012	OPSD
701.013	OPSD
401.010 - TYPE 'B' OPEN	OPSD
705.010	OPSD
400.020	OPSD
PVC DR 35	
PVC DR 35	
CONC. CLASS HE-II	
CONC. CLASS HE-II	
PVC DR 35	
	701.010 701.011 701.012 701.013 401.010 - TYPE 'B' OPEN 705.010 400.020 PVC DR 35 PVC DR 35 CONC. CLASS HE-II CONC. CLASS HE-II

INDICATED. ALL STORM MANHOLES WITH PIPE SIZES 900mm AND LARGER ARE TO BE BENCHED.

- SEWER TRENCH BEDDING (GRANULAR 'A')
  COVER (GRANULAR 'A')
- 3. PIPE BEDDING, COVER AND BACKFILL ARE TO BE COMPACTED TO AT LEAST 95% OF THE STANDARD PROCTOR MAXIMUM DRY DENSITY. THE USE OF CLEAR CRUSHED STONE AS A BEDDING LAYER SHALL NOT BE PERMITTED.
- 4. FLEXIBLE CONNECTIONS ARE REQUIRED FOR CONNECTING PIPES TO MANHOLES (FOR EXAMPLE KOR-N-SEAL, PSX: POSITIVE SEAL AND DURASEAL). THE CONCRETE CRADLE FOR THE PIPE CAN BE ELIMINATED.
- 5. ALL STORM MANHOLES MANHOLES WITH PIPE SIZES LESS THAN 900mm ARE TO HAVE 300mm SUMPS UNLESS OTHERWISE
- 6. CONTRACTOR TO TELEVISE ALL PROPOSED SEWERS 200mm OR GREATER IN DIAMETER TO ENSURE THAT THEY ARE CLEAN AND OPERATIONAL. UPON COMPLETION OF CONTRACT, THE CONTRACTOR IS RESPONSIBLE TO FLUSH AND CLEAN ALL SEWERS & APPURTENANCES. OBTAIN APPROVAL FROM THE CITY'S SEWER OPERATIONS. PROVIDE THE CCTV INSPECTION AND REPORT TO THE ENGINEER FOR REVIEW AND APPROVAL.
- 7. CONTRACTOR TO PROVIDE THE CONSULTANT WITH A GENERAL PLAN OF SERVICES INDICATING ALL APPLICABLE SERVICING AS-BUILT INFORMATION SHOWN ON THIS PLAN. AS-BUILT INFORMATION MUST INCLUDE: PIPE MATERIAL, SIZES, LENGTHS, SLOPES, INVERT AND T/G ELEVATIONS, STRUCTURE LOCATIONS AND ANY ALIGNMENT CHANGES, ETC.
- 8. THE OWNER SHALL REQUIRE THAT THE SITE SERVICING CONTRACTOR PERFORM FIELD TESTS FOR QUALITY CONTROL OF ALL SANITARY SEWERS. LEAKAGE TESTING SHALL BE COMPLETED IN ACCORDANCE WITH OPSS 410.07.16, 410.07.16.04 AND 407.07.24. DYE TESTING IS TO BE COMPLETED ON ALL SANITARY SERVICES TO CONFIRM PROPER CONNECTION TO THE SANITARY SEWER MAIN. THE FIELD TESTS SHALL BE PERFORMED IN THE PRESENCE OF A CERTIFIED PROFESSIONAL ENGINEER WHO SHALL SUBMIT A CERTIFIED COPY OF THE TEST RESULTS.

# WATERMAIN NOTES:

THE POSITION OF ALL POLE LINES, CONDUITS,

STRUCTURES IS NOT NECESSARILY SHOWN ON

THE ACCURACY OF THE POSITION OF SUCH

STRUCTURES AND ASSUME ALL LIABILITY FOR

LOCATION OF ALL SUCH UTILITIES AND

DAMAGE TO THEM.

THE CONTRACT DRAWINGS, AND WHERE SHOWN,

UTILITIES AND STRUCTURES IS NOT GUARANTEED.

BEFORE STARTING WORK, DETERMINE THE EXACT

UNDERGROUND AND OVERGROUND UTILITIES AND

WATERMAINS, SEWERS AND OTHER

1. SUPPLY AND CONSTRUCT ALL WATERMAIN AND APPURTENANCES IN ACCORDANCE WITH THE MOST CURRENT CITY OF

2. SPECIFICATIONS:

- 3. SUPPLY AND CONSTRUCT ALL WATERMAINS AND APPURTENANCES IN ACCORDANCE WITH THE CITY OF OTTAWA STANDARD AND SPECIFICATIONS. EXCAVATION, INSTALLATION, BACKFILL AND RESTORATION OF ALL WATERMAINS BY THE CONTRACTOR. CONNECTIONS AND SHUT-OFFS AT THE MAIN AND CHLORINATION OF THE WATER SYSTEM SHALL BE
- PERFORMED BY CITY OFFICIALS.

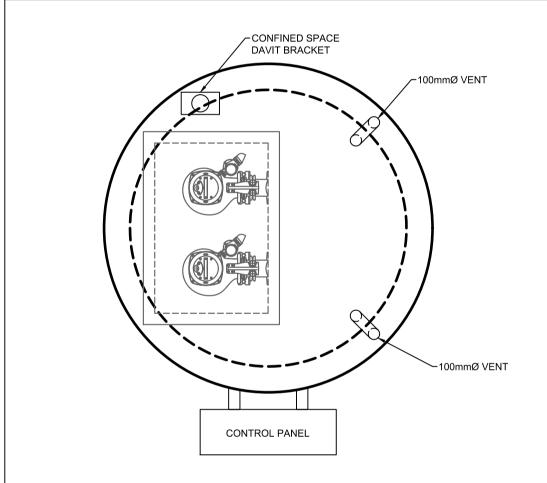
  4. WATERMAIN SHALL BE MINIMUM 2.4m DEPTH BELOW GRADE UNLESS OTHERWISE INDICATED.
- 5. PROVIDE MINIMUM 0.5m CLEARANCE BETWEEN OUTSIDE OF PIPES AT ALL CROSSINGS.
- 6. WATER SERVICE IS TO BE CONSTRUCTED TO WITHIN 1.0m OF FOUNDATION WALL AND CAPPED, UNLESS OTHERWISE INDICATED.

WATERMAIN NOTES ARE APPLICABLE FOR DOMESTIC SERVICES ONLY. REFER TO NOTES AND SPECIFICATIONS PREPARED BY CIVELEC CONSULTANTS INC. FOR FIRE PROTECTION WATERMAIN REQUIREMENTS.

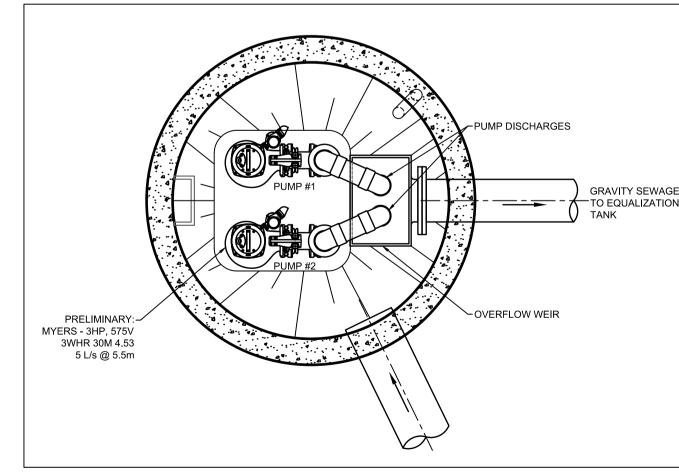
STATION	SURFACE	T/WM	COMMENTS
	ELEVATION	ELEVATION	CROSS BELOW 150mmØ SAN AS PER CITY O
0+031.9	76.39	73.65	OTTAWA STANDARD W25 (±0.50m CLEARANC
0+050.0	76.39	73.77	-
0+069.2 0+070.2	76.39 76.39	73.77	HYDRANT CONNECTION  250mm x 250mm x 250mm TEE
0+070.2	76.39	73.77	PIV
0+072.3	76.39	73.77	250mm x 250mm x 250mm TEE
0+100.0	76.39	73.77	-
0+150.0	76.39	73.77	-
0+200.0	76.39	73.77	-
0+208.9	76.55	73.77	250mm x 250mm x 250mm TEE
0+209.9	76.55	73.77	PIV
0+211.0	76.55	73.77	250mm x 250mm x 250mm TEE
0+212.8	76.39	73.77	HYDRANT CONNECTION
0+216.5	76.39	73.77	CROSS ABOVE 75mmØ WM (±0.30m CLEARAN
0+243.8	76.55	73.52	CROSS BELOW 150mmØ SAN AS PER CITY O OTTAWA STANDARD W25 (±0.50m CLEARANC
0+250.0	76.55	73.77	-
0+300.0	76.55	73.77	-
0+320.9	76.55	73.52	CROSS BELOW 150mmØ SAN AS PER CITY O OTTAWA STANDARD W25 (±0.50m CLEARANC
0+350.9	76.55	73.77	250mm x 250mm x 250mm TEE
0+351.9	76.39	73.77	PIV
0+352.9	76.39	73.77	250mm x 250mm x 250mm TEE
0+353.9	76.39	73.77	HYDRANT CONNECTION
0+400.0	76.39	73.77	<u>.</u>
0+450.0 0+494.2	76.39 76.39	73.77	250mm x 250mm x 250mm TEE
0+494.2	76.39	73.77 73.77	PIV
0+496.3	76.39	73.77	250mm x 250mm x 250mm TEE
0+497.3	76.39	73.77	HYDRANT CONNECTION
0+547.7	76.55	73.53	CROSS BELOW 150mmØ SAN AS PER CITY O
0+570.8	76.39	73,77	OTTAWA STANDARD W25 (±0.50m CLEARANC CROSS ABOVE 250mmØ SAN (±1.11m CLEARAN
0+573.8	76.30	73.68	90° HORIZONTAL BEND
0+587.4	76.65	73.76	CROSS BELOW 956mm x 1524mm STM AS PER
0+600.0	76.65	74.25	OF OTTAWA STANDARD W25 (±0.50m CLEARAN
0+650.0	76.80	74.40	-
0+697.9	76.71	74.31	250mm x 250mm x 250mm TEE
0+702.3	76.72	74.32	PIV
0+706.8	76.71	74.31	250mm x 250mm x 250mm TEE
0+750.6	76.27	73.76	CROSS BELOW 956mm x 1524mm STM AS PER OF OTTAWA STANDARD W25 (±0.50m CLEARAN
0+767.5	75.94	73.54	90° HORIZONTAL BEND
0+800.0	76.13	73.73	-
0+850.0	76.13	73.73	-
0+860.9	76.13	73.73	250mm x 250mm x 250mm TEE
0+862.0	76.13	73.73	PIV
0+863.0	76.13	73.73	250mm x 250mm x 250mm TEE
0+900.0	76.13	73.73	-
0+950.0	76.13	73.73	-
0+977.1	76.13	73.73	250mm x 250mm x 250mm TEE
0+978.2	76.13	73.73	PIV 250mm x 250mm x 250mm TEE
0+979.2	76.13	73.73	250mm x 250mm x 250mm TEE
1+000.0	76.13 76.28	73.73 73.73	-
1+100.0	76.13	73.73	-
1+110.4	76.13	73.73	CROSS ABOVE 25mmØ WM (±0.30m CLEARAN
1+111.4	76.13	73.06	CROSS BELOW 250mmØ SAN AS PER CITY O
1+120.2	76.13	73.73	OTTAWA STANDARD W25 (±0.50m CLEARANC 250mm x 250mm x 250mm TEE
1+121.3	76.13	73.73	PIV
1+122,3	76.13	73.73	250mm x 250mm x 250mm TEE
1+150.0	76.13	73.73	_
1+200.0	76.28	73.73	-
1+250.0	76.13	73.73	-
1+260.5	76.13	73.73	250mm x 250mm x 250mm TEE
1+261.6	76.13	73.73	PIV
1+262.6	76.13	73.73	250mm x 250mm x 250mm TEE
1+300.0	76.13	73.73	-
1+341.4	76.76	74.36	90° HORIZONTAL BEND
1+350.0	76.80	74.40	-
1+400.0	76.79	74.39	-
1+450.0	76.91	74.51	-
1+500.0	76.72	74.32	-

