

Site Servicing & Stormwater Management Report

2465070 Ontario Ltd 2375 St-Laurent Blvd., Ottawa, ON

Prepared for:

Graebeck Construction Ltd. 160 Terence Matthews Crescent, Kanata, ON K2M 0B2

Attention: Mr. Evan Cory

LRL File No.: 130828 December 13, 2017

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1 Introduction

LRL Associates Ltd. (LRL) has been retained by Graebeck Construction Ltd. to prepare a site servicing and stormwater management report in support of their site plan control application for a proposed site development. This report presents the proposed servicing plan for the proposed development in regards to water and sanitary services, as well as stormwater management.

This report has been prepared in consideration of the survey carried out by Annis, O'Sullivan, Vollebekk Ltd. dated August 11th, 2017. Should there be any discrepancies in the existing infrastructure and/or connections to existing services, which may relate to site servicing considerations, LRL should be advised in order to review the report recommendations. This report should be read in conjunction with the Civil plans prepared by LRL.

2 SITE DESCRIPTION

The subject property is located within the suburban boundary of the City of Ottawa; Ward 10 Gloucester-Southgate, within the Greens Creek Study Area. The proposed development will be a motorsports warehouse, located at 2375 St-Laurent Blvd. The total area of the property is approximately 0.659 ha.

The proposed development is located in an industrial area bounded by other light industrial properties and a parks and open space zone to the south. The property is currently a virgin site.

The proposed development will include a two-storey warehouse/garage with office space. The total footprint area of the proposed main building is 930m². There will also be a future building addition of 1000m² which will be built at a later date. The service calculations take into account both the proposed building and the future expansion.

3 SCOPE OF WORK

As per applicable guidelines, the scope of work includes the following:

Water services

- Calculate the expected water supply demand at average and peak conditions.
- Calculate the fire flow as per the Fire Underwriter Survey (FUS) method.
- Describe the proposed water distribution network and connection to the existing system.

Sanitary services

- Describe the existing sanitary sewers available to receive wastewater from the building.
- Calculate peak allowable release flow rate for the subject site.
- Calculate peak actual release flow rate and compare to allowable release.
- Describe the proposed sanitary sewer system.

Stormwater management

- Calculate the allowable stormwater release rate.
- Calculate the anticipated post development stormwater release rates.
- Demonstrate how the target quality and quantity objectives will be achieved.
- Describe the proposed storm sewer system.

4 WATER SUPPLY AND FIRE PROTECTION

4.1 Existing Water Supply Services

An existing 300mm dia. watermain extending along St-Laurent Blvd. is present north of the subject property. From this watermain, a 200mm dia. water service extends into the subject site and is capped off just inside the property line at the northeast corner. There are two existing fire hydrants near the northeast and northwest corners of the property on St-Laurent Blvd. The subject site is located in Pressure Zone 2C. Please refer to Appendix H for the St-Laurent Blvd. As-Built Drawings.

4.2 Water Supply Demand

As per MOE and City of Ottawa Design Guidelines, the average water demand for the subject light industrial development was calculated. A daily and hourly peak factor of **1.5** and **1.8**, respectively were used. The average daily water demand for the site is **0.27L/s**, maximum daily is **0.40L/s**, and maximum hourly is **0.72L/s**. Please refer to Appendix A for the water demand calculation sheet.

The fire flow demand was estimated in accordance with the Fire Underwriters Survey (FUS). This method is based on the floor area of the building to be protected, type and combustibility of the structural frame and the separation distances with adjoining buildings. The fire flow demand was calculated to be **150.0L/s**. Please refer to Appendix A for the fire flow calculation sheet.

The City of Ottawa has provided boundary conditions to LRL Associates for this project. Please refer to Appendix I for boundary conditions. Using the provided HGLs, minimum, maximum and maximum day + fire pressures were calculated at the St-Laurent Blvd. connection. Head losses were then calculated from the connection to the proposed building for the maximum daily demand, maximum hourly demand and maximum daily demand + fire flow. For each of these scenarios, the relevant pressures were determined. Adequate water supply/pressure is available and meets the City of Ottawa standards as per section 4.2.2 of the Ottawa Design Guidelines – Water distribution. For the maximum daily demand, a minimum and maximum pressure of **60.89** and **69.57** psi were calculated; these land within the 50 to 80 psi MOE range.

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For the maximum hourly demand, a minimum and maximum pressure of **60.63** and **69.31** psi were calculated; these land within the 40 to 80 psi MOE range. For the maximum daily demand + fire flow, a pressure of **57.33** psi was calculated; this is above the minimum 20 psi MOE requirement. A pressure reducing valve is not required based on the above analysis. Please refer to Appendix A for pressure loss calculations.

Summa	ry Table
Average Water Demand Rate	23065 L/day
Factors	1.5(max daily) & 1.8(max hourly)
Average Day Demand (L/s)	0.27
Maximum Daily Demand (L/s)	0.40
Peak Hour Demand (L/s)	0.72
FUS Fire Flow Requirement (L/s)	150.0
Max Day+Fire Flow (L/s)	150.4

4.3 Water supply servicing design

The proposed building will be serviced by a new 50mm dia. HDPE "Gold Stripe" water service; to be installed 2.4m below grade. The proposed service will connect to the existing 200mm dia. service stubbed at the property line; located at the northeast corner of the site. One 200mm x 100mm reducer and one 100mm x 50mm reducer will be installed to allow for the proposed water service.

Fire flow protection is to be provided by the existing fire hydrants located near the northeast and northwest corners of the property on St-Laurent Blvd. The existing northwest hydrant is located 40m from the proposed building's front entrance.

5 SANITARY DRAINAGE

5.1 Existing Sanitary Sewer Services

An existing 300mm dia. sanitary sewer extending along St-Laurent Blvd. is present north of the subject property. Please refer to Appendix H for the St-Laurent Blvd. As-Built Drawings.

5.2 Sanitary Sewer Servicing Design

The new building, including the future addition, will be serviced with a new 150mm dia. sanitary service, which will connect to the existing 300mm dia. sanitary sewer on St-Laurent Blvd. A new monitoring manhole (SAN MH1) is to be installed along the proposed 150mm service; near the property line. The new proposed 150mm PVC sanitary service will be installed at a minimum slope of 1.0%, as per the City of Ottawa Sewer Design Guidelines.

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The parameters used to calculate the site's allowable sanitary flows are: Light Industrial average flow demand of 35,000 L/ha/day, an industrial peaking factor of 7.25 (as per Appendix 4-B of the Ottawa Sewer Design Guidelines) and an infiltration rate of 0.28 L/s/ha. Based on these parameters and the total site area of 0.659 ha, the total allowable sanitary flow was estimated to be **2.12 L/s**. Refer to Appendix B for the site's sanitary sewer design sheet.

As per Table 8.2.1.3.B of the Ontario Building Code, the site's anticipated sanitary flow is **3,700** L/day (0.04 L/s). The proposed building and future addition will have 2 water closets and 12 loading bays. Under the "Warehouse" item: 2 water closets x 950 L/day = 1900 L/day and 12 loading bays x 150 L/day = 1800 L/day; for a total of 3,700 L/day (0.04 L/s).

The site's anticipated sanitary flow is lower than its allowable flow. The proposed sanitary service has been sized to accommodate the peak allowable flow.

6 STORMWATER MANAGEMENT

6.1 Existing Stormwater Infrastructure

An existing 1200mm dia. storm sewer extending along St-Laurent Blvd. is present north of the subject property. Please refer to Appendix H for the St-Laurent Blvd. As-Built Drawings.

6.2 Stormwater management Concept

The information below should be read in conjunction with LRL drawings C401 and C701, as well as Appendix C (the stormwater management design sheets). The pervious and impervious runoff coefficients have been increased by 25% for the 100yr event; as per the Ottawa Sewer Design Guidelines.

The pre-development 5yr allowable release rate has been calculated using a C coefficient of 0.5 as per the City Pre-Application Consultation Memo, a calculated time of concentration of 36 minutes using the FAA/Rational Method, a calculated intensity of 47.2mm/hr as per City of Ottawa guidelines, and a total site area of 0.659ha. The allowable release rate was calculated to be **29.98L/s**.

The post-development conditions (100 year storm event) were designed using a restricted release flow of **43.22L/s** using Hydrovex Vertical Vortex Flow Regulator model 150VHV-2 to be installed in proposed CBMH5.

The 100year storm runoff from proposed catchment areas CA-01 to CA-06 will be controlled at proposed CBMH5. Runoff above the 100year will back out of all proposed CBMHs and pond around each drainage structure until it flows overland, making its way to St-Laurent Blvd. through the spill out point located at the northeast side of the entrance at the property line. Stormwater will not back up through the system and make its way out of CB1 (located at the bottom of the loading dock area) due to a proposed Armtec flap gate to be installed on the CB's

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south inlet. Stormwater from the 5yr storm event will always remain underground; it will never back up/out of the drainage structures and pond overland.

The 100yr storage required for this site is **219.82m3**. The 100yr storage provided is **222.41m3**. This is a combination of the overland ponding storage of 62.78m3 (refer to Appendix J for the Overland Ponding Volume Table), StormTech chambers storage of 133.00m3 (refer to Appendix E for StormTech System Design Sheets) and the underground pipes and drainage structures storage of 26.63m3. This storage capacity will be possible using a Hydrovex Vertical Vortex Flow Regulator model 150VHV-2 to be installed in proposed CBMH5 at an allowable release rate of **43.22L/s**. Refer to Appendix D for Hydrovex Vertical Vortex Flow Regulator Report.

6.3 Design Criteria

Stormwater quantity and quality control measures are taken into account for this site to reduce post development stormwater runoff to allowable levels.

6.3.1 Water Quality

The enhanced 80% TSS removals requirement will be met though the proposed Stormceptor STC 300 oil/grit separator which will provide adequate water quality treatment. Please refer to Appendix F for the Stormceptor Report. An isolator row has been incorporated into the StormTech system as well providing additional on-site quality treatment.

6.3.2 Water Quantity

All storm events up to and including the 100 year event will be controlled to the 5 year predevelopment level. The site's major overland flow route has been designed to ensure that storm events beyond the 100 year design storm can be safely conveyed overland towards the St-Laurent Blvd. right of way. The minor system (the on-site storm sewer system) is sized to convey the 5 year storm event flows from the site to the municipal storm sewer on St-Laurent Blvd.

6.4 Method of Analysis

The Rational Method was used to calculate the runoff from the development. The Intensity-Duration-Frequency (IDF) curve formulas of the MacDonald Cartier International Airport, City of Ottawa, were used to calculate the peak storm flows.

6.5 Allowable Release Rate

The pre-development 5yr allowable release rate has been calculated using a C coefficient of 0.5 as per the City Pre-Application Consultation Memo, a calculated time of concentration of 36

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minutes using the FAA/Rational Method, a calculated intensity of 47.2mm/hr as per City of Ottawa guidelines, and a total site area of 0.659ha.

7 EROSION AND SEDIMENT CONTROL

During construction, erosion and sediment controls will be provided primarily via a sediment control fence to be erected along the perimeter of the site where runoff has the potential of leaving the site. Inlet sediment control devices are also to be provided in any catchbasin and/or manhole in and around the site that may be impacted by the site construction. Construction and maintenance requirements for erosion and sediment controls are to comply with Ontario Provincial Standard Specification (OPSS) # 577. Refer to LRL drawing C.101 for erosion and sediment control details.

8 CONCLUSIONS

In accordance with the report objectives, the analyses of the proposed development can be summarized as follows:

Water Service

- The anticipated maximum domestic water demand of the site is 0.72L/s.
- The maximum required fire flow was calculated at 150.0L/s using the FUS method.
- There are two existing fire hydrants located near the northeast and northwest corners of the property on St-Laurent Blvd. within a 90m radius. The existing northwest hydrant is located 40m from the proposed building's front entrance.
- The new development will be serviced with by a new 150mm dia. water service connected to the existing 200mm dia. service stubbed at the property line; located at the northeast corner of the site.

Sanitary Service

- The total allowable sanitary flow was estimated to be 2.12 L/s.
- The site's anticipated sanitary flow is 0.04 L/s.
- The proposed building will be serviced by a new 150mm sanitary service which will be connected to the existing 300mm dia. sanitary sewer on St-Laurent Blvd.
- A new monitoring manhole will be installed on the proposed 150mm sanitary service.

Stormwater Management

- The proposed storm system's 100yr post-development release rate of 43.22 L/s will meet the 5yr pre-development allowable release rate of 43.22 L/s.
- Stormwater quantity control objectives will be met through on-site stormwater storage.

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• Stormwater quality control objectives will be met on-site through the use of a Stormceptor STC 300 oil/grit separator. An isolator row has been incorporated into the StormTech system as well providing additional on-site quality treatment.

9 LIMITATIONS AND USE OF REPORT

The report conclusions are applicable only to the project described in the report. Any changes require a review by LRL Associates Ltd. to insure compatibility with the recommendations contained in this report. We trust the information presented in this report meets City of Ottawa requirements. Please do not hesitate to contact us should you have any questions or concerns.

Prepared by:

LRL Associates Ltd.

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APPENDIX A

Water Demand and Fire Flow Calculations



Water Service Calculations

LRL File No.: 170721

Project: 2465070 Ontario Ltd

Date: December 13, 2017

Designed by: Guillaume Courtois

Water Demand

Total site area:

0.659 ha

 $Q_{average} = 35$ $m^3 / ha \cdot day$ (As per MOE guidelines) $Q_{average} = 23.065$ m^3 / day $Q_{average} = 23065$ L / day $Q_{average} = 0.27$ L / s

Maximum daily peak factor: 1.5

Maximum daily demand = 34598 L / day

0.40 L/s

Maximum hour peak factor: 1.8

Maximum hour demand = 62276 L / day

= 0.72 L/s

Water Service Pipe Sizing

Q = VA Where: V = velocity

A = area of watermain pipe Q = water supply flow rate

By deriving the above formula, we can obtain the diameter of the pipe:

Minimum pipe diameter: $d = (4Q/\pi V)^{1/2}$

d = 0.023 m d = 23 mm

Proposed pipe diameter: 50 mm (I.D. = 41mm)



Fire Flow Calculations

LRL File No. : 170721

Project: 2465070 Ontario Ltd

Date: December 13, 2017

Method: Fire Underwriters Survey (FUS)

Designed by: Guillaume Courtois

Step	Task	Term	Options	Multiplier	Choose:	Value	unit	Fire Flow		
			Structural Framing M	aterial						
			Wood Frame	1.5						
	Choose frame used for	Coefficient C	Ordinary Construction	1.0						
1	building	related to the type of	Non-combustible construction	0.8	Non-combustible construction	0.8				
	Dallaling	construction	Fire resistive construction <2 hrs	0.7						
			Fire resistive construction >2 hrs	0.6						
Floor Space Area										
			Single family dwelling	0						
2	Choose type of housing	Type of housing	Townhouse - no. of units	0	Building - no. of units per floor	1	unit(s)			
			Building - no. of units per floor	1						
3	Enter area of a unit	Enter floor space area of	f one unit (excluding basement)	1	1930.0		sq.m.			
4	Obtain fire flow before	Required fire flow	Et a Ela	w = 220 x C x	L/min	8,000				
4	reductions	Required life flow	Fire Fig	W = 220 X C X	Area ⁿ		L/s	133.3		
Reductions or surcharge due to factors affecting burning										
	Choose combustibility of contents		Non-combustible	-0.25						
		Occupancy hazard	Limited combustible	-0.15						
5		reduction or surcharge	Combustible	0	Combustible	0				
		Toduction of suronarge	Free burning	0.15			L/min	8,000		
			Rapid burning	0.25			L/s	133.3		
			Sprinklers (NFPA13)	-0.30	False	0				
6	Choose reduction for sprinklers	Sprinkler reduction	Water supply is standard for both the system and fire department hose lines	-0.10	False	0	L/min	8,000		
			Fully supervised system	-0.10	False	0	L/s	133.3		
			North side	Over 45m	0					
7	Change congration	Exposure distance	East side	10.1 to 20m	0.15					
7	Choose separation	between units	South side	Over 45m	0		L/min	9,000		
			West side	Over 45m	0	0.15	L/s	150.0		
			Net required fire fl	ow						
	Obtain fire flow,			Minimum	required fire flow rate (rounded to ne	arest 1000)	L/min	9,000		
8	duration, and volume				Minimum required f	ire flow rate	L/s	150.0		
	daration, and volume				Required duration	of fire flow	hr	2		

Note: The above calculations take into account both the current proposed building of 930m² and the future proposed building of 1000m².



