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Proposed High-Rise Residential Development 829 Carling Avenue

Serviceability and Stormwater Management Report



Proposed High-Rise Residential Development 829 Carling Avenue

Serviceability and Stormwater Management Report

Prepared for:

Claridge Homes

Prepared By:

NOVATECH

Suite 200, 240 Michael Cowpland Drive Ottawa, Ontario K2M 1P6

April 15, 2021

Novatech File: 121008 Ref No. R-2021-055



April 15, 2021

City of Ottawa Planning, Infrastructure and Economic Development Department Planning and Infrastructure Approvals Branch 110 Laurier Avenue West, 4th Floor Ottawa ON, K1P 1J1

Attention: Mr. Shawn Wessel, A.Sc.T.,rcji

Dear Sir:

Reference: 829 Carling Avenue - Claridge Development

Serviceability and Stormwater Management Report

Enclosed is the Serviceability and Stormwater Management Report for the proposed 829 Carling Avenue development located along Sidney Street, Preston Street and Carling Avenue in the City of Ottawa. This report is submitted in support of the OPA, zoning amendment and site plan application and outlines how the site will be serviced with public infrastructure.

Trusting this report is adequate for your purposes. Should you have any questions, or require additional information, please contact me.

Yours truly,

NOVATECH

Greg MacDonald, P. Eng.

Director, Land Development and Public Sector Infrastructure

cc: Vincent, Denomme, Claridge Homes

829 Carling Avenue Serviceability Report

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1.0 INTRODUCTION

This Serviceability Study has been prepared in support of Official Plan Amendment, Zoning By-Law Amendment and Site Plan Control applications for the Claridge lands located at 829 Carling Avenue, as shown in **Figure 1 – Key Plan of Subject Site**. The subject site is currently occupied by a CIBC banking centre. The subject site is currently served by one driveway to Carling Avenue, and one driveway to Sidney Street. The proposed redevelopment will include a total of 459 apartment dwellings, and 387 parking spaces.

The subject site has an approximate area of 0.15 hectares, and is surrounded by the following:

- Sidney Street and future high-rise residential development to the north;
- Carling Avenue and Dow's Lake Public Parking to the south;
- Preston Street and future high-rise residential development to the east; and
- An existing auto dealership to the west.

The most recent aerial view of the subject site is provided in **Figure 1**.



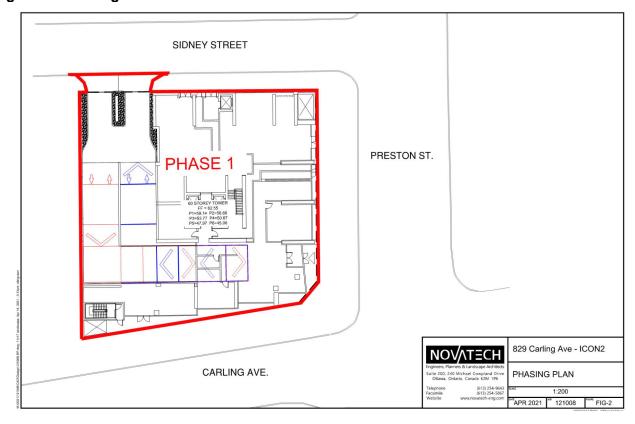
1.1 Proposed Development

The subject site is located within the 'Mixed Use Centre' on Schedule B of the City of Ottawa's Official Plan. The implemented zoning for the property is 'Arterial Mainstreet' (AM1), and the site is within the Preston-Carling District Secondary Plan, which permits the proposed land uses. However, a Zoning By-Law Amendment is required to permit certain attributes of the proposed development, such as building height.

The proposed development will be constructed in one phase as shown in **Figure 2 – Phasing Plan** and as described below.

- Phase 1 (Tower):
 - o 62-storey high-rise including 7-storey podium with 459 dwellings.

Figure 2 Phasing Plan



In total, the proposed development will consist of 459 apartment dwellings. The entire site will include 387 parking spaces for residents and visitors and will be accessed via full-movement driveway to Sidney Street. Phase 1 of the development is anticipated to be built out by 2028.

A copy of the Site Plan is included in **Appendix A – Site Plan**.

2.0 SANITARY SEWER

The development will be serviced by the existing 450mm diameter combined sewer on Sidney Street as shown on the general plan of services.

The service will be a 300mm diameter sanitary sewer to Sidney.

The proposed development flows are based on the City of Ottawa Sewer Design Guidelines and are provided below.

2.1 Proposed Sanitary Flows from Development Site

Proposed sanitary flows are summarized in **Table 2.1 – Proposed Sanitary Flows** with detailed calculations below. Development statistics are summarized in **Table 2.2 – Development Statistics**. A Phasing Plan is shown in **Figure 2 – Phasing Plan**.

Table 2.1 Proposed Sanitary Flows

Phase	Peak Sanitary Flow (L/sec)
Tower	8.78
Total	8.78

Table 2.2 Development Statistics

Building Component	Area (ha)	Bachelor (x1.4)	1 Bdr (x1.4)	2 Bdr (x2.1)	3 Bdr (x3.1)	Total
Tower						
Tower (incl. Podium)	-	50	193	189	27	459
Total	0.15	50	193	189	27	459
Grand Total	0.15	50	193	189	27	459

Sanitary Flows - Tower

Area = 0.15 ha

Tower (incl. Podium): 70.0 + 270.2 + 396.9 + 83.7 = 820.8 people

Total: 821 people

Sanitary flows are calculated below using the City's new Sewer Design Criteria.