Р	ROPOSED	) WATERMA	IN (25mm DOMESTIC) TABLE
STATION SURFACE T/WM ELEVATION			COMMENTS
3+001.0	76.24	73.84	CAP 1.0m FROM BUILDING FACE
3+005.0	76.20	73.80	CROSS BELOW 864mm x 1346mm STM AS PER CITY OF OTTAWA STANDARD W25 (±0.50m CLEARANCE)
3+009.0	76.16	73.76	CROSS ABOVE 250mmØ SAN AS PER CITY OF OTTAWA STANDARD W25 (±0.50m CLEARANCE)
3+012.0	76.13	73.15	CROSS BELOW 250mmØ WM (±0.30m CLEARANCE)
3+025.0	76.00	73.60	-
3+050.0	75.75	73.35	-
3+075.0	77.00	74.60	-
3+100.0	77.03	74.63	-
3+102.0	77.20	74.80	CAP 1.0m FROM BUILDING FACE

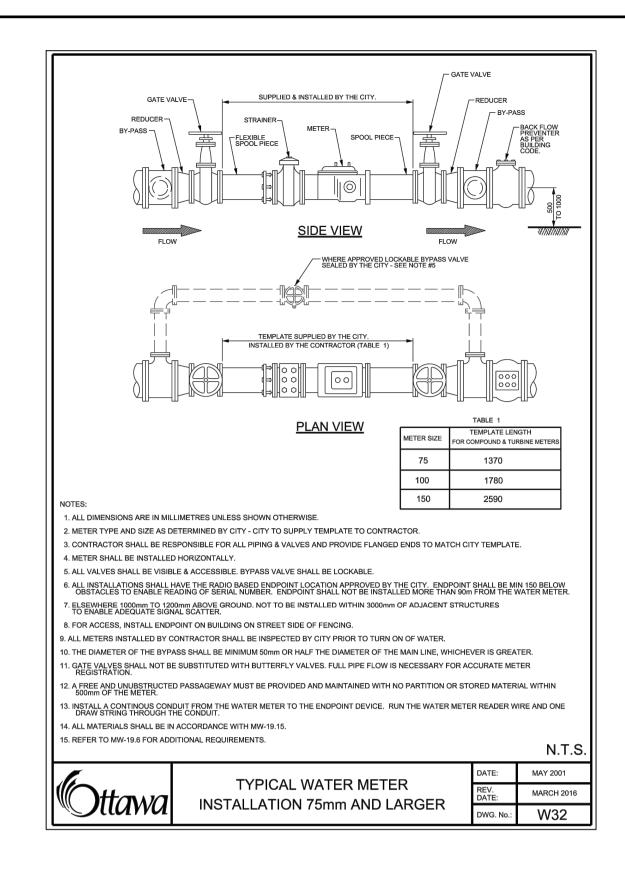
PROPOSED WATERMAIN (75mm DOMESTIC) TABLE						
STATION	SURFACE ELEVATION	T/WM ELEVATION	COMMENTS			
2+009.5	77.55	75.15	TEE CONNECTION TO EX. 75mmØ WM			
2+026.2	77.35	74.95	VALVE CHAMBER			
2+0.50.0	77.15	74.75	-			
2+075.0	76.86	74.46	-			
2+088.2	77.16	74.76	11.25° HORIZONTAL BEND			
2+091.0	77.21	74.81	45° HORIZONTAL BEND			
2+097.0	77.28	74.66	CROSS BELOW BOX CULVERT (±0.50m CLEARANCE), INSULATE PER CITY OF OTTAWA STANDARD W21			
2+125.0	77.02	74.62	-			
2+150.0	76.73	74.33	-			
2+175.0	76.86	74.46	-			
2+200.0	76.82	74.42	-			
2+225.0	76.73	74.33	-			
2+250.0	76.83	74.43	-			
2+275.0	76.84	74.44	-			
2+300.0	76.73	74.33	-			
2+325.0	76.64	74.24	-			
2+345.8	76.50	74.10	45° HORIZONTAL BEND			
2+355.3	76.38	73.71	45° HORIZONTAL BEND			
2+375.0	76.33	73.71	-			
2+400.0	76.33	73.71	-			
2+425.0	76.33	73.71	-			
2+450.0	76.33	73.71	-			
2+475.0	76.33	73.71	-			
2+500.0	76.33	73.71	-			
2+525.0	76.33	73.71	-			
2+550.0	76.33	73.71	-			
2+565.7	76.33	73.71	45° HORIZONTAL BEND			
2+567.7	76.35	73.73	45° HORIZONTAL BEND			
2+569.3	76.36	73.09	CROSS BELOW 250mmØ SAN AS PER CITY OF OTTAWA STANDARD W25 (±0.50m CLEARANCE)			
2+572.3	76.39	73.19	CROSS BELOW 250mmØ WM (±0.30m CLEARANCE)			
2+576.3	76.43	73.81	CROSS BELOW 750mmØ STM (±0.95m CLEARANCE)			
2+579.3	77.44	73.84	CAP 1.0m FROM BUILDING FACE			



2400mmØ SANITARY PUMP STATION WET WELL - PLAN VIEW SCALE: N.T.S.



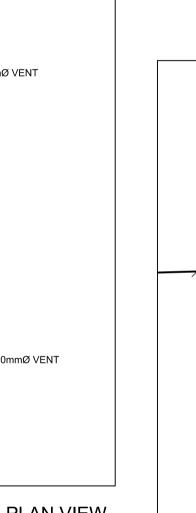
2400mmØ SANITARY PUMP STATION WET WELL - PLAN VIEW SCALE: N.T.S.



√75mmØ SAN DISCHARGE

EXIST. 77.00±

-REDUCING ELBOW



ACCESS LADDER

ACCESS LADDER

ASSIME

FLOAT SWITCH

PRESSURE TRANSDUCER

2500 SANITARY INLET

2400mmØ SANITARY PUMP STATION WET WELL - SECTION SCALE: N.T.S.

COMMENTS	
0m FROM BUILD <b>I</b> NG FACE	
364mm x 1346mm STM AS PER CITY NDARD W25 (±0.50m CLEARANCE) 5 250mmØ SAN AS PER CITY OF DARD W25 (±0.50m CLEARANCE)	PRELIMIN, MYERS - 3HP, { 3WHR 30M 5 L/s @
250mmØ WM (±0.30m CLEARANCE)	
-	
-	
-	
-	
0m FROM BUILDING FACE	<u>240</u>

OWNER/APPLICANT INFORMATION:
BOUNDARY ROAD DEVELOPMENT INC.