Pipe Pressure Losses Calculations

LRL File No.: 170721

Project: 2465070 Ontario Ltd

Date: December 13, 2017

Designed: Guillaume Courtois

Piezometric Head Equation (Derived from Bernoulli's Equation)

$$h = \frac{p}{\gamma} + z$$

Where:

 $_{h\,=\,}\,\text{HGL (m)}$

p = Pressure (Pa)

 γ_{\pm} Specific weight (N/m3) =

9810

 $_{\rm Z}=$ Elevation of centreline of pipe (m) =

80.91

Water Pressure at St-Laurent Blvd. Connection									
HCI (m)		Pres	ssure						
HGL (m)		kPa	psi						
Minimum =	124.5	427.62	62.02						
Maximum =	130.6	487.46	70.70						
Max. Day + Fire =	124	422.71	61.31						

Hazen Williams Equation

$$h_f = \frac{10.67 \times Q^{1.95} \times L}{C^{1.95} \times d^{4.97}}$$

Where:

 h_f = Head loss over the length of pipe (m)

Q = Volumetric flow rate (m³/s)

L = Length of pipe (m)

C = Pipe roughness coefficient

d = Pipe diameter (m)

Scenario 1: maximum daily demand

Q (L/s)	0.40	
C (= 0)	150	
L (m.)	31.5	
I.D. (mm)	41	
V (m/s)	0.30	
h _f (m)	0.09	
Head Loss (psi)	0.13	
Min. Pressure (psi)	61.89	
Max. Pressure (psi)	70.57	
Service Obv. @ Street Connection (m)	81.10	
Service Obv. @ Building Connection (m)	81.80	
Pressure Adjustment (psi)	-1.00	(due to service elevation difference from street to building)
Adjusted Min. Pressure (psi)	60.89	(must not be less than 50psi)
Adjusted Max. Pressure (psi)	69.57	(must not be more than 80psi)

Scenario 2: maximum hourly demand

Q (L/s)	0.72	1
C	150	1
L (m.)	31.5	1
I.D. (mm)	41	
V (m/s)	0.55	-
h _f (m)	0.28	
Head Loss (psi)	0.39	
Min. Pressure (psi)	61.63	
Max. Pressure (psi)	70.31	
Service Obv. @ Street Connection (m)	81.10	
Service Obv. @ Building Connection (m)	81.80	
Pressure Adjustment (psi)	-1.00	(due to service elevation difference from street to building)
Adjusted Min. Pressure (psi)	60.63	(must not be less than 40psi)
Adjusted Max. Pressure (psi)	69.31	(must not be more than 80psi)

Scenario 3: maximum daily demand + fire flow (from street connection to hydrant at northwest of site)

Q (L/s)	150.40	
C	150	
L (m.)	9.3	
I.D. (mm)	155	
V (m/s)	7.97	
h _f (m)	2.47	
Head Loss (psi)	3.51	
Pressure (psi)	57.80	_
Service Obv. @ Street Connection (m)	81.12	
Service Obv. @ Hydrant Connection (m)	81.45	
Pressure Adjustment (psi)	-0.47	(due to service elevation difference from street to hydrant)
Adjusted Pressure (psi)	57.33	(must not be less than 20psi)

APPENDIX B

Sanitary Sewer Calculation Sheet



LRL File No. 170721

Project: 2465070 Ontario Ltd Location: 2375 St-Laurent Blvd., Ottawa, ON

Date: December 13, 2017

Sanitary Design Parameters

Industrial Peak Factor = as per Appendix 4-B = 7.25 Extraneous Flow = 0.28 L/s/gross ha Pipe Design Parameters

Minimum Velocity = 0.60 m/s Manning's n = 0.013

	LOCATION			RESIDEN	ITIAL AREA	AND POPU	JLATION		COMM	ERCIAL	11	NDUSTRI <i>A</i>	\L	INSTITU	JTIONAL	C+I+I	IN	IFILTRATIO	ON	TOTAL				PIPE				MAN	HOLE
CATCHMENT / STREET	FROM MH	то мн	AREA (Ha)	POP.	AREA (Ha)	POP.	PEAK FACT.	PEAK FLOW (I/s)	AREA (Ha)	ACCU. AREA (Ha)	AREA (Ha)	ACCU. AREA (Ha)	PEAK FACT.	AREA (Ha)	ACCU. AREA (Ha)	PEAK FLOW (l/s)	TOTAL AREA (Ha)	ACCU. AREA (Ha)	INFILT. FLOW (l/s)	FLOW (I/s)	LENGTH (m)	DIA. (mm)	SLOPE (%)	MATERAIL	CAP. (FULL) (I/s)	VEL. (FULL) (m/s)	Ratio (Q/Q _{FULL})		DOWN INVERT (m)
Site	Blda	MH01	0.000	0.0	0.0	0.0	4.0	0.00	0.000	0.000	0.659	0.659	7.25	0.0	0.0	1.94	0.659	0.659	0.18	2.12	18.3	150	1.00%	PVC	15.23	0.86	0.14		
	MH01	TRUNK	0.000	0.0	0.0	0.0	4.0	0.00	0.000	0.000	0.000	0.659	7.25	0.0	0.0	1.94	0.000	0.659	0.18	2.12	16.8	150	1.00%	PVC	15.23	0.86	0.14		
	Existing inverts	and slopes a	re estimate	ed. They are		NOTES med on-site								Designed: PROJECT: G.C. 2465070 Ontario Ltd						-									
										Checked: LOCATION: G.C. 2375 St-Laurent Blvd., Ottawa, ON																			
						Dwg. Ref	erence: C.401		File Ref.:	170	721		Date:	Decemb	er 13, 201	7			Sheet No. 1 of 1		ļ								

Average Daily Flow = 350 L/p/day Commercial & Institutional Flow = 50000 L/ha/day

Light Industrial Flow = 35000 L/ha/day

Heavy Industrial Flow = 55000 L/ha/day
Maximum Residential Peak Factor = 4.0
Commercial & Institutional Peak Factor = 1.5

APPENDIX C

Stormwater Management Design Sheets

LRL Associates Ltd.

Storm Design Sheet



LRL File No. 170721

Project: 2465070 Ontario Ltd

Location: 2375 St-Laurent, Ottawa, ON

Date: 13 Dec 2017

Designed: Guillaume Courtois

Drawing Reference: C701

		Post-devel	opment Cate	chments	
CATCHMENT	Grass C=0.20	Gravel C=0.80	Bldg. / Asph. / Conc. C=0.90	Total Area (ha)	Combined C
CA-01	0.054	0.000	0.303	0.357	0.79
CA-02	0.000	0.000	0.012	0.012	0.90
CA-03	0.007	0.000	0.097	0.104	0.85
CA-04	0.019	0.000	0.034	0.053	0.65
CA-05	0.021	0.000	0.058	0.079	0.71
CA-06	0.010	0.000	0.044	0.054	0.77



LRL File No. 170721

Project: 2465070 Ontario Ltd **Location:** 2375 St-Laurent, Ottawa, ON

Date: 13 Dec 2017

Designed: Guillaume Courtois

Drawing Ref.: C701

Stormwater Management Design Sheet

Allowable Release Rate (5 Year Pre-development)

Time of Concentration:

Tc= G(1.1 - c)L^{0.5} / (100 x S)^{1/3} as per FAA/Rational Method Equation

where: c = 0.5 Runoff Coefficient as per City pre-consultation application memo

G = 3.26 Constant

L = 137.65 Longest watercourse length (in meters) in watershed

S = 0.0025 Average slope of watercouse

Tc = 36 min

Intensity:

 $I_5 = 998.071 / (Tc + 6.053)^{0.814}$ as per City of Ottawa Guidelines

where: Tc = 36 Time of Concentration in min.

I₅ = 47.2 mm/hr

Allowable Release:

Q = 2.78 x C x I x A

where: C = 0.5 Runoff Coefficient as per City pre-consultation application memo

I = 47.2 mm/hr

Tc = 36 min Total Site Area = 0.659 ha

 $Q = \frac{43.22}{\text{L/s}}$

Catchment Area and Runoff Coeffecient (Post-development)

	Individual Watersheds	Total Area (ha)	Grass Area (ha)	Gravel Area (ha)	Bldg. / Asph. / Conc. Area (ha)	∑C * A	C weighted (1:5 yr)	C weighted (1:100 yr)
	CA-1	0.357	0.054	0.000	0.303	0.284	0.79	0.99
	CA-2	0.012	0.000	0.000	0.012	0.011	0.90	1.00
Controlled	CA-3	0.104	0.007	0.000	0.097	0.089	0.85	1.00
Contr	CA-4	0.053	0.019	0.000	0.034	0.034	0.65	0.81
	CA-5	0.079	0.021	0.000	0.058	0.056	0.71	0.89
	CA-6	0.054	0.010	0.000	0.044	0.042	0.77	0.96

					1:5 YEAR	1:100 YEAR
	Total Site Area =	0.659	ha	ΣC=	0.78	0.98
	Bldg. / Asph. / Conc. Area =	0.548	ha	C=	0.90	1.00
Controlled	Gravel Area =	0.000	ha	C=	0.80	1.00
Cont	Grass Area =	0.111	ha	C=	0.20	0.25
	Total Controlled =	0.659	ha	Σc=	0.78	0.98



LRL File No. 170721

Project: 2465070 Ontario Ltd **Location:** 2375 St-Laurent, Ottawa, ON

Date: 13 Dec 2017

Designed: Guillaume Courtois

Drawing Ref.: C701

Stormwater Management Design Sheet

Post-development Stormwater Management

5 Year Post-development:

 $I_5 = 998.071 / (Tc + 6.053)^{0.814}$

as per City of Ottawa Guidelines

where: I = intensity in mm/hr
Tc = Time of Concentration

	1:5 YEAR STORM EVENT												
Time	Intensity	Peak Flow	Release Rate	Storage Rate	Storage								
(min)	(mm/hr)	(L/s)	(L/s)	(L/s)	Volume (m ³)								
10	104.2	149.29	43.22	106.07	63.64								
15	83.6	119.72	43.22	76.50	68.85								
20	70.3	100.66	43.22	57.43	68.92								
25	60.9	87.25	43.22	44.03	66.05								
30	53.9	77.27	43.22	34.05	61.28								
35	48.5	69.52	43.22	26.29	55.22								
40	44.2	63.31	43.22	20.09	48.21								
45	40.6	58.21	43.22	14.99	40.48								
50	37.7	53.95	43.22	10.73	32.18								
55	35.1	50.33	43.22	7.10	23.44								
60	32.9	47.20	43.22	3.98	14.33								

100 Year Post-development:

Intensity:

 $I_{100} = 1735.688 / (Tc + 6.014)^{0.820}$

as per City of Ottawa Guidelines

where: I = intensity in mm/hr
Tc = Time of Concentration

		1:100 YE	AR STORM EVENT		
Time	Intensity	Peak Flow	Release Rate	Storage Rate	Storage
(min)	(mm/hr)	(L/s)	(L/s)	(L/s)	Volume (m ³)
10	178.6	319.80	43.22	276.58	165.95
15	142.9	255.93	43.22	212.70	191.43
20	120.0	214.83	43.22	171.61	205.93
25	103.8	185.99	43.22	142.77	214.15
30	91.9	164.54	43.22	121.32	218.37
35	82.6	147.90	43.22	104.68	219.82
40	75.1	134.59	43.22	91.36	219.27
45	69.1	123.67	43.22	80.45	217.21
50	64.0	114.54	43.22	71.32	213.96
55	59.6	106.79	43.22	63.57	209.76
60	55.9	100.11	43.22	56.89	204.79

Onsite Stormwater Retention

Total Storage Required =	219.82 m ³	
Overland Ponding Storage =	62.78 m ³	refer to LRL Plan C601
Pipe Storage =	11.61 m ³	
Drainage Structures Storage =	15.02 m ³	
Stormtech Chambers Storage =	133.00 m ³	refer to LRL Plan C902
Total Available Storage =	222.41 m ³	
Supplementary Storage Required =	0.00 m ³	

LRL Associates Ltd. Storm Design Sheet

LRL File No. 170721

2465070 Ontario Ltd Project:

Location: 2375 St-Laurent, Ottawa, ON Date:

13 Dec 2017 Designed: Guillaume Courtois

Drawing Reference: C701

Storm Design Parameters Rational Method Q = 2.78CIA

Q = Peak flow in litres per second (L/s) Runoff Coefficient (C) IDF Curve Ottawa Macdonald-Cartier International Airport

A = Drainage area in hectares (ha) 0.2 Grass Storm Event 5 years C = Runoff coefficient Gravel 8.0 Formula

 $I = a / (T_c + b)^c$

I = Rainfall intensity (mm/hr) Bldg. / Asph. / Conc. 0.9 a = 998.07 6.053 c = 0.814 b =

Minimum velocity = 0.80 m/s Maximum velocity = 3.00 m/s Manning's Coeff. "n" = 0.013

Pipe Design Parameters

	LOCATION		,	AREA (ha	1)				FLOW						5	STORM SE	WER							MANHO	DLE			WAT	ERSHED		AVAILABL	STORAGE	=
CATCHMENT / STREET	From Structure	To Structure		Gravel C=0.80			Accum. 2.78AC	Time of Conc. (min.)	Rainfall Intensity (mm/hr)	Peak Flow Q (L/s)	ICD Controlled Flow Q (L/s)	Pipe Diameter (mm)	Туре	Slope (%)		Capacity Full (L/s)	Spare Capacity (L/s)	Velocity Full (m/s)	Time of Flow (min.)	Ratio (Q/Q _{FULL})	Up Invert (m)	l -	T/G Up Stream (m)	T/G Down Stream (m)	Up Depth obv (m)	Down Depth obv (m)	Up Depth inv (m)	Total Area (ha)	Combined C	Pipe Storage (m³)	Upstream CB/MH Size (m)	Water Depth (m)	CB/MH Storage (m³)
CA-01	CBMH1	CBMH2	0.054	0.000	0.303	0.79	0.79	36.43	47.2	37.19		300	PVC	0.34%	45.0	56.39	19.20	0.80	0.94	0.66	80.95	80.80	83.25	83.30	2.00	2.20	2.30	0.357	0.79	3.18	1.20	2.30	2.60
CA-02	CB1	CBMH2	0.000	0.000	0.012	0.03	0.03	36.43	47.2	1.42		200	PVC	1.00%	16.0	32.80	31.38	1.04	0.26	0.04	81.03	80.87	82.93	83.30	1.70	2.23	1.90	0.012	0.90	0.50	0.60	1.90	0.68
CA-03	CBMH2	CBMH5	0.007	0.000	0.097	0.25	1.06	37.37	46.4	49.35		300	PVC	1.19%	28.5	105.49	56.14	1.49	0.32	0.47	80.77	80.43	83.30	83.30	2.23	2.57	2.53	0.104	0.85	2.01	1.20	2.53	2.86
CA-04	CBMH3	CBMH4	0.019	0.000	0.034	0.10	0.10	36.43	47.2	4.51		300	PVC	0.34%	63.2	56.39	51.87	0.80	1.32	0.08	80.95	80.74	83.25	83.30	2.00	2.26	2.30	0.053	0.65	4.47	1.20	2.30	2.60
CA-05	CBMH4	CBMH5	0.021	0.000	0.058	0.16	0.25	37.75	46.0	11.62		300	PVC	1.23%	20.4	107.25	95.63	1.52	0.22	0.11	80.68	80.43	83.30	83.30	2.32	2.57	2.62	0.079	0.71	1.44	1.20	2.62	2.96
CA-06	CBMH5	STC300	0.010	0.000	0.044	0.12	1.43	37.97	45.8	65.67	43.22	300	PVC	4.00%	5.0	193.40	150.18	2.74	0.03	0.22	80.37	80.17	83.30	83.54	2.63	3.07	2.93	0.054	0.77	N/A	1.20	2.93	3.31
	STC300	EX. MH	0.000	0.000	0.000	0.00	1.43	38.00	45.8	65.63	43.22	300	PVC	0.34%	16.3	56.39	13.16	0.80	0.34	0.77	80.10	80.04	83.54	83.37	3.14	3.03	3.44	N/A	N/A	N/A	N/A	N/A	N/A

11.61

15.02

HWL	83.47
Total Storage	26.63

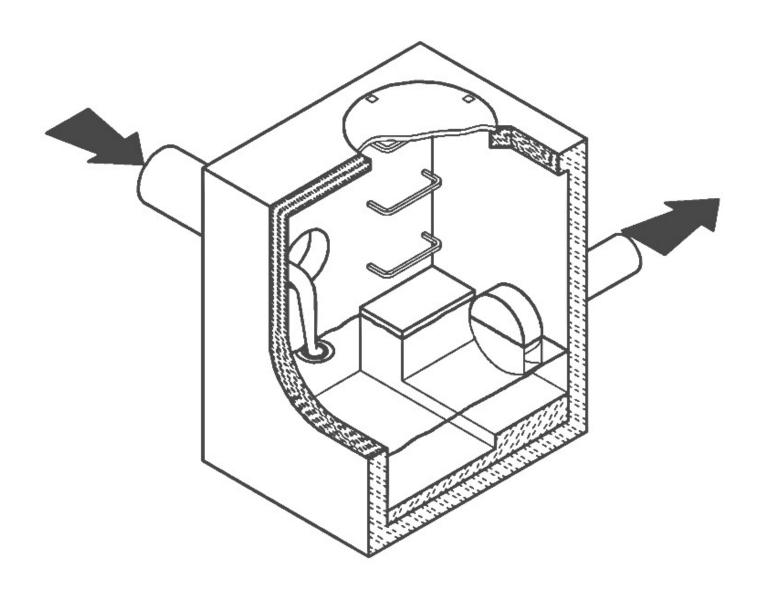
APPENDIX D

Hydrovex Vertical Vortex Flow Regulator Report

CSO/STORMWATER MANAGEMENT



• HYDROVEX® VHV / SVHV Vertical Vortex Flow Regulator



JOHN MEUNIER

HYDROVEX® VHV / SVHV VERTICAL VORTEX FLOW REGULATOR

APPLICATIONS

One of the major problems of urban wet weather flow management is the runoff generated after a heavy rainfall. During a storm, uncontrolled flows may overload the drainage system and cause flooding. Due to increased velocities, sewer pipe wear is increased dramatically and results in network deterioration. In a combined sewer system, the wastewater treatment plant may also experience significant increases in flows during storms, thereby losing its treatment efficiency.

A simple means of controlling excessive water runoff is by controlling excessive flows at their origin (manholes). **John Meunier Inc.** manufactures the **HYDROVEX**[®] **VHV** / **SVHV** line of vortex flow regulators to control stormwater flows in sewer networks, as well as manholes.

The vortex flow regulator design is based on the fluid mechanics principle of the forced vortex. This grants flow regulation without any moving parts, thus reducing maintenance. The operation of the regulator, depending on the upstream head and discharge, switches between orifice flow (gravity flow) and vortex flow. Although the concept is quite simple, over 12 years of research have been carried out in order to get a high performance.

The HYDROVEX® VHV / SVHV Vertical Vortex Flow Regulators (refer to Figure 1) are manufactured entirely of stainless steel, and consist of a hollow body (1) (in which flow control takes place) and an outlet orifice (7). Two rubber "O" rings (3) seal and retain the unit inside the outlet pipe. Two stainless steel retaining rings (4) are welded on the outlet sleeve to ensure that there is no shifting of the "O" rings during installation and use.

- 1. BODY
- 2. SLEEVE
- 3. O-RING
- RETAINING RINGS (SQUARE BAR)
- 5. ANCHOR PLATE
- 6. INLET
- 7. OUTLET ORIFICE

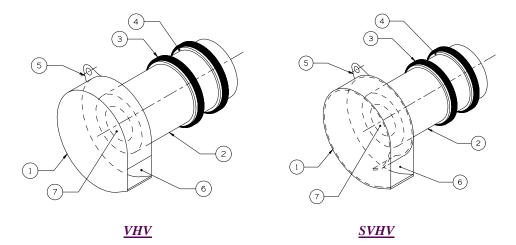


FIGURE 1: HYDROVEX® VHV-SVHV VERTICAL VORTREX FLOW REGULATORS

ADVANTAGES

- The **HYDROVEX**® **VHV** / **SVHV** line of flow regulators are manufactured entirely of stainless steel, making them durable and corrosion resistant.
- Having no moving parts, they require minimal maintenance.
- The geometry of the HYDROVEX® VHV / SVHV flow regulators allows a control equal to an orifice plate, having a cross section area 4 to 6 times smaller. This decreases the chance of blockage of the regulator, due to sediments and debris found in stormwater flows. Figure 2 illustrates the comparison between a regulator model 100 SVHV-2 and an equivalent orifice plate. One can see that for the same height of water, the regulator controls a flow approximately four times smaller than an equivalent orifice plate.
- Installation of the **HYDROVEX**® **VHV** / **SVHV** flow regulators is quick and straightforward and is performed after all civil works are completed.
- Installation requires no special tools or equipment and may be carried out by any contractor.
- Installation may be carried out in existing structures.

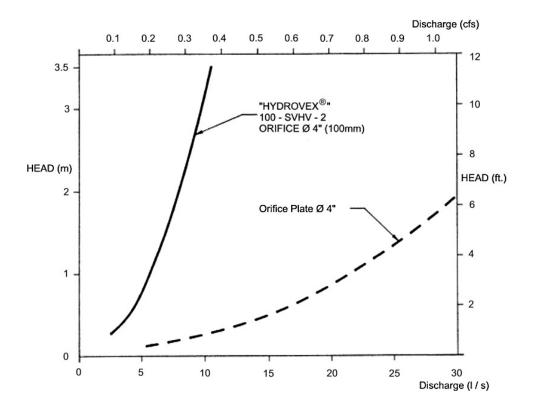


FIGURE 2: DISCHARGE CURVE SHOWING A HYDROVEX® FLOW REGULATOR VS AN ORIFICE PLATE

SELECTION

Selection of a **VHV or SVHV** regulator can be easily made using the selection charts found at the back of this brochure (see **Figure 3**). These charts are a graphical representation of the maximum upstream water pressure (head) and the maximum discharge at the manhole outlet. The maximum design head is the difference between the maximum upstream water level and the invert of the outlet pipe. All selections should be verified by John Meunier Inc. personnel prior to fabrication.