Population = 821 people Peak Factor = 1 + $14/(4 + (P/1000)^{1/2}) \times 0.80 = 3.28$ Area = 0.15 ha

Q
$$_{\text{Tower}} = \frac{(821)(280)}{86,400}(3.28) + (0.15)(0.33) = 8.78 \text{ L/sec}$$

Therefore, the total peak sanitary flow for **Tower is 8.78 L/sec.**

Furthermore, the total peak sanitary flow for all **Phases is 8.78 L/sec.**

3.0 STORM SEWER AND STORMWATER MANAGEMENT

As part of this development, stormwater will be controlled on-site and discharged via a 300mm dia. service that will connect to the existing 450mm dia. combined sewer on Sidney Street as shown on the general plan of services.

The site has an overall slope towards Sidney Street. The majority of storm runoff from the site is self-contained with some being conveyed overland towards Sidney Street, Preston Street, Carling Avenue and neighboring property.

3.1 Storm Water Management Criteria

Stormwater management (SWM) design criteria for the proposed development were established by the City of Ottawa Sewer Design Guidelines (October 2012) and correspondence with the City of Ottawa. The SWM design criteria are as follows:

- Control post-development peak flows up-to and including the 100-year storm event to the
 allowable release rate. Provide on-site water quantity control for all flow in excess of the
 allowable release rate. The allowable release rate is to be determined by applying the
 following parameters to the site area:
 - A runoff coefficient of 0.4
 - o A time of concentration of 20 minutes
 - A 2-year intensity using the City of Ottawa Intensity-Duration-Frequency (IDF) curves
- Minimize the impact on the downstream receiving watercourses by minimizing the potential erosion and volume of sediment entering the watercourses both on a temporary basis (during construction) and on a permanent basis.
- Provide guidelines to ensure that site preparation and construction is in accordance with the current Best Management Practices for Erosion and Sediment Control.

3.2 Hydrologic and Hydraulic Modelling

The allowable release rate for the 0.15 ha site was determined to be 8.68 L/s based on the SWM criteria provided by the City of Ottawa.

The rational method was used to estimate post-development peak flows (quantity control targets) and determine approximate storage requirements for the site.

The post-development drainage areas were delineated based on the proposed development grading. Refer to **Drawing 121008-GR** for the proposed site grading and **Drawing 121008-STM** for the drainage areas. The storage requirements are based on meeting the allowable release rate generated for the site.

The site will be graded such that flows in excess of the 100-year storm event will be conveyed overland to Sidney Street, Preston Street and Carling Avenue.

Design Storms

The design storms are based on City of Ottawa design storms. Design storms were used for the 5 and 100-year return periods (i.e. storm events).

Model Parameters

Post-development catchments were modelled based on the proposed site plan and grading as shown on **Drawing 121008-STM**. All the sub-catchments are assumed to be 100% impervious with exception to the grassed areas which are 0% impervious. The building roofs were assumed to have no depression storage.

A summary of the allowable release rate, post-development parameters and output for the 5 and 100-year storm events are provided in **Appendix C – Stormwater Management Calculations**.

3.3 Water Quantity Control

On-site stormwater management will be implemented to control post-development stormwater discharge to the allowable release rate of 8.68 L/s and will be achieved using an internal stormwater tank that will be pumped to the combined sewer on Sidney Street.

Runoff from the surrounding areas (Sub-catchments A-1, A-2, A-3 and A-4) will be uncontrolled and will drain towards Sidney Street, Preston Street, Carling Avenue and neighboring property. The total uncontrolled flows from the site in the 100-year event will be 2.17 L/s which requires the remaining areas of the site to be controlled to 6.51 L/s, as shown in **Table 3.1**, in order to meet the allowable release rate.

Table 3.1 Controlled Release Rates

Phase	Drainage Area (ha)	Allowable Release Rate (L/s)
Tower	0.15	6.51
Total	0.15	6.51

The runoff will be collected into at least one tank located within the development. The site was modeled so that the pump rate was equal to the allowable release rate. The tank will be pumped to the combined sewer in Sidney Street at 6.51 L/sec and will have an emergency overflow that will connect to the ground surface. The required storage in the 100-year event is summarized in **Table 3.2**.

Table 3.2 Required Tank Storage for the 100-year Storm

Phase	Required Storage Volume (m ³)
Tower	60
Total	60

The storage provided allows for the proposed development to meet the allowable release rate of 8.68 L/s. The total release rate from the site during the 100-year storm event is provided in **Table 3.3**.

Table 3.3 Overall Site Release Rate for the 100-year Storm

Phase	Drainage Area (ha)	Allowable Release Rate (L/s)
Tower	0.15	6.51
Uncontrolled	0.00	2.17
Total	0.15	8.68

3.4 Water Quality Control

Runoff from the roofs, podiums, and uncontrolled areas would be considered clean and will not require treatment. Additionally, the storage tank will allow for some settling of particulates in the stored runoff from the remaining site areas. Additional water quality treatment will not be required. Erosion and sediment control measures will be implemented during all phases of construction and inspected regularly.

Cistern from Tower will discharge to the existing combined sewer on Sidney Street.

The site will be graded such that flows in excess of the 100-year storm event will be conveyed overland to Sidney Street, Preston Street and Carling Avenue.

4.0 WATERMAIN

4.1 Domestic Water Demand

The proposed development will be serviced by the 150mm dia. watermain on Sidney Street as shown on the General Plan of Services. Shutoff valves will be provided at property lines as per City of Ottawa Specifications. The water meter will be in the basement level mechanical room of the building. Similarly, remote receptacle will be located at the surface near the entrance to the building on the exterior.

The services will be two (2) 150mm diameter water services to Sidney.

Estimated domestic water demands for the development are provided below with a detailed breakdown per phase:

Watermain Flows - Tower

Average Day Demand = 3.33 L/sec

Maximum Day Demand (x2.5) = 8.33 L/sec

Peak Hour Demand (x2.2) = 18.32 L/sec

4.2 Fire Demand

An estimate of the water required to meet firefighting demands is described below.