BOUNDARY ROAD DEVELOPMENT INC. 16766 TRANSCANADIENNE, SUITE 500 KIRKLAND, QUÉBEC H9H 4M7

				SCALE	DESIGN	
					MS	
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				AS NOTED	MS/JLS	ı
					DRAWN	ı
3.	ISSUED FOR SITE PLAN APPLICATION	APR 12/18	LKS	-	LKS	ı
2.	ISSUED FOR FINAL COORDINATION	APR 9/18	LKS		MS/JLS	l
1.	ISSUED FOR FINAL COORDINATION	APR 2/18	LKS		APPROVED	i I
No.	REVISION	DATE	BY		MS	

FOR REVIEW ONLY

OF ESSIONAL TRANSPORTED TO THE PROPERTY OF ONLY

M. SAVIC 100102651

APR 12/18

OF ONLY

Engineers, Planners & Landscape Architects
Suite 200, 240 Michael Cowpland Drive
Ottawa, Ontario, Canada K2M 1P6
Telephone (613) 254-9643

Facsimile Website (613) 254-5867

www.novatech-eng.com

CITY OF OTTAWA 5371 BOUNDARY ROAD - YOW1

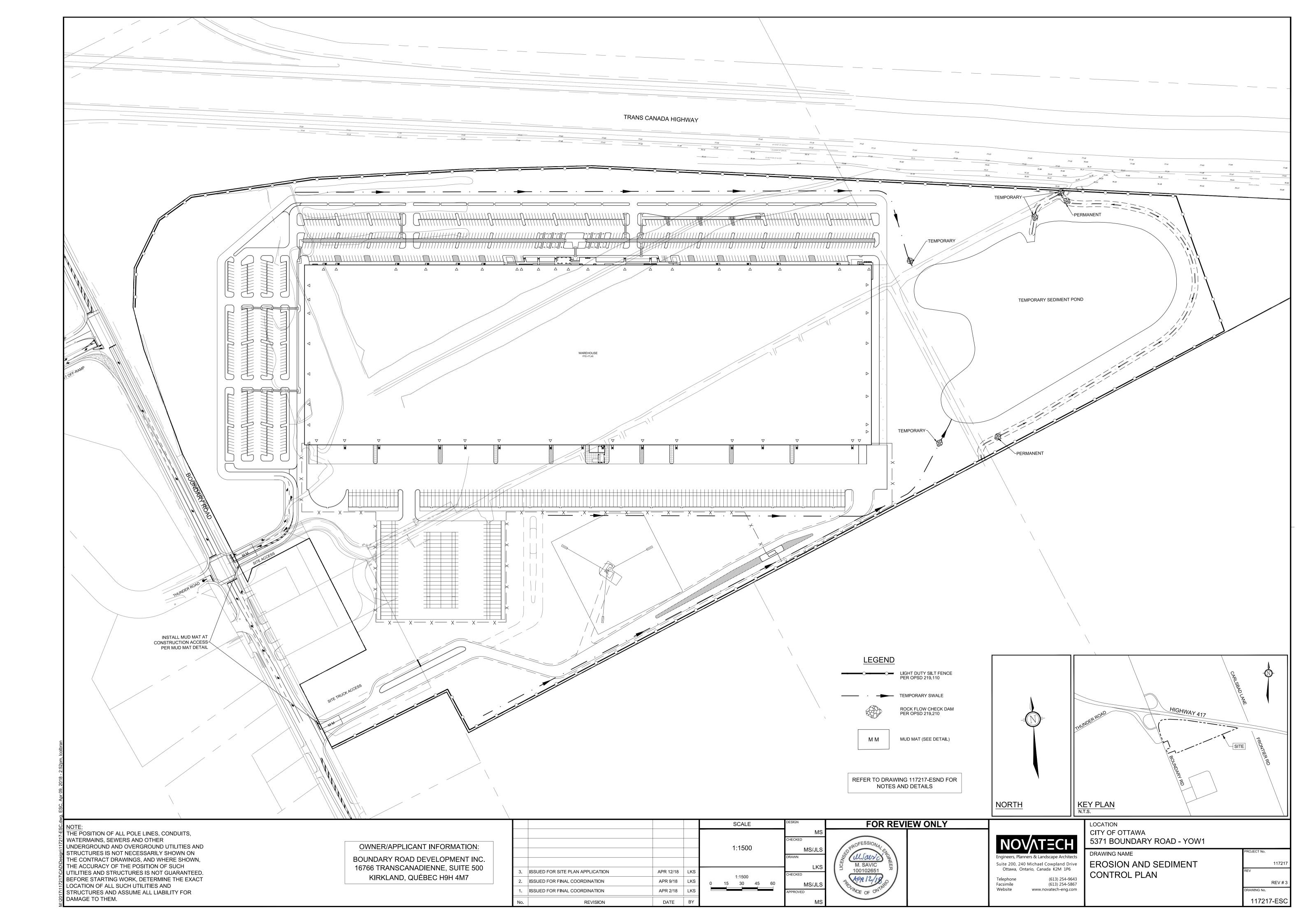
DRAWING NAME
SERVICING NOTES AND DETAILS

REV # 3

ORAWING No.

117217-GPND

117217

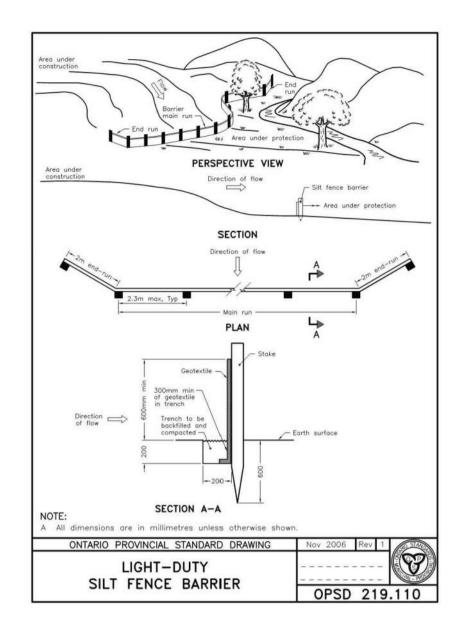


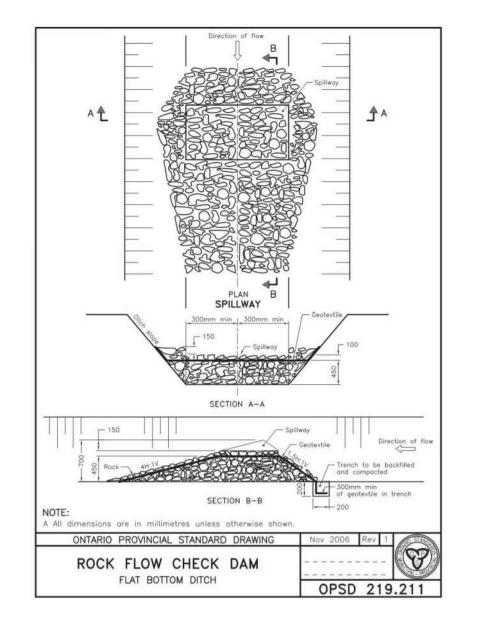
### **GENERAL NOTES:**

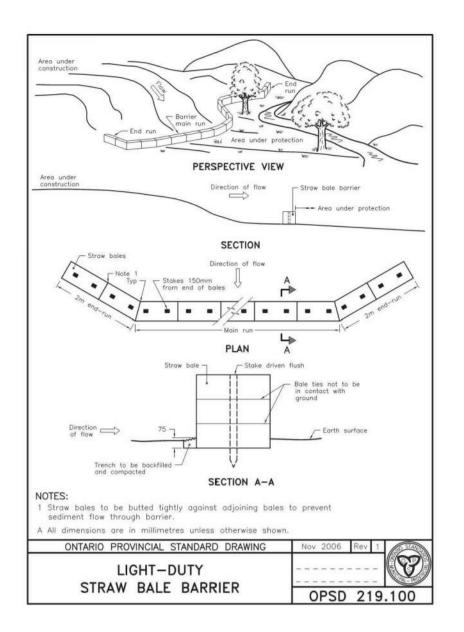
- 1. COORDINATE AND SCHEDULE ALL WORK WITH OTHER TRADES AND CONTRACTORS.
- 2. DETERMINE THE EXACT LOCATION, SIZE, MATERIAL AND ELEVATION OF ALL EXISTING UTILITIES PRIOR TO COMMENCING CONSTRUCTION. PROTECT AND ASSUME RESPONSIBILITY FOR ALL EXISTING UTILITIES WHETHER OR NOT SHOWN ON THIS DRAWING.
- 3. OBTAIN ALL NECESSARY PERMITS AND APPROVALS FROM THE CITY OF OTTAWA BEFORE COMMENCING CONSTRUCTION.
- 4. BEFORE COMMENCING CONSTRUCTION OBTAIN AND PROVIDE PROOF OF COMPREHENSIVE, ALL RISK AND OPERATIONAL LIABILITY INSURANCE FOR \$2,000,000.00. INSURANCE POLICY TO NAME OWNERS, ENGINEERS AND ARCHITECTS AS COLINSURED.
- 5. RESTORE ALL DISTURBED AREAS ON-SITE AND OFF-SITE, INCLUDING TRENCHES AND SURFACES ON PUBLIC ROAD ALLOWANCES TO EXISTING CONDITIONS OR BETTER TO THE SATISFACTION OF MUNICIPAL AUTHORITIES.
- 6. REMOVE FROM SITE ALL EXCESS EXCAVATED MATERIAL, ORGANIC MATERIAL AND DEBRIS UNLESS OTHERWISE INSTRUCTED BY ENGINEER. EXCAVATE AND REMOVE FROM SITE ANY CONTAMINATED MATERIAL. ALL CONTAMINATED MATERIAL SHALL BE DISPOSED OF AT A LICENSED LANDFILL FACILITY.
- 7. ALL ELEVATIONS ARE GEODETIC.
- 8. REFER TO GEOTECHNICAL INVESTIGATION REPORT NO. PG4366-1 (DATED FEBRUARY 9, 2018) PREPARED BY PATERSON GROUP INC. FOR SUBSURFACE CONDITIONS, CONSTRUCTION RECOMMENDATIONS AND GEOTECHNICAL INSPECTION REQUIREMENTS. THE GEOTECHNICAL CONSULTANT IS TO REVIEW ON-SITE CONDITIONS AFTER EXCAVATION PRIOR TO PLACEMENT OF THE GRANULAR MATERIAL.
- 9. REFER TO ARCHITECT'S AND LANDSCAPE ARCHITECT'S DRAWINGS FOR BUILDING AND HARD SURFACE AREAS AND
- 10. REFER TO THE STORMWATER MANAGEMENT REPORT (R-2018-034) PREPARED BY NOVATECH.
- 11. SAW CUT AND KEYGRIND ASPHALT AT ALL ROAD CUTS AND ASPHALT TIE IN POINTS AS PER CITY OF OTTAWA STANDARDS (R10 AND R25).