Example:

✓ Maximum design head 2m (6.56 ft.) ✓ Maximum discharge 6 L/s (0.2 cfs)

✓ Using **Figure 3** - VHV model required is a **75 VHV-1**

INSTALLATION REQUIREMENTS

All HYDROVEX® VHV / SVHV flow regulators can be installed in circular or square manholes. Figure 4 gives the various minimum dimensions required for a given regulator. It is imperative to respect the minimum clearances shown to ensure easy installation and proper functioning of the regulator.

SPECIFICATIONS

In order to specify a **HYDROVEX**® regulator, the following parameters must be defined:

- The model number (ex: 75-VHV-1)
- The diameter and type of outlet pipe (ex: 6" diam. SDR 35)
- The desired discharge (ex: 6 l/s or 0.21 CFS)
- The upstream head (ex: 2 m or 6.56 ft.) *
- The manhole diameter (ex: 36" diam.)
- The minimum clearance "H" (ex: 10 inches)
- The material type (ex: 304 s/s, 11 Ga. standard)
- * Upstream head is defined as the difference in elevation between the maximum upstream water level and the invert of the outlet pipe where the HYDROVEX® flow regulator is to be installed.

PLEASE NOTE THAT WHEN REQUESTING A PROPOSAL, WE SIMPLY REQUIRE THAT YOU PROVIDE US WITH THE FOLLOWING:

- project design flow rate
- pressure head
- > chamber's outlet pipe diameter and type



Typical VHV model in factory



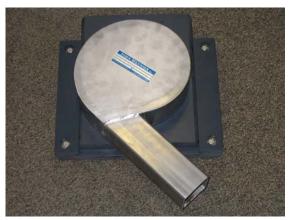
FV – SVHV (mounted on sliding plate)



VHV-1-O (standard model with odour control inlet)



VHV with Gooseneck assembly in existing chamber without minimum release at the bottom



FV – VHV-O (mounted on sliding plate with odour control inlet)



VHV with air vent for minimal slopes



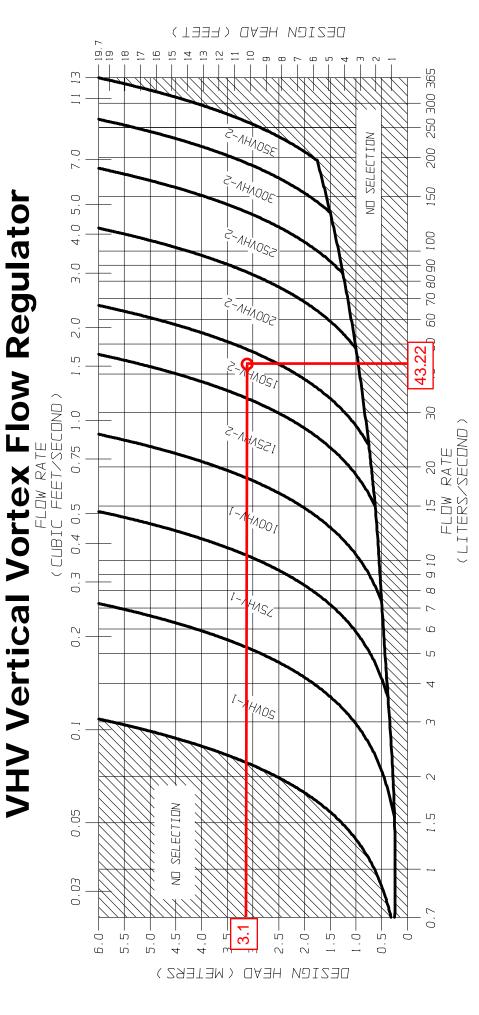
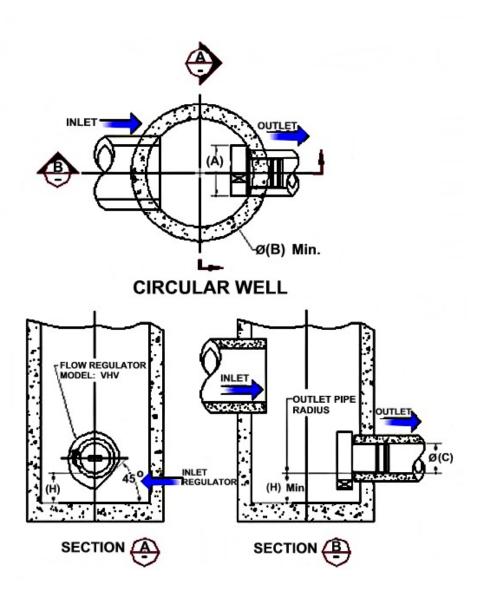


FIGURE 3 - VHV

JOHN MEUNIER

FLOW REGULATOR TYPICAL INSTALLATION IN CIRCULAR MANHOLE FIGURE 4 (MODEL VHV)

Model Number		ulator neter		Manhole neter		n Outlet ameter	Minimum Clearance			
	A (mm)	A (in.)	B (mm)	B (in.)	C (mm)	C (in.)	H (mm)	H (in.)		
50VHV-1	150	6	600	24	150	6	150	6		
75VHV-1	250	10	600	24	150	6	150	6		
100VHV-1	325	13	900	36	150	6	200	8		
125VHV-2	275	11	900	36	150	6	200	8		
150VHV-2	350	14	900	36	150	6	225	9		
200VHV-2	450	18	1200	48	200	8	300	12		
250VHV-2	575	23	1200	48	250	10	350	14		
300VHV-2	675	27	1600	64	250	10	400	16		
350VHV-2	800	32	1800	72	300	12	500	20		



INSTALLATION

The installation of a HYDROVEX® regulator may be undertaken once the manhole and piping is in place. Installation consists of simply fitting the regulator into the outlet pipe of the manhole. **John Meunier Inc.** recommends the use of a lubricant on the outlet pipe, in order to facilitate the insertion and orientation of the flow controller.

MAINTENANCE

HYDROVEX® regulators are manufactured in such a way as to be maintenance free; however, a periodic inspection (every 3-6 months) is suggested in order to ensure that neither the inlet nor the outlet has become blocked with debris. The manhole should undergo periodically, particularly after major storms, inspection and cleaning as established by the municipality

GUARANTY

The HYDROVEX® line of VHV / SVHV regulators are guaranteed against both design and manufacturing defects for a period of 5 years. Should a unit be defective, John Meunier Inc. is solely responsible for either modification or replacement of the unit.

ISO 9001: 2008 **Head Office**

4105 Sartelon

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APPENDIX E

StormTech System Design Sheets





2465070 ONTARIO LTD

2375 ST-LAURENT BLVD., OTTAWA, ON

STORMTECH CHAMBER SPECIFICATIONS

- CHAMBERS SHALL BE STORMTECH MC-3500 OR APPROVED EQUAL.
- 2. CHAMBERS SHALL BE MADE FROM VIRGIN, IMPACT-MODIFIED POLYPROPYLENE COPOLYMERS.
- 3. CHAMBER ROWS SHALL PROVIDE CONTINUOUS, UNOBSTRUCTED INTERNAL SPACE WITH NO INTERNAL SUPPORT PANELS THAT WOULD IMPEDE FLOW OR LIMIT ACCESS FOR INSPECTION.
- 4. THE STRUCTURAL DESIGN OF THE CHAMBERS, THE STRUCTURAL BACKFILL, AND THE INSTALLATION REQUIREMENTS SHALL ENSURE THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, SECTION 12.12, ARE MET FOR: 1) LONG-DURATION DEAD LOADS AND 2) SHORT-DURATION LIVE LOADS, BASED ON THE AASHTO DESIGN TRUCK WITH CONSIDERATION FOR IMPACT AND MULTIPLE VEHICLE PRESENCES.
- 5. CHAMBERS SHALL MEET THE REQUIREMENTS OF ASTM F2418, "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- 6. CHAMBERS SHALL BE DESIGNED AND ALLOWABLE LOADS DETERMINED IN ACCORDANCE WITH ASTM F2787, "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- 7. ONLY CHAMBERS THAT ARE APPROVED BY THE SITE DESIGN ENGINEER WILL BE ALLOWED. THE CHAMBER MANUFACTURER SHALL SUBMIT THE FOLLOWING UPON REQUEST TO THE SITE DESIGN ENGINEER FOR APPROVAL BEFORE DELIVERING CHAMBERS TO THE PROJECT SITE:
 - a. A STRUCTURAL EVALUATION SEALED BY A REGISTERED PROFESSIONAL ENGINEER THAT DEMONSTRATES THAT THE SAFETY FACTORS ARE GREATER THAN OR EQUAL TO 1.95 FOR DEAD LOAD AND 1.75 FOR LIVE LOAD, THE MINIMUM REQUIRED BY ASTM F2787 AND BY AASHTO FOR THERMOPLASTIC PIPE.
 - b. A STRUCTURAL EVALUATION SEALED BY A REGISTERED PROFESSIONAL ENGINEER THAT DEMONSTRATES THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, SECTION 12.12, ARE MET. THE 50 YEAR CREEP MODULUS DATA SPECIFIED IN ASTM F2418 MUST BE USED AS PART OF THE AASHTO STRUCTURAL EVALUATION TO VERIFY LONG-TERM PERFORMANCE.
 - c. STRUCTURAL CROSS SECTION DETAIL ON WHICH THE STRUCTURAL EVALUATION IS BASED.
- 8. CHAMBERS AND END CAPS SHALL BE PRODUCED AT AN ISO 9001 CERTIFIED MANUFACTURING FACILITY.

IMPORTANT - NOTES FOR THE BIDDING AND INSTALLATION OF MC-3500 CHAMBER SYSTEM

- STORMTECH MC-3500 CHAMBERS SHALL NOT BE INSTALLED UNTIL THE MANUFACTURER'S REPRESENTATIVE HAS COMPLETED A
 PRE-CONSTRUCTION MEETING WITH THE INSTALLERS.
- 2. STORMTECH MC-3500 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH MC-3500/MC-4500 CONSTRUCTION GUIDE".
- 3. CHAMBERS ARE NOT TO BE BACKFILLED WITH A DOZER OR AN EXCAVATOR SITUATED OVER THE CHAMBERS.

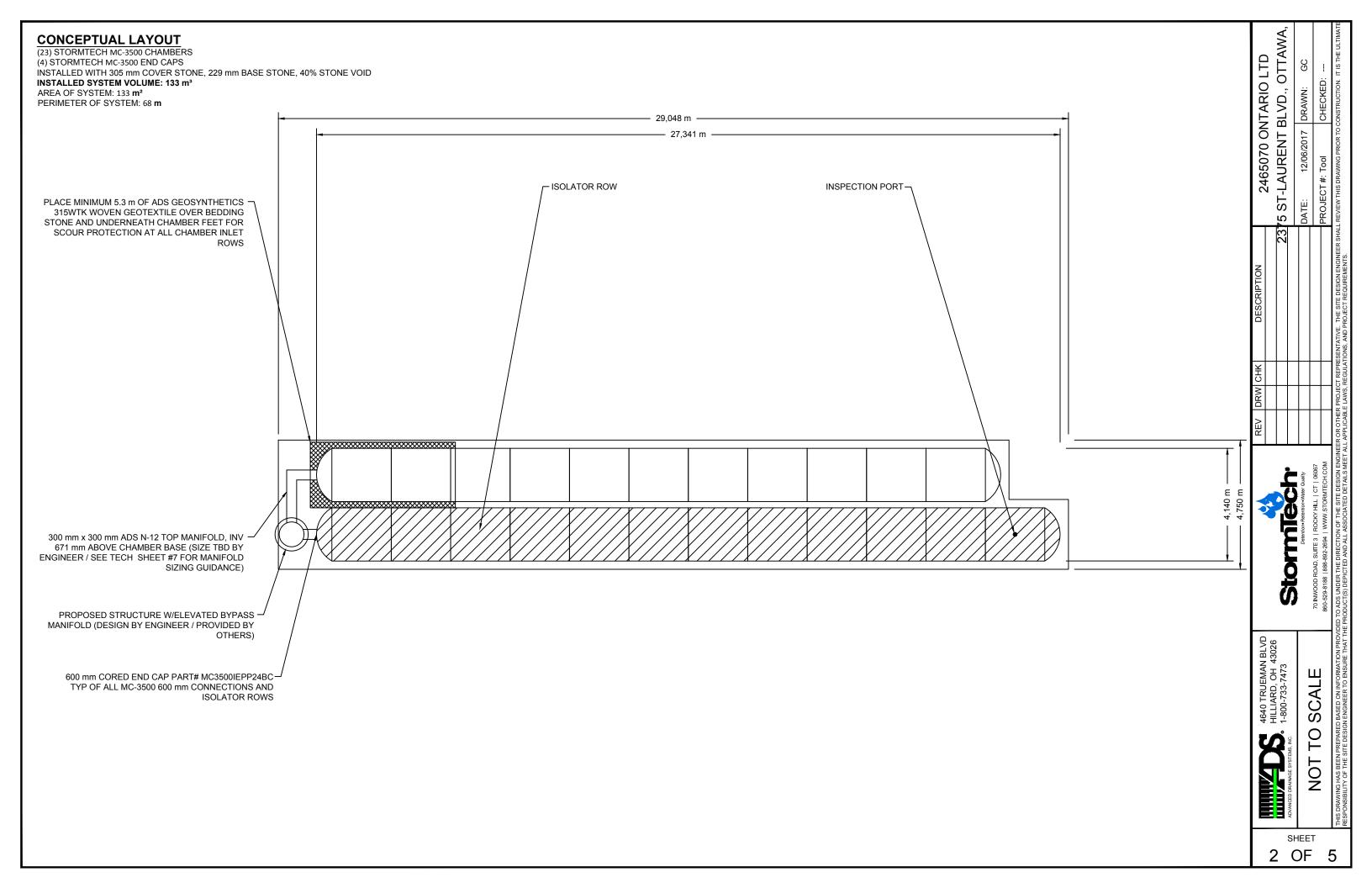
STORMTECH RECOMMENDS 3 BACKFILL METHODS:

- STONESHOOTER LOCATED OFF THE CHAMBER BED.
- BACKFILL AS ROWS ARE BUILT USING AN EXCAVATOR ON THE FOUNDATION STONE OR SUBGRADE.
- BACKFILL FROM OUTSIDE THE EXCAVATION USING A LONG BOOM HOE OR EXCAVATOR.
- 4. THE FOUNDATION STONE SHALL BE LEVELED AND COMPACTED PRIOR TO PLACING CHAMBERS.
- 5. JOINTS BETWEEN CHAMBERS SHALL BE PROPERLY SEATED PRIOR TO PLACING STONE.
- 6. MAINTAIN MINIMUM 9" (230 mm) SPACING BETWEEN THE CHAMBER ROWS.
- 7. INLET AND OUTLET MANIFOLDS MUST BE INSERTED A MINIMUM OF 12" (300 mm) INTO CHAMBER END CAPS.
- 8. EMBEDMENT STONE SURROUNDING CHAMBERS MUST BE A CLEAN, CRUSHED, ANGULAR STONE 3/4-2" (20-50 mm) MEETING THE AASHTO M43 DESIGNATION OF #3 OR #4.^J
- 9. STONE MUST BE PLACED ON THE TOP CENTER OF THE CHAMBER TO ANCHOR THE CHAMBERS IN PLACE AND PRESERVE ROW SPACING..^J
- 0. ADS RECOMMENDS THE USE OF "FLEXSTORM CATCH IT" INSERTS DURING CONSTRUCTION FOR ALL INLETS TO PROTECT THE SUBSURFACE STORMWATER MANAGEMENT SYSTEM FROM CONSTRUCTION SITE RUNOFF.

NOTES FOR CONSTRUCTION EQUIPMENT

- 1. STORMTECH MC-3500 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH MC-3500/MC-4500 CONSTRUCTION GUIDE".^J
- . THE USE OF EQUIPMENT OVER MC-3500 CHAMBERS IS LIMITED:
- NO EQUIPMENT IS ALLOWED ON BARE CHAMBERS.
- NO RUBBER TIRED LOADER, DUMP TRUCK, OR EXCAVATORS ARE ALLOWED UNTIL PROPER FILL DEPTHS ARE REACHED IN ACCORDANCE WITH THE "STORMTECH MC-3500/MC-4500 CONSTRUCTION GUIDE".
- WEIGHT LIMITS FOR CONSRUCTION EQUIPMENT CAN BE FOUND IN THE "STORMTECH MC-3500/MC-4500 CONSTRUCTION GUIDE".
- 3. FULL 36" (900 mm) OF STABILIZED COVER MATERIALS OVER THE CHAMBERS IS REQUIRED FOR DUMP TRUCK TRAVEL OR DUMPING.^J
 USE OF A DOZER TO PUSH EMBEDMENT STONE BETWEEN THE ROWS OF CHAMBERS MAY CAUSE DAMAGE TO CHAMBERS AND IS NOT AN ACCEPTABLE
 BACKFILL METHOD. ANY CHAMBERS DAMAGED BY USING THE "DUMP AND PUSH" METHOD ARE NOT COVERED UNDER THE STORMTECH STANDARD
 WARRANTY.

CONTACT STORMTECH AT 1-888-892-2694 WITH ANY QUESTIONS ON INSTALLATION REQUIREMENTS OR WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT.