Section 4.2.11 of the City of Ottawa Water Design Guidelines reads:

"When calculating the fire flow requirements and affected pipe sizing, designers shall use the method developed by the Fire Underwriters Survey", and

"The requirements for levels of fire protection on private property are covered in Section 7.2.11 of the Ontario Building Code."

The Fire Underwriters Survey is used to assess the performance of the water distribution system on a "City Block" basis rather than an individual building basis. The Ontario Building Code governs the assessment of fire demand for individual buildings.

Section 7.2.11.1 of the Ontario Building Code states that the design, construction, installation and testing of fire service mains and water service pipe combined with fire service mains shall be in conformance with NFPA 24.

NFPA 24 is the standard for the "Installation of Private Fire Service Mains and their Appurtenances". Chapter 13 of NFPA 24 discusses sizing the private service fire mains for fire protection systems which shall be approved by the authority having jurisdiction, considering the following factors:

- Construction and Occupancy of the Building
- Fire Flow and Pressure of the Water Required
- Adequacy of the Water Supply

It is expected that any future building on the site will be sprinklered per Section 3.2.2.45 of the OBC. Section 3.2.5.7 of the OBC requires that an adequate water supply for fire fighting be provided to each building, and references Appendix A of the OBC. Sentence 3 of Section A 3.2.5.7 of the OBC (Appendix A) states that NFPA 13 be used for determining both sprinkler and hose stream demands for a sprinklered building.

The design of the sprinkler system is completed by a Fire Protection Engineer, or typically computed by the sprinkler contractor and approved by the Fire Protection Engineer. This process involves detailed hydraulic calculations based on building layout, pipe runs, head losses, fire pump requirements, etc. At this stage in the planning and site design process, these details are not available. Therefore, this report will confirm the maximum anticipated sprinkler and hose stream demands as per NFPA 13.

Section 11.2.3 of the NFPA 13, "Water Demand Requirements – Hydraulic Calculations Methods" was used to estimate the sprinkler and hose stream demands. Figure 11.2.3.1.1 – Area/Density Curves confirms the sprinkler demand, assuming Ordinary 1 construction. Table 11.2.3.1.2 confirms the hose stream allowance and water supply demand requirements, assuming ordinary hazard construction.

For Ordinary 1 type construction, design is based on a density of 0.15 gpm (US), and a maximum area of sprinkler operation limited to 1500 ft² (139 m²). As per NFPA 13 Figure 11.2.3.1.1, the maximum anticipated sprinkler demand is 225 gpm (US). As per NFPA 13 Table 11.2.3.1.2, the maximum total combined inside and outside hose demand is 250 gpm (US) with a duration of 60-90 minutes.

Based on the calculations above, the total estimated sprinkler and hose demand for the development is 475 gpm (US). However, because the development has not been finalized to-date, it is recommended to add a 50% contingency. Therefore, a sprinkler demand of 713 gpm (US), 2700L/min, should be anticipated at this stage. Refer to **Appendix E – Fire Demand Calculations.**

Boundary conditions are requested from the City of Ottawa using a fire demand calculated using the **Fire Underwriters Insurance** procedure. This method is used by municipalities to assess their systems on a more global basis and results in a more conservative fire demand for individual sites, as compared to Building Code calculations. The estimated fire demand using FUS for each of the phases is provided in **Table 4.1 – Calculated Fire Demand.** Detailed calculations are included in **Appendix D – Fire Demand.**

Table 4.1 Calculated Fire Demand

Phase	Fire Demand (L/min)				
Tower	5000				

5.0 CONCLUSIONS

Based on the foregoing, report conclusions are:

- Adequate sanitary sewer capacity is available on Sidney Street.
- On site stormwater management will be implemented to control post-development flows to that
 value calculated using a tc of 20 minutes, run-off coefficient of 0.40 and 2-year storm. This will
 be implemented through construction of a cistern in underground parking structure as
 summarized below. Uncontrolled flow from surrounding areas will drain overland to Sidney
 Street, Preston Street and Carling Avenue.

Phase	Cistern Volume (m³)	Discharge (L/s)	Street Sewer
Tower	60	6.51	Sidney Street
1-4	Uncontrolled	2.17	Uncontrolled to Sidney Street, Preston Street and Carling Avenue
Total	60	8.68	

Adequate water services are available on Sidney Street for domestic demand. It is expected
that adequate water supply is available for firefighting which will be confirmed once boundary
conditions are received from the City. Calculated fire demand ranged from 5000 L/min. The
buildings will be equipped with fire pumps and sprinklers.

NOVATECH

Prepared by:

Jazmine Gauthier, B.A.Sc.

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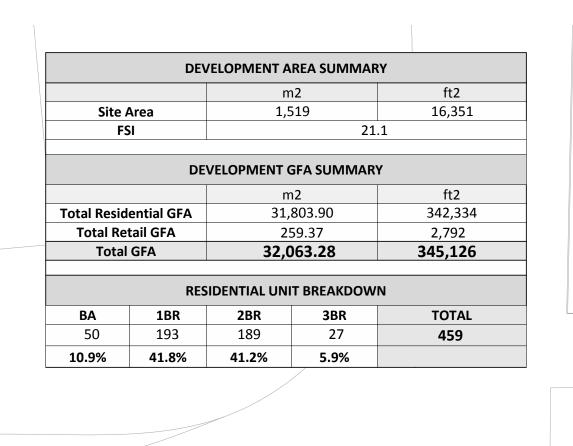
Project Manager | Land Development

Reviewed by:

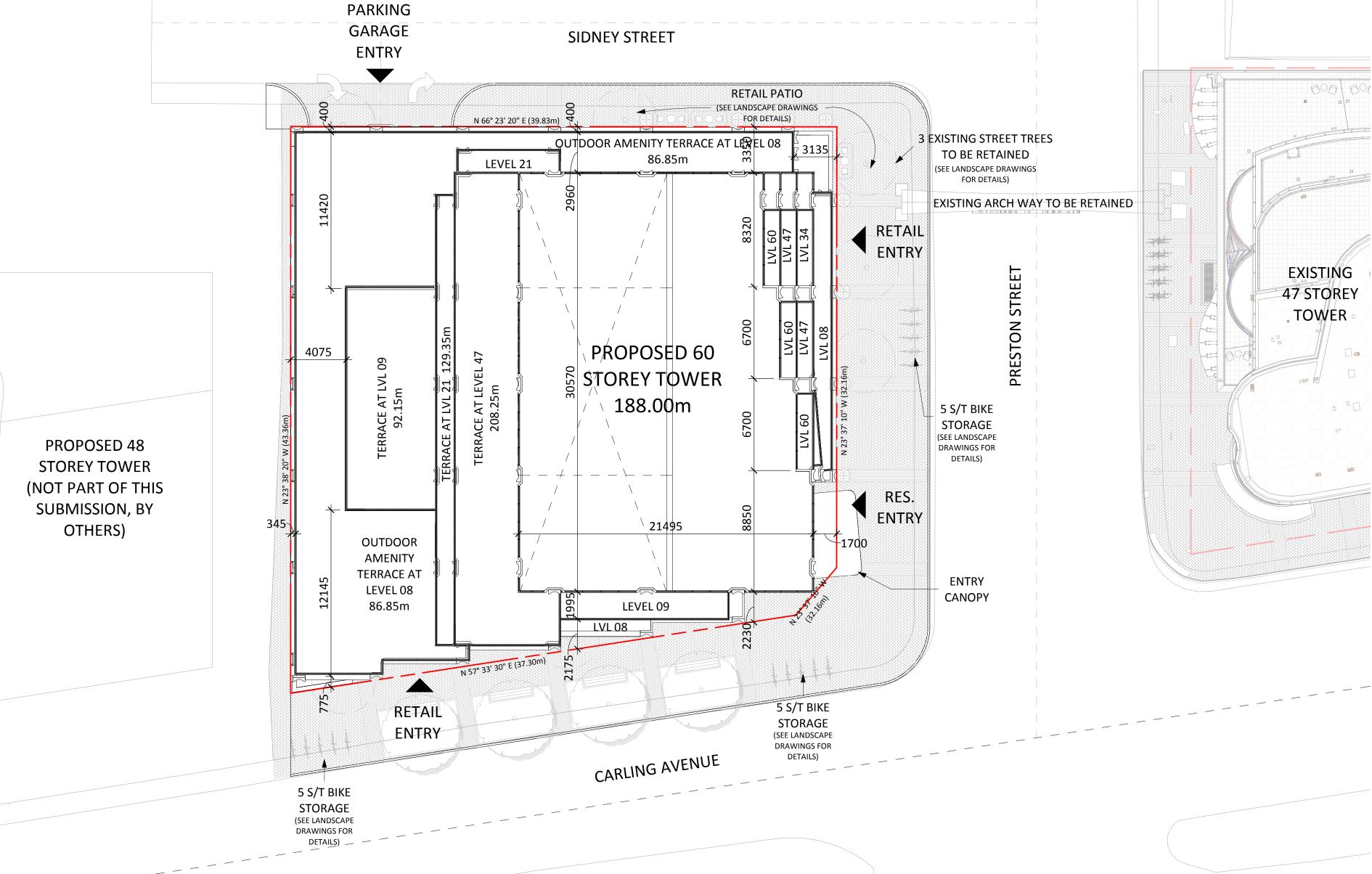


Greg MacDonald, P.Eng.
Director Land Development and Public Sector
Infrastructure

APPENDIX A Site Plan



PROPOSED 30 STOREY TOWER
(NOT PART OF THIS
SUBMISSION, BY OTHERS)



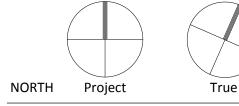
General Notes

These Contract Documents are the property of the
Architect. The Architect bears no responsibility for the
interpretations of these documents by the contractor.
Upon written application the Architect will provide
written/graphic clarification or supplementary information
regarding the intent of the Contract Documents. The
Architect will review Shop Drawings submitted by the

Contractor for design conformance only.

2. Drawings are not to be scaled for construction. Contractor to verify all existing conditions and dimensions required to perform the Work and report any discrepancies with the Contract Documents to the Architect before commencing

Positions of exposed or finished mechanical or electrical devices, fittings, and fixtures are indicated on the Architectural drawings. The locations shown on the Architectural drawings govern over the Mechanical and Electrical drawings. Those items not clearly located will be located as directed by the Architect.



KEYPLAN

PROJECT TEAM

T CLARIDGE HOMES

ARCHITECT HARIRI PONTARINI ARCHITECTS

LANDSCAPE JAMES B. LENNOX + ASSOCIATES

PLANNING FOTENN PLANNING + DESIGN
STRUCTURAL GOODEVE STRUCTURAL INC.

CIVIL/TRAFFIC NOVATECH GROUP

GEOTECH PATERSON GROUP INC.

WIND GRADIENT WIND ENGINEERING

SURVEYOR ANNIS, O'SULLIVAN,

VOLLEBEKK LTD.