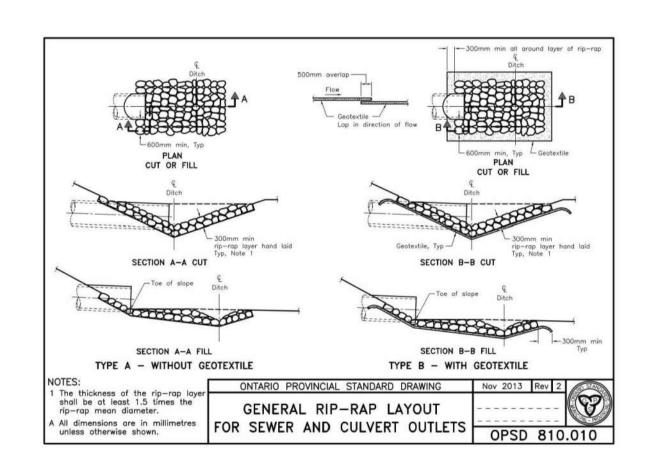
## **EROSION AND SEDIMENT CONTROL NOTES:**

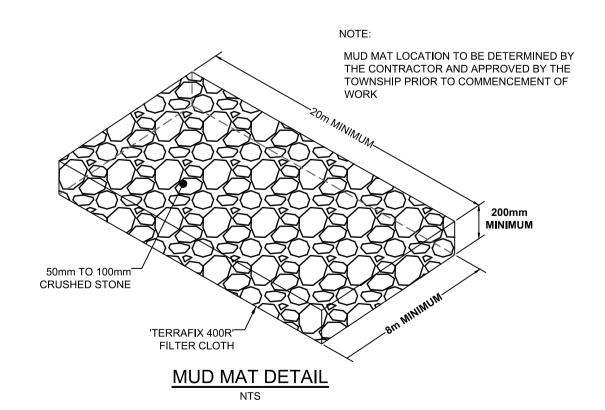
- THE CONTRACTOR SHALL IMPLEMENT BEST MANAGEMENT PRACTICES, TO PROVIDE FOR PROTECTION OF THE AREA DRAINAGE SYSTEM AND THE RECEIVING WATERCOURSE, DURING CONSTRUCTION ACTIVITIES. THE CONTRACTOR ACKNOWLEDGES THAT FAILURE TO IMPLEMENT APPROPRIATE EROSION AND SEDIMENT CONTROL MEASURES MAY BE SUBJECT TO PENALTIES IMPOSED BY ANY APPLICABLE REGULATORY AGENCY.
- 1. ALL EROSION AND SEDIMENT CONTROLS ARE TO BE INSTALLED TO THE SATISFACTION OF THE ENGINEER AND THE CITY OF OTTAWA. THEY ARE TO BE APPROPRIATE TO THE SITE CONDITIONS, PRIOR TO UNDERTAKING ANY SITE ALTERATIONS (FILLING, GRADING, REMOVAL OF VEGETATION, ETC.) AND DURING ALL PHASES OF SITE PREPARATION AND CONSTRUCTION. THESE PRACTICES ARE TO BE IMPLEMENTED IN ACCORDANCE WITH THE CURRENT BEST MANAGEMENT PRACTICES FOR EROSION AND SEDIMENT CONTROL AND SHOULD INCLUDE AS A MINIMUM THOSE MEASURES INDICATED ON THE PLAN.
- 2. EROSION AND SEDIMENT CONTROL MEASURES WILL BE IMPLEMENTED DURING CONSTRUCTION IN ACCORDANCE WITH THE "GUIDELINES ON EROSION AND SEDIMENT CONTROL FOR URBAN CONSTRUCTION SITES" (GOVERNMENT OF ONTARIO, MAY 1987). THE CONTRACTOR SHALL BE SOLELY RESPONSIBLE FOR MEETING ALL REGULATORY AGENCY REQUIREMENTS.
- 3. TO PREVENT SURFACE EROSION FROM ENTERING ANY STORM SEWER SYSTEM DURING CONSTRUCTION, FILTER CLOTH WILL BE PLACED UNDER GRATES OF NEARBY CATCHBASINS AND STRUCTURES. A LIGHT DUTY SILT FENCE BARRIER WILL ALSO BE INSTALLED AROUND THE CONSTRUCTION AREA (WHERE APPLICABLE). THESE CONTROL MEASURES WILL REMAIN IN PLACE UNTIL CONSTRUCTION IS COMPLETE.
- 4. TO LIMIT EROSION: MINIMIZE THE AMOUNT OF EXPOSED SOILS AT ANY GIVEN TIME, RE-VEGETATE EXPOSED AREAS AND SLOPES AS SOON AS POSSIBLE AND PROTECT EXPOSED SLOPES WITH NATURAL OR SYNTHETIC MULCHES.
- 5. FOR MATERIAL STOCKPILING: MINIMIZE THE AMOUNT OF EXPOSED MATERIALS AT ANY GIVEN TIME; APPLY TEMPORARY SEEDING, TARPS, COMPACTION AND/OR SURFACE ROUGHENING AS REQUIRED TO STABILIZE STOCKPILED MATERIALS THAT WILL NOT BE USED WITHIN 14 DAYS.
- 6. THE SEDIMENT CONTROL MEASURES SHALL ONLY BE REMOVED WHEN, IN THE OPINION OF THE ENGINEER, THE MEASURES ARE NO LONGER REQUIRED. NO CONTROL MEASURES MAY BE PERMANENTLY REMOVED WITHOUT PRIOR AUTHORIZATION FROM THE ENGINEER.
- 7. THE CONTRACTOR SHALL IMMEDIATELY REPORT TO THE ENGINEER ANY ACCIDENTAL DISCHARGES OF SEDIMENT MATERIAL INTO ANY STORM SEWER SYSTEM. APPROPRIATE RESPONSE MEASURES, INCLUDING ANY REPAIRS TO EXISTING CONTROL MEASURES OR THE IMPLEMENTATION OF ADDITIONAL CONTROL MEASURES, SHALL BE CARRIED OUT BY THE CONTRACTOR WITHOUT DELAY.
- 8. THE CONTRACTOR ACKNOWLEDGES THAT FAILURE TO IMPLEMENT EROSION AND SEDIMENT CONTROL MEASURES MAY BE SUBJECT TO PENALTIES IMPOSED BY ANY APPLICABLE REGULATORY AGENCY.
- 9. ROADWAYS ARE TO BE SWEPT AS REQUIRED OR AS DIRECTED BY THE ENGINEER AND/OR THE REPRESENTATIVE OF THE MUNICIPALITY.
- 10.THE CONTRACTOR SHALL ENSURE PROPER DUST CONTROL IS PROVIDED WITH THE APPLICATION OF WATER (AND IF REQUIRED, CALCIUM CHLORIDE) DURING DRY PERIODS. MONITOR DUST LEVELS DURING SITE PREPARATION/EXCAVATION, AND CONSTRUCTION ACTIVITIES, AND WHEN DUST LEVELS BECOME VISUALLY APPARENT SPRAY WATER TO MINIMIZE THE RELEASE OF DUST FROM GRAVEL, PAVED AREAS AND EXPOSED SOILS. USE CHEMICAL DUST SUPPRESSANTS ONLY WHERE NECESSARY ON PROBLEM AREAS











NOTE:
THE POSITION OF ALL POLE LINES, CONDUITS,
WATERMAINS, SEWERS AND OTHER
UNDERGROUND AND OVERGROUND UTILITIES AND
STRUCTURES IS NOT NECESSARILY SHOWN ON
THE CONTRACT DRAWINGS, AND WHERE SHOWN,
THE ACCURACY OF THE POSITION OF SUCH
UTILITIES AND STRUCTURES IS NOT GUARANTEED.
BEFORE STARTING WORK, DETERMINE THE EXACT
LOCATION OF ALL SUCH UTILITIES AND
STRUCTURES AND ASSUME ALL LIABILITY FOR

DAMAGE TO THEM.

OWNER/APPLICANT INFORMATION:

BOUNDARY ROAD DEVELOPMENT INC.

16766 TRANSCANADIENNE, SUITE 500

KIRKLAND, QUÉBEC H9H 4M7

DESIGN	SCALE				
CHECKED					
MS/JLS DRAWN	AS SHOWN				
LKS		LKS	APR 12/18	ISSUED FOR SITE PLAN APPLICATION	3.
MS/JLS		LKS	APR 9/18	ISSUED FOR FINAL COORDINATION	2.
APPROVED		LKS	APR 2/18	ISSUED FOR FINAL COORDINATION	1.
MS		BY	DATE	PEVISION	No.