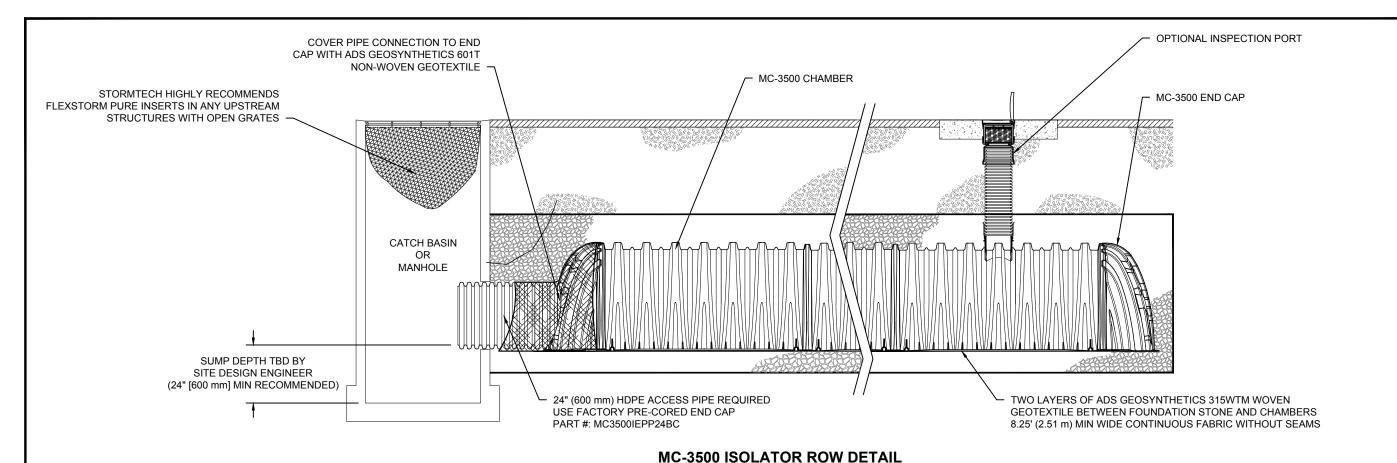
ACCEPTABLE FILL MATERIALS: STORMTECH MC-3500 CHAMBER SYSTEMS

C A M DE	EGIN COMPACTIONS AFTER 24" mm) OF MATERIAL OVER THE CHAMBERS IS REACHED. COMPA ADDITIONAL LAYERS IN 12" (300 I MAX LIFTS TO A MIN. 95% PROCT ENSITY FOR WELL GRADED MATE AND 95% RELATIVE DENSITY FOR	EMBEDMENT STONE: FILL SURROUNDING THE CHAMBERS FROM THE FOUNDATION STONE ('A' LAYER) TO THE 'C' LAYER ABOVE.	SIZE DISTRIBUTION BETWEEN 3/4-2 INCH (20-50 mm)	AASHTO M43 ¹ 3, 4
D	D A	FOUNDATION STONE: FILL BELOW CHAMBERS FROM THE SUBGRADE UP TO THE FOOT (BOTTOM) OF THE CHAMBER.	CLEAN, CRUSHED, ANGULAR STONE, NOMINAL SIZE DISTRIBUTION BETWEEN 3/4-2 INCH (20-50 mm)	AASHTO M43 ¹ 3, 4 NO COMPACTION REQUIRED.
1. ET FLA 2SUR 3.CEV	MPA OR OR STARTS FROM THE TOP OF THE EMBED O SECOND ('B' LAYER) TO 24" (600 mm) ABOV THE LISTED OF THE CHEMBER TOTE THAT BAYE ANGULAR WO. 2" (A&SHTOMAS) STONE" HE 'C' LA	MENT FINES OR PROCESSED AGGREGATE.	ULAR. FOR EXAMPLE, A SPECIFICATION FOR #	OVERAGES WITH A VIBRATORY COMPACTOR.
		601T NON-WOVEN GEOTEXTILE ALL), ANGULAR STONE IN A & B LAYERS	PAVEMENT LAY BY SITE DESIGN	
1	METER STONE (SEE NOTE 6) AVATION WALL OR VERTICAL) 6" (150 mm) MIN	MC-3500 END CAP SUBGRADE SOILS (SEE NOTE 5)	TO BOTTOM OF FLEXIBLE PAVEMENT. FOR UNPAY INSTALLATIONS WHERE RUTING FROM VEHICLES MAY INCREASE COVER TO 30" (750 mm). 9" (230 mm) MIN 77" (1950 mm)	

NOTES:

- MC-3500 CHAMBERS SHALL CONFORM TO THE REQUIREMENTS OF ASTM F2418 "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".^J MC-3500 CHAMBERS SHALL BE DESIGNED IN ACCORDANCE WITH ASTM F2787 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".^J
- "ACCEPTABLE FILL MATERIALS" TABLE ABOVE PROVIDES MATERIAL LOCATIONS, DESCRIPTIONS, GRADATIONS, AND COMPACTION REQUIREMENTS FOR FOUNDATION, EMBEDMENT, AND FILL MATERIALS."
- THE "SITE DESIGN ENGINEER" REFERS TO THE ENGINEER RESPONSIBLE FOR THE DESIGN AND LAYOUT OF THE STORMTECH CHAMBERS FOR THIS PROJECT. A
- THE SITE DESIGN ENGINEER IS RESPONSIBLE FOR ASSESSING THE BEARING RESISTANCE (ALLOWABLE BEARING CAPACITY) OF THE SUBGRADE SOILS AND THE DEPTH OF FOUNDATION STONE WITH CONSIDERATION FOR THE RANGE OF EXPECTED SOIL MOISTURE CONDITIONS.^J
- PERIMETER STONE MUST BE EXTENDED HORIZONTALLY TO THE EXCAVATION WALL FOR BOTH VERTICAL AND SLOPED EXCAVATION WALLS.
- ONCE LAYER 'C' IS PLACED, ANY SOIL/MATERIAL CAN BE PLACED IN LAYER 'D' UP TO THE FINISHED GRADE. MOST PAVEMENT SUBBASE SOILS CAN BE USED TO REPLACE THE MATERIAL REQUIREMENTS OF LAYER 'C' OR 'D' AT THE SITE DESIGN ENGINEER'S DISCRETION.

2465070 ONTARIO LTD ST-LAURENT BLVD., OTTAWA, DRAWN: 12/06/2017 2 StormTe SHEET 3 OF



INSPECTION & MAINTENANCE

INSPECT ISOLATOR ROW FOR SEDIMENT

A. INSPECTION PORTS (IF PRESENT)

- REMOVE/OPEN LID ON NYLOPLAST INLINE DRAIN
- REMOVE AND CLEAN FLEXSTORM FILTER IF INSTALLED
- USING A FLASHLIGHT AND STADIA ROD, MEASURE DEPTH OF SEDIMENT AND RECORD ON MAINTENANCE LOG LOWER A CAMERA INTO ISOLATOR ROW FOR VISUAL INSPECTION OF SEDIMENT LEVELS (OPTIONAL)
- IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2. IF NOT, PROCEED TO STEP 3.

B. ALL ISOLATOR ROWS

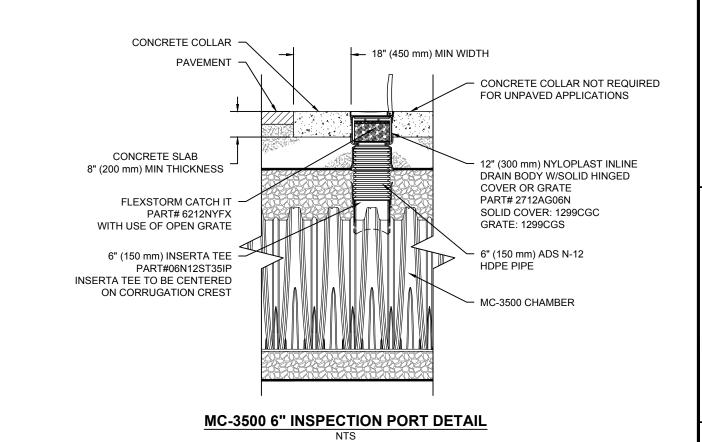
- REMOVE COVER FROM STRUCTURE AT UPSTREAM END OF ISOLATOR ROW
- USING A FLASHLIGHT, INSPECT DOWN THE ISOLATOR ROW THROUGH OUTLET PIPE^Ji) MIRRORS ON POLES OR CAMERAS MAY BE USED TO AVOID A CONFINED SPACE ENTRY^Jii) FOLLOW OSHA REGULATIONS FOR CONFINED SPACE ENTRY IF ENTERING MANHOLE
- IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2. IF NOT, PROCEED TO STEP 3.

CLEAN OUT ISOLATOR ROW USING THE JETVAC PROCESS

- A. A FIXED CULVERT CLEANING NOZZLE WITH REAR FACING SPREAD OF 45" (1.1 m) OR MORE IS PREFERRED
- APPLY MULTIPLE PASSES OF JETVAC UNTIL BACKFLUSH WATER IS CLEAN
- C. VACUUM STRUCTURE SUMP AS REQUIRED
- REPLACE ALL COVERS, GRATES, FILTERS, AND LIDS; RECORD OBSERVATIONS AND ACTIONS.
- STEP 4) INSPECT AND CLEAN BASINS AND MANHOLES UPSTREAM OF THE STORMTECH SYSTEM.

NOTES

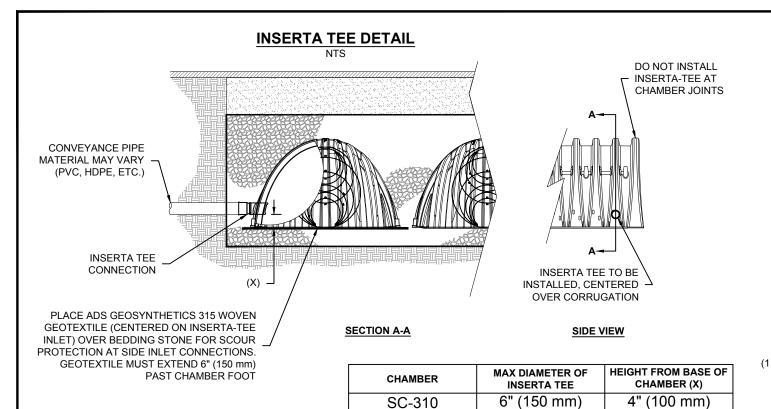
- INSPECT EVERY 6 MONTHS DURING THE FIRST YEAR OF OPERATION. ADJUST THE INSPECTION INTERVAL BASED ON PREVIOUS OBSERVATIONS OF SEDIMENT ACCUMULATION AND HIGH WATER ELEVATIONS.^J
- 2. CONDUCT JETTING AND VACTORING ANNUALLY OR WHEN INSPECTION SHOWS THAT MAINTENANCE IS NECESSARY.



2465070 ONTARIO LTD ST-LAURENT BLVD., OTTAWA, 12/06/2017 2 Stormi 4640 TRUEMAN BLVD HILLIARD, OH 43026 1-800-733-7473 SHEET OF

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DRAWN:



MC-4500 12" (300 mm) PART NUMBERS WILL VARY BASED ON INLET PIPE MATERIALS. INSERTA TEE FITTINGS AVAILABLE FOR SDR 26, SDR 35, SCH 40 IPS CONTACT STORMTECH FOR MORE INFORMATION. GASKETED & SOLVENT WELD, N-12, HP STORM, C-900 OR DUCTILE IRON

MC-SERIES END CAP INSERTION DETAIL

SC-740

DC-780

MC-3500

10" (250 mm)

10" (250 mm)

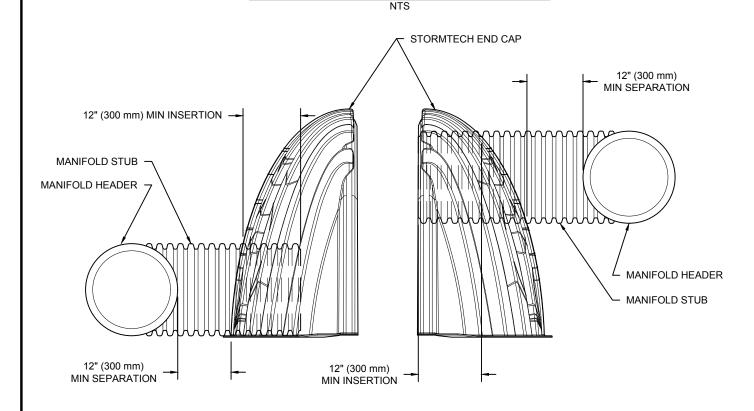
12" (300 mm)

4" (100 mm)

4" (100 mm)

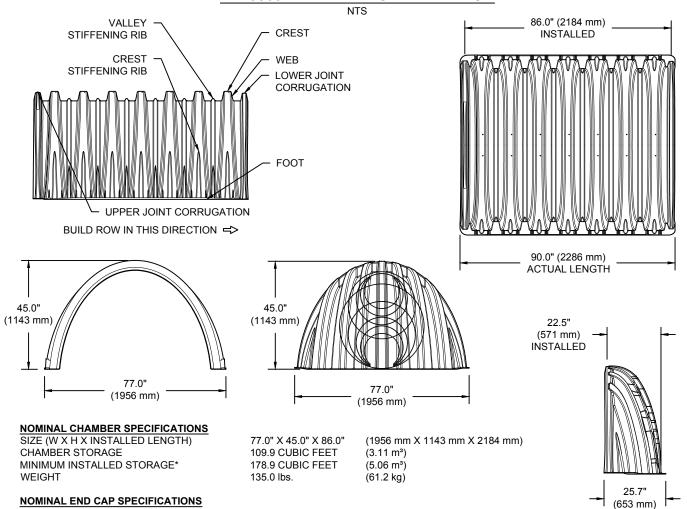
6" (150 mm)

8" (200 mm)



NOTE: MANIFOLD STUB MUST BE LAID HORIZONTAL FOR A PROPER FIT IN END CAP OPENING.

MC-3500 TECHNICAL SPECIFICATION



(1956 mm X 1143 mm X 571 mm)

(0.42 m³)

(1.30 m³)

(22.7 kg)

*ASSUMES 12" (305 mm) STONE ABOVE, 9" (229 mm) STONE FOUNDATION AND BETWEEN CHAMBERS, 12" (305 mm) STONE PERIMETER IN FRONT OF END CAPS AND 40% STONE POROSITY

50.0 lbs.

77.0" X 45.0" X 22.5"

14.9 CUBIC FEET

46.0 CUBIC FEET

STUBS AT BOTTOM OF END CAP FOR PART NUMBERS ENDING WITH "B"

SIZE (W X H X INSTALLED LENGTH)

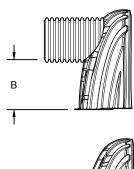
MINIMUM INSTALLED STORAGE*

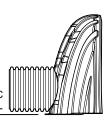
END CAP STORAGE

WEIGHT

PART#	STUB	В	С		
MC3500IEPP06T	6" (150 mm)	33.21" (844 mm)			
MC3500IEPP06B	0 (100 11111)		0.66" (17 mm)		
MC3500IEPP08T	8" (200 mm)	31.16" (791 mm)			
MC3500IEPP08B	6 (200 111111)		0.81" (21 mm)		
MC3500IEPP10T	10" (250 mm)	29.04" (738 mm)			
MC3500IEPP10B	10 (250 11111)		0.93" (24 mm)		
MC3500IEPP12T	12" (300 mm)	26.36" (670 mm)			
MC3500IEPP12B	12 (300 11111)		1.35" (34 mm)		
MC3500IEPP15T	15" (375 mm)	23.39" (594 mm)			
MC3500IEPP15B	15 (3/5111111)		1.50" (38 mm)		
MC3500IEPP18TC	18" (450 mm)	20.03" (509 mm)			
MC3500IEPP18BC	16 (45011111)		1.77" (45 mm)		
MC3500IEPP24TC	24" (600 mm)	14.48" (368 mm)			
MC3500IEPP24BC	24 (000 111111)		2.06" (52 mm)		
MC3500IEPP30BC	30" (750 mm)				

CUSTOM PRECORED INVERTS ARE AVAILABLE UPON REQUEST. INVENTORIED MANIFOLDS INCLUDE 12-24" (300-600 mm) SIZE ON SIZE AND 15-48" (375-1200 mm) ECCENTRIC MANIFOLDS. CUSTOM INVERT LOCATIONS ON THE MC-3500 END CAP CUT IN THE FIELD ARE NOT RECOMMENDED FOR PIPE SIZES GREATER THAN 10" (250 mm) THE INVERT LOCATION IN COLUMN 'B' ARE THE HIGHTEST POSSIBLE FOR THE PIPE SIZE.





Storm

BLVD., OTTAWA,

ST-LAURENT

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ONTARIO

2465070

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DRAWN:

12/06/2017

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OF

APPENDIX F
Stormceptor Reports





Brief Stormceptor Sizing Report - 2465070 ONTARIO LTD

Project Information & Location						
Project Name	2465070 ONTARIO LTD	2465070 ONTARIO LTD Project Number				
City	Ottawa	State/ Province	Ontario			
Country	Canada	Date	12/7/2017			
Designer Informatio	n	EOR Information (optional)				
Name	Guillaume Courtois	Name				
Company	Company LRL Associates Ltd.					
Phone #	Phone # 613-842-3434					
Email	Email gcourtois@Irl.ca					

Stormwater Treatment Recommendation

The recommended Stormceptor Model(s) which achieve or exceed the user defined water quality objective for each site within the project are listed in the below Sizing Summary table.

Site Name	Proposed Yonaka Warehouse		
Target TSS Removal (%)	80		
TSS Removal (%) Provided	81		
Recommended Stormceptor Model	STC 300		

The recommended Stormceptor Model achieves the water quality objectives based on the selected inputs, historical rainfall records and selected particle size distribution.