MAINIC STATUS

DRAWING STATUS

NOT FOR CONSTRUCTION

1 2021-04-15 ISSUED FOR OPA/ZBA/SPA

DESCRIPTION

NO. YYYY-MM-DD

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Project Title:

829 Carling Ave Mixed-Use Development

829 CARLING AVE. OTTAWA, ON

SITE PLAN

Project number: 2030
Scale: 1:200
Sheet Start Date: 11/23/20

Drawn / Checked by: HPA HPA

Drawing No.:

A102



Revision:

APPENDIX B Stormwater Management Calculations



Runoff Coefficients

Drainage Area	Total Area	Hard Surf	ace Area	Grass	Area	5-Year Runoff	100-Year Runoff	
	(m)	Area (m ²)	С	Area (m ²)	С	Coefficient	Coefficient	
A-01	19.0	19.0	0.95	0.0	0.20	0.95	1.00	
A-02	18.0	18.0	0.95	0.0	0.20	0.95	1.00	
A-03	5.9	5.9	0.95	0.0	0.20	0.95	1.00	
A-04	0.8	0.8	0.95	0.0	0.20	0.95	1.00	
Total	43.72	43.7	0.95	0.0	0.20	0.95	1.00	



Controlled Flow

5 YR

Area No.	Area (ha)	C _{5yr}	Time (min)	intensity mm/hr	Uncontrolled runoff L/s	Control System	Zurn Model Number	Release Rate (L/s/m of head)	Notches	Depth (m)	Controlled Flow (L/s)	Storage available (m³)	Storage used (m³)
A-01	0.0019	0.95	10.00	104.19	0.52	no control	-	-	-	-	-	-	-
A-02	0.0018	0.95	10.00	104.19	0.50	no control	-	-	-	-	-	-	-
A-03	0.0006	0.95	10.00	104.19	0.16	no control	-	-	-	-	-	-	-
A-04	0.0001	0.95	10.00	104.19	0.02	no control	i	-	-	-	-	-	-
CB Storage	-	-	-	-	-	-	-	-	-	-	-	-	-
Total:	0.3716				1.20						40.67	69.90	27.72



100 YR

Area ID	Area (ha)	C _{100yr}	Time (min)	intensity mm/hr	Uncontrolled runoff L/s	Control System	Zurn Model Number	Release Rate (L/s/m of head)	Notches	Depth (m)	Controlled Flow (L/s)	Storage available (m³)	Storage used (m³)
A-01	0.0019	1.00	10.00	178.56	0.94	no control	-	-	-	-	-	-	-
A-02	0.0018	1.00	10.00	178.56	0.89	no control	-	-	-	-	-	-	-
A-03	0.0006	1.00	10.00	178.56	0.29	no control	-	-	-	-	-	-	-
A-04	0.0001	1.00	10.00	178.56	0.04	no control	-	-	-	-	-	-	-
CB Storage	-	-	-	-	-	-	ı	-	-	-	-	-	-
Total:	0.3716				2.17						69.90	69.90	57.41

Note: In all cases, there is only one notch in the Zurn roof drain and and flows through each drain is further reduced with and adjustable weir. See Zurn roof drains

sheet and adjustable weir specification for more details on the reduction of flow.



Allowable release rate

Area	0.15	ha				
С	0.4					
tc	20	min				
i ₂	52.03					
Q allowable = 2.78 x C x i x A 8.68 L/s						



REQUIRED S	REQUIRED STORAGE - 5-YEAR EVENT						
AREA	Tower			: TANK			
OTTAWA IDF	CURVE						
Area =	0.1475	ha		Qallow =	6.51		
C =	0.95			Vol(max) =	26.10		
Time	Intensity	Q _{Uncontrolled}	Q Controlled	Qnet	Vol		
(min)	(mm/hr)	(L/s)	(L/s)	(L/s)	(m ³)		
5	141.18	55.01	0.00	48.50	14.55		
10	104.19	40.60	0.00	34.09	20.45		
15	83.56	32.56	0.00	26.05	23.44		
20	70.25	27.37	0.00	20.86	25.04		
25	60.90	23.73	0.00	17.22	25.83		
30	53.93	21.01	0.00	14.50	26.10		
35	48.52	18.90	0.00	12.39	26.03		
40	44.18	17.22	0.00	10.71	25.69		
45	40.63	15.83	0.00	9.32	25.17		
50	37.65	14.67	0.00	8.16	24.48		
55	35.12	13.69	0.00	7.18	23.68		
60	32.94	12.84	0.00	6.33	22.77		
65	31.04	12.10	0.00	5.59	21.79		
70	29.37	11.44	0.00	4.93	20.73		
75	27.89	10.87	0.00	4.36	19.60		
80	26.56	10.35	0.00	3.84	18.43		
85	25.37	9.88	0.00	3.37	17.21		
90	24.29	9.46	0.00	2.95	15.95		
95	23.31	9.08	0.00	2.57	14.65		
100	22.41	8.73	0.00	2.22	13.32		
105	21.58	8.41	0.00	1.90	11.97		
110	20.82	8.11	0.00	1.60	10.58		
115	20.12	7.84	0.00	1.33	9.17		
120	19.47	7.59	0.00	1.08	7.74		
125	18.86	7.35	0.00	0.84	6.29		
130	18.29	7.13	0.00	0.62	4.82		
135	17.76	6.92	0.00	0.41	3.34		
140	17.27	6.73	0.00	0.22	1.84		
145	16.80	6.55	0.00	0.04	0.32		
150	16.36	6.38	0.00	-0.13	-1.21		
155	15.95	6.21	0.00	-0.30	-2.75		
160	15.56	6.06	0.00	-0.45	-4.31		
165	15.18	5.92	0.00	-0.59	-5.88		
170	14.83	5.78	0.00	-0.73	-7.45		