FOR REVIEW ONLY

SPENSIONAL HILLIAN

M. SAVIC

100102651

APR 12/18

OF ONT REPORT OF

Engineers, Planners & Landscape Architects
Suite 200, 240 Michael Cowpland Drive
Ottawa, Ontario, Canada K2M 1P6
Telephone (613) 254-9643

Facsimile

Website

(613) 254-5867

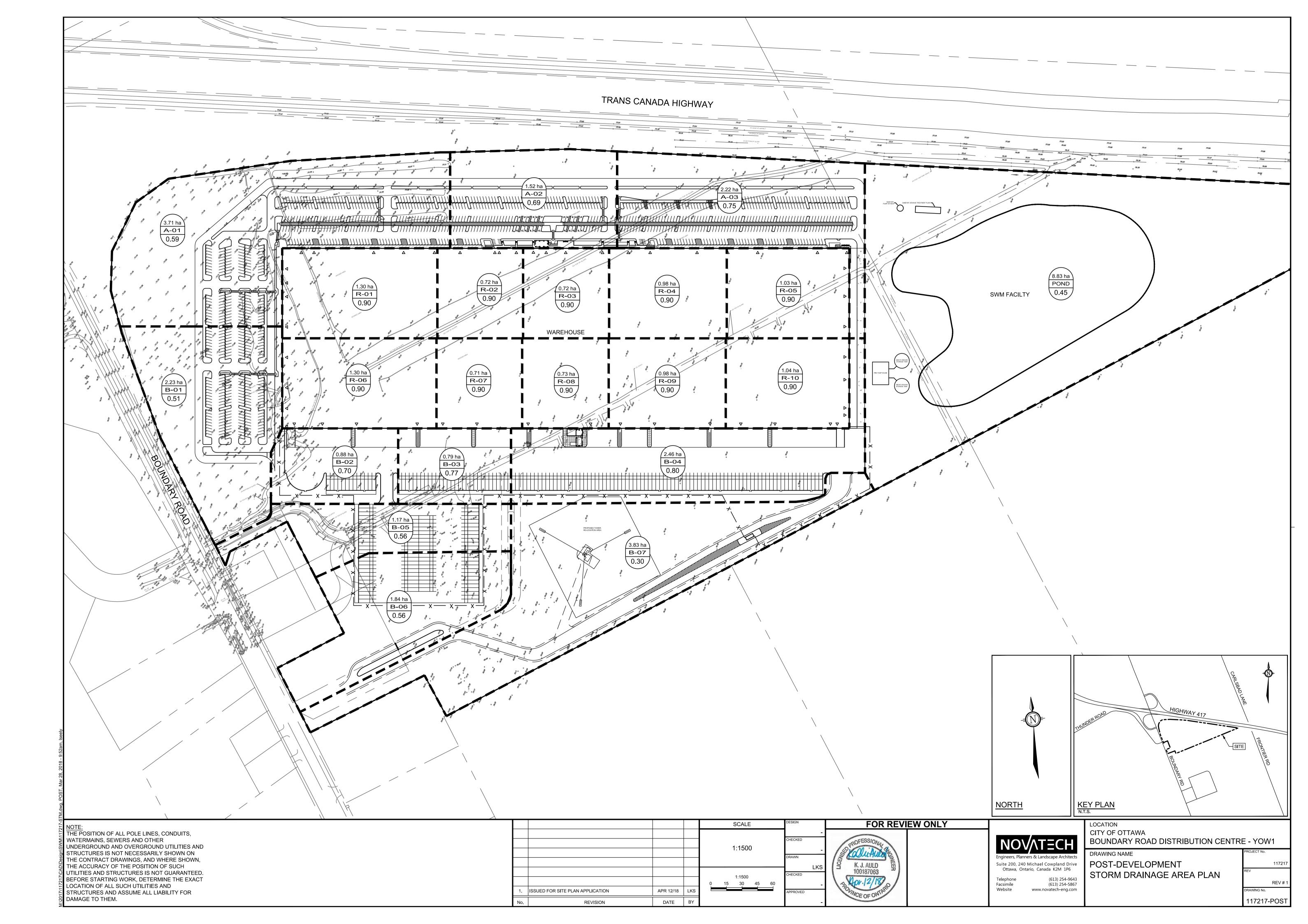
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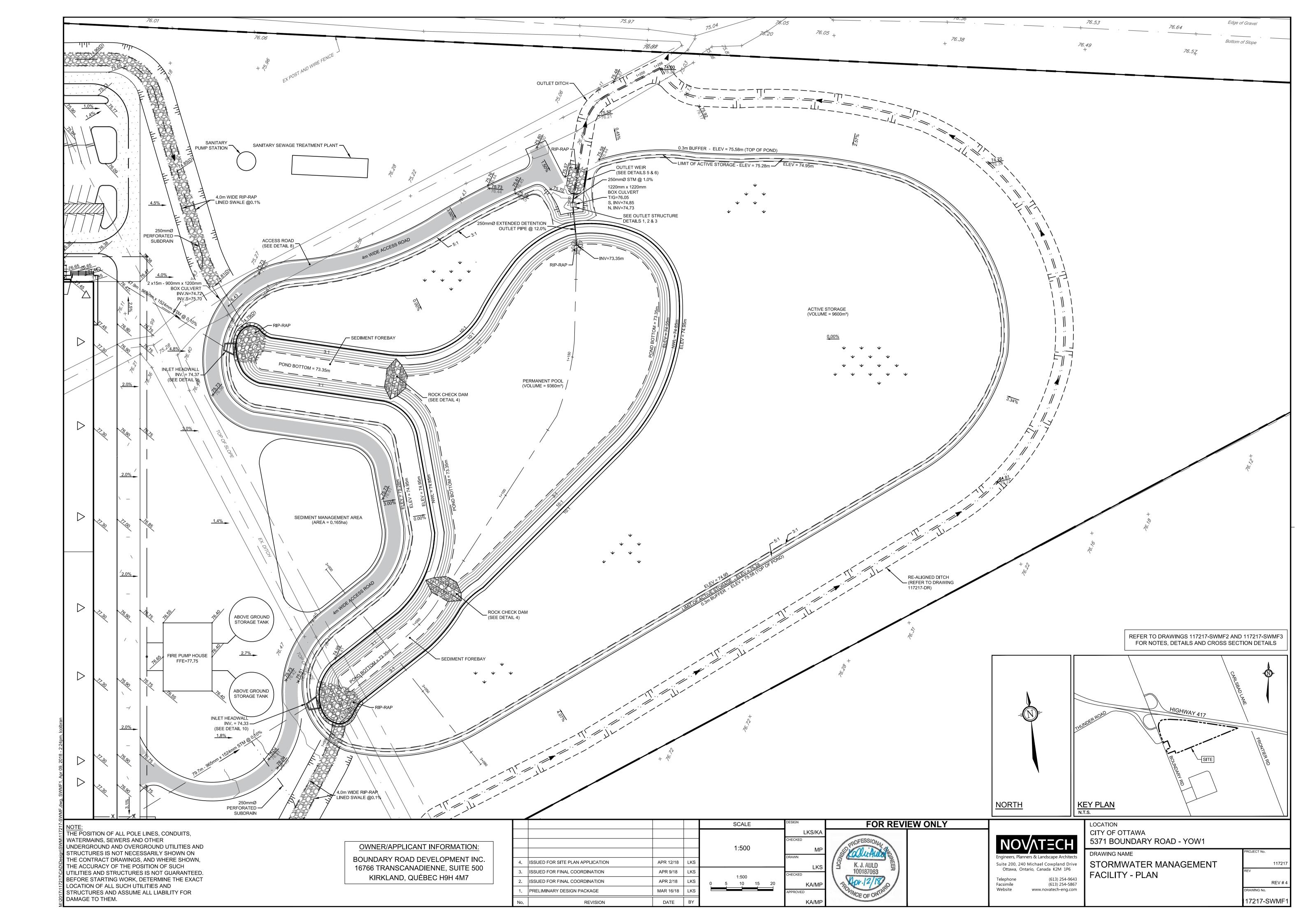
LOCATION
CITY OF OTTAWA
5371 BOUNDARY ROAD - YOW1