Stormceptor Sizing Summary					
Stormceptor Model	% TSS Removal Provided				
STC 300	81				
STC 750	87				
STC 1000	88				
STC 1500	87				
STC 2000	89				
STC 3000	90				
STC 4000	92				
STC 5000	92				
STC 6000	93				
STC 9000	95				
STC 10000	95				
STC 14000	96				
StormceptorMAX	Custom				





Sizing Details						
Drainage	Water Quality Objective					
Total Area (ha)	0.659	TSS Removal (80.0			
Imperviousness %	83.0	Runoff Volume Cap				
Rainfa	Oil Spill Capture Volume (L)					
Station Name	OTTAWA MACDONALD- CARTIER INT'L A	Peak Conveyed Flow Rate (L/s)				
State/Province	Ontario	Water Quality Flow Rate (L/s)				
Station ID #	6000	Up Stream Storage				
Years of Records	37	Storage (ha-m)	Discharge (cms)			
Latitude	45°19'N	0.000	0.000			
Longitude	Longitude 75°40'W		0.043			

Up Stream Flow Diversion

Max. Flow to Stormceptor (cms)

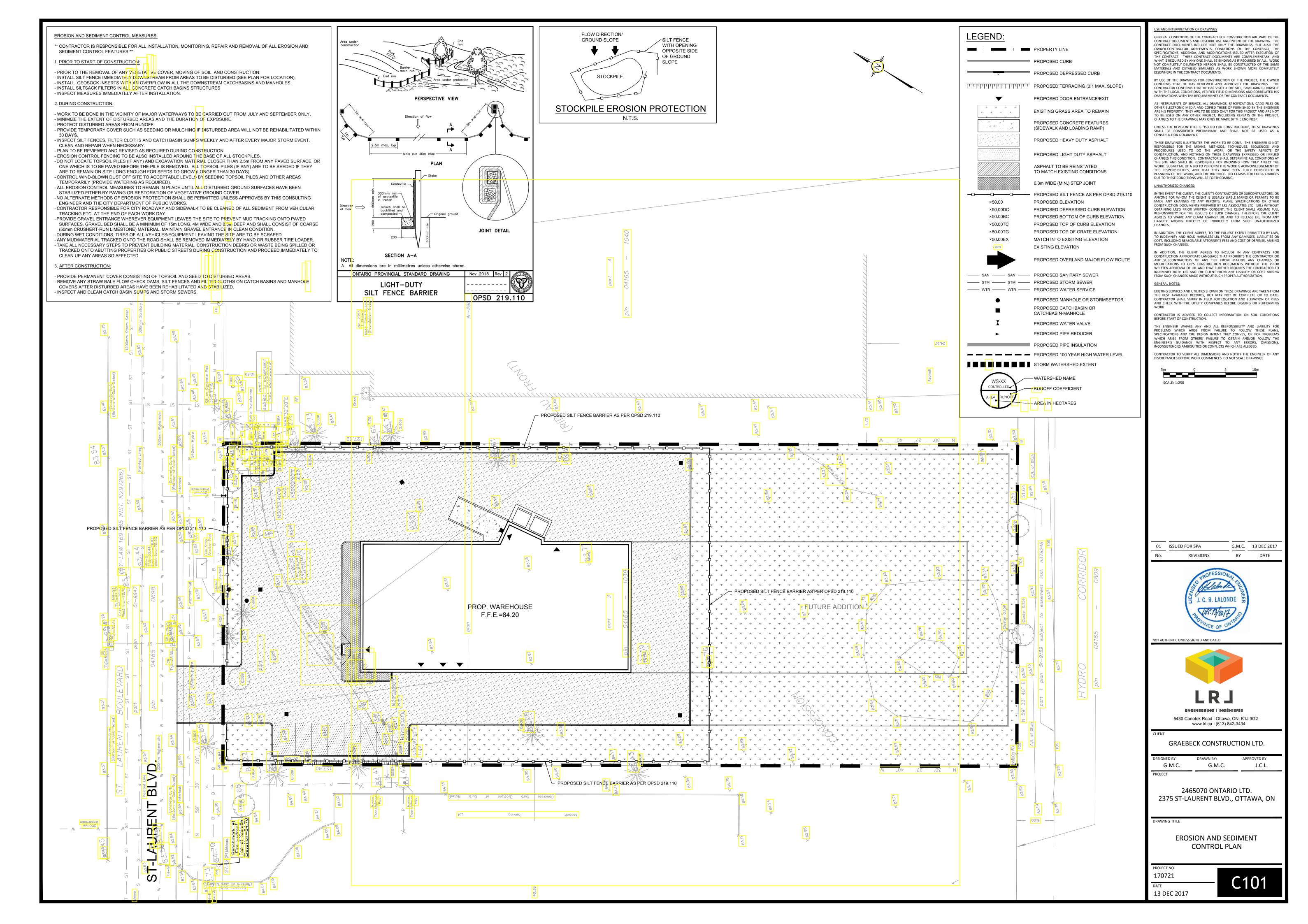
Particle Size Distribution (PSD) The selected PSD defines TSS removal						
Fine Distribution						
Particle Diameter Distribution Specific Grav (microns) %						
20.0	20.0	1.30				
60.0	20.0	1.80				
150.0	20.0	2.20				
400.0	20.0	2.65				
2000.0	20.0	2.65				

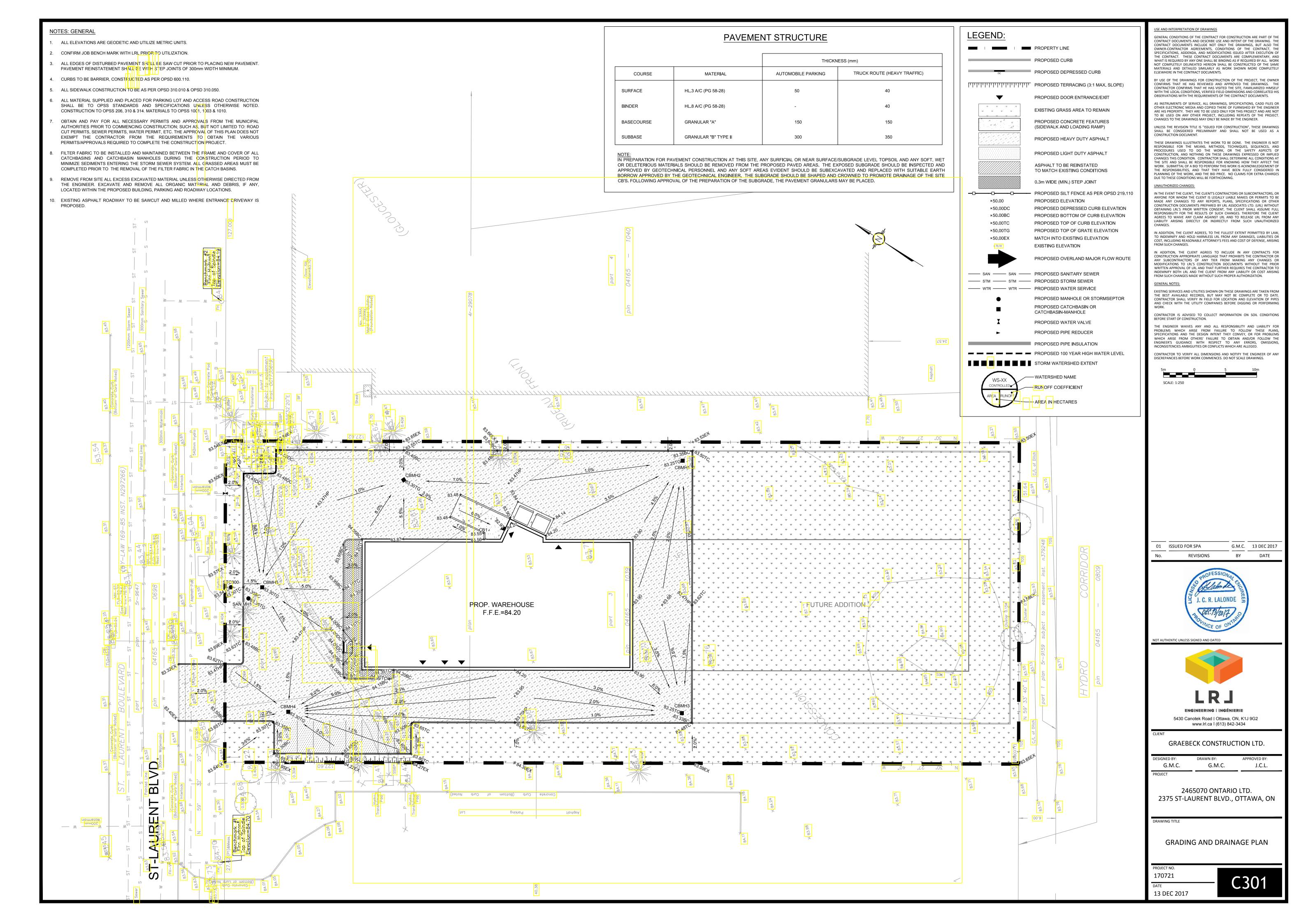
Notes

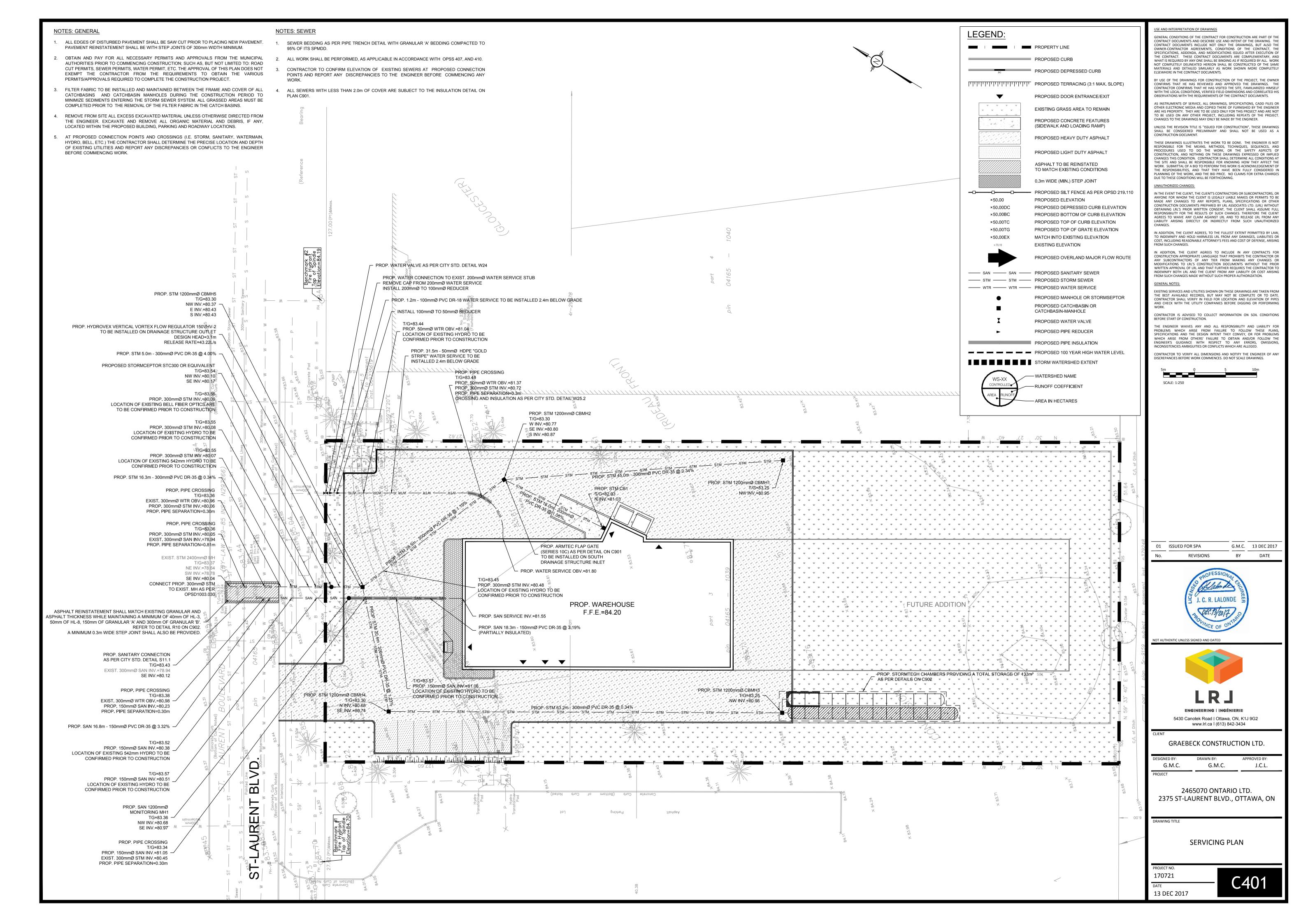
- Stormceptor performance estimates are based on simulations using PCSWMM for Stormceptor, which uses the EPA Rainfall and Runoff modules.
- Design estimates listed are only representative of specific project requirements based on total suspended solids (TSS) removal defined by the selected PSD, and based on stable site conditions only, after construction is completed.
- For submerged applications or sites specific to spill control, please contact your local Stormceptor representative for further design assistance.

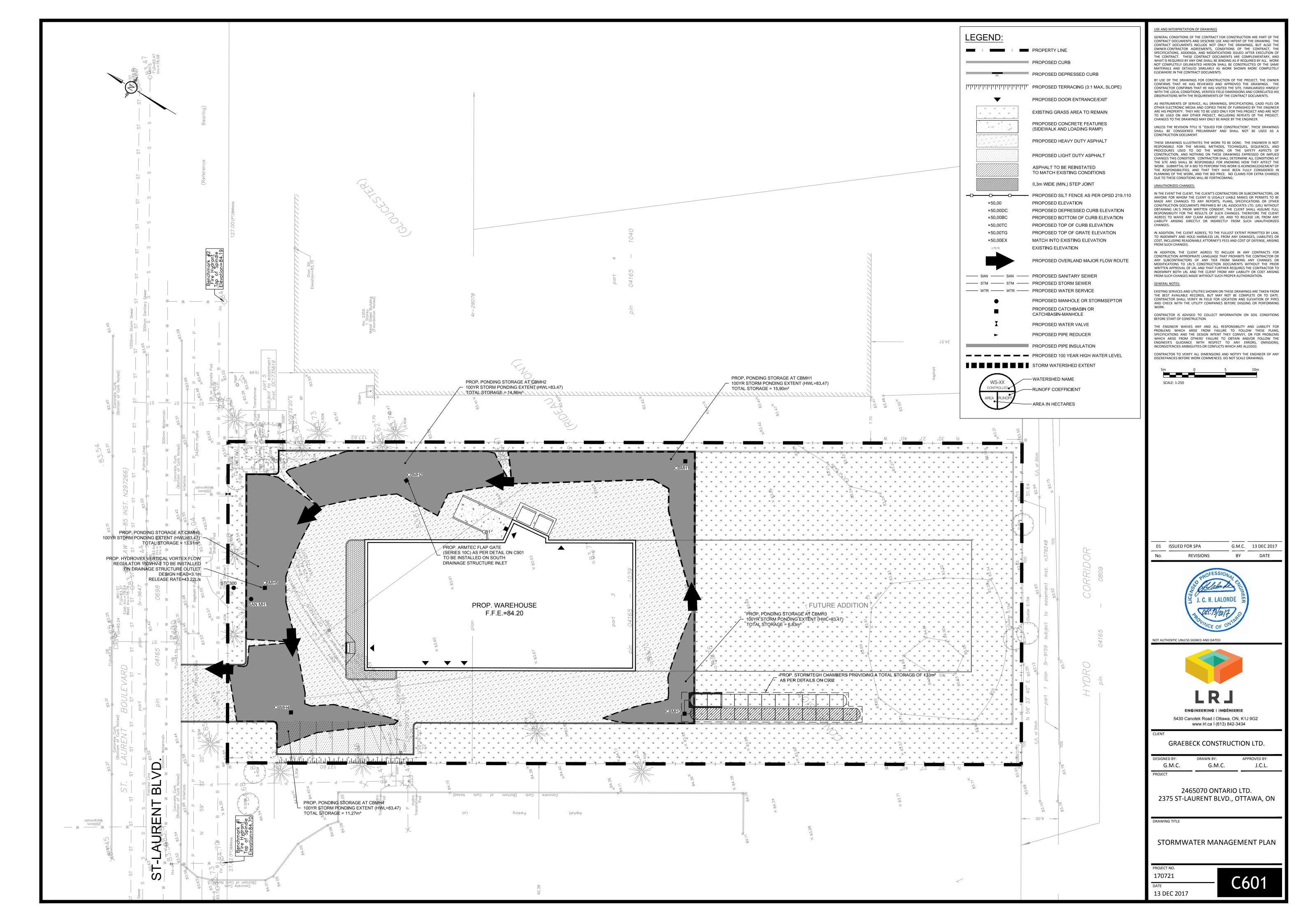
For Stormceptor Specifications and Drawings Please Visit: http://www.imbriumsystems.com/technical-specifications APPENDIX G