REQUIRED S	STORAGE - 10	NT			
AREA	Tower			: TANK	
OTTAWA IDF	CURVE				
Area =	0.1475	ha		Qallow =	6.51
C =	1.00			Vol(max) =	59.22
Time	Intensity	Q _{Uncontrolled}	Q Controlled	Qnet	Vol
(min)	(mm/hr)	(L/s)	(L/s)	(L/s)	(m ³)
5	242.70	99.55	0.00	93.04	27.91
10	178.56	73.24	0.00	66.73	40.04
15	142.89	58.61	0.00	52.10	46.89
20	119.95	49.20	0.00	42.69	51.23
25	103.85	42.59	0.00	36.08	54.12
30	91.87	37.68	0.00	31.17	56.11
35	82.58	33.87	0.00	27.36	57.46
40	75.15	30.82	0.00	24.31	58.35
45	69.05	28.32	0.00	21.81	58.89
50	63.95	26.23	0.00	19.72	59.16
55	59.62	24.45	0.00	17.94	59.22
60	55.89	22.93	0.00	16.42	59.09
65	52.65	21.59	0.00	15.08	58.82
70	49.79	20.42	0.00	13.91	58.43
75	47.26	19.38	0.00	12.87	57.92
80	44.99	18.45	0.00	11.94	57.33
85	42.95	17.62	0.00	11.11	56.65
90	41.11	16.86	0.00	10.35	55.90
95	39.43	16.17	0.00	9.66	55.09
100	37.90	15.55	0.00	9.04	54.22
105	36.50	14.97	0.00	8.46	53.29
110	35.20	14.44	0.00	7.93	52.33
115	34.01	13.95	0.00	7.44	51.32
120	32.89	13.49	0.00	6.98	50.27
125	31.86	13.07	0.00	6.56	49.19
130	30.90	12.67	0.00	6.16	48.07
135	30.00	12.30	0.00	5.79	46.93
140	29.15	11.96	0.00	5.45	45.75
145	28.36	11.63	0.00	5.12	44.55
150	27.61	11.32	0.00	4.81	43.33
155	26.91	11.04	0.00	4.53	42.09
160	26.24	10.76	0.00	4.25	40.82
165	25.61	10.50	0.00	3.99	39.53
170	25.01	10.26	0.00	3.75	38.23

PREPARED BY: NOVATECH DATE: APRIL 15, 2021

APPENDIX C Fire Demand Calculations

FUS - Fire Flow Calculations

As per 1999 Fire Underwriter's Survey Guidelines

Novatech Project #: 121008

Project Name: 829 Carling Avenue

Date: 4/15/2021

Input By: Jazmine Gauthier
Reviewed By: Greg MacDonald

Legend

Input by User

No Information or Input Required

Engineers, Planners & Landscape Architects

Building Description: 62 Storey Building with 7 Storey Podium

Fire Resistive Construction

Step			Choose		Value Used	Total Fire Flow (L/min)
	•	Base Fire Flo	w			, ,
	Construction Ma	iterial		Multi	iplier	
	Coefficient	Wood frame		1.5		
1	Coefficient related to type	Ordinary construction		1		
•	of construction	Non-combustible construction		0.8	0.6	
	C	Modified Fire resistive construction (2 hrs)	Yes	0.6		
	Ŭ	Fire resistive construction (> 3 hrs)		0.6		
	Floor Area					
		Podium Level Footprint (m ²)	1411			
		Total Floors/Storeys (Podium)	7			
	Α	Tower Footprint (m ²)	1463			
2	A	Total Floors/Storeys (Tower)	55			
		Protected Openings (1 hr)	Yes			
		Area of structure considered (m ²)			2,117	
	F	Base fire flow without reductions				C 000
	F	$F = 220 \text{ C (A)}^{0.5}$				6,000
		Reductions or Surc	harges		·	
	Occupancy haza	ard reduction or surcharge		Reduction/	Surcharge	
	(1)	Non-combustible		-25%		5,100
3		Limited combustible	Yes	-15%		
·		Combustible		0%		
		Free burning		15%		
		Rapid burning		25%		
	Sprinkler Reduc	tion		Redu	ction	
		Adequately Designed System (NFPA 13)	Yes	-30%	-30%	
4	(0)	Standard Water Supply	Yes	-10%	-10%	0.550
	(2)	Fully Supervised System	Yes	-10%	-10%	-2,550
			Cum	ulative Total	-50%	
	Exposure Surch	arge (cumulative %)			Surcharge	
		North Side	10.1 - 20 m		15%	
-		East Side	20.1 - 30 m		10%	
5	(3)	South Side	30.1- 45 m		5%	2,805
		West Side	0 - 3 m		25%	
			Cum	nulative Total	55%	
		Results				
		Total Required Fire Flow, rounded to nearest 1000L/min			L/min	5,000
6	(1) + (2) + (3)	(2,000 L/min < Fire Flour < 45,000 L/min)		or	L/s	83
		(2,000 L/min < Fire Flow < 45,000 L/min)		or	USGPM	1,321
	1				11	4 75
7	Storage Volume	Required Duration of Fire Flow (hours)			Hours	1.75