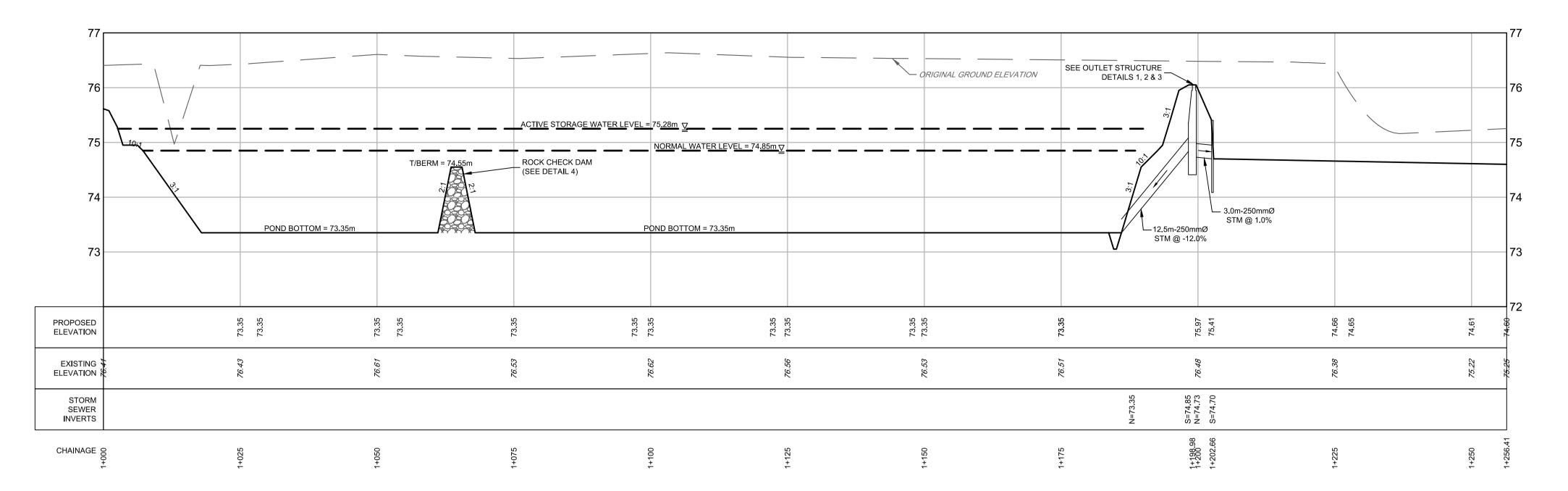
EROSION AND SEDIMENT
CONTROL NOTES AND DETAILS

REV # 3
DRAWING No.
117217-ESND

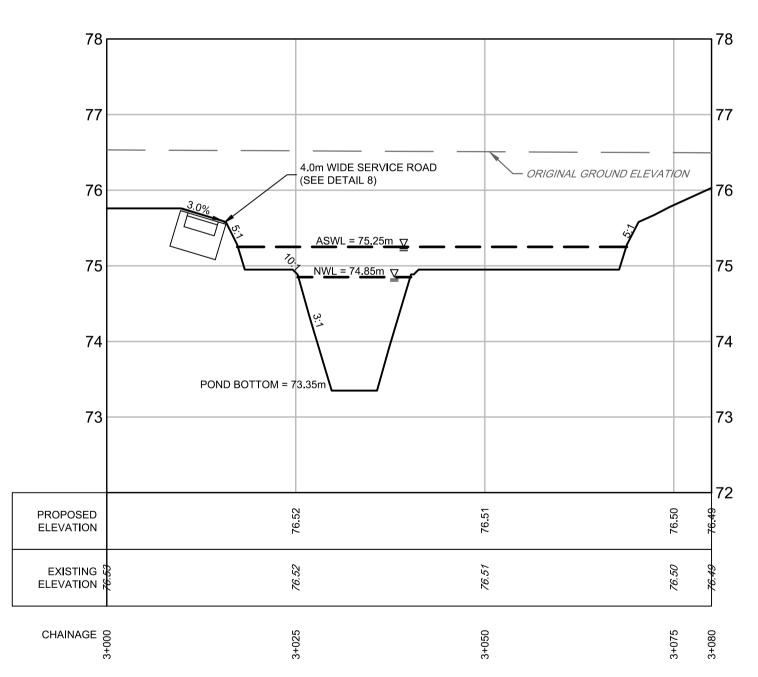








## POND FLOW PATH SECTION



POND FOREBAY SECTION

THE POSITION OF ALL POLE LINES, CONDUITS,

UNDERGROUND AND OVERGROUND UTILITIES AND

STRUCTURES IS NOT NECESSARILY SHOWN ON

THE ACCURACY OF THE POSITION OF SUCH

STRUCTURES AND ASSUME ALL LIABILITY FOR

LOCATION OF ALL SUCH UTILITIES AND

DAMAGE TO THEM.

THE CONTRACT DRAWINGS, AND WHERE SHOWN,

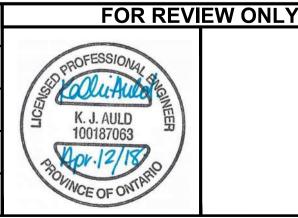
UTILITIES AND STRUCTURES IS NOT GUARANTEED.

BEFORE STARTING WORK, DETERMINE THE EXACT

WATERMAINS, SEWERS AND OTHER

OWNER/APPLICANT INFORMATION:
BOUNDARY ROAD DEVELOPMENT INC.
16766 TRANSCANADIENNE, SUITE 500
KIRKLAND, QUÉBEC H9H 4M7

SCALE LKS/KA 0 5 10 15 20 HORIZONTAL ISSUED FOR SITE PLAN APPLICATION APR 12/18 ISSUED FOR FINAL COORDINATION APR 9/18 ISSUED FOR FINAL COORDINATION APR 2/18 0.5 1.0 1.5 2.0 KA/MF PRELIMINARY DESIGN PACKAGE MAR 16/18 VERTICAL DATE KA/MF REVISION





www.novatech-eng.com

Website

LOCATION
CITY OF OTTAWA
5371 BOUNDARY ROAD - YOW1

DRAWING NAME

STORMWATER MANAGEMENT

**FACILITY - SECTIONS** 

REV # 4
DRAWING No.

117217-SWMF2

1. COORDINATE AND SCHEDO

**GENERAL NOTES:** 

1. COORDINATE AND SCHEDULE ALL WORK WITH OTHER TRADES AND CONTRACTORS.

**KEY PLAN** 

N.T.S.

2. DETERMINE THE EXACT LOCATION, SIZE, MATERIAL AND ELEVATION OF ALL EXISTING UTILITIES PRIOR TO COMMENCING CONSTRUCTION. PROTECT AND ASSUME RESPONSIBILITY FOR ALL EXISTING UTILITIES WHETHER OR NOT SHOWN ON THIS DRAWING

3. OBTAIN ALL NECESSARY PERMITS AND APPROVALS FROM THE CITY OF OTTAWA BEFORE COMMENCING CONSTRUCTION.

4. BEFORE COMMENCING CONSTRUCTION OBTAIN AND PROVIDE PROOF OF COMPREHENSIVE, ALL RISK AND OPERATIONAL LIABILITY INSURANCE FOR \$2,000,000.00. INSURANCE POLICY TO NAME OWNERS, ENGINEERS AND ARCHITECTS AS CO-INSURED.

5. RESTORE ALL DISTURBED AREAS ON-SITE AND OFF-SITE, INCLUDING TRENCHES AND SURFACES ON PUBLIC ROAD ALLOWANCES TO EXISTING CONDITIONS OR BETTER TO THE SATISFACTION OF MUNICIPAL AUTHORITIES.

6. REMOVE FROM SITE ALL EXCESS EXCAVATED MATERIAL, ORGANIC MATERIAL AND DEBRIS UNLESS OTHERWISE INSTRUCTED BY ENGINEER. EXCAVATE AND REMOVE FROM SITE ANY CONTAMINATED MATERIAL. ALL CONTAMINATED MATERIAL SHALL BE DISPOSED OF AT A LICENSED LANDFILL FACILITY.

7. ALL ELEVATIONS ARE GEODETIC.

8. REFER TO GEOTECHNICAL INVESTIGATION REPORT NO. PG4366-1 (DATED FEBRUARY 9, 2018) PREPARED BY PATERSON GROUP INC. FOR SUBSURFACE CONDITIONS, CONSTRUCTION RECOMMENDATIONS AND GEOTECHNICAL INSPECTION REQUIREMENTS. THE GEOTECHNICAL CONSULTANT IS TO REVIEW ON-SITE CONDITIONS AFTER EXCAVATION PRIOR TO PLACEMENT OF THE GRANULAR MATERIAL.

9. REFER TO ARCHITECT'S AND LANDSCAPE ARCHITECT'S DRAWINGS FOR BUILDING AND HARD SURFACE AREAS AND DIMENSIONS.

10. REFER TO THE STORMWATER MANAGEMENT REPORT (R-2018-034) PREPARED BY NOVATECH.

11. SAW CUT AND KEYGRIND ASPHALT AT ALL ROAD CUTS AND ASPHALT TIE IN POINTS AS PER CITY OF OTTAWA STANDARDS (R10 AND R25).

## **SEWER NOTES:**

1. SUPPLY AND CONSTRUCT ALL SEWERS AND APPURTENANCES IN ACCORDANCE WITH THE MOST CURRENT CITY OF OTTAWA STANDARDS AND SPECIFICATIONS.

2. SPECIFICATIO

SPECIFICATIONS:		
<u>ITEM</u>	SPEC. No.	REFERENCE
SANITARY/STORM/CATCHBASIN MANHOLE (1200Ø)	701.010	OPSD
STORM MANHOLE (1500Ø)	701.011	OPSD
STORM MANHOLE (1800Ø)	701.012	OPSD
STORM MANHOLE (2400Ø)	701.013	OPSD
STORM/CATCHBASIN MH FRAME AND COVER	401.010 - TYPE 'B' OPEN	OPSD
CATCHBASIN (600x600)	705.010	OPSD
CATCHBASIN FRAME AND COVER	400.020	OPSD
STORM SEWER (750mmØ)	PVC DR 35	
STORM SEWER (864mm x 1346mm)	CONC. 65-D	
STORM SEWER (965mm x 1524mm)	CONC. 65-D	
SANITARY SEWER	PVC DR 35	
OFINED TRENCH REPRING (ORANIU ARIA)		

SEWER TRENCH - BEDDING (GRANULAR 'A')
COVER (GRANULAR 'A')

PIPE BEDDING, COVER AND BACKFILL ARE TO BE COMPACTED TO AT LEAST 95% OF THE STANDARD PROCTOR MAXIMUM DRY DENSITY. THE USE OF CLEAR CRUSHED STONE AS A BEDDING LAYER SHALL NOT BE PERMITTED.
 FLEXIBLE CONNECTIONS ARE REQUIRED FOR CONNECTING PIPES TO MANHOLES (FOR EXAMPLE KOR-N-SEAL, PSX: POSITIVE

SEAL AND DURASEAL). THE CONCRETE CRADLE FOR THE PIPE CAN BE ELIMINATED.