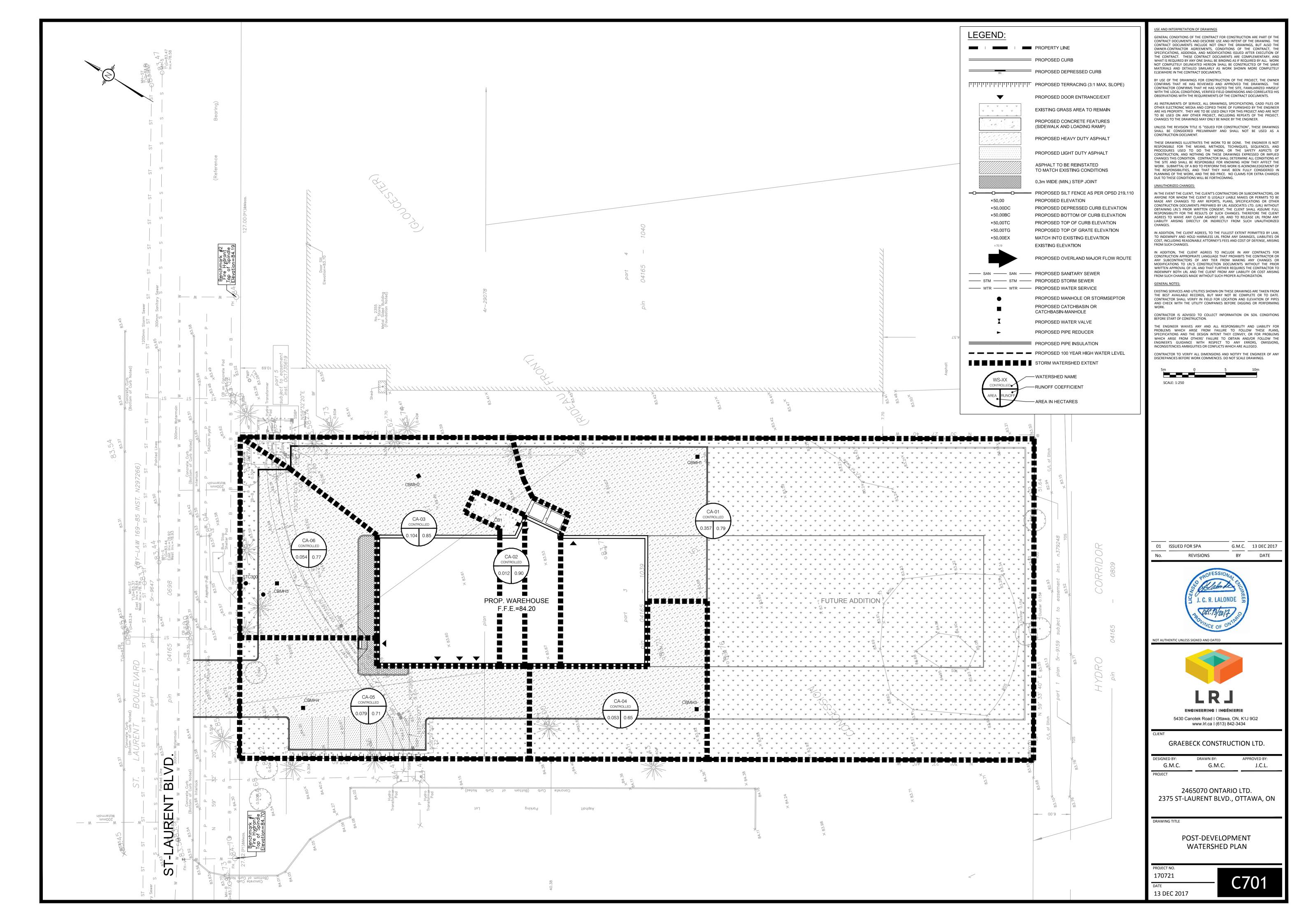
Complete Set of Civil Plans

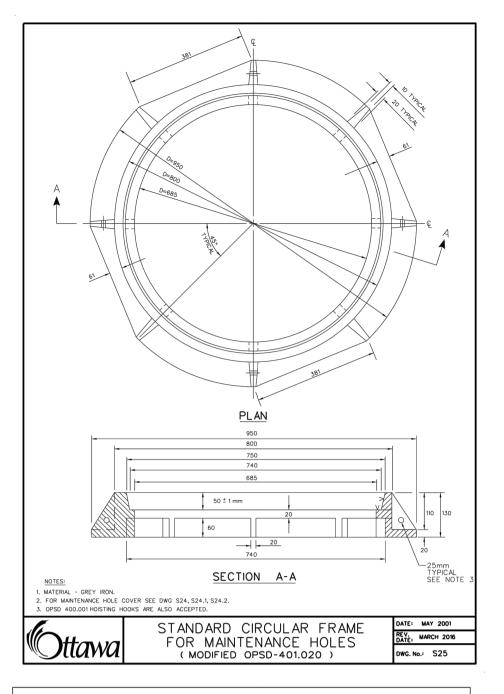


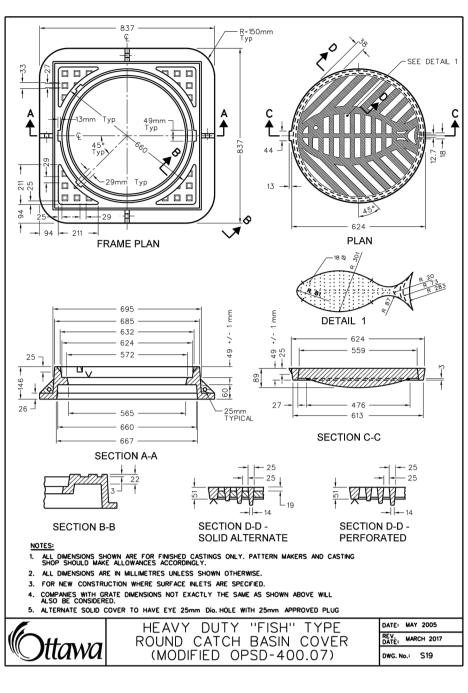


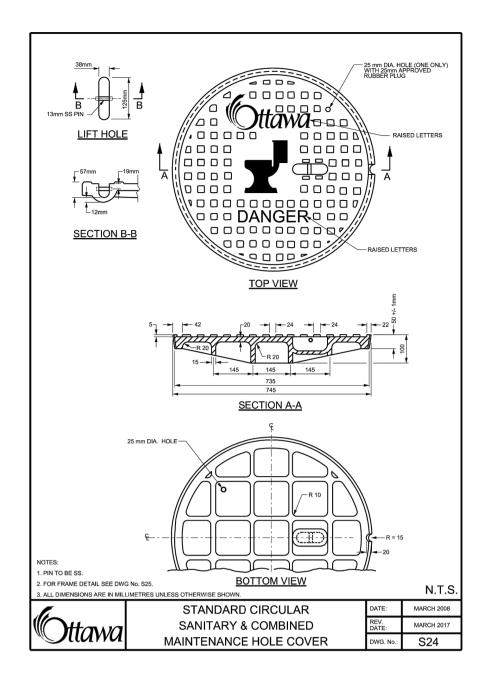


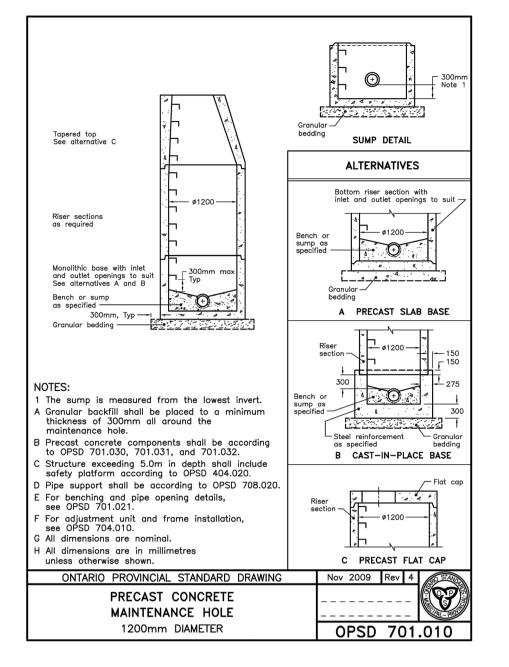


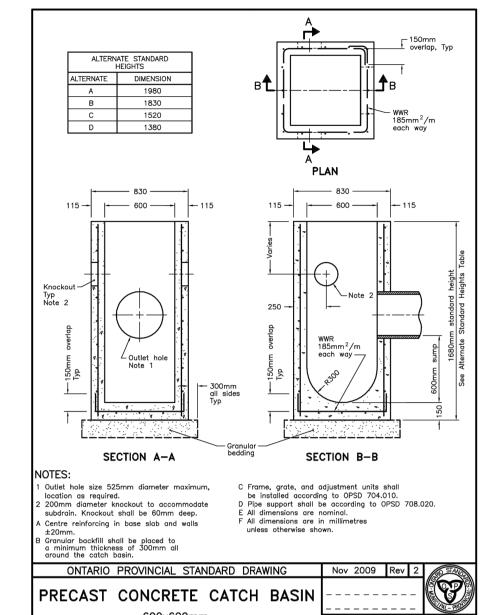


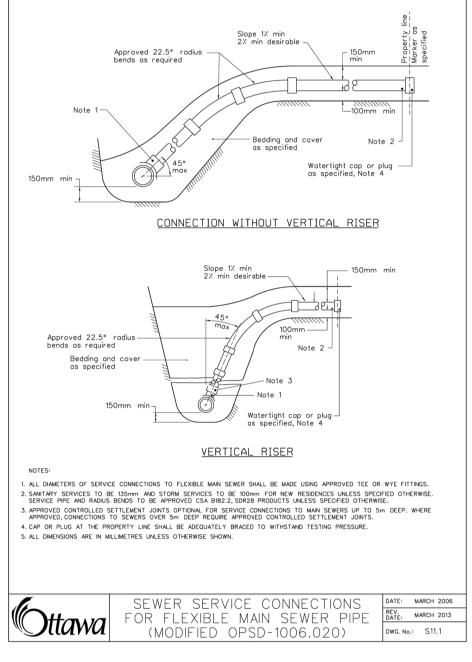


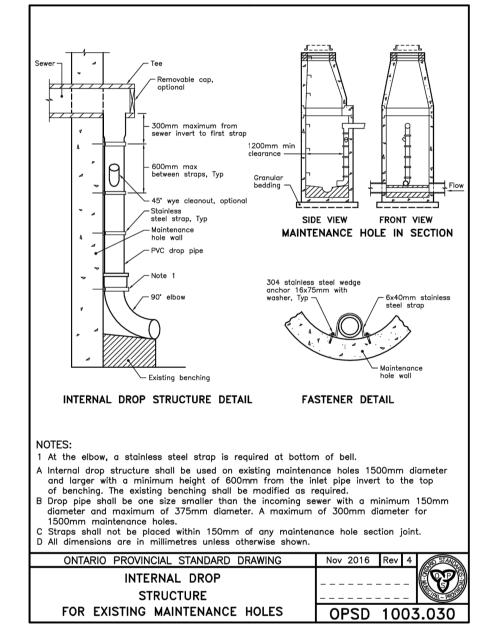


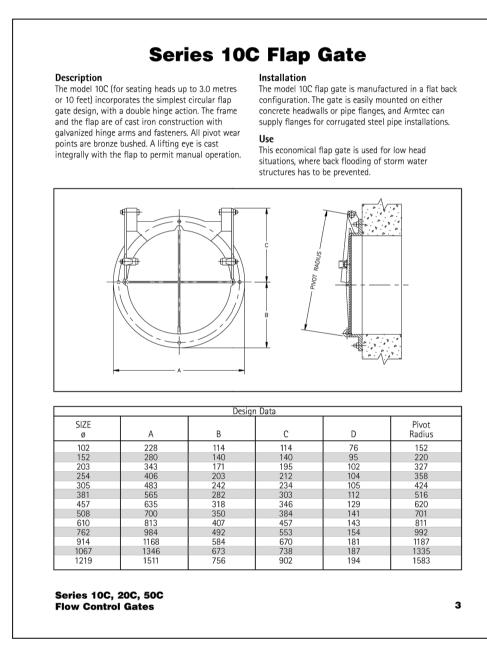


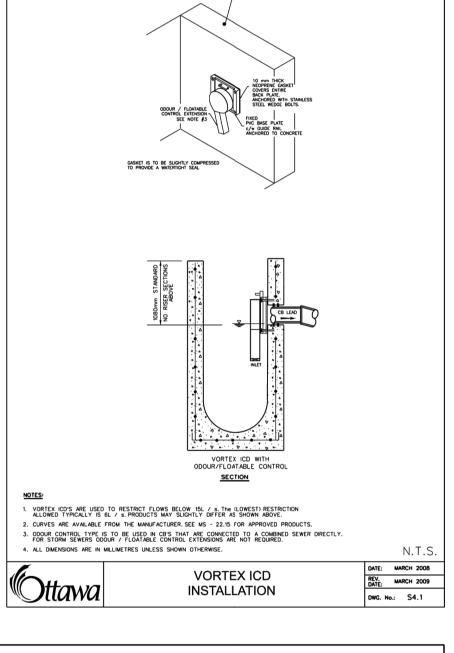


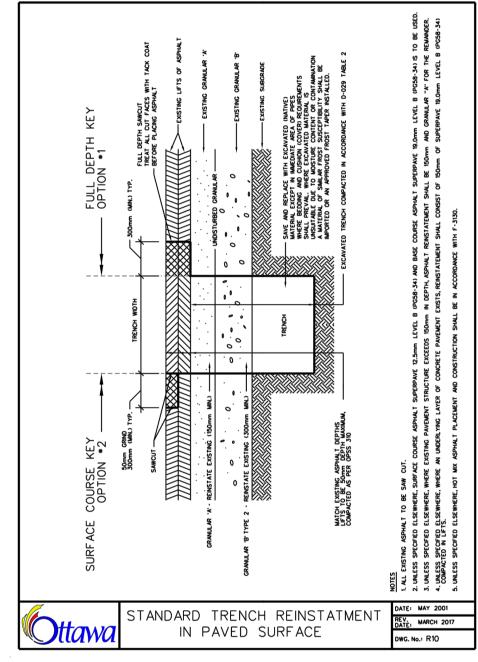


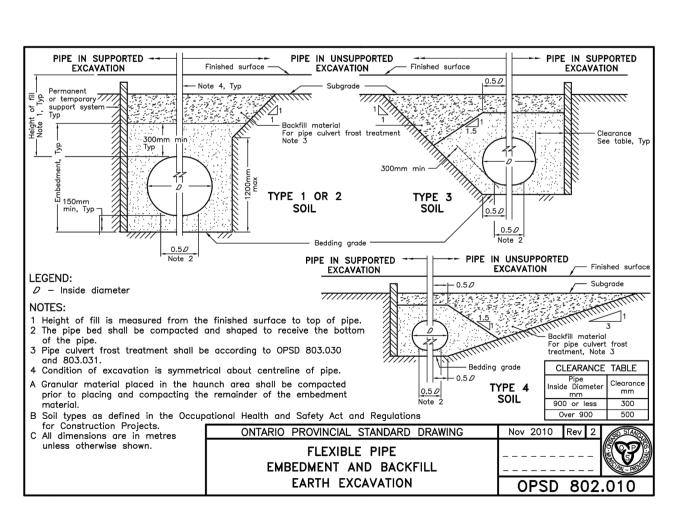


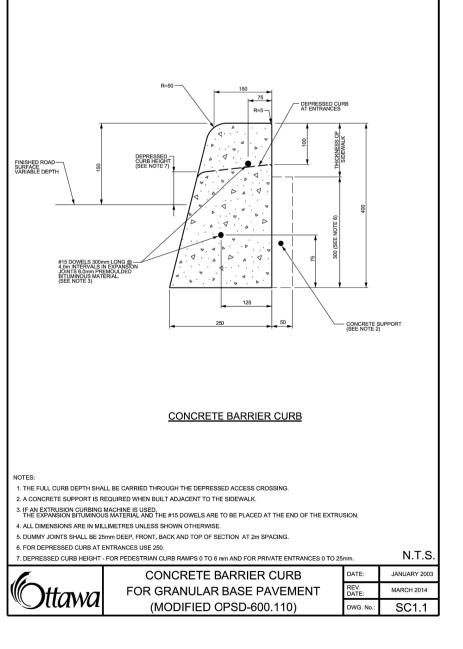


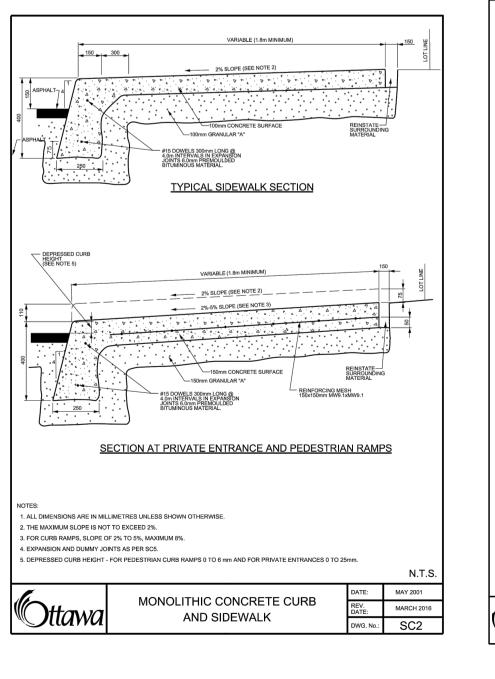


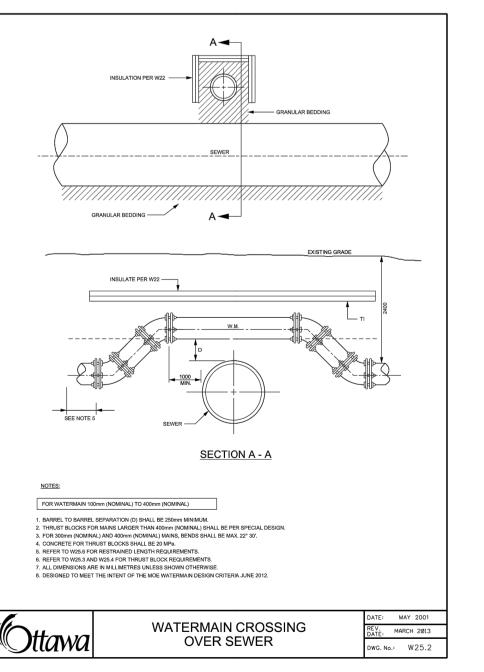


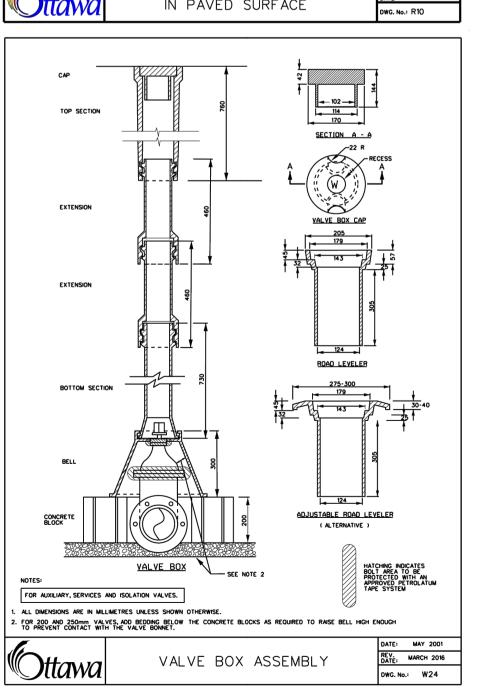












GENERAL CONDITIONS OF THE CONTRACT FOR CONSTRUCTION ARE PART OF THE CONTRACT DOCUMENTS AND DESCRIBE USE AND INTENT OF THE CONTRACT DOCUMENTS AND DESCRIBE USE AND INTENT OF THE DRAWING. THE CONTRACT DOCUMENTS INCLUDE NOT ONLY THE DRAWINGS, BUT ALSO THE OWNER-CONTRACTOR AGREEMENTS, CONDITIONS OF THE CONTRACT, TH SPECIFICATIONS, ADDENDA, AND MODIFICATIONS ISSUED AFTER EXECUTION OF THE CONTRACT. THESE CONTRACT DOCUMENTS ARE COMPLEMENTARY, AND CONFIRMS THAT HE HAS REVIEWED AND APPROVED THE DRAWINGS. THE CONTRACTOR CONFIRMS THAT HE HAS VISITED THE SITE, FAMILIARIZED HIMSELF

WHAT IS REQUIRED BY ANY ONE SHALL BE BINDING AS IF REQUIRED BY ALL. WORK NOT COMPLETELY DELINEATED HEREON SHALL BE CONSTRUCTED OF THE SAME MATERIALS AND DETAILED SIMILARLY AS WORK SHOWN MORE COMPLETELY BY USE OF THE DRAWINGS FOR CONSTRUCTION OF THE PROJECT, THE OWNER

USE AND INTERPRETATION OF DRAWINGS

WITH THE LOCAL CONDITIONS, VERIFIED FIELD DIMENSIONS AND CORRELATED HIS OBSERVATIONS WITH THE REQUIREMENTS OF THE CONTRACT DOCUMENTS. AS INSTRUMENTS OF SERVICE, ALL DRAWINGS, SPECIFICATIONS, CADD FILES O OTHER ELECTRONIC MEDIA AND COPIED THERE OF FURNISHED BY THE ENGINEER ARE HIS PROPERTY. THEY ARE TO BE USED ONLY FOR THIS PROJECT AND ARE NOT

UNLESS THE REVISION TITLE IS "ISSUED FOR CONSTRUCTION", THESE DRAWINGS SHALL BE CONSIDERED PRELIMINARY AND SHALL NOT BE USED AS A CONSTRUCTION DOCUMENT.

CHANGES TO THE DRAWINGS MAY ONLY BE MADE BY THE ENGINEER.

THESE DRAWINGS ILLUSTRATES THE WORK TO BE DONE. THE ENGINEER IS NOT RESPONSIBLE FOR THE MEANS, METHODS, TECHNIQUES, SEQUENCES, AND PROCEDURES USED TO DO THE WORK, OR THE SAFETY ASPECTS O CONSTRUCTION, AND NOTHING ON THESE DRAWINGS EXPRESSED OR IMPLIED CHANGES THIS CONDITION. CONTRACTOR SHALL DETERMINE ALL CONDITIONS AT THE SITE AND SHALL BE RESPONSIBLE FOR KNOWING HOW THEY AFFECT TH WORK. SUBMITTAL OF A BID TO PERFORM THIS WORK IS ACKNOWLEDGEMENT OF THE RESPONSIBILITIES, AND THAT THEY HAVE BEEN FULLY CONSIDERED IN PLANNING OF THE WORK, AND THE BID PRICE. NO CLAIMS FOR EXTRA CHARGES

UNAUTHORIZED CHANGES:

GENERAL NOTES:

OPSD 705.010

IN THE EVENT THE CLIENT, THE CLIENT'S CONTRACTORS OR SUBCONTRACTORS, OR ANYONE FOR WHOM THE CLIENT IS LEGALLY LIABLE MAKES OR PERMITS TO BE MADE ANY CHANGES TO ANY REPORTS, PLANS, SPECIFICATIONS OR OTHER CONSTRUCTION DOCUMENTS PREPARED BY LRL ASSOCIATES LTD. (LRL) WITHOUT OBTAINING LRL'S PRIOR WRITTEN CONSENT, THE CLIENT SHALL ASSUME FULL RESPONSIBILITY FOR THE RESULTS OF SUCH CHANGES. THEREFORE THE CLIEN AGREES TO WAIVE ANY CLAIM AGAINST LRL AND TO RELEASE LRL FROM ANY LIABILITY ARISING DIRECTLY OR INDIRECTLY FROM SUCH UNAUTHORIZED

IN ADDITION, THE CLIENT AGREES, TO THE FULLEST EXTENT PERMITTED BY LAW, TO INDEMNIFY AND HOLD HARMLESS LRL FROM ANY DAMAGES, LIABILITIES OR COST, INCLUDING REASONABLE ATTORNEY'S FEES AND COST OF DEFENSE, ARISING

IN ADDITION, THE CLIENT AGREES TO INCLUDE IN ANY CONTRACTS FOR CONSTRUCTION APPROPRIATE LANGUAGE THAT PROHIBITS THE CONTRACTOR OF MODIFICATIONS TO LRL'S CONSTRUCTION DOCUMENTS WITHOUT THE PRIOR WRITTEN APPROVAL OF LRL AND THAT FURTHER REQUIRES THE CONTRACTOR TO INDEMNIFY BOTH LRL AND THE CLIENT FROM ANY LIABILITY OR COST ARISING FROM SUCH CHANGES MADE WITHOUT SUCH PROPER AUTHORIZATION.