	Novatech Project #: 121008	 Please use Flow Calcula 		when completing the FUS Fire	
	Project Name: 829 Carling Avenue	-		. 4	
	Date: 4/15/2021		oubt, confirm construction m	aterial, firewalls, etc. with	
	Input By: Jazmine Gauthier	architect/own			
ŀ	Reviewed By: Greg MacDonald Note: This form only applies for Fire Resistive	• vv nen in do	oubt, err on conservative side	9	
	Enter a description of the building or unit being cons	sidered, i.e. us	e/most stringent condition/a	ddress	
			Construction Type	Fire Resistive Construction	
ı			Construction Type	THE RESISTIVE CONSTITUCTOR	
ı			Floor Area Considered	2,117 m ²	
L			Occupancy Reduction	-15%	
Ī	Base Fire Flow		Sprinkler Reduction	-50%	
1	Construction Material		Exposure Surcharge	55%	
	Does not apply for this form		Total Fire Flow	5,000 L/min	
	Does not apply for this form		Project Manager Review	·	
I	Does not apply for this form		Da	ate:	
	Only Use if can be confirmed with client/architect (IS		Name:		
_	Only Use if can be confirmed with client/architect (IS	SO CI 6)			
	Floor Area f considered gross floor area, then enter 1 floor/stor	If E' "	Signatu		
Ļ	Protected 2 = number of additional important protected 2 = number				
ļ	For unprotected openings scenario only, can be	e mix of podi	um and tower		
+	Paduations or Surpharacs				
+	Reductions or Surcharges				
	Occupancy hazard reduction or surcharge Residential - with no garage				
	Residential - with no garage Residential - with garage				
	General Commercial - Generally, no reduction				
	Check usage with FUS				
	Check usage with FUS				
ŀ	Sprinkler Reduction				
-	Only Use if can be confirmed with client/architect				
	Only Use if can be confirmed with client/architect	· ·			
	•				
(Only Use if can be confirmed with client/architect				
0	Only Use if can be confirmed with client/architect Exposure Surcharge (cumulative %)				
1		minimum 2 hou	ur rating per NBC.		
-	Exposure Surcharge (cumulative %)	minimum 2 hou	ur rating per NBC.		
1	Exposure Surcharge (cumulative %)	ninimum 2 hou	ur rating per NBC.		
<u> </u>	Exposure Surcharge (cumulative %)	ninimum 2 hou	ur rating per NBC.		
	Exposure Surcharge (cumulative %) For Fire walls: FUS considers a Fire wall to have a r			is value at 10,000L/min	
	Exposure Surcharge (cumulative %) For Fire walls: FUS considers a Fire wall to have a r			is value at 10,000L/min	
	Exposure Surcharge (cumulative %) For Fire walls: FUS considers a Fire wall to have a results Results NOTE: Refer to City Technical Bulletin ISDTB-2014			is value at 10,000L/min	

APPENDIX D

Servicing Study Guidelines Checklist



Date: April 2021

4.1 General Content	Addressed (Y/N/NA)	Section	Comments
Executive Summary (for larger reports only).	NA		
Date and revision number of the report.	Υ	p.1	
Location map and plan showing municipal address, boundary, and layout of proposed development.	Υ	Dwgs	GP, GR, STM
Plan showing the site and location of all existing services.	Υ	Dwg	GP
Development statistics, land use, density, adherence to zoning and official plan, and reference to applicable subwatershed and watershed plans that provide context to which individual developments must adhere.	Υ	Intro	
Summary of Pre-consultation Meetings with City and other approval agencies.	N		
Reference and confirm conformance to higher level studies and reports (Master Servicing Studies, Environmental Assessments, Community Design Plans), or in the case where it is not in conformance, the proponent must provide justification and develop a defendable design criteria.	Y	Report	All sections
Statement of objectives and servicing criteria.	Υ	Report	
Identification of existing and proposed infrastructure available in the immediate area.	Υ	Dwg	GP
Identification of Environmentally Significant Areas, watercourses and Municipal Drains potentially impacted by the proposed development (Reference can be made to the Natural Heritage Studies, if available).	NA		
Concept level master grading plan to confirm existing and proposed grades in the development. This is required to confirm the feasibility of proposed stormwater management and drainage, soil removal and fill constraints, and potential impacts to neighboring properties. This is also required to confirm that the proposed grading will not impede existing major system flow paths.	Υ	Report	



Date: April 2021

4.1 General Content	Addressed (Y/N/NA)	Section	Comments
Identification of potential impacts of proposed piped services on private services (such as wells and septic fields on adjacent lands) and mitigation required to address potential impacts.	NA		
Proposed phasing of the development, if applicable.	Υ		
Reference to geotechnical studies and recommendations concerning servicing.	Υ	Report	
All preliminary and formal site plan submissions should have the following information:			
Metric scale	Υ		All Drawings
North arrow (including construction North)	Υ		All Drawings
Key plan	Υ		All Drawings
Name and contact information of applicant and property owner	Υ		Drawings/Report
Property limits including bearings and dimensions	Υ		Report
Existing and proposed structures and parking areas	Υ		All Drawings
Easements, road widening and rights-of-way	Υ		All Drawings
Adjacent street names	Υ		All Drawings



Date: April 2021

4.2 Water	Addressed (Y/N/NA)	Section	Comments
Confirm consistency with Master Servicing Study, if	NA		
available.	IVA		
Availability of public infrastructure to service proposed	V		
development.	Υ		
Identification of system constraints.	NA		
Identify boundary conditions.	NA		
Confirmation of adequate domestic supply and pressure.	NA		
Confirmation of adequate fire flow protection and confirmation that fire flow is calculated as per the Fire Underwriter's Survey. Output should show available fire flow at locations throughout the development.	Y		Appendix
Provide a check of high pressures. If pressure is found to be high, an assessment is required to confirm the application of pressure reducing valves.	NA		
Definition of phasing constraints. Hydraulic modeling is required to confirm servicing for all defined phases of the project including the ultimate design.	NA		
Address reliability requirements such as appropriate location of shut-off valves.	Υ		Drawings
Check on the necessity of a pressure zone boundary modification.	NA		
Reference to water supply analysis to show that major infrastructure is capable of delivering sufficient water for the proposed land use. This includes data that shows that the expected demands under average day, peak hour and fire flow conditions provide water within the required pressure range.			
Description of the proposed water distribution network, including locations of proposed connections to the existing system, provisions for necessary looping, and appurtenances (valves, pressure reducing valves, valve chambers, and fire hydrants) including special metering provisions.	Υ	Report	
Description of off-site required feedermains, booster pumping stations, and other water infrastructure that will be ultimately required to service proposed development, including financing, interim facilities, and timing of implementation.	NA		
Confirmation that water demands are calculated based on the City of Ottawa Design Guidelines.	Y	Report	
Provision of a model schematic showing the boundary conditions locations, streets, parcels, and building locations for reference.	NA		