5. ALL STORM MANHOLES MANHOLES WITH PIPE SIZES LESS THAN 900mm ARE TO HAVE 300mm SUMPS UNLESS OTHERWISE

INDICATED. ALL STORM MANHOLES WITH PIPE SIZES 900mm AND LARGER ARE TO BE BENCHED.
6. CONTRACTOR TO TELEVISE ALL PROPOSED SEWERS 200mm OR GREATER IN DIAMETER TO ENSURE THAT THEY ARE CLEAN AND OPERATIONAL. UPON COMPLETION OF CONTRACT, THE CONTRACTOR IS RESPONSIBLE TO FLUSH AND CLEAN ALL SEWERS & APPURTENANCES. OBTAIN APPROVAL FROM THE CITY'S SEWER OPERATIONS. PROVIDE THE CCTV INSPECTION AND REPORT TO THE ENGINEER FOR REVIEW AND APPROVAL.

7. CONTRACTOR TO PROVIDE THE CONSULTANT WITH A GENERAL PLAN OF SERVICES INDICATING ALL APPLICABLE SERVICING AS-BUILT INFORMATION SHOWN ON THIS PLAN. AS-BUILT INFORMATION MUST INCLUDE: PIPE MATERIAL, SIZES, LENGTHS, SLOPES, INVERT AND T/G ELEVATIONS, STRUCTURE LOCATIONS AND ANY ALIGNMENT CHANGES, ETC.

8. THE OWNER SHALL REQUIRE THAT THE SITE SERVICING CONTRACTOR PERFORM FIELD TESTS FOR QUALITY CONTROL OF ALL SANITARY SEWERS. LEAKAGE TESTING SHALL BE COMPLETED IN ACCORDANCE WITH OPSS 410.07.16, 410.07.16.04 AND 407.07.24. DYE TESTING IS TO BE COMPLETED ON ALL SANITARY SERVICES TO CONFIRM PROPER CONNECTION TO THE SANITARY SEWER MAIN. THE FIELD TESTS SHALL BE PERFORMED IN THE PRESENCE OF A CERTIFIED PROFESSIONAL ENGINEER WHO SHALL SUBMIT A CERTIFIED COPY OF THE TEST RESULTS.

# GRADING NOTES:

1. ALL TOPSOIL, ORGANIC OR DELETERIOUS MATERIAL MUST BE ENTIRELY REMOVED FROM BENEATH THE PROPOSED BUILDING AND PAVED AREAS.

2. EXPOSED SUBGRADES IN PROPOSED PAVED AREAS SHOULD BE PROOF ROLLED WITH A LARGE STEEL DRUM ROLLER AND ANY SOFT AREAS EVIDENT FROM THE PROOF ROLLING SHOULD BE SUBEXCAVATED AND REPLACED WITH SUITABLE MATERIAL THAT IS FROST COMPATIBLE WITH THE EXISTING SOILS.

3. THE PAVEMENT GRANULAR BASE AND SUBBASE SHOULD BE PLACED IN MAXIMUM 300mm THICK LIFTS AND COMPACTED TO A MINIMUM OF 98% OF THE MATERIAL'S STANDARD PROCTOR MAXIMUM DRY DENSITY VALUE.

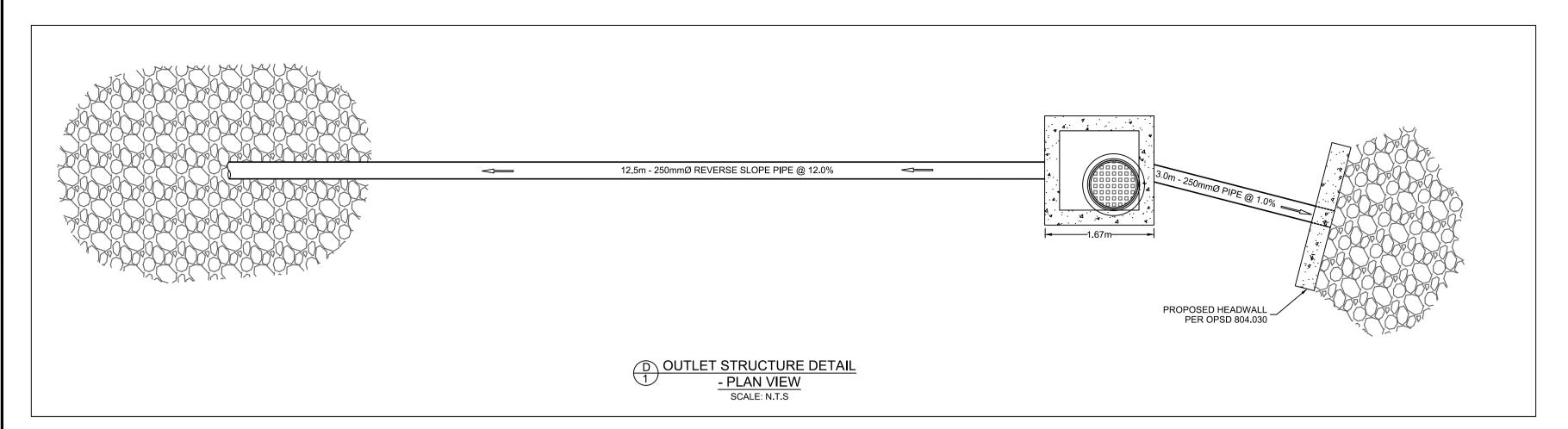
4. GRADE AND/OR FILL BEHIND PROPOSED CURB AND BETWEEN BUILDINGS AND CURBS, WHERE REQUIRED TO PROVIDE POSITIVE DRAINAGE.

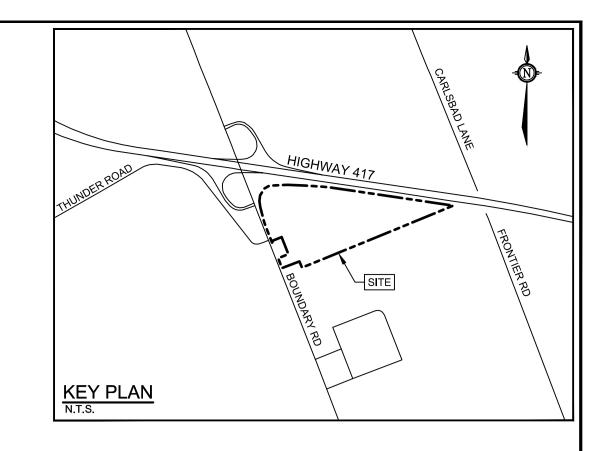
5. MINIMUM OF 2% GRADE FOR ALL GRASS AREAS UNLESS OTHERWISE NOTED.

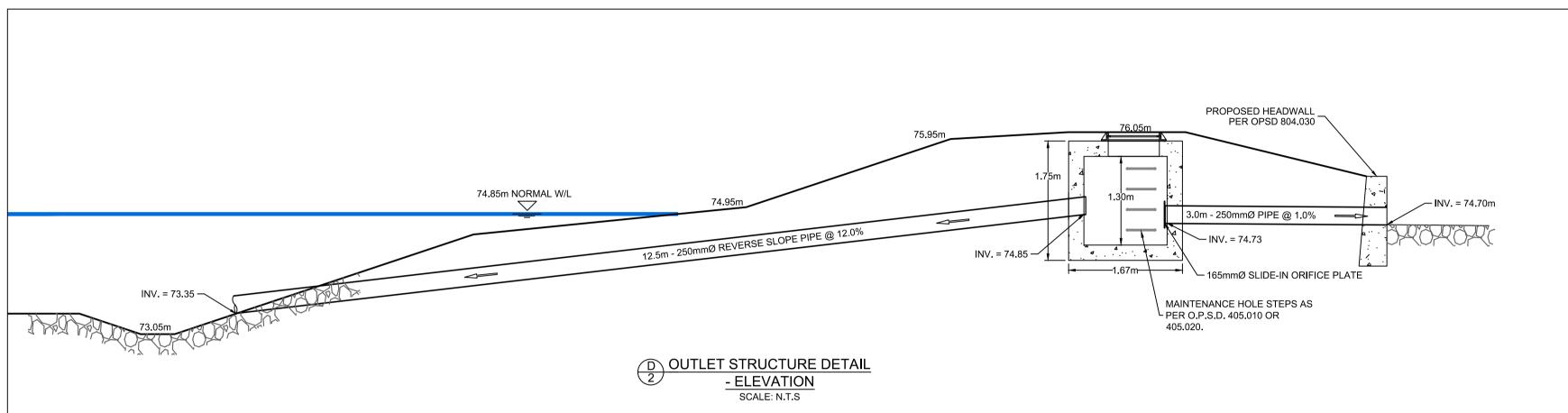
6. ALL GRADES BY CURBS ARE EDGE OF PAVEMENT GRADES UNLESS OTHERWISE INDICATED.

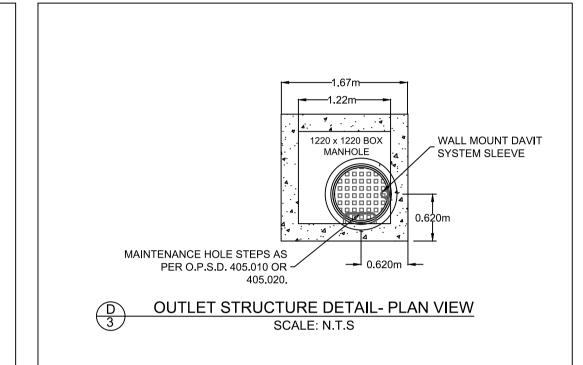
7. REFER TO LANDSCAPE PLAN FOR PLANTING AND OTHER LANDSCAPE FEATURE DETAILS.