EXISTING SERVICES AND UTILITIES SHOWN ON THESE DRAWINGS ARE TAKEN FROM THE BEST AVAILABLE RECORDS, BUT MAY NOT BE COMPLETE OR TO DATE. CONTRACTOR SHALL VERIFY IN FIELD FOR LOCATION AND ELEVATION OF PIPES AND CHECK WITH THE UTILITY COMPANIES BEFORE DIGGING OR PERFORMING WORK.

CONTRACTOR IS ADVISED TO COLLECT INFORMATION ON SOIL CONDITIONS BEFORE START OF CONSTRUCTION. THE ENGINEER WAIVES ANY AND ALL RESPONSIBILITY AND LIABILITY FOR PROBLEMS WHICH ARISE FROM FAILURE TO FOLLOW THESE PLANS, SPECIFICATIONS AND THE DESIGN INTENT THEY CONVEY, OR FOR PROBLEMS WHICH ARISE FROM OTHERS' FAILURE TO OBTAIN AND/OR FOLLOW THE ENGINEER'S GUIDANCE WITH RESPECT TO ANY ERRORS, OMISSIONS, INCONSISTENCIES AMBIGUITIES OR CONFLICTS WHICH ARE ALLEGED.

DISCREPANCIES BEFORE WORK COMMENCES. DO NOT SCALE DRAWINGS.

01 ISSUED FOR SPA G.M.C. 13 DEC 2017 BY REVISIONS DATE J. C. R. LALONDE IOT AUTHENTIC LINEESS SIGNED AND DATED 5430 Canotek Road | Ottawa, ON, K1J 9G2 www.lrl.ca I (613) 842-3434

G.M.C.

CONSTRUCTION DETAIL PLAN

GRAEBECK CONSTRUCTION LTD.

G.M.C.

2465070 ONTARIO LTD.

2375 ST-LAURENT BLVD., OTTAWA, ON

170721

13 DEC 2017

J.C.L.





2465070 ONTARIO LTD

2375 ST-LAURENT BLVD., OTTAWA, ON

STORMTECH CHAMBER SPECIFICATIONS

- . CHAMBERS SHALL BE STORMTECH MC-3500 OR APPROVED EQUAL
- 2. CHAMBERS SHALL BE MADE FROM VIRGIN, IMPACT-MODIFIED POLYPROPYLENE COPOLYMERS.
- CHAMBER ROWS SHALL PROVIDE CONTINUOUS, UNOBSTRUCTED INTERNAL SPACE WITH NO INTERNAL SUPPORT PANELS THAT WOULD IMPEDE FLOW OR LIMIT ACCESS FOR INSPECTION.
- THE STRUCTURAL DESIGN OF THE CHAMBERS, THE STRUCTURAL BACKFILL, AND THE INSTALLATION REQUIREMENTS SHALL ENSURE THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, SECTION 12.12, ARE MET FOR: 1) LONG-DURATION DEAD LOADS AND 2) SHORT-DURATION LIVE LOADS, BASED ON THE AASHTO DESIGN TRUCK WITH CONSIDERATION FOR IMPACT AND MULTIPLE VEHICLE PRESENCES
- CHAMBERS SHALL MEET THE REQUIREMENTS OF ASTM F2418, "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- ONLY CHAMBERS THAT ARE APPROVED BY THE SITE DESIGN ENGINEER WILL BE ALLOWED. THE CHAMBER MANUFACTURER SHALL SUBMIT THE FOLLOWING UPON REQUEST TO THE SITE DESIGN ENGINEER FOR APPROVAL BEFORE DELIVERING CHAMBERS TO THE PROJECT SITE:
- a. A STRUCTURAL EVALUATION SEALED BY A REGISTERED PROFESSIONAL ENGINEER THAT DEMONSTRATES THAT THE SAFETY FACTORS ARE GREATER THAN OR EQUAL TO 1.95 FOR DEAD LOAD AND 1.75 FOR LIVE LOAD, THE MINIMUM REQUIRED BY ASTM
- F2787 AND BY AASHTO FOR THERMOPLASTIC PIPE. A STRUCTURAL EVALUATION SEALED BY A REGISTERED PROFESSIONAL ENGINEER THAT DEMONSTRATES THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, SECTION 12.12, ARE MET. THE 50 YEAR CREEP MODULUS DATA SPECIFIED IN ASTM F2418 MUST BE USED AS PART OF THE AASHTO STRUCTURAL EVALUATION TO VERIFY LONG-TERM PERFORMANCE.
- c. STRUCTURAL CROSS SECTION DETAIL ON WHICH THE STRUCTURAL EVALUATION IS BASED. 8. CHAMBERS AND END CAPS SHALL BE PRODUCED AT AN ISO 9001 CERTIFIED MANUFACTURING FACILITY.

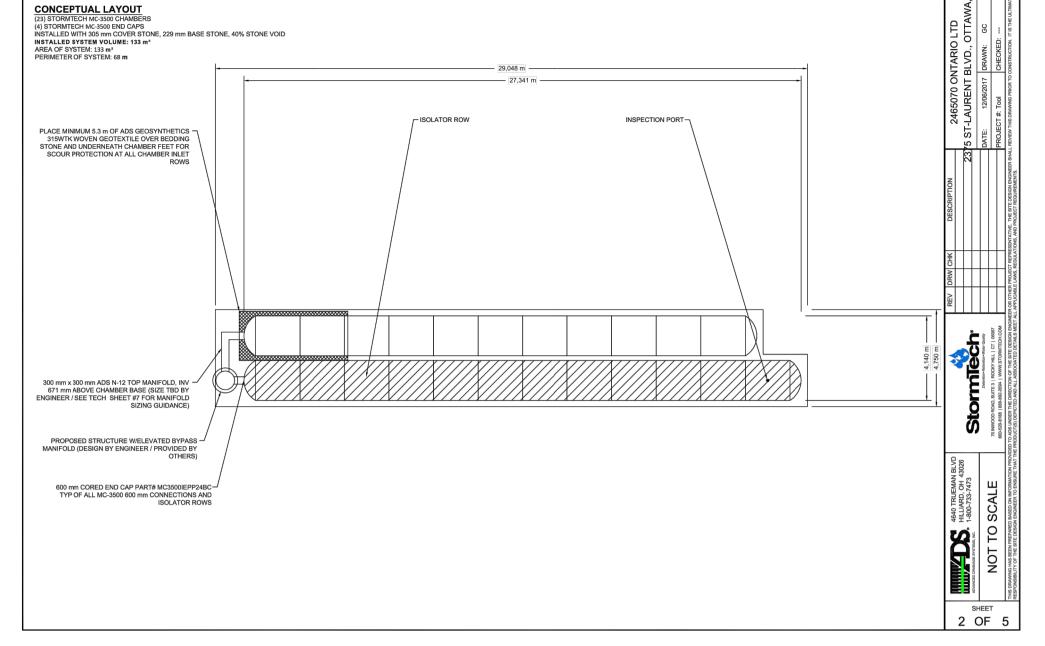
- IMPORTANT NOTES FOR THE BIDDING AND INSTALLATION OF MC-3500 CHAMBER SYSTEM
- STORNTECH MC-3500 CHAMBERS SHALL NOT BE INSTALLED UNTIL THE MANUFACTURER'S REPRESENTATIVE HAS COMPLETED A
 PRE-CONSTRUCTION MEETING WITH THE INSTALLERS.
- 2. STORMTECH MC-3500 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH MC-3500/MC-4500 CONSTRUCTION GUIDE". 3. CHAMBERS ARE NOT TO BE BACKFILLED WITH A DOZER OR AN EXCAVATOR SITUATED OVER THE CHAMBERS.
- STORMTECH RECOMMENDS 3 BACKFILL METHODS:
 STONESHOOTER LOCATED OFF THE CHAMBER BED.
 BACKFILL AS ROWS ARE BUILT USING AN EXCAVATOR ON THE FOUNDATION STONE OR SUBGRADE.
 BACKFILL FROM OUTSIDE THE EXCAVATION USING A LONG BOOM HOE OR EXCAVATOR.
- 4. THE FOUNDATION STONE SHALL BE LEVELED AND COMPACTED PRIOR TO PLACING CHAMBERS.
- 5. JOINTS BETWEEN CHAMBERS SHALL BE PROPERLY SEATED PRIOR TO PLACING STONE.
- 6. MAINTAIN MINIMUM 9" (230 mm) SPACING BETWEEN THE CHAMBER ROWS. 7. INLET AND OUTLET MANIFOLDS MUST BE INSERTED A MINIMUM OF 12" (300 mm) INTO CHAMBER END CAPS.
- EMBEDMENT STONE SURROUNDING CHAMBERS MUST BE A CLEAN, CRUSHED, ANGULAR STONE 3/4-2" (20-50 mm) MEETING THE AASHTO M43 DESIGNATION OF #3 OR #4.^U STONE MUST BE PLACED ON THE TOP CENTER OF THE CHAMBER TO ANCHOR THE CHAMBERS IN PLACE AND PRESERVE ROW SPACING...\J ADS RECOMMENDS THE USE OF "FLEXSTORM CATCH IT" INSERTS DURING CONSTRUCTION FOR ALL INLETS TO PROTECT THE SUBSURFACE STORMWATER MANAGEMENT SYSTEM FROM CONSTRUCTION SITE RUNOFF. NOTES FOR CONSTRUCTION EQUIPMENT
- STORMTECH MC-3500 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH MC-3500/MC-4500 CONSTRUCTION GUIDE".\(^1\)
 THE USE OF EQUIPMENT OVER MC-3500 CHAMBERS IS LIMITED:

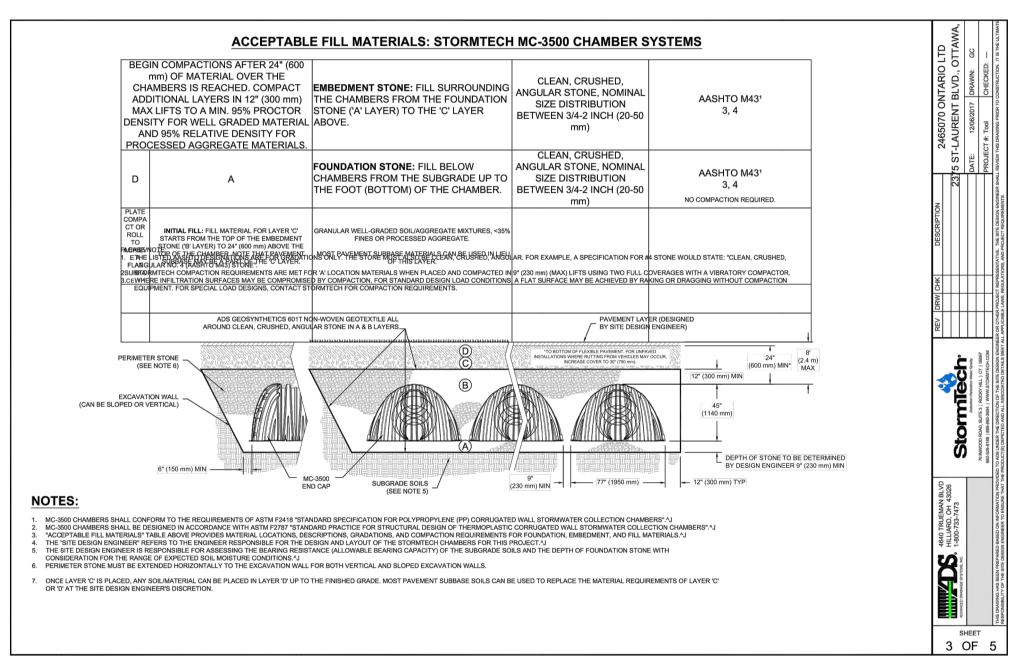
 NO ROUIPMENT IS ALLOWED ON BARE CHAMBERS.

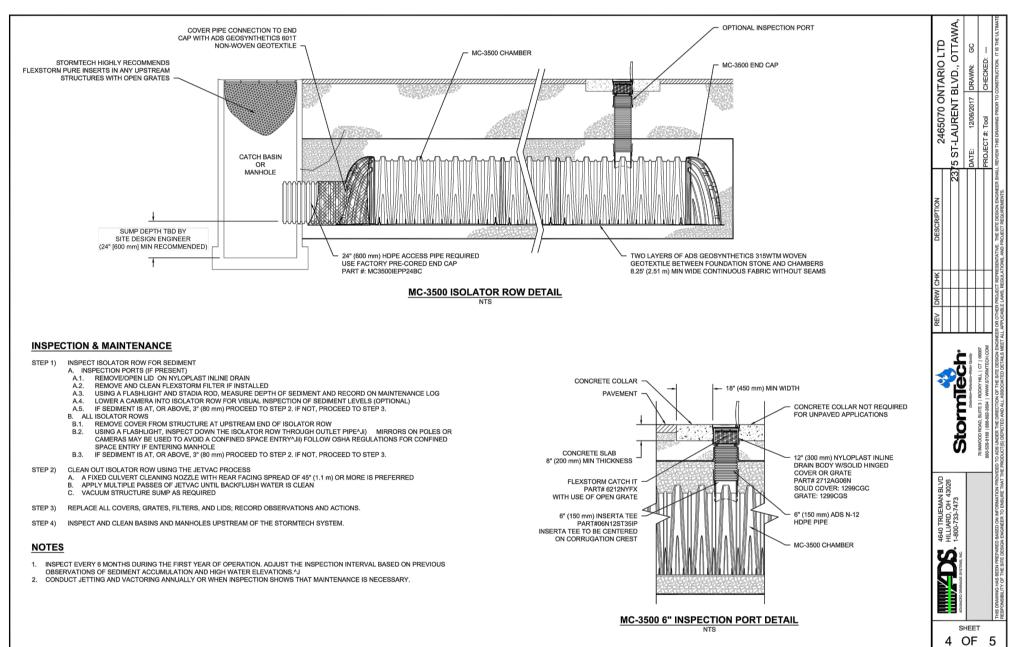
 NO RUBBER TIRED LOADER, DUMP TRUCK, OR EXCAVATORS ARE ALLOWED UNTIL PROPER FILL DEPTHS ARE REACHED IN ACCORDANCE WITH THE "STORMTECH MC-3500/MC-4500 CONSTRUCTION GUIDE".

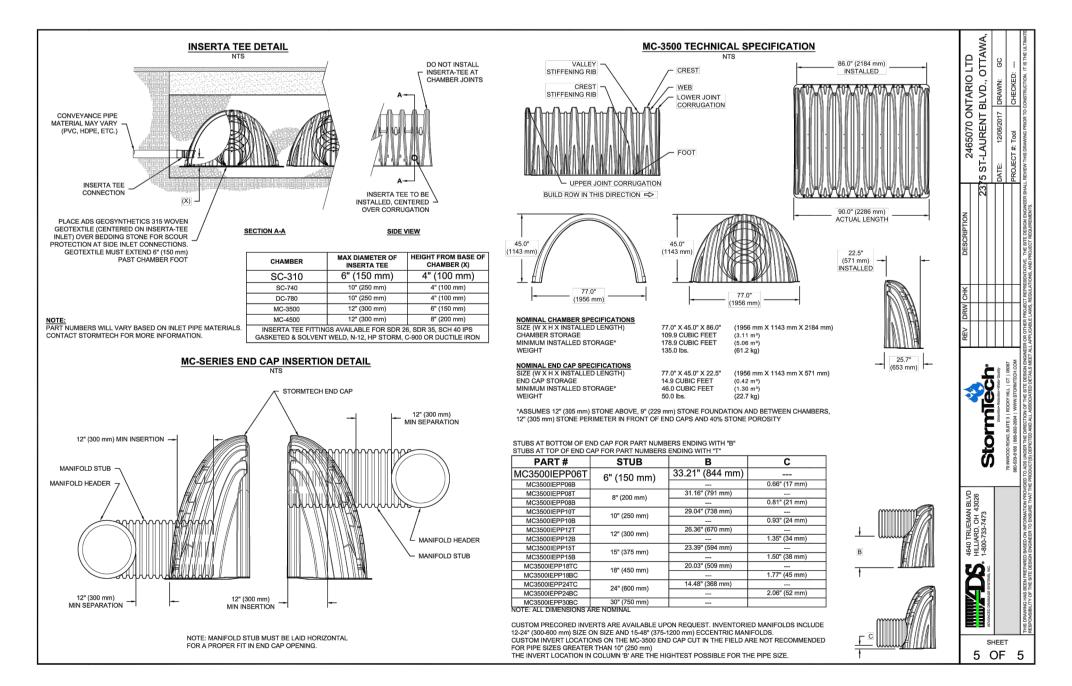
 WEIGHT LIMITS FOR CONSRUCTION EQUIPMENT CAN BE FOUND IN THE "STORMTECH MC-3500/MC-4500 CONSTRUCTION GUIDE".

CONTACT STORMTECH AT 1-888-892-2694 WITH ANY QUESTIONS ON INSTALLATION REQUIREMENTS OR WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT









USE AND INTERPRETATION OF DRAWINGS

GENERAL CONDITIONS OF THE CONTRACT FOR CONSTRUCTION ARE PART OF THE CONTRACT DOCUMENTS AND DESCRIBE USE AND INTENT OF THE DRAWING. THE CONTRACT DOCUMENTS INCLUDE NOT ONLY THE DRAWINGS, BUT ALSO THE OWNER-CONTRACTOR AGREEMENTS, CONDITIONS OF THE CONTRACT, THE SPECIFICATIONS, ADDENDA, AND MODIFICATIONS ISSUED AFTER EXECUTION OF THE CONTRACT. THESE CONTRACT DOCUMENTS ARE COMPLEMENTARY, AND WHAT IS REQUIRED BY ANY ONE SHALL BE BINDING AS IF REQUIRED BY ALL. WORK NOT COMPLETELY DELINEATED HEREON SHALL BE CONSTRUCTED OF THE SAME MATERIALS AND DETAILED SIMILARLY AS WORK SHOWN MORE COMPLETELY

BY USE OF THE DRAWINGS FOR CONSTRUCTION OF THE PROJECT. THE OWNER CONFIRMS THAT HE HAS REVIEWED AND APPROVED THE DRAWINGS. THE CONTRACTOR CONFIRMS THAT HE HAS VISITED THE SITE, FAMILIARIZED HIMSELF WITH THE LOCAL CONDITIONS, VERIFIED FIELD DIMENSIONS AND CORRELATED HIS OBSERVATIONS WITH THE REQUIREMENTS OF THE CONTRACT DOCUMENTS.