Date: April 2021

4.3 Wastewater	Addressed (Y/N/NA)	Section	Comments
Summary of proposed design criteria (Note: Wet-weather flow criteria should not deviate from the City of Ottawa Sewer Design Guidelines. Monitored flow data from relatively new infrastructure cannot be used to justify capacity requirements for proposed infrastructure).	Υ	Report	
Confirm consistency with Master Servicing Study and/or justifications for deviations.	NA		
Consideration of local conditions that may contribute to extraneous flows that are higher than the recommended flows in the guidelines. This includes groundwater and soil conditions, and age and condition of sewers.	NA		
Description of existing sanitary sewer available for discharge of wastewater from proposed development.	Υ	Report	Drawings
Verify available capacity in downstream sanitary sewer and/or identification of upgrades necessary to service the proposed development. (Reference can be made to previously completed Master Servicing Study if applicable)	Υ	Report	Appendix
Calculations related to dry-weather and wet-weather flow rates from the development in standard MOE sanitary sewer design table (Appendix 'C') format.	NA		
Description of proposed sewer network including sewers, pumping stations, and forcemains.	Υ		
Discussion of previously identified environmental constraints and impact on servicing (environmental constraints are related to limitations imposed on the development in order to preserve the physical condition of watercourses, vegetation, soil cover, as well as protecting against water quantity and quality).	NA		
Pumping stations: impacts of proposed development on existing pumping stations or requirements for new pumping station to service development.	NA		
Forcemain capacity in terms of operational redundancy, surge pressure and maximum flow velocity.	NA		
Identification and implementation of the emergency overflow from sanitary pumping stations in relation to the hydraulic grade line to protect against basement flooding.	NA		
Special considerations such as contamination, corrosive environment etc.	NA		



Date: April 2021

4.4 Stormwater	Addressed (Y/N/NA)	Section	Comments
Description of drainage outlets and downstream	-		
constraints including legality of outlet (i.e. municipal	Υ	Report	
drain, right-of-way, watercourse, or private property). Analysis of the available capacity in existing public infrastructure.	NA		
A drawing showing the subject lands, its surroundings, the receiving watercourse, existing drainage patterns and	Y		GR, STM
proposed drainage patterns.			
Water quantity control objective (e.g. controlling post- development peak flows to pre-development level for storm events ranging from the 2 or 5 year event (dependent on the receiving sewer design) to 100 year return period); if other objectives are being applied, a rationale must be included with reference to hydrologic analyses of the potentially affected subwatersheds, taking into account long-term cumulative effects.	Υ	Report	
Water Quality control objective (basic, normal or enhanced level of protection based on the sensitivities of the receiving watercourse) and storage requirements.	Υ	Report	
Description of stormwater management concept with			
facility locations and descriptions with references and	Υ	Report	
supporting information.	'	перин	
Set-back from private sewage disposal systems.	NA		
Watercourse and hazard lands setbacks.	Y		
Record of pre-consultation with the Ontario Ministry of Environment and the Conservation Authority that has jurisdiction on the affected watershed.	N		
Confirm consistency with sub-watershed and Master Servicing Study, if applicable study exists.	N		
Storage requirements (complete with calcs) and conveyance capacity for 5 yr and 100 yr events.	Υ		Appendix
Identification of watercourse within the proposed development and how watercourses will be protected, or, if necessary, altered by the proposed development with applicable approvals.	NA		
Calculate pre and post development peak flow rates including a description of existing site conditions and proposed impervious areas and drainage catchments in comparison to existing conditions.	Υ		Appendix
Any proposed diversion of drainage catchment areas	NA		
from one outlet to another.	IVA		
Proposed minor and major systems including locations and sizes of stormwater trunk sewers, and SWM facilities.	Υ	Report	And Appendix
If quantity control is not proposed, demonstration that downstream system has adequate capacity for the post-development flows up to and including the 100-year return period storm event.	Υ	Report	And Appendix



Date: April 2021

4.4 Stormwater	Addressed (Y/N/NA)	Section	Comments
Identification of municipal drains and related approval requirements.	Υ	Report	
Description of how the conveyance and storage capacity will be achieved for the development.	Υ	Report	
100 year flood levels and major flow routing to protect proposed development from flooding for establishing minimum building elevations (MBE) and overall grading.	Y		Appendix
Inclusion of hydraulic analysis including HGL elevations.	Υ		Appendix
Description of approach to erosion and sediment control during construction for the protection of receiving watercourse or drainage corridors.	Υ	Report	Drawings
Identification of floodplains – proponent to obtain relevant floodplain information from the appropriate Conservation Authority. The proponent may be required to delineate floodplain elevations to the satisfaction of the Conservation Authority if such information is not available or if information does not match current conditions.	NA		
Identification of fill constrains related to floodplain and geotechnical investigation.	NA		



Date: April 2021

4.5 Approval and Permit Requirements	Addressed (Y/N/NA)	Section	Comments
Conservation Authority as the designated approval agency for modification of floodplain, potential impact on fish habitat, proposed works in or adjacent to a watercourse, cut/fill permits and Approval under Lakes and Rivers Improvement Act. The Conservation Authority is not the approval authority for the Lakes and Rivers Improvement Act. Where there are Conservation Authority regulations in place, approval under the Lakes and Rivers Improvement Act is not required, except in cases of dams as defined in the Act.			
Application for Certificate of Approval (CofA) under the Ontario Water Resources Act.	NA		
Changes to Municipal Drains.	NA		
Other permits (National Capital Commission, Parks			
Canada, Public Works and Government Services Canada,	NA		
Ministry of Transportation etc.)			

4.6 Conclusion	Addressed (Y/N/NA)	Section	Comments
Clearly stated conclusions and recommendations.	Υ	Report	
Comments received from review agencies including the City of Ottawa and information on how the comments were addressed. Final sign-off from the responsible reviewing agency.	NA		
All draft and final reports shall be signed and stamped by a professional Engineer registered in Ontario.	Y	Report	