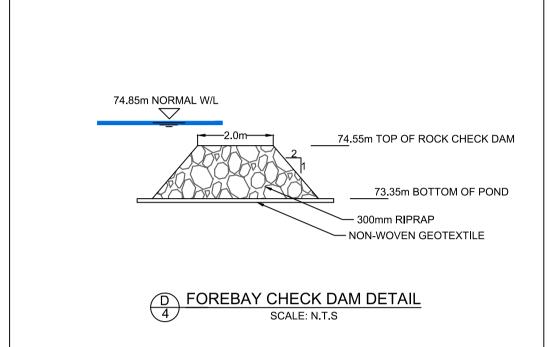
8. CONTRACTOR TO PROVIDE THE CONSULTANT WITH A GRADING PLAN INDICATING THE AS-BUILT ELEVATION OF EVERY DESIGN GRADE SHOWN ON THIS PLAN.

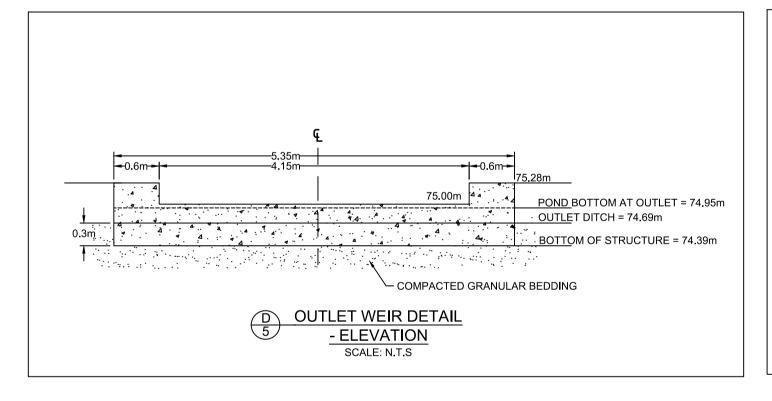


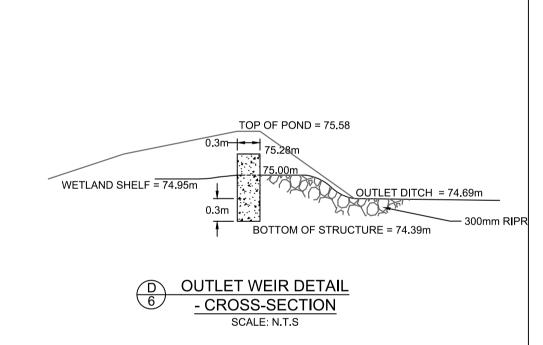


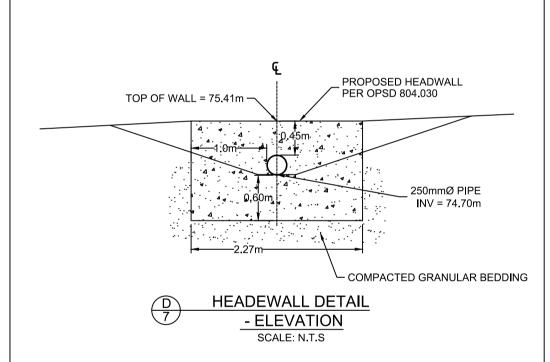


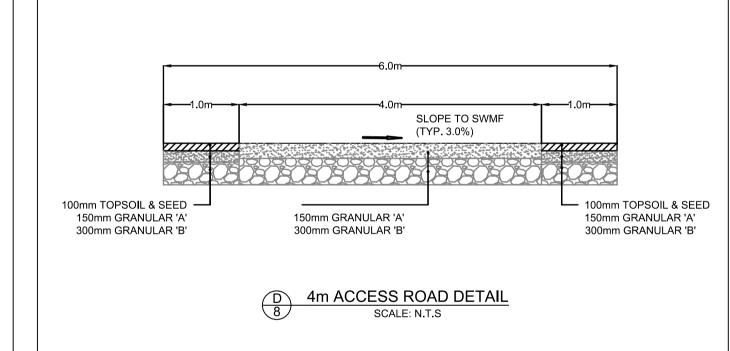


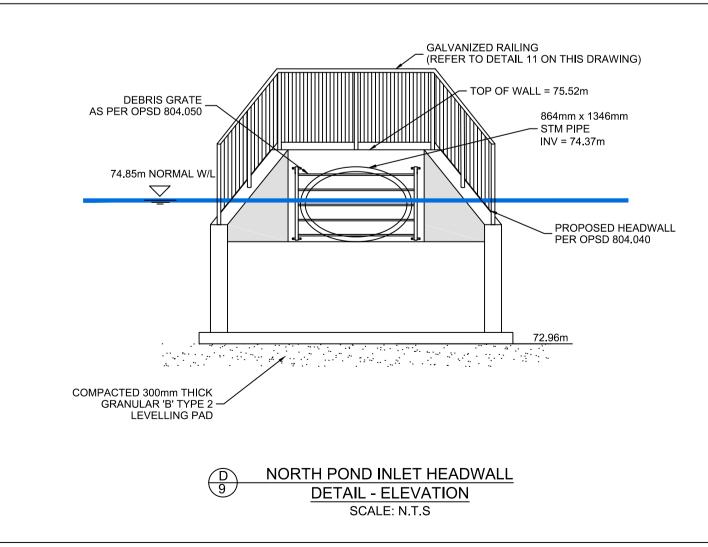


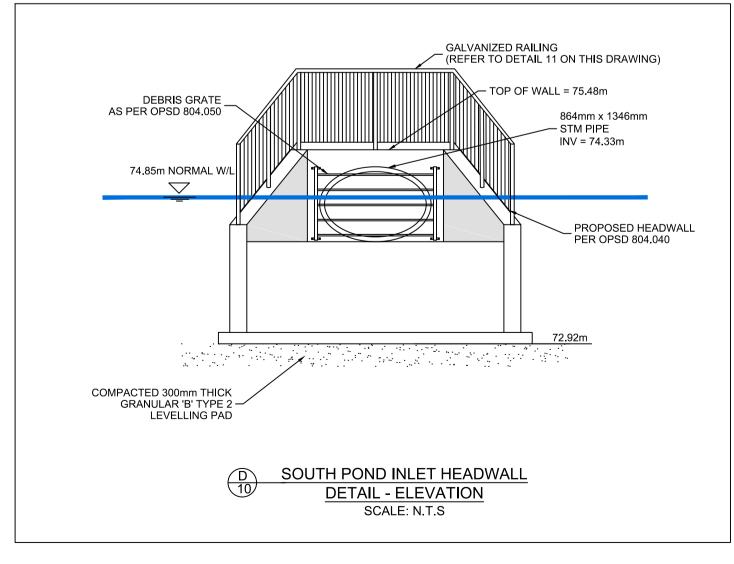


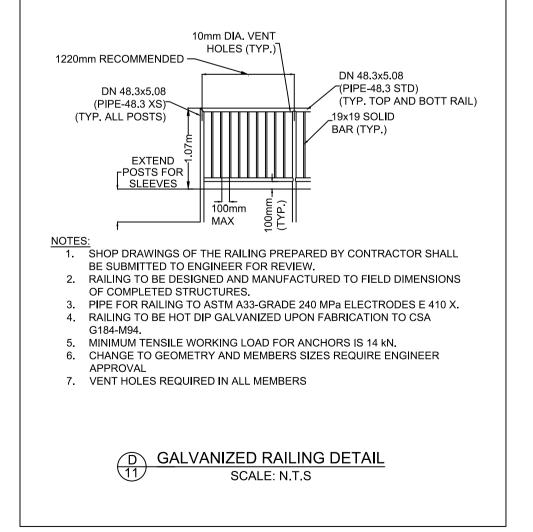












NOTE:
THE POSITION OF ALL POLE LINES, CONDUITS,
WATERMAINS, SEWERS AND OTHER
UNDERGROUND AND OVERGROUND UTILITIES AND
STRUCTURES IS NOT NECESSARILY SHOWN ON
THE CONTRACT DRAWINGS, AND WHERE SHOWN,
THE ACCURACY OF THE POSITION OF SUCH
UTILITIES AND STRUCTURES IS NOT GUARANTEED.
BEFORE STARTING WORK, DETERMINE THE EXACT
LOCATION OF ALL SUCH UTILITIES AND
STRUCTURES AND ASSUME ALL LIABILITY FOR
DAMAGE TO THEM.

OWNER/APPLICANT INFORMATION:
BOUNDARY ROAD DEVELOPMENT INC.
16766 TRANSCANADIENNE, SUITE 500
KIRKLAND, QUÉBEC H9H 4M7

				SCALE	DESIGN	
					LKS/KA	
					CHECKED	
				AS NOTED	MP	
	LOCUED FOR OUTE BLANKARDINGATION	10/10			DRAWN	
4.	ISSUED FOR SITE PLAN APPLICATION	APR 12/18	LKS		LKS	
3.	ISSUED FOR FINAL COORDINATION	APR 9/18	LKS		CHECKED	
2.	ISSUED FOR FINAL COORDINATION	APR 2/18	LKS		KA/MP	
1.	PRELIMINARY DESIGN PACKAGE	MAR 16/18	LKS		APPROVED	
No.	REVISION	DATE	BY		KA/MP	

FOR REVIEW ONLY

INDIVIDUAL
Engineers, Planners & Landscape Architects
Suite 200, 240 Michael Cowpland Drive
Ottawa, Ontario, Canada K2M 1P6

Telephone (613) 254-9643
Facsimile (613) 254-5867
Website www.novatech-eng.com

LOCATION
CITY OF OTTAWA
5371 BOUNDARY ROAD - YOW1

DRAWING NAME
STORMWATER MANAGEMENT
FACILITY - DETAILS

117217
REV REV # 4
DRAWING No.
117217-SWMF3