AS INSTRUMENTS OF SERVICE, ALL DRAWINGS, SPECIFICATIONS, CADD FILES OR OTHER ELECTRONIC MEDIA AND COPIED THERE OF FURNISHED BY THE ENGINEER ARE HIS PROPERTY. THEY ARE TO BE USED ONLY FOR THIS PROJECT AND ARE NOT TO BE USED ON ANY OTHER PROJECT, INCLUDING REPEATS OF THE PROJECT. CHANGES TO THE DRAWINGS MAY ONLY BE MADE BY THE ENGINEER.

UNLESS THE REVISION TITLE IS "ISSUED FOR CONSTRUCTION", THESE DRAWINGS SHALL BE CONSIDERED PRELIMINARY AND SHALL NOT BE USED AS A

THESE DRAWINGS ILLUSTRATES THE WORK TO BE DONE. THE ENGINEER IS NOT RESPONSIBLE FOR THE MEANS, METHODS, TECHNIQUES, SEQUENCES, AND PROCEDURES USED TO DO THE WORK OR THE SAFETY ASPECTS OF CONSTRUCTION, AND NOTHING ON THESE DRAWINGS EXPRESSED OR IMPLIEC CHANGES THIS CONDITION. CONTRACTOR SHALL DETERMINE ALL CONDITIONS AT THE SITE AND SHALL BE RESPONSIBLE FOR KNOWING HOW THEY AFFECT TH WORK. SUBMITTAL OF A BID TO PERFORM THIS WORK IS ACKNOWLEDGEMENT OF THE RESPONSIBILITIES, AND THAT THEY HAVE BEEN FULLY CONSIDERED IN PLANNING OF THE WORK, AND THE BID PRICE. NO CLAIMS FOR EXTRA CHARGES DUE TO THESE CONDITIONS WILL BE FORTHCOMING.

UNAUTHORIZED CHANGES:

IN THE EVENT THE CLIENT, THE CLIENT'S CONTRACTORS OR SUBCONTRACTORS, OR ANYONE FOR WHOM THE CLIENT IS LEGALLY LIABLE MAKES OR PERMITS TO BE MADE ANY CHANGES TO ANY REPORTS, PLANS, SPECIFICATIONS OR OTHER CONSTRUCTION DOCUMENTS PREPARED BY LRL ASSOCIATES LTD. (LRL) WITHOUT OBTAINING LRL'S PRIOR WRITTEN CONSENT, THE CLIENT SHALL ASSUME FULL RESPONSIBILITY FOR THE RESULTS OF SUCH CHANGES. THEREFORE THE CLIEN AGREES TO WAIVE ANY CLAIM AGAINST LRL AND TO RELEASE LRL FROM ANY LIABILITY ARISING DIRECTLY OR INDIRECTLY FROM SUCH UNAUTHORIZED

IN ADDITION, THE CLIENT AGREES, TO THE FULLEST EXTENT PERMITTED BY LAW, TO INDEMNIFY AND HOLD HARMLESS LRL FROM ANY DAMAGES, LIABILITIES OR COST, INCLUDING REASONABLE ATTORNEY'S FEES AND COST OF DEFENSE, ARISING FROM SUCH CHANGES.

IN ADDITION, THE CLIENT AGREES TO INCLUDE IN ANY CONTRACTS FOR CONSTRUCTION APPROPRIATE LANGUAGE THAT PROHIBITS THE CONTRACTOR OF MODIFICATIONS TO LRL'S CONSTRUCTION DOCUMENTS WITHOUT THE PRIOR WRITTEN APPROVAL OF LRL AND THAT FURTHER REQUIRES THE CONTRACTOR TO INDEMNIFY BOTH LRL AND THE CLIENT FROM ANY LIABILITY OR COST ARISING FROM SUCH CHANGES MADE WITHOUT SUCH PROPER AUTHORIZATION.

GENERAL NOTES:

EXISTING SERVICES AND UTILITIES SHOWN ON THESE DRAWINGS ARE TAKEN FROM THE BEST AVAILABLE RECORDS. BUT MAY NOT BE COMPLETE OR TO DATE CONTRACTOR SHALL VERIFY IN FIELD FOR LOCATION AND ELEVATION OF PIPES AND CHECK WITH THE UTILITY COMPANIES BEFORE DIGGING OR PERFORMING

CONTRACTOR IS ADVISED TO COLLECT INFORMATION ON SOIL CONDITIONS BEFORE START OF CONSTRUCTION.

THE ENGINEER WAIVES ANY AND ALL RESPONSIBILITY AND LIABILITY FOR PROBLEMS WHICH ARISE FROM FAILURE TO FOLLOW THESE PLANS SPECIFICATIONS AND THE DESIGN INTENT THEY CONVEY, OR FOR PROBLEMS WHICH ARISE FROM OTHERS' FAILURE TO OBTAIN AND/OR FOLLOW THE ENGINEER'S GUIDANCE WITH RESPECT TO ANY ERRORS, OMISSIONS, INCONSISTENCIES AMBIGUITIES OR CONFLICTS WHICH ARE ALLEGED.

DISCREPANCIES BEFORE WORK COMMENCES. DO NOT SCALE DRAWINGS.

01 ISSUED FOR SPA G.M.C. 13 DEC 2017 REVISIONS BY DATE



IOT AUTHENTIC UNLESS SIGNED AND DATED



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GRAEBECK CONSTRUCTION LTD.

G.M.C. G.M.C. J.C.L.

2465070 ONTARIO LTD. 2375 ST-LAURENT BLVD., OTTAWA, ON

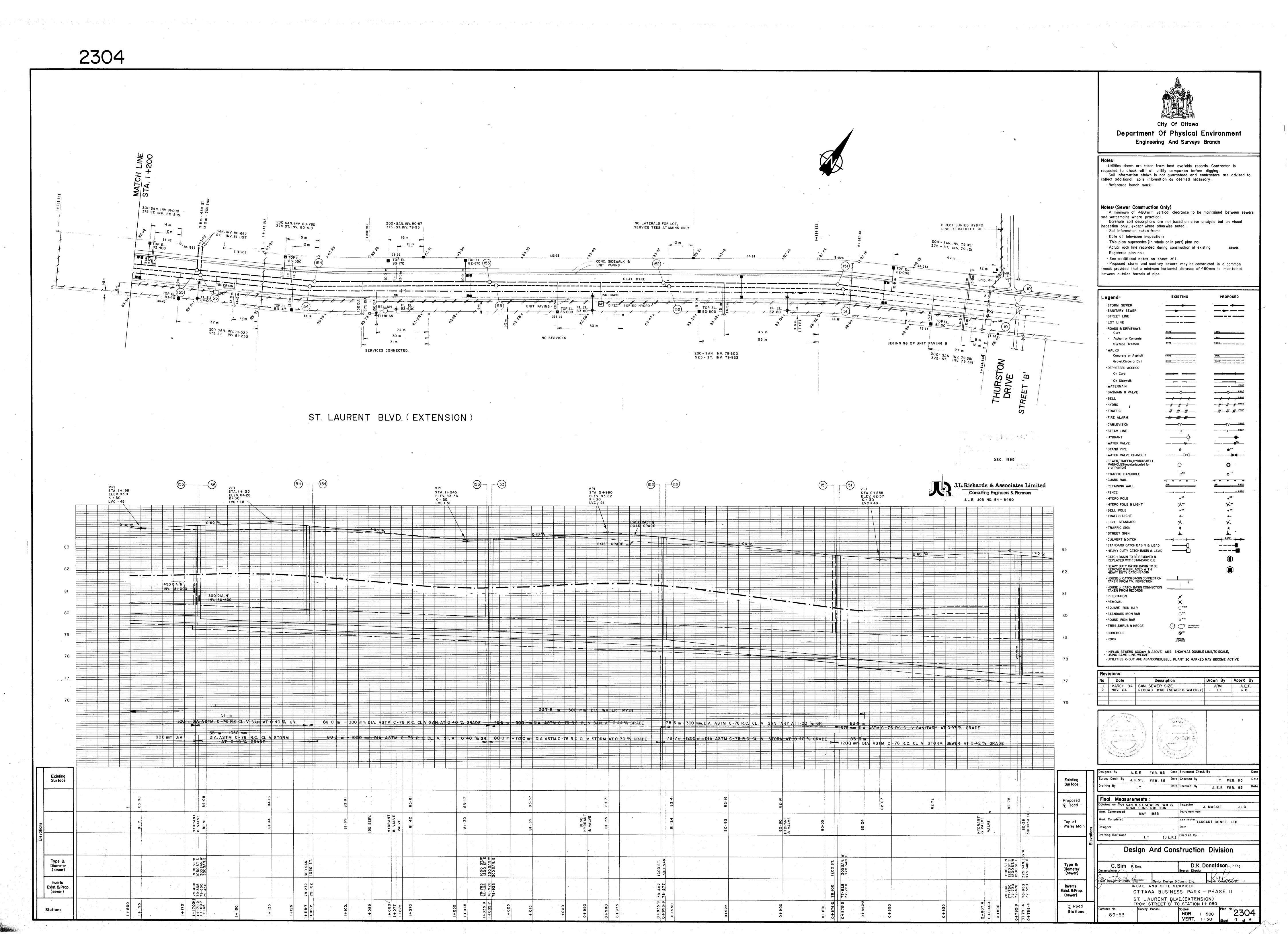
CONSTRUCTION DETAIL PLAN

170721

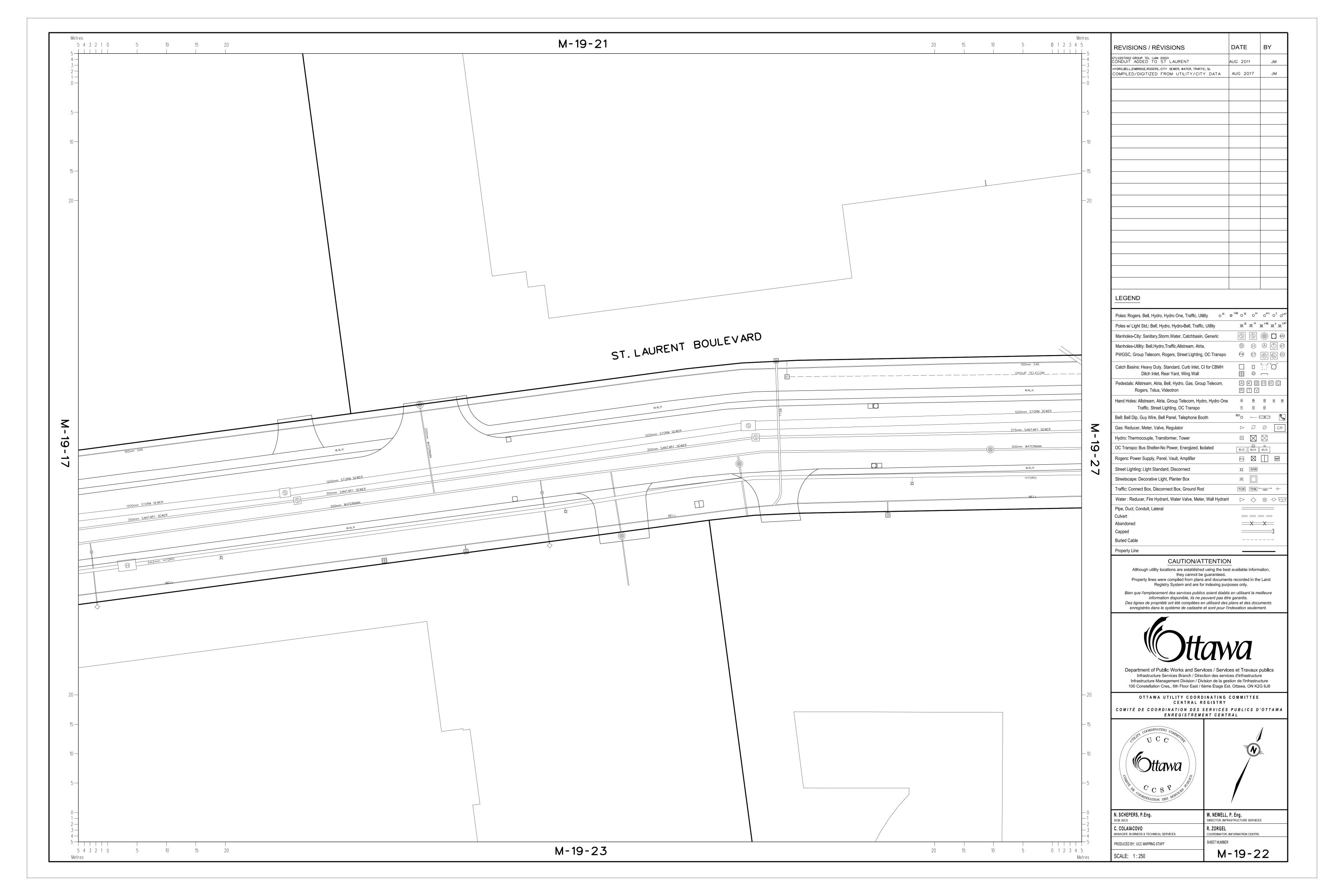
13 DEC 2017

APPENDIX H

St-Laurent Blvd. As-Built Drawings







APPENDIX I

Boundary Conditions

Guillaume Courtois

From: Baker, Adam <adam.baker@ottawa.ca>

Sent: December-13-17 9:18 AM **To:** Guillaume Courtois

Cc: Oram, Cody

Subject: 2375 St-Laurent - Water Boundary Conditions

Attachments: 2375 St-Laurent Dec 2017.pdf

Follow Up Flag: Follow up Flag Status: Flagged

Hi Guillaume,

Please find attached the boundary conditions requested for 2375 St-Laurent Blvd:

The following are boundary conditions, HGL, for hydraulic analysis at 2375 St-Laurent (zone 2C) assumed to be connected to the 305mm on St-Laurent (see attached PDF for location).

Minimum HGL = 124.5m

Maximum HGL = 130.6m

Max Day + Fire Flow (150 L/s) = 124.0m

These are for current conditions and are based on computer model simulation.

Disclaimer: The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation.

If you have any questions, let me know.

Thanks,

Adam Baker, E.I.T.

Engineering Intern

Planning, Infrastructure and Economic Development Department - Services de la planification, de l'infrastructure et du développement économique

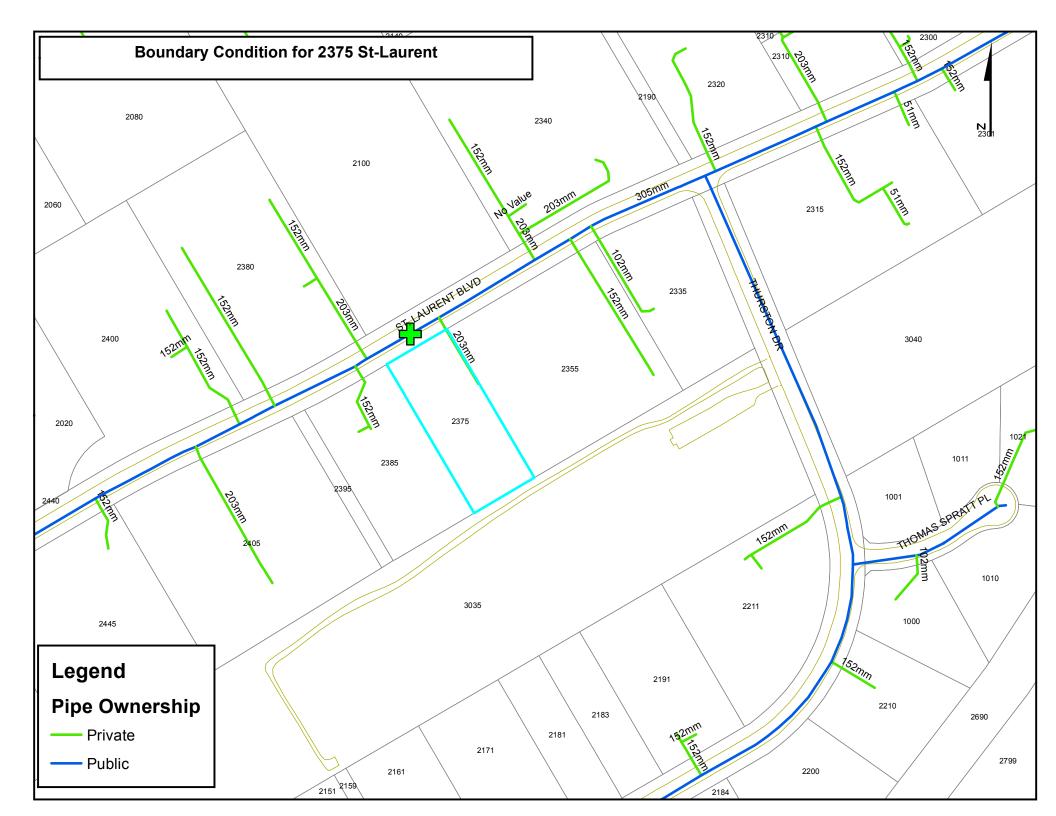
Development Review - South Branch

City of Ottawa | Ville d'Ottawa

110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1

613.580.2424 ext./poste 26552, Adam.Baker@ottawa.ca

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APPENDIX J Overland Ponding Volume Table

Overland Ponding Volume Report

Generated: 2017-12-07 14:40:49

By user: gcourtois

Drawing: W:\FILES 2017\170721\06 CivilDesign\Drawings\LRL Civil Plans\W:\FILES 2017\170721\06 CivilDesign\Drawings\LRL Civil Plans\170721-02.dwg

Volume Summary							
Name	Туре	Cut Factor	Fill Factor	2d Area (hectares)	Cut (Cu. M.)	Fill (Cu. M.)	Net (Cu. M.)
CBMH1 PONDING VOLUME HWL83.47	full	1.00	1.00	0.02	0.00	15.90	15.90 <fill></fill>
CBMH2 PONDING VOLUME HWL83.47	full	1.00	1.00	0.02	0.00	14.87	14.86 <fill></fill>
CBMH3 PONDING VOLUME HWL83.47	full	1.00	1.00	0.01	0.00	6.83	6.83 <fill></fill>
CBMH4 PONDING VOLUME HWL83.47	full	1.00	1.00	0.02	0.00	11.27	11.27 <fill></fill>
CBMH5 PONDING VOLUME HWL83.47	full	1.00	1.00	0.02	0.00	13.91	13.91 <fill></fill>

Totals				
	2d Area (hectares)	Cut (Cu. M.)	Fill (Cu. M.)	Net (Cu. M.)
Total	0.09	0.01	62.78	62.78 <fill></fill>

^{*} Value adjusted by cut or fill factor other than 1.